



Canonical Normalization



Solution Magnitudes

Solution for **orbits** generally involves **distances** and time periods that are quite **large**, even in the context of **Earth**.

In case we have an **inter-planetary** motion, distances and velocities can be **extremely** large quantities.



Canonical Normalization Concept

Therefore, in order to **manage** the number of **significant** digits, without losing **accuracy**, we commonly employ canonical **normalization**, based on the context.

E.g. for **earth** bound missions, radius of **earth** is the parameter used for **distance** normalization (DU), while for **heliocentric** motion, Earth's orbital **radius** is used.



Canonical Normalization Method

With regard to **velocity**, value corresponding to **circular** motion on earth's surface (**SU**) is used, while for **time** normalization, **time** taken for one radian (**TU**) is used.

The above **normalizations** keep all quantities of **similar** magnitude, which helps in their **manipulation**.



Canonical Normalization Result

A **logical** consequence of such a **normalization** is to make gravitational parameter, $\mu = 1$, as shown below.

$$1 \text{ SU} = \frac{1 \text{ DU}}{1 \text{ TU}} = \sqrt{\frac{\mu}{1 \text{ DU}}}; \quad \mu = \frac{1 \text{ DU}^3}{1 \text{ TU}^2} = 1$$



Position / Velocity Vector Solutions



Orbital Parameter Modification

In the context of **space** missions, we generally convert '**r**' and '**v**' at the end of the ascent mission in to **orbital** parameters e.g. '**a**', '**e**', '**T₀**', '**Ω**', '**ω**', '**θ (or M)**' and '**i**'.

While, this is **sufficient** for operationalizing most spacecraft, there are **many** missions in which **final** objective is **different** from end of the **ascent** mission.

Typically, this **situation** is addressed by suitably **modifying** the orbit through input of **additional energy**.



Orbital Parameter Modification

In this **regard**, it is to be noted that **orbital** parameters acquire new **values** and hence, need **new** set of values for 'r' and 'v'.

An example is **return** mission, where we need **fix** 'r' and 'v' **vectors** with respect to **ECI frame**, for propagating the applicable **equations** of motion.



‘r’ and ‘v’ from Orbital Parameters

Another case arises when **we** need to shift the **spacecraft** to an entirely **new** orbit and need to **locate** it back in the **ECI** for assessing changes.

Thus, we need a **strategy** to back-calculate **‘r’ and ‘v’** vectors from the **available** orbital parameters.

This is the **reverse** of the process **employed** for obtaining the orbital **parameters** from **‘r’ and ‘v’** and is **initiated** in the **orbital** plane, as explained next.

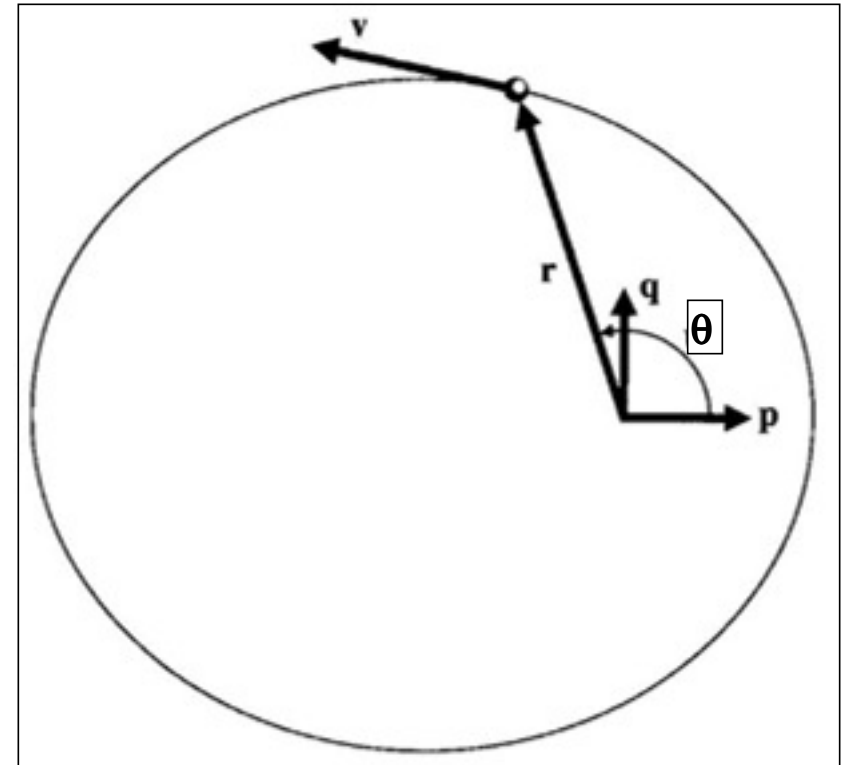


Orbital Velocity Solution

Consider **orbital plane** as shown alongside.

Here, ' \mathbf{r} ', ' \mathbf{v} ' are vectors in the **orbital plane**.

Further, ' \mathbf{p} ' and ' \mathbf{q} ' are unit **vectors** defining the orbital **plane**.





‘r’ and ‘v’ in Orbital Plane

We can now **obtain** position & velocity as **follows**.

$$\begin{aligned}\vec{r} &= r \cos \theta \hat{p} + r \sin \theta \hat{q}; \quad h = r(r\dot{\theta}) = \sqrt{\mu p} \\ \vec{v} &= \dot{\vec{r}} = (\dot{r} \cos \theta - r\dot{\theta} \sin \theta) \hat{p} + (\dot{r} \sin \theta + r\dot{\theta} \cos \theta) \hat{q} \\ r\dot{\theta} &= v_t = \frac{h}{r} = \sqrt{\frac{\mu}{p}} \cdot (1 + e \cos \theta), \quad \dot{r} = r\dot{\theta} \cdot \frac{e \sin \theta}{1 + e \cos \theta} \\ \dot{r} &= \sqrt{\frac{\mu}{p}} \cdot e \sin \theta; \quad \vec{v} = \sqrt{\frac{\mu}{p}} \cdot [-\sin \theta \hat{p} + (e + \cos \theta) \hat{q}]\end{aligned}$$

Vectors ‘**r**’ and ‘**v**’ capture the **motion** of spacecraft within the **orbital** plane, with respect to **origin** (focus).



r & v in Geographical Frame

Next, **r & v** in orbital plane can be **transformed** into geographical frame (**ECI**) as follows.

$$\begin{aligned}\vec{r}_{ijk} &= [R] \vec{r}_{pqw}; \quad \vec{v}_{ijk} = [R] \vec{v}_{pqw}; \quad [R] \rightarrow \text{Rotation Matrix} \\ [R] &= R_{\omega} \cdot R_i \cdot R_{\Omega}; \quad \rightarrow \text{Elementary Rotations} \\ \Omega, i, \omega &\rightarrow \text{Euler angles for rigid body dynamics} \\ [R] &= [\hat{p} \mid \hat{q} \mid \hat{w}]; \quad \hat{p} = \frac{\vec{e}}{|\vec{e}|}, \quad \hat{w} = \frac{\vec{H}}{|\vec{H}|}, \quad \hat{q} = \hat{w} \times \hat{p}\end{aligned}$$

Thus, we can **switch** between initial **conditions** and orbital elements, as per the **need**.



Rotation Matrix Derivation

The rotation matrix **[R]** can be obtained as **follows**.

$$(x, y, z) = (p, q, w)[R] = (p, q, w)[R_\omega] \cdot [R_i] \cdot [R_\Omega]$$

$$[R_\Omega] = \begin{bmatrix} \cos \Omega & \sin \Omega & 0 \\ -\sin \Omega & \cos \Omega & 0 \\ 0 & 0 & 1 \end{bmatrix}; \quad [R_i] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos i & \sin i \\ 0 & -\sin i & \cos i \end{bmatrix}$$

$$[R_\omega] = \begin{bmatrix} \cos \omega & \sin \omega & 0 \\ -\sin \omega & \cos \omega & 0 \\ 0 & 0 & 1 \end{bmatrix}; \quad [R] = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_2 & n_3 \end{bmatrix}$$

Next, we can now perform the **above** multiplications and arrive at **nine** scalar components of **[R] matrix**.



R Matrix Scalar Elements

The scalar **elements** of **[R]** are as follows.

$$l_1 = \cos \omega \cos \Omega - \sin \omega \sin \Omega \cos i$$

$$m_1 = \cos \omega \sin \Omega + \sin \omega \cos \Omega \cos i$$

$$n_1 = \sin \omega \sin i$$

$$l_2 = -\sin \omega \cos \Omega - \cos \omega \sin \Omega \cos i$$

$$m_2 = -\sin \omega \sin \Omega + \cos \omega \cos \Omega \cos i$$

$$n_2 = \cos \omega \sin i$$

$$l_3 = \sin \Omega \sin i; \quad m_3 = -\cos \Omega \sin i; \quad n_3 = \cos i$$



Position/Velocity Scalar Elements

The scalar **elements of \mathbf{r} & \mathbf{v}** are as follows.

$$x = l_1 r \cos \theta + l_2 r \sin \theta$$

$$y = m_1 r \cos \theta + m_2 r \sin \theta$$

$$z = n_1 r \cos \theta + n_2 r \sin \theta$$

$$\frac{dx}{dt} = \frac{\mu}{h} [-l_1 \sin \theta + l_2 (e + \cos \theta)]$$

$$\frac{dy}{dt} = \frac{\mu}{h} [-m_1 \sin \theta + m_2 (e + \cos \theta)]$$

$$\frac{dz}{dt} = \frac{\mu}{h} [-n_1 \sin \theta + n_2 (e + \cos \theta)]$$

$(\mathbf{x}, \mathbf{y}, \mathbf{z})$ are defined in the **ECI** frame, as shown earlier.



Summary

Canonical normalization is a useful **tool** for ensuring the accuracy of **numerical** calculations.

We further **note** that it is possible to go back to **initial** conditions from orbital **information** through a standard form of **transformation**.