



## *Constant Pitch Formulation and Rate Solution*



## *‘V’ and ‘θ’ Solutions*

In this case, rocket is **commanded** to track a specified pitch **rate** i.e. (dθ/dt), so that velocity **solution** is obtained **directly**, as shown below.

$$\dot{\theta} = q_0 \rightarrow \theta(t) = q_0 t + \theta_0; \quad \dot{\theta} = q_0 = \frac{\tilde{g} \sin \theta}{V(t)} \rightarrow V(t) = \frac{\tilde{g} \sin \theta}{q_0}$$

We see that ‘V’ is a sinusoidal function of ‘θ’ and is also **inversely** proportional to ‘q<sub>0</sub>’, indicating a higher ‘V’ for both higher ‘θ’ and lower ‘q<sub>0</sub>’.



## ***‘V’ & ‘θ’ Solution Constraints***

As  $q_0$  is **constant**, we can write the following **relation** also at the **start** of the gravity **turn**.

$$q_0 = \frac{\tilde{g} \sin \theta_0}{V_0} \neq 0 \text{ or } \infty \rightarrow \theta_0 = 0 \text{ and/or } V_0 = 0 \text{ Not admissible.}$$

This means that **gravity** turn can only be **started** from a non-zero **‘θ’**, after it acquires a finite **‘V’**.



## ***‘V’ & ‘ $\theta$ ’ Solution Constraints***

This **requirement** is usually met by giving a **‘pitch kick’** to the vehicle at **appropriate** time.

Also, out of **‘ $q_0$ ’, ‘ $V_0$ ’ & ‘ $\theta_0$ ’, only **two** can be specified.**



## *‘m’ Solution*

The **tangential** equilibrium can then be **rewritten** as,

$$\dot{V} = -\frac{\dot{m}g_0I_{sp}}{m(t)} - \tilde{g} \cos \theta; \quad \frac{dV}{dt} = \dot{V} = \frac{d}{dt} \left( \frac{\tilde{g} \sin \theta}{q_0} \right) = \tilde{g} \cos \theta$$
$$\frac{dm}{m} = -\frac{2\tilde{g} \cos \theta dt}{g_0I_{sp}} = -\frac{2\tilde{g} \cos \theta d\theta}{q_0g_0I_{sp}}$$



## *‘m’ Solution*

**Integrating** both the sides, we get,

$$\ln m = -\frac{2\tilde{g} \sin \theta}{q_0 g_0 I_{sp}} + C \rightarrow \ln \frac{m_0}{m} = \frac{2\tilde{g}}{q_0 g_0 I_{sp}} (\sin \theta - \sin \theta_0)$$

It is seen that, **similar** to velocity, **mass** is also a **sinusoidal** function of ‘ $\theta$ ’ as well as **inversely** proportional to  $q_0$ .



## ***‘m’ Solution Features***

This **indicates** that for small ‘ $q_0$ ’, large ‘ $m_0$ ’ is **needed** to achieve **terminal** conditions.

Also, a **large** ‘ $q_0$ ’ will **reduce** terminal **velocity**.

Therefore, the **design** of ascent mission under **constant**  $q_0$  needs its **careful** selection.



## *‘t’ & ‘θ’ Solutions as Function of ‘m’*

We can **solve** for the flight **time**, as follows.

$$t_b = \frac{(\theta_b - \theta_0)}{q_0}$$

We can also **determine** the final burnout inclination, ‘ $\theta_b$ ’, from mass **solution**, as follows.

$$\theta_b = \sin^{-1} \left\{ \left( \frac{g_0 q_0 I_{sp}}{2\tilde{g}} \ln \frac{m_0}{m_b} \right) + \sin \theta_0 \right\}$$





## ***‘h’ Solution as Function of ‘θ’***

The **altitude** profile can be obtained by **resolving** the velocity **V** in vertical direction as **follows**.

$$\begin{aligned}\frac{dh}{dt} &= V \cos \theta \rightarrow \frac{dh}{d\theta} = \frac{V \cos \theta}{q_0} = \frac{\tilde{g} \sin \theta \cos \theta}{q_0^2} \\ \frac{dh}{d\theta} &= \frac{\tilde{g} \sin 2\theta}{2q_0^2} \rightarrow h(\theta) = \frac{\tilde{g}}{4q_0^2} (\cos 2\theta_0 - \cos 2\theta) + h_0\end{aligned}$$

We find that **altitude** is a cosine function of **‘2θ’**, indicating that it **reaches** its peak value for **θ = 90°**.



## ***‘x’ Solution as Function of ‘θ’***

**Final** parameter of interest is the **horizontal** distance, ‘x’ along **Earth’s** surface, which also impacts ‘θ’ solution. The requisite **relation** can be obtained as **follows**.

$$\begin{aligned}\frac{dx}{dt} &= V \sin \theta \rightarrow \int dx = \int V \sin \theta dt = \int \frac{\tilde{g} \sin^2 \theta}{q_0^2} d\theta \\ x &= \frac{1}{2q_0^2} \int \tilde{g} (1 - \cos 2\theta) d\theta + C = \frac{\tilde{g}}{2q_0^2} \left[ \theta - \left( 1 - \frac{\sin 2\theta}{2} \right) \right] + C \\ x(\theta) &= \frac{\tilde{g}}{2q_0^2} \left[ (\theta - \theta_0) - \frac{(\sin 2\theta - \sin 2\theta_0)}{2} \right] + x(\theta_0)\end{aligned}$$



## *Summary*

Therefore, to **summarize**, it is possible to obtain **closed** form solutions for **trajectory** under the assumption of **constant** pitch rate.

We also **note** that the solution, so **obtained**, fixes the trajectory **time** once the starting and **terminal** angles are specified.