



Hohmann Manoeuvre



Single Impulse Change Restrictions

The **single** impulse based orbit change **solution**, seen previously, does not **provide** complete freedom due to **under-actuation**.

I.e., **we** have only one **input** impulse, but **want** to change **three** degrees-of-freedom, 'a', 'e' and ' ω '.



Unconditional Orbit Changes

Thus, we find that only **one** degree-of-freedom will be as per our **requirement**, while the other **two** would take **specific** values, as dictated by the **constraint**.

This situation can be **remedied** by increasing the number of **inputs**.



Two-impulse Orbit Changes

It should be noted that while **we** need three degrees-of-freedom to **change** all unconditionally, in general there is a **greater** need for change in **shape** and size of the **orbit**.

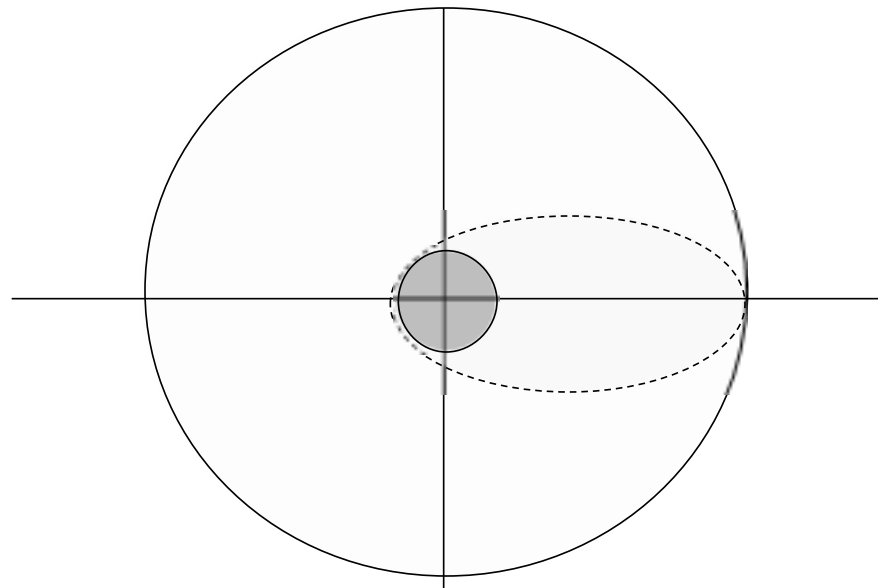
Thus, we can **restrict** ourselves to only **two** velocity impulses for the task of changing '**a**' and '**e**'.

Among the **many** possibilities, we consider the **one** which preserves ' **ω** ' and is also a **minimum** time solution, called '**Hohmann**' transfer.



Hohmann Transfer Concept

Hohmann strategy involves two **impulses**, first one given at **perigee** and second one at **apogee**, as shown below.





Two-Impulse Transfer Strategy

In this case, **first** impulse is given at the **perigee** to put the **satellite** on a transfer **ellipse**.

Second **impulse** is given once the satellite **reaches** apogee of the transfer **ellipse** (after half a cycle), so that orbit becomes the outer circle.

Thus, total **tangential** velocity impulse is the **sum** of the two velocity **impulse** magnitudes.



Two-Impulse Transfer Strategy

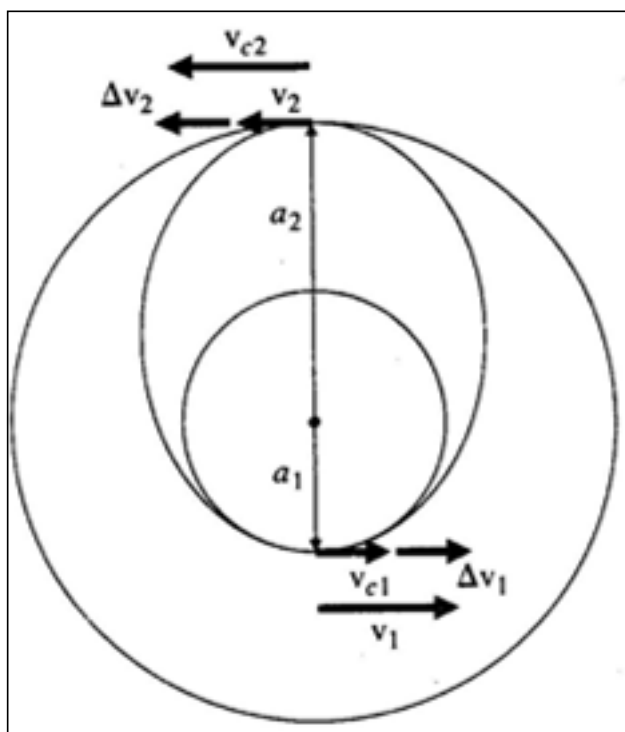
This **manoeuvre** is found to be most **fuel** efficient and also is a **good** solution for total ' ΔV '.

Hohmann transfer can be used between **any** two orbits, and can also be **employed** for inter-planetary **transfers**.



Hohmann Transfer Solution - Circles

Hohmann transfer between **circles** is as shown below.



$$a = \frac{a_1 + a_2}{2}, \quad V^2 = \mu \left(\frac{2}{r} - \frac{1}{a} \right)$$

$$\Delta V_1 = \sqrt{\frac{2\mu}{a_1} - \frac{2\mu}{a_1 + a_2}} - \sqrt{\frac{\mu}{a_1}}$$

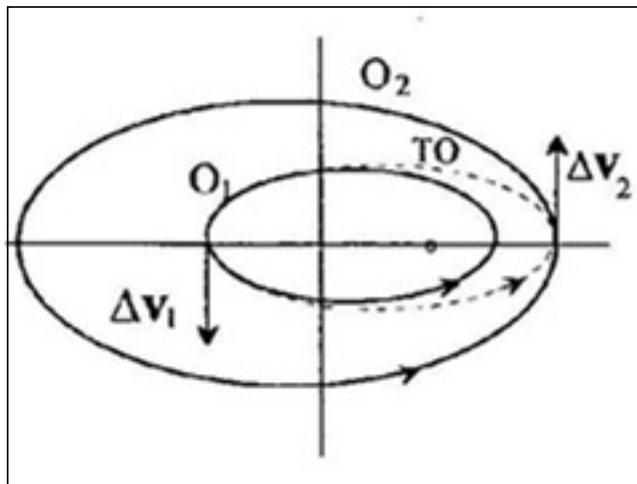
$$\Delta V_2 = \sqrt{\frac{\mu}{a_2}} - \sqrt{\frac{2\mu}{a_2} - \frac{2\mu}{a_1 + a_2}}$$

$$\Delta V = \Delta V_1 + \Delta V_2; \quad \Delta t = \pi \sqrt{\frac{a^3}{\mu}}$$



Hohmann Transfer Solution - Ellipses

Solution for **Hohmann** transfer between two **ellipses**, is as shown below.



$$r_{aTO} = r_{a2}, \quad r_{pTO} = r_{p1}, \quad a_{TO} = \frac{r_{p1} + r_{a2}}{2}$$

$$\Delta V_1 = \sqrt{\frac{2\mu}{r_{pTO}} - \frac{\mu}{a_{TO}}} - \sqrt{\frac{2\mu}{r_{pTO}} - \frac{\mu}{a_1}}$$

$$\Delta V_2 = \sqrt{\frac{2\mu}{r_{TO}} - \frac{\mu}{a_2}} - \sqrt{\frac{2\mu}{r_{aTO}} - \frac{\mu}{a_{TO}}}$$

$$\Delta V = \Delta V_1 + \Delta V_2; \quad \Delta t = \pi \sqrt{\frac{a_{TO}^3}{\mu}}$$



Low Thrust Orbital Transfer



Impulsive Manoeuvre Drawback

Impulsive orbital manoeuvres, discussed previously, require **large** thrusts, to achieve even a modest ' ΔV '.

However, for **small** orbital drifts, **low** thrust orbit corrections are **preferred**, as time is not a major **issue**.



Low Thrust Orbit Transfer Concept

Such manoeuvres can be **performed** using either **small** plasma **jets** or even solar **pressure**.

However, it can take **large** time as **energy** per transfer cycle is quite **small**.

Transfer path for such **manoeuvres** is an approximate circular **spiral**.



Low Thrust Formulation & Solution

Consider the **transfer** between two **circular** orbits.

If 'A' is **acceleration** applied in the **direction** of instantaneous **velocity**, we can obtain $\Delta \mathbf{V}$ as follows.

$$\begin{aligned}\varepsilon(t) &= -\frac{\mu}{2a(t)} \rightarrow \frac{d\varepsilon}{dt} = \frac{\mu}{2a^2} \cdot \frac{da}{dt} = \vec{A} \cdot \vec{v}(t); \quad v(t) = \sqrt{\frac{\mu}{a(t)}} \\ \frac{da}{dt} &= \frac{2}{\sqrt{\mu}} a^{3/2} \cdot A \rightarrow \int_{t_0}^{t_1} A \cdot dt = \frac{\sqrt{\mu}}{2} \int_{a_0}^{a_1} \frac{da}{a^{3/2}} = \frac{\sqrt{\mu}}{2} \left[-2a^{-1/2} \right]_{a_0}^{a_1} \\ A \cdot \Delta t &= \Delta V = \sqrt{\frac{\mu}{a_0}} - \sqrt{\frac{\mu}{a_1}}; \quad \Delta t = \frac{\Delta V}{A}\end{aligned}$$



Low Thrust Orbit Transfer Attributes

We see that in case of **low** thrust transfer, required velocity **impulse** is exactly equal to the **difference** between the velocities in **respective** circular orbits.

However, for the **same** orbit change, ΔV for **Hohmann** transfer is as given **below**.

$$\Delta V = \left(1 - \frac{a_0}{a_1}\right) \sqrt{\frac{2\mu a_1}{a_0(a_0 + a_1)}} - \left(\sqrt{\frac{\mu}{a_0}} - \sqrt{\frac{\mu}{a_1}}\right)$$



Summary

Hohmann transfer strategy is an **elegant** two-impulse model that is **able** to achieve all kinds of **orbits** in a reasonably efficient **manner**.

We also see that low thrust **orbital** transfer provides an **alternative** method to change orbits, where **time** is not a major **concern**.