

Flight Mechanics/Dynamics

Dr. Shashi Ranjan Kumar

Assistant Professor
Department of Aerospace Engineering
Indian Institute of Technology Bombay
Powai, Mumbai, 400076 India

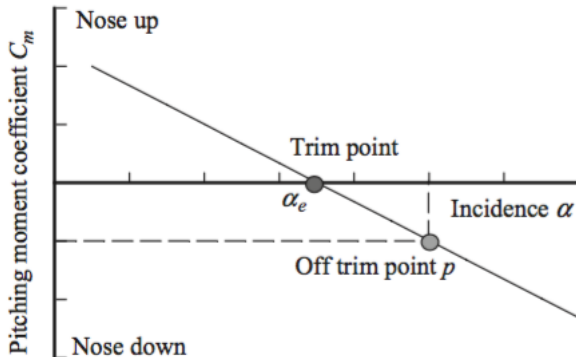




- Notions of stability: Static or Dynamic
- **Static stability:** If the forces and moments on the body caused by a disturbance tend initially to return the body toward its equilibrium position, the body is statically stable.
 - ⇒ No requirement of actual return of vehicle to equilibrium.
 - ⇒ If the forces and moments are such that the body continues to move away from its equilibrium position after being disturbed, the body is statically unstable.
- **Dynamic stability:** A body is dynamically stable if, of its own accord, it eventually returns to and remains at its equilibrium position over time.
- Static stability is related to initial tendency while dynamic stability focus on final state.



- An airplane can continue in steady unaccelerated flight only when the resultant external force and moment about the CG both vanish.
- Longitudinal balance: Zero pitching moment
- Nonzero pitching moment \Rightarrow Rotation in direction of unbalanced moment

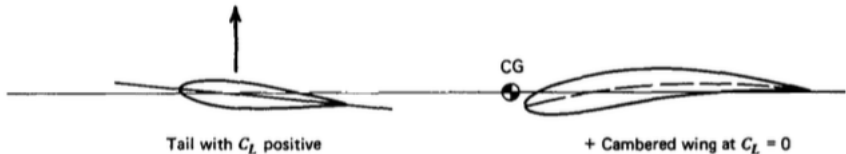




How most of airplanes are using positive camber airfoil?



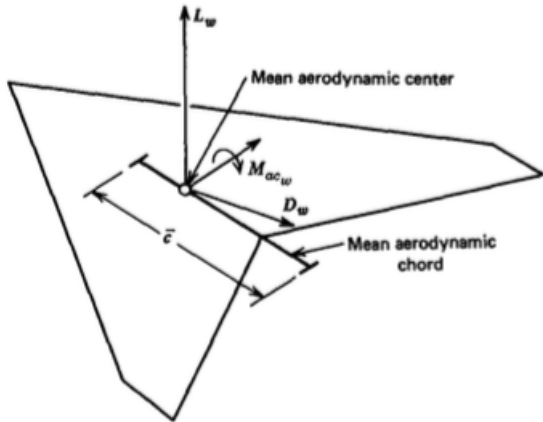
Any other possible configurations?

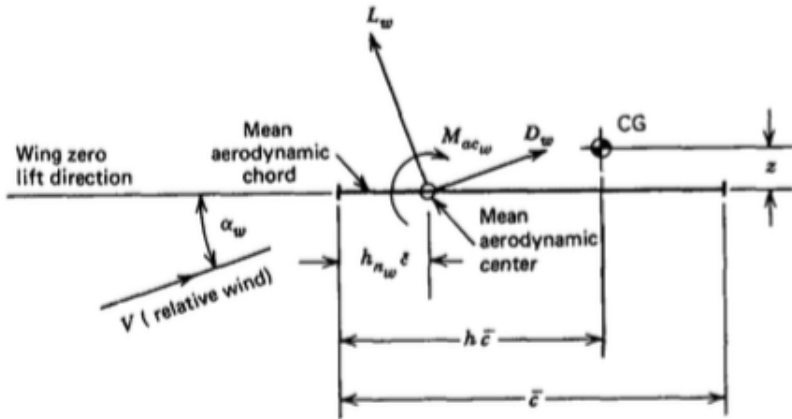


What about angle of attack for both configurations?



- How to obtain lift and pitching moment?
- Depends on $\alpha, \rho, \delta_i, M, T_i$, etc.
- Through wind tunnel test
- Contributions of various parts of airplane
- Aerodynamic forces and moment





- Pitching moment about CG

$$M_w = M_{ac_w} + (L_w \cos \alpha_w + D_w \sin \alpha_w)(h - h_{n_w})\bar{c} + (L_w \sin \alpha_w - D_w \cos \alpha_w)z$$



- For small α_w

$$M_w = M_{ac_w} + (L_w + D_w \alpha_w)(h - h_{n_w})\bar{c} + (L_w \alpha_w - D_w)z$$

- On dividing by $(1/2)\rho V^2 S \bar{c}$,

$$C_{m_w} = C_{m_{ac_w}} + \underbrace{(C_{L_w} + C_{D_w} \alpha_w)}_{\ll C_{L_w}}(h - h_{n_w}) + \underbrace{(C_{L_w} \alpha_w - C_{D_w})z/\bar{c}}_{\text{negligible}}$$

- On simplification,

$$\begin{aligned} C_{m_w} &= C_{m_{ac_w}} + C_{L_w}(h - h_{n_w}) \\ &= C_{m_{ac_w}} + \alpha_w a_w(h - h_{n_w}) \end{aligned}$$

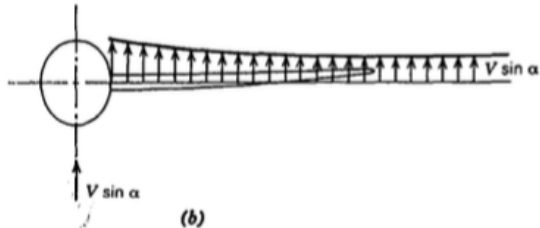
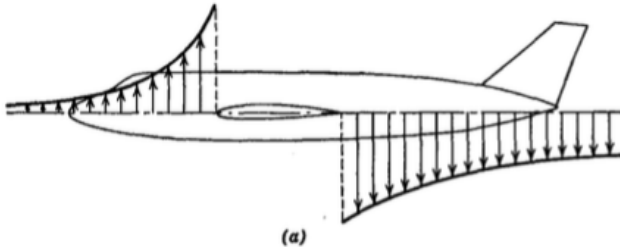
where a_w is the lift-curve slope of the wing.



- What is the effect of adding body and nacelles to the wing, on a moment coefficient?
- Will superposition of aerodynamic forces hold here?
- When wing and body are put together, however, a simple superposition of the aerodynamic forces that act upon them separately does not give a correct result.
- For wing-body combination,

$$\begin{aligned}C_{m_{wb}} &= C_{m_{ac_{wb}}} + C_{L_{wb}}(h - h_{n_{wb}}) \\ &= C_{m_{ac_{wb}}} + \alpha_{wb}a_{wb}(h - h_{n_{wb}})\end{aligned}$$

where a_{wb} is the lift-curve slope of the wing-body-nacelle combination.





Example 1

For a given wing-body combination, the aerodynamic center lies 0.05 chord length ahead of CG. Moment coefficient about the aerodynamic center is -0.016. If the lift coefficient is 0.45, calculate the moment coefficient about the CG.

- Moment coefficient about the CG

$$\begin{aligned}C_{m_{wb}} &= C_{m_{ac_{wb}}} + C_{L_{wb}}(h - h_{n_{wb}}) \\ &= -0.016 + 0.45 \times 0.05 = 0.0065\end{aligned}$$

Example 2

A wing-body model is tested in a subsonic wind tunnel. The lift is found to be zero at geometric $\alpha = -1.5^\circ$. At $\alpha = 5^\circ$ the lift coefficient is measured as 0.52. Also, at $\alpha = 1^\circ$ and 7.88° , the moment coefficients about CG are measured as -0.01 and 0.05, respectively. The CG is located at $0.35c$. Calculate the location of ac $h_{n_{wb}}$ and moment coefficient about aerodynamic center, $C_{m_{ac,wb}}$.



- Lift slope

$$a_{wb} = \frac{dC_L}{d\alpha} = \frac{0.52 - 0}{5 - (-1.5)} = 0.08/\text{deg}$$

- Moment coefficient about the CG

$$C_{m_{wb}} = C_{m_{ac_{wb}}} + a_{wb}\alpha_{wb}(h - h_{n_{wb}})$$

- On substituting values, we obtain

$$-0.01 = C_{m_{ac_{wb}}} + 0.08(1 + 1.5)(h - h_{n_{wb}})$$

$$0.05 = C_{m_{ac_{wb}}} + 0.08(7.88 + 1.5)(h - h_{n_{wb}})$$

- As $h = 0.35$, $h_{n_{wb}} = 0.24$ and $C_{m_{ac_{wb}}} = -0.032$.





- Lift and drag \perp and parallel to V' .
- Tail angle i_t is positive.
- Contribution of tail lift to the airplane lift $\perp V$ is $L_t \cos \epsilon - D_t \sin \epsilon$.
- As ϵ is always small, contribution reduces to L_t .
- Lift coefficient of the tail

$$C_{L_t} = \frac{L_t}{\frac{1}{2}\rho V^2 S_t}$$

- What about difference in V and V' magnitude?
 - \Rightarrow Accounted in tail lift-slope a_t
 - \Rightarrow Tail efficiency factor η_t
- Total lift of airplane $L = L_{wb} + L_t$, thus total lift coefficient

$$C_L = C_{L_{wb}} + \frac{S_t}{S} C_{L_t}$$



- Pitching moment about CG

$$M_t = M_{ac_t} - l_t [L_t \cos(\alpha_{wb} - \epsilon) + D_t \sin(\alpha_{wb} - \epsilon)] \\ - z_t [D_t \cos(\alpha_{wb} - \epsilon) - L_t \sin(\alpha_{wb} - \epsilon)]$$

- For small α_{wb} , with only dominant term

$$M_t = -l_t L_t = -l_t C_{L_t} \frac{1}{2} \rho V^2 S_t$$

- On dividing by $(1/2)\rho V^2 S \bar{c}$,

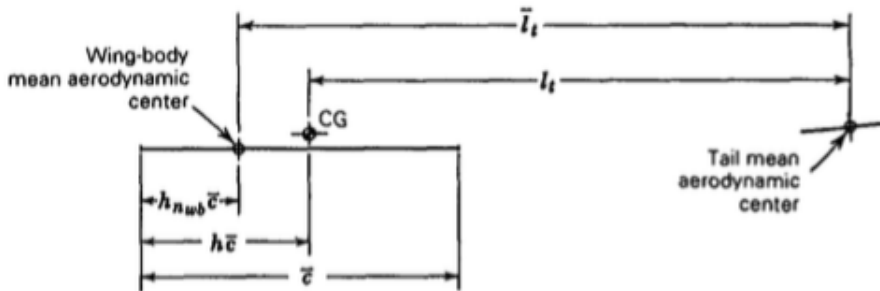
$$C_{m_t} = \frac{M_t}{(1/2)\rho V^2 S \bar{c}} = -\frac{l_t}{\bar{c}} \frac{S_t}{S} C_{L_t}$$

- On defining $V_H = \frac{l_t S_t}{\bar{c} S}$, we have

$$C_{m_t} = -V_H C_{L_t}$$



- What does V_H represent?
- A ratio of two volume characteristic of airplane geometry, called “horizontal tail volume ratio” or “tail volume”



- CG is not fixed so better to compute M_t about fixed point, mean aerodynamic center of wing-body combination.



- Define

$$\bar{V}_H = \frac{\bar{l}_t S_t}{\bar{c} S}$$

- We have the relation between two volume ratios

$$V_H = \bar{V}_H - \frac{S_t}{S}(h - h_{n_{wb}})$$

- Moment of the tail about the wing-body mean aerodynamic center

$$\bar{C}_{m_t} = -\bar{V}_H C_{L_t}$$

- Moment of tail about the CG

$$C_{m_t} = -\bar{V}_H C_{L_t} + C_{L_t} \frac{S_t}{S}(h - h_{n_{wb}}) = \bar{C}_{m_t} + C_{L_t} \frac{S_t}{S}(h - h_{n_{wb}})$$

- Pitching moment due to propulsive system, C_{m_p}



- Total pitching moments

$$C_m = C_{m_{ac_{wb}}} + C_L(h - h_{n_{wb}}) - \bar{V}_H C_{L_t} + C_{m_p}$$

- Pitch stiffness is given by $-C_{m_\alpha}$.

$$C_{m_\alpha} = \frac{\partial C_{m_{ac_{wb}}}}{\partial \alpha} + C_{L_\alpha}(h - h_{n_{wb}}) - \bar{V}_H \frac{\partial C_{L_t}}{\partial \alpha} + \frac{\partial C_{m_p}}{\partial \alpha}$$

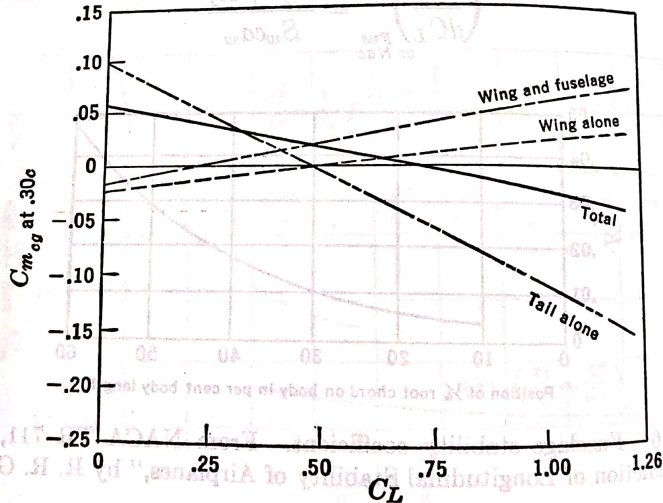
- As $\frac{\partial C_{m_{ac_{wb}}}}{\partial \alpha} = 0$, we have

$$C_{m_\alpha} = C_{L_\alpha}(h - h_{n_{wb}}) - \bar{V}_H \frac{\partial C_{L_t}}{\partial \alpha} + \frac{\partial C_{m_p}}{\partial \alpha}$$

- As C_{L_α} is large, magnitude of C_{m_α} is dictated by h .
- C_{m_α} can always be made negative by a suitable choice of h , CG location.
- When is $C_{m_\alpha} = 0$?

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Moment: Contributions from Components





- **Neutral point (NP):** A CG position h , for which $C_{m_\alpha} = 0$. Also known as “vehicle aerodynamic center”.
- A boundary between positive and negative pitch stiffness
- NP is given by

$$h_n = h_{n_{wb}} - \frac{1}{C_{L_\alpha}} \left[\frac{\partial C_{m_{acwb}}}{\partial \alpha} - \bar{V}_H \frac{\partial C_{L_t}}{\partial \alpha} + \frac{\partial C_{m_p}}{\partial \alpha} \right]$$

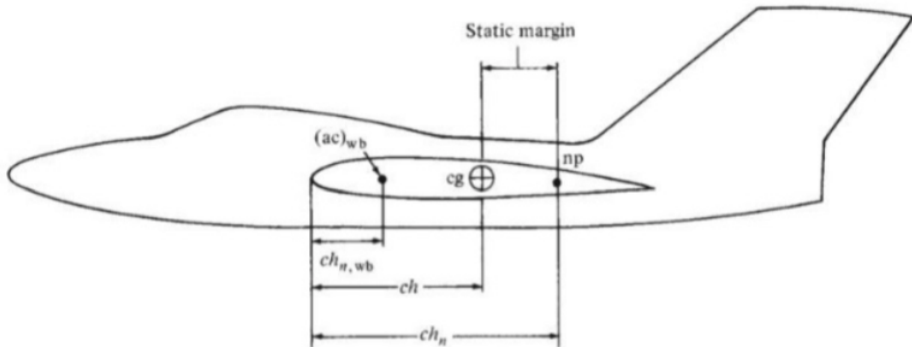
- C_{m_α} in terms of NP

$$C_{m_\alpha} = C_{L_\alpha} (h - h_n)$$

- **Static margin:** Difference between CG position and NP

$$K_n = h_n - h$$

- $K_n > 0 \implies C_{m_\alpha} < 0$, a positive stiffness
- For positive stiffness, CG must be forward to NP





- Farther forward CG \implies greater K , and in the sense of “static stability” a more stable vehicle.
- NP is sometimes defined as the CG location for which $\frac{dC_m}{dC_L} = 0$.
- Why is it so?
- C_L is a unique function of α under some restrictions and $\frac{dC_m}{dC_L} = \frac{\frac{\partial C_m}{\partial \alpha}}{\frac{\partial C_L}{\partial \alpha}}$
- Both $\frac{dC_m}{dC_L} = 0 = \frac{\partial C_m}{\partial \alpha}$ simultaneously.



Reference

- ① John Anderson Jr., *Introduction to Flight*, McGraw-Hill Education, Sixth Edition, 2017.
- ② Bernard Etkin and Llyod Duff Reid, *Dynamics of Flight Stability and Control*, John Wiley and Sons, Third Edition, 1996.

Thank you for your attention !!!