



Constant ‘V’ Solution



Constant 'V' Concept

Gravity turn can also be **employed**, when the **vehicle** has reached desired **velocity** but does not have **inclination**.

Such a **manoeuvre** can be done either at the **start** of the mission or **towards** the end.

These **solutions** are simpler to obtain and **implement**.



Basic Formulation

Applicable **equations** for the case of **constant ‘V’** are as given below.

$$V = V_0; \quad \dot{\theta} = \frac{\tilde{g} \sin \theta}{V_0}; \quad \frac{1}{\sin \theta} d\theta = \frac{\tilde{g}}{V_0} dt$$
$$\dot{V} = -\frac{\dot{m} g_0 I_{sp}}{m(t)} - \tilde{g} \cos \theta = 0; \quad -\frac{dm}{m} = \frac{V_0 \cot \theta}{g_0 I_{sp}} d\theta$$

We see that we can **obtain** the solution for **‘θ’** as an **explicit** function of **‘t’**. Further, **‘m’** solution is obtained as function of **‘θ’**, which **becomes** the primary **variable**.



‘ θ ’ Solution as a Function of ‘ t ’

The solution for **pitch angle profile** is as given below.

$$\begin{aligned} dt &= \frac{V_0}{\tilde{g}} \frac{d\theta}{\sin \theta}; \quad \int dt = \frac{V_0}{\tilde{g}} \int \frac{d\theta}{\sin \theta} \rightarrow t = \frac{V_0}{\tilde{g}} \ln \tan \frac{\theta}{2} + C \\ t - t_0 &= \Delta t = \frac{V_0}{\tilde{g}} \left(\ln \tan \frac{\theta}{2} - \ln \tan \frac{\theta_0}{2} \right) \\ \Delta t &= \frac{V_0}{\tilde{g}} \ln \left(\frac{\tan \frac{\theta}{2}}{\tan \frac{\theta_0}{2}} \right) \rightarrow \tan \frac{\theta}{2} = \tan \frac{\theta_0}{2} e^{\frac{\tilde{g} \Delta t}{V_0}} \end{aligned}$$

We see that a **higher ‘ Δt ’** would give **higher ‘ θ ’**.



‘m’ Solution as a Function of ‘θ’

The **mass** solution for constant **V** **case** is as follows.

$$\int \frac{dm}{m} = -\frac{V_0}{g_0 I_{sp}} \int \frac{\cos \theta}{\sin \theta} d\theta \rightarrow \ln m = -\frac{V_0}{g_0 I_{sp}} \ln(\sin \theta) + C$$
$$m(\theta) = k(\sin \theta)^{-\frac{V_0}{g_0 I_{sp}}}; \quad k = m_0(\sin \theta_0)^{\frac{V_0}{g_0 I_{sp}}}; \quad \frac{m}{m_0} = \left(\frac{\sin \theta}{\sin \theta_0} \right)^{-\frac{V_0}{g_0 I_{sp}}}$$

It is found that a **higher ‘θ’** results in higher **propellant** to be burnt.



‘h’ & ‘x’ Solutions

Applicable **equations** & solutions for **‘h’ & ‘x’** profiles are as given below.

$$\begin{aligned}\frac{dh}{dt} &= V_0 \cos \theta \rightarrow \int dh = \frac{V_0^2}{\tilde{g}} \int \frac{\cos \theta}{\sin \theta} d\theta; \quad h = \frac{V_0^2}{\tilde{g}} \ln \sin \theta + C \\ h - h_0 &= \frac{V_0^2}{\tilde{g}} (\ln \sin \theta - \ln \sin \theta_0); \quad \Delta h = \frac{V_0^2}{\tilde{g}} \ln \frac{\sin \theta}{\sin \theta_0} \\ \frac{dx}{dt} &= V_0 \sin \theta \rightarrow \int dx = \frac{V_0^2}{\tilde{g}} \int d\theta; \quad x = \frac{V_0^2}{\tilde{g}} \theta + C; \quad \Delta x = \frac{V_0^2}{\tilde{g}} \Delta \theta\end{aligned}$$



Summary

To **summarize**, we note that constant **velocity** solutions are simpler to **obtain**.

Further, these **solutions** provide explicit control over **propellant** mass for a desired velocity and **inclination**.