

Parallel Staging Benefits



Parallel Staging Design Benefits

The **bulky** booster stage provides the **following** benefits.

Firstly, it **limits** the velocity during the **dense** atmosphere, leading to lower **losses** due to drag and lesser **impact** of the atmospheric **disturbances**.

Secondly, it **marginally** improves the efficiency of the **first** stage, which needs to propel a **lower** mass and also can **use** the gravity turn manoeuvre **more** effectively.



Parallel Staging Operational Benefits

In addition, there are other aspects of parallel staging which provide mission operational flexibility, as explained below.

In many missions, in order to achieve a specific trajectory profile, we can sequence the firing of booster and first stages in a parallel mode, without the risk of interference.



Parallel Staging Operational Benefits

This **aspect** is evident from the **operation** of both PSLV and Space Shuttle, as **described** below.

In case of **PSLV**, which has **6** strap-on motors, **4**, along with the first stage, are **ignited** at lift-off, while the remaining **2** are ignited 25 s **later**.

Similarly, in Space shuttle, both the **boosters** operate along with the **first** stage, in order to provide a **heavy** lift capability (~ 29 T) at the **lift-off**.



Formulation for parallel staging is similar to the series staging in situations where strap-on stage is allowed to complete before the ignition of first stage.

However, in cases where **both** strap-on and first stage **operate** together, while the **basic** formulation **remains** same, actual **mass** solution depends on operational mode.



In **this** context, we consider the **general** case, when more than one rocket **engines** fire together.

In **such** a case, we know that **total** thrust is the algebraic **sum** of thrust of all the rocket **engines** firing together.

However, in **order** to use the already developed **relations**, we represent the multiple **rockets** as a single equivalent **rocket**, as shown next.



Following are the applicable equations for a equivalent single rocket stage.

$$\begin{split} T_0 &= \sum_{i=1}^n T_{0-i} = -g_0 \sum_{i=1}^n \dot{m}_{0-i} I_{sp0-i}; \quad \dot{m}_0 = \sum_{i=1}^n \dot{m}_{0-i} \\ T_0 &= -g_0 \dot{m}_0 I_{sp0}; \quad I_{sp-0} = \frac{T_0}{g_0 \dot{m}_0} = \frac{\sum_{i=1}^n \dot{m}_{0-i} I_{sp0-i}}{\sum_{i=1}^n \dot{m}_{0-i}} \end{split}$$

We see that I_{sp0} is now an **effective** mean I_{sp} of 0^{th} -stage.



In **such** a case, the stage-wise **ratios** that have been defined **earlier**, can be re-written as **follows**.

$$\in_{0} = \frac{\sum_{i=1}^{n} m_{z \cdot 0-i}}{\sum_{i=1}^{n} \left(m_{z \cdot 0-i} + m_{p \cdot 0-i} \right)}; \quad \pi_{0} = \frac{m_{01}}{m_{0}} = \frac{m_{0} - \sum_{i=1}^{n} \left(m_{z \cdot 0-i} + m_{p \cdot 0-i} \right)}{m_{0}}$$

We see that with these **definitions** for the booster stage, we can make use of the **velocity** and mass fraction relations **derived** previously for the series staging **case**.



Summary

To **summarize**, parallel staging formulation is **similar** to serial staging **formulation** in an overall manner.

However, we **need** to take into account the **differences** in the various rockets that **fire** together and also for **different** durations, leading to extra **numerical** effort.