

By Superposition, considering only AC Source

iac = Vm lin (wt - 0) Vw2 12 + R2

where $\phi = \tan\left(\frac{\omega L}{R}\right) \left[\frac{1}{R} \operatorname{mark}\right]$

Considering only DC Source.

At steady state,

Tyde inductor acts as short

circuit for DC.

ide = + xde | 1 mark

. Net current out steady state

1 for t >0,

(t) = Vm Sm (wt - p) - vde + ke-t/J. (J= L/R).

\[\tau^2 L^2 + R ? \]
\[\tau \tau^2 L^2 + R ? \] at t=0, 1=0

VW2 12 TRZ R

$$\frac{1}{\sqrt{R^2 + \omega^2 L^2}} = \frac{Vm}{R} = \frac{Vdc}{R} = \frac{1}{1 \text{ mark}}$$

$$\frac{1}{\sqrt{R^2 + w^2 L^2}} = \frac{\sqrt{R} + \sqrt{R} + \sqrt{R}}{\sqrt{R^2 + w^2 L^2}} = \frac{-Rt}{\sqrt{L}}$$

= 4.2 LA5° = 8 LA5° 1 1 = 8/2 cos (1000+ + 450) = 11.313 cos (1000t + 45°) Ztn = 4+j0 = 4 Lo. (2 mark.)

Taking the current as the reference phasor, the se phasor diagram of the circuit is # shown in the figure assuming V, to be the voltage drop (2 marks) for across the inductor. $(230)^2 = (200 - 40)^2 + 20^2$ a, v,2 - 400v, -12500 = 0 · V, = A29.12, -29.12 Negative of V, means et is (2 marks for taking lagging I by an angle goothe decision of tre-ve

lagging I by an angle 900 the decision of tre-re not possible for an inductor, hence this negative value is discarded.

". V, = A29.12V

 $I = \frac{429.12}{160} = 4.29 A$



If no reasoning is provided why the tre value is considered deduct I mark 84. Time period of p is 5 ms, therefore f = 200 Hz Frequency of the source is therefore 200 H2 = 100HZ Let the equation of the instantaneous power is b = X small + y - - - - (1) W = 2xf = 2xx 200 = 1256.637. A - B - T - 7 AD = AB+ BC + CD = 5ms or, 2AB + BC = 5 ms c, 2AB = (5-1-666) ms or, AB = 1-667 ms Considering (1) . Pmax will occur at wt = 1/2 or t = 1-25 ms : 100 = X+A --- (5) b=0 will be at t= (+25+1-667)ms=2.917 ms

b = 0 will be at t = (1.25 + 1.667) ms = 2.917 ms. $0 = x \sin(1.256.637 \times 2.917 \times 10^{-3})$ ty 0 = -0.5x + y = --(3)

Solving (2) and (3) , X= 66-67 , Y= 33-33

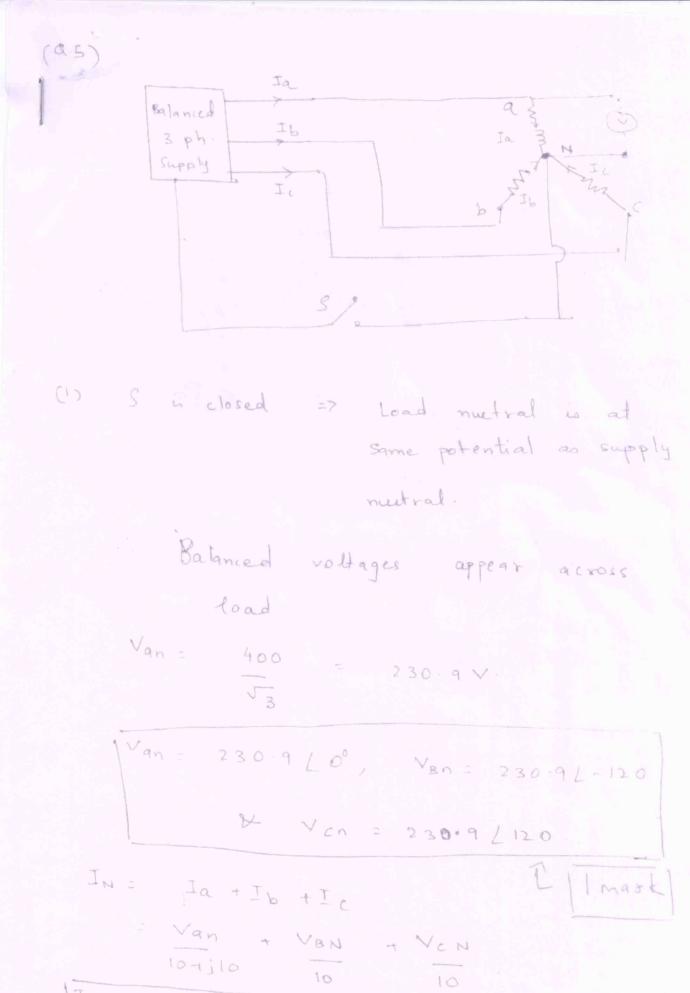
. The ownerage value of the weekerform provider 33-33 wat.

** NOW \$ = 1.667 × 360 = 59.97 = 600

VICOS \$ = 33.33 => VI = 33.33

Readive power = VISIND = 60.66 sinbo = 57-27 WAR

4 Marks



IN= 16.33 L-135 [| Imart

's' is open 2 => Load and supply nuetrals are not connected => Load phase-nuetral voltages are Not balanced

YAB = I, (10+j10) + (I,+Iz) 10 = 400L0

V(B = 10 I2 + (I, + I2) 10 = -400 [-120

Solving,

27, (lotilo) + 20 I, +20 Iz - 20 Iz - 10 I = 800 LO+ 400 L-120

30 I, + j I, (20) = 800 L O 7 400 L-120

I, = 800 L0 + 400 L-120

30 + j 20

= 1921 L-63.69 A.

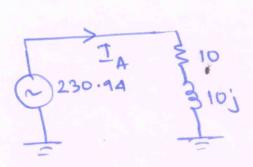
and IV, = I, (10+j10)

271.63 V () I mark

(26) Thre reading of Waltmeler is the ing THOUSE SOUND X CORX EL STORY (2 marks). W= IA VBC COS (90-4) - JA VBC Sin D = V3 Vph Iph Sint tanp = 10 = 1 2 marks · Sin 0 = 1/52 1 II = 230.94. - 16.32 1 mark. V102 7102 W = V3 x230.94 x 16.32 x Sin (45)

4615.99 m. 1 mark.

Per phase equivalent ckt:



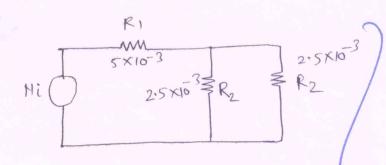
: Prwn = \(\int 3 \times 400 \times 16.32 \times 105 45 \\
: 7995.13 W.

Reactive = \(\int \frac{13 \times 400 \times 16.32 \times \frac{1}{32} \times \frac{1 = 7995.13 W = 53 x A615.99

Later L

= =

1 A row A



$$R_1 = \frac{24 \times 10^{-2}}{4 \times 12 \times 10^{4}}$$

$$R_2 = \frac{72 \times 10^{-2}}{4 \times 6 \times 10^{-4}}$$

mmf required for
$$R_1 = \frac{24\times10^2}{4\times10^{12}\times10^9} \times 5\times10^3$$
 1 mark

mmf required for
$$R_2 = \frac{72 \times 10^2}{4 \times 6 \times 10^{-3}} \times 2.5 \times 10^{-3}$$

$$\frac{24 \times 5 \times 10^{3}}{4 \times 10^{4}} + \frac{72 \times 2.5 \times 10^{5}}{4 \times 6 \times 10^{4}} = 756 \times 0.5$$

$$\frac{1}{4} + \frac{1}{22 \times 25} = 375$$

$$L[1+3] = 375$$

$$\frac{4}{4} = 375$$

$$M = \frac{4}{375} \cong 0.01066$$

$$4.4r = \frac{4}{375}$$

$$M_{r} = \frac{4}{375 \times 44 \times 10^{7}} = 8488.26$$

calculation mistake deduct 1 mark.