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#### Selection of Sensor



- Factors affecting selection of sensors
- Environmental factors
  - ☐ Temperature change
  - ☐ Humidity effect
  - □ Size
  - ☐ Susceptibility to EM interference
  - □ Ruggedness
  - □ Power consumption
  - ☐ Self-test capability
- Economical factors
  - ☐ Cost
    - □ Availability
    - ☐ Lifetime

- Sensor characteristics
  - Sensitivity
  - ☐ Range
  - ☐ Stability
  - □ Repeatability□ Linearity
  - ☐ Error
  - ☐ Response time

Sensor Errors



•	<b>Fixed bias</b> : Sensor output even in the absence of an applied input rotation
	<ul> <li>□ Residual torques from flexible leads within the sensor</li> <li>□ Spurious magnetic fields and temperature gradients</li> <li>□ Acceleration-independent bias</li> </ul>
•	<b>Acceleration-dependent bias (</b> $g$ <b>-dependent bias)</b> : Biases proportional to the magnitude of applied acceleration.
	☐ Mass unbalance in the rotor suspension
	☐ Non-coincidence of the rotor centre of gravity and the centre of the suspension mechanism
	$\ \square$ Fixed bias in the measured rate for a steady acceleration
•	<b>Anisoelastic bias (</b> $g^2$ <b>-dependent bias)</b> : Biases proportional to product of acceleration along orthogonal pairs of axes
	<ul> <li>Unequal finite compliances of gyroscope rotor suspension structure in different directions.</li> </ul>

#### Sensor Errors



•	<b>Anisoinertia errors</b> : Biases owing to inequalities in gyroscope moments of inertia about different axes
	<ul> <li>Proportional to the product of angular rates applied about pairs of orthogona axes</li> </ul>
•	<b>Scale-factor errors</b> : Errors in the ratio relating the change in the output signal to a change in the input rate
	☐ Scale-factor non-linearity: deviations from the least-squares straight line or non-linear function fitted to the measurements
	<ul> <li>Scale-factor asymmetry: differences in the magnitude of the output signal for equal rotations of the sensor in opposite directions</li> </ul>
•	<b>Cross-coupling errors</b> : Gyroscope sensitivity to turn rates about axes normato the input axis

☐ Non-orthogonality of the sensor axes

#### Sensor Errors Types



- ☐ Fixed or repeatable terms:
  - A bias component which is predictable
  - Always present whenever the sensor is switched on
  - Can therefore be corrected
- ☐ Temperature induced variations:
  - A temperature-dependent bias component
  - Can be corrected with suitable calibration
- ☐ Switch-on to switch-on variations:
  - A random bias which varies from gyroscope switch-on to switch-on
  - Constant for any one run
- □ In-run variations:
  - An in-run random bias which varies throughout a run
  - Precise form of this error varies from one type of sensor to another
- ☐ First two may be corrected to large extent, but later two types of errors persists.

Inertial Sensors

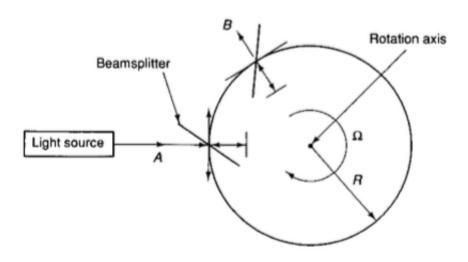
#### Ring Laser Gyro



- Optical sensor: Sensors using properties of EM radiation to sense rotation.
- Ring Laser Gyro (RLG): Principles of general relativity
  - ☐ A resonant optical cavity containing two oppositely directed traveling light waves generated by stimulated emission of radiation
  - An inherent capability to operate in the strapdown mode
  - $\ \square$  Scale factor linearity over the full dynamic range
  - ☐ Easy interface with digital systems
- Detection of rotation with light was demonstrated by Sagnac in 1913.
- Principle: Two light waves acquire a phase difference by propagating in opposite directions around a loop interferometer
- These beams travel the same path in opposite directions around a closed ring.
- Solid-state sensor with no moving parts.
- It detects and measures differential angular rotations by measuring the frequency difference between the two contrarotating beams.

Passive Sagnac Interferometer





#### Passive Sagnac Interferometer



- Consider a circular interferometer.
- Assume the light beam is splitted into two beams rotating in opposite directions.
- After one rotation they combine at the beamsplitter.
- In absence of rotation, transit time taken by light to complete rotation

$$t=\frac{2\pi R}{c}$$

where, c is the speed of light, and R is the radius of circular path.

- If the interferometer is rotated with constant angular velocity  $\Omega$  then the travel time for both the beams will be different.
- ullet Note that the beamsplitter is moved to new location at B.
- With respect to inertial space, the light moving in the direction of rotation must travel a longer distance than the light traveling in the opposite direction.

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#### Passive Sagnac Interferometer



- Let X be the inertial space distance between points A and B.
- Positive (+) and negative (-) signs refer to the beam traveling in the direction of rotation and opposite to the direction of rotation, respectively.
- Total closed-path transit for the light

$$ct_{\pm} = 2\pi R \pm X_{\pm}, \quad X_{\pm} = R\Omega t_{\pm}$$

• On solving above equations,

$$t_{\pm} = \frac{2\pi R}{c} \pm \frac{R\Omega t_{\pm}}{c} \Rightarrow t_{\pm} = \frac{2\pi R}{c \mp R\Omega}$$

• Transit time  $\Delta t$ 

$$\begin{split} \Delta t = & t_+ - t_- = \frac{2\pi R}{c - R\Omega} - \frac{2\pi R}{c + R\Omega} \\ = & 2\pi R \left[ \frac{2R\Omega}{c^2 - R^2\Omega^2} \right] = \frac{4\pi R^2\Omega}{c^2 - R^2\Omega^2} \end{split}$$



• Transit time  $\Delta t$ 

$$\Delta t = \frac{4\pi R^2 \Omega}{c^2 - R^2 \Omega^2} = \frac{\left(\frac{4\pi R}{c}\right) \left(\frac{R\Omega}{c}\right)}{1 - \left(\frac{R\Omega}{c}\right)^2}$$

• On neglecting smaller terms, we get equation called as "Sagnac effect"

$$\Delta t = \frac{4\pi R^2 \Omega}{c^2 - R^2 \Omega^2} = \left(\frac{4\pi R}{c}\right) \left(\frac{R\Omega}{c}\right) = \frac{4\pi \Omega R^2}{c^2} = \frac{4A\Omega}{c^2}$$

where,  $A=4\pi R^2$  is the area of circular optical path.



ullet Optical path difference  $\Delta L$ 

$$\Delta L = c\Delta t = \frac{4c\pi\Omega R^2}{c^2} = \frac{4\Omega\pi R^2}{c} = \frac{4A\Omega}{c}$$

- This result holds in general for any geometric closed path.
- Issue: The path difference is small even with a large area.
- If  $\Omega$  is very low then it is difficult to measure these angular rates as required closed area is very large.
- Ratio of total enclosed area to the wavelength must be large to sense low angular rate.
- Lack of sensitivity because the path difference for light traveling in the two directions is much less than wavelength.

#### Active Ring Laser Interferometer



- Improvement of sensitivity
  - ☐ By replacing the beamsplitter with a mirror
  - ☐ Form a resonant circuital optical cavity supporting traveling-wave modes for the counterrotating beams.
- These modes could be made self-sustaining by placing the lasing medium in the cavity.
- Laser frequency is dependent on the cavity length.
- Two oppositely directed traveling waves oscillate independently, each with its own frequency and amplitude.
- Fractional difference between these two frequencies corresponds to the fractional difference in optical path lengths traveled by each wave and, therefore, is proportional to the angular velocity.

Inertial Sensors

#### Active Ring Laser Interferometer



- To sustain oscillation, there must be enough gain in the medium to overcome losses in the cavity.
- Optical length of beam also need to satisfy

$$N\lambda_{\pm} = L_{\pm}$$

where,  $L_{\pm}$  is the optical length of each beam,  $\lambda_{\pm}$  is the wavelength, and N is large integer (10<sup>5</sup> to 10<sup>6</sup>).

- Cavity geometry determines the wavelengths of a given mode.
- Fractional frequency shift equals the fractional path length

$$\frac{\Delta \nu}{\nu} = \frac{\Delta L}{L} \quad (Proof?)$$

• As  $\lambda = c/\nu$ , we have beat frequency  $\Delta t$  given by

$$\Delta \nu = \frac{\Delta L \nu}{L} = \frac{4A\Omega}{c} \frac{c}{\lambda L} = \left(\frac{4A}{L\lambda}\right) \Omega$$



Ideal RLG equation

$$\Delta 
u = \underbrace{\left(\frac{4A}{L\lambda}\right)}_{\text{Geometric or ideal scale factor } S}$$

where,  $\lambda$  and L are the wavelength of laser light and optical path length or cavity length, respectively.

• On integration of ideal RLG equation

$$\int_{t_1}^{t_2} \Delta \nu dt = S \int_{t_1}^{t_2} \Omega dt \Rightarrow N = S\theta$$

where, N is total phase shift or beats counted during measurement time and  $\theta$  is total angle of rotation.

ullet Laser gyro is rate integrating gyro as it gives N counts when turned through angle heta.

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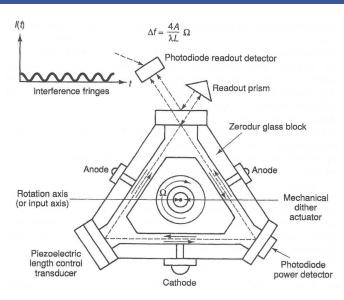
#### Ring Laser Gyro



- RLG is a triangular or square cavity filled with gas, in which two oppositely traveling light waves are generated by stimulated emission of radiation.
- Active laser gyro: A two-mode, continuous wave (cw)
- Passive laser gyro: Lasing medium is external to the cavity.
- Laser gyro combines the properties of an optical oscillator and general relativity to produce the function of the conventional mechanical gyroscopes.
- Components of RLG
  - □ Block material
  - Mirrors
  - Gain medium (He-Ne plasma cavity)
  - Readout mechanism
  - Associated electronics

#### Ring Laser Gyro







## RLG: Example

Consider an equilateral triangular RLG with its side length and height given by 7.239 and 6.2687 cm. Assume input angular velocity is 1 deg/h. The operating wavelength is assumed to be 0.6328  $\mu$ m. Compute measurable beat frequency.

- Total optical length = 3(7.29)=21.717 cm
- Area of triangle  $A = (1/2)bh = 3.1695(6.2687) = 22.6895 \text{ cm}^2$
- $\bullet~\Omega=1~{\rm deg/h}=4.85{\times}10^{-6}~{\rm rad/s}$
- Measurable beat frequency

$$\Delta\nu = \left(\frac{4A}{L\lambda}\right)\Omega = \frac{4(2.27\times10^{-3})(4.85\times10^{-6})}{2.172\times10^{-1}(0.6328\times10^{-6})}$$
 = 0.32 Hz

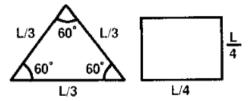
#### Active Ring Laser Interferometer



- How can we increase scale factor sensitivity of RLG?
- Ideal RLG equation

$$\Delta \nu = S\Omega = \left(\frac{4A}{L\lambda}\right)\Omega$$

- Sensitivity of scale factor
  - $\square$  Increase enclosed area A
  - $\square$  Decrease wavelength  $\lambda$  or optical length L
- How does geometric form of the closed path affect scale factor?



#### Active Ring Laser Interferometer



• For equilateral triangle and square shape

$$\begin{split} S_{ET} = & \frac{4}{L\lambda} \frac{\sqrt{3}}{4} \left( \frac{L}{3} \right)^2 = \frac{1}{\lambda} \left( \frac{L}{3\sqrt{3}} \right) \\ S_{SQ} = & \frac{4}{L\lambda} \frac{L}{4} \frac{L}{4} = \frac{1}{\lambda} \left( \frac{L}{4} \right) \end{split}$$

For a general shape of closed path

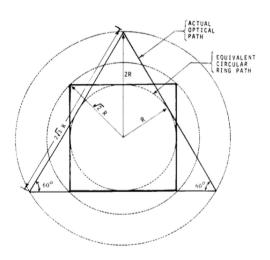
$$S = \frac{1}{\lambda}$$
 (Diameter of inscribed circle)

- $\bullet$  Accuracy of RLG  $\propto$  Area enclosed by the path and inversely proportional to path length.
- A square laser gyro encloses a greater area for a given path length than triangular one, thus having greater potential accuracy.
- Square configuration: package into a smaller-sized inertial navigation unit.

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Active Ring Laser Interferometer





**Equivalent circular RLG**: One that gives the same ideal scale factor as the actual polygonal ring laser.

Text/References



#### Reference

- G. M. Siouris, *Aerospace Avionics Systems: A Modern Synthesis*, Academic Press, Inc. 1993.
- ② D. H. Titterton and J. L. Weston, *Strapdown Inertial Navigation Technology*, Progress in Astronautics and Aeronautics, Vol. 207, ed. 2, ch. 4.

Thank you for your attention !!!