



## *Planetary Flyby Concept*



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If an **arriving** spacecraft does not **impact**, it will **pass** the planet **by** if no further **action** is taken.

This motion is termed **flyby** as the spacecraft **flies** around the **planet** and, in the process, gets **influenced** by its gravitational field, **without** forming an **orbit**.



## ***Planetary Flyby Description***

However, as **spacecraft** remains in planet's **gravitational** field, there are **changes** to its energy and angular momentum that need to be **characterized**.

**Flybys** are extremely useful **techniques** to travel great distances in **space**.

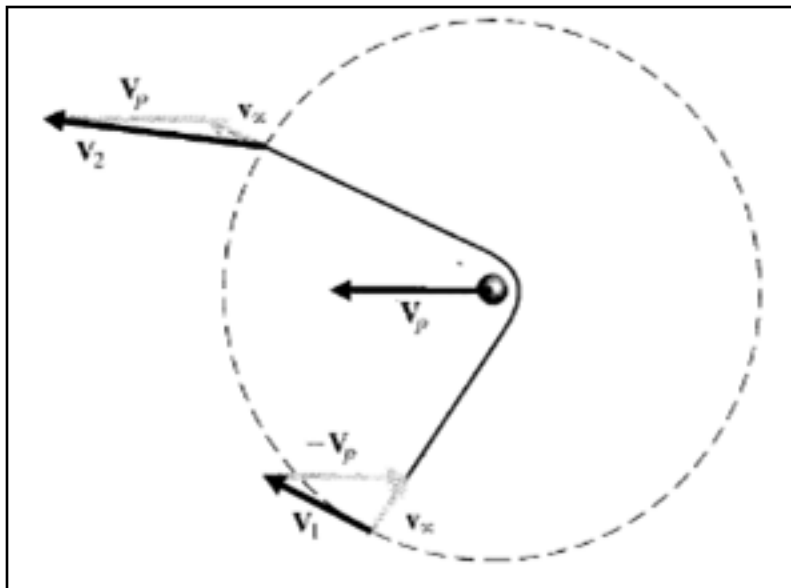


## *Unconstrained Flyby Solution*



## *Planetary Flyby Concept*

Consider the **schematic** of a **flyby** as given below.





## *Unconstrained Flyby Solution*

Here,  $V_1$  is the approach **velocity**,  $V_p$  is the planet orbital **velocity** and  $V_2$  is the exit velocity.

Also, subscript '**1**' is for the **entry** and subscript '**2**' is for the **exit** parameters.



## *Unconstrained Flyby Solution*

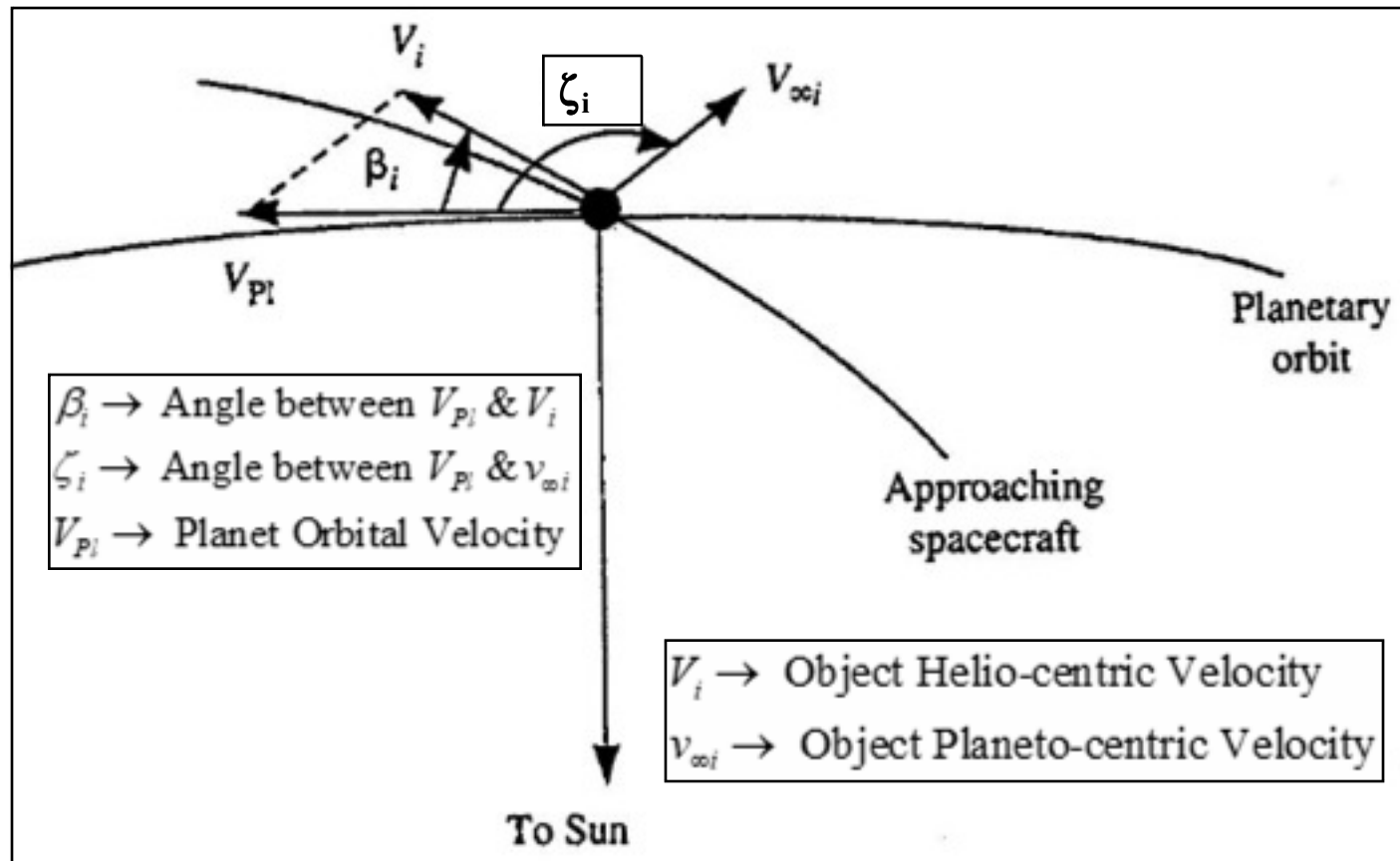
It is seen that the **velocity** vector gets **modified** due to the gravitational **field** of the planet.

As all **flybys** are executed on a **hyperbolic** path (arrival on **one** arm and departure on **other** arm), we can suitably **orient** it, in order to achieve specific **velocity** & direction.



## *General Flyby Formulation – Entry*

Consider the **schematic** of general **flyby**, as given below.







## *General Flyby Formulation – Entry*

The **basic** relations are as **follows**.

$$v_{\infty i} = \sqrt{V_{PI}^2 + V_i^2 - 2V_{PI}V_i \cos \beta_i}; \quad \frac{v_{\infty i}}{\sin \beta_i} = \frac{V_i}{\sin(180^\circ - \zeta_i)}$$
$$180^\circ - \zeta_i = \sin^{-1}\left(\frac{V_i \sin \beta_i}{v_{\infty i}}\right); \quad \text{If } \beta_i = 0^\circ \rightarrow \zeta_i = 180^\circ \text{ or } 0^\circ$$

It is to be **noted** that if  $V_i \cos \beta_i < V_{PI}$ , then  $\zeta_i > 90^\circ$ , otherwise,  $\zeta_i < 90^\circ$ . This means that when  $\beta_i = 0$ , then  $\zeta_i = 180^\circ$  for  $V_{PI} > V_i$  and  $\zeta_i = 0^\circ$  for  $V_{PI} < V_i$ .



## *General Flyby Formulation – Exit*

**Exit** parameters after a **flyby**, are obtained as follows.

$$\alpha = 180^\circ - \zeta_o; \quad v_{\infty i} = v_{\infty o} = v_\infty; \quad \cos \alpha = -\cos \zeta_o$$

$$V_o = \sqrt{V_{pl}^2 + v_\infty^2 + 2V_{pl}v_\infty \cos \zeta_o}; \quad \zeta_o = \zeta_i \pm \delta; \quad \delta = 2 \sin^{-1} \frac{1}{e}$$

$$\beta_o = \sin^{-1} \left( \frac{v_\infty \sin \zeta_o}{V_o} \right); \quad \varepsilon = \frac{v_{\infty i}^2}{2} = \frac{v_{\infty o}^2}{2} = \frac{v_\infty^2}{2}; \quad e = \sqrt{1 + \frac{2\varepsilon h^2}{\mu_{pl}^2}}$$

$$v_{periapsis} = \sqrt{2 \left( \varepsilon + \frac{\mu_{pl}}{r_{periapsis}} \right)}; \quad h = dV_\infty = r_{periapsis} v_{periapsis}$$





## *Summary*

Therefore, **we** see that flyby is executed on a **hyperbolic** path, and its nature is determined by the **arrival** parameters e.g. speed, **elevation** angle and the stand-off distance.