

Info:  $C_f = .001$ ,  $C_d = 1$  for sphere assumption

Source: Introduction to Flight

#### EXAMPLE 8.11

Consider two bodies in circular orbit around the earth at an altitude of 800 km above the surface of the earth. Each body has a mass of 1800 kg. One body is a slender cone with a total vertex angle of  $10^\circ$ . The other body is a sphere. For the cone, the pressure drag coefficient at hypersonic Mach numbers is 0.017 and the skin friction drag coefficient is 0.01. For the sphere, the pressure drag coefficient is 1.0 and the friction drag coefficient is 0.001. Calculate and compare the total aerodynamic heating input to each body during atmospheric entry.

#### ■ Solution

The entry velocity of both bodies from orbit is obtained from Eq. (8.57), where  $r = r_e + h_0$ , and  $r_e$  is the radius of the earth,  $r_e = 6.4 \times 10^6$  m, and  $h_0$  is the geometric altitude above sea level,  $h_0 = 800$  km  $= 0.8 \times 10^6$  m.

$$V_E = \sqrt{\frac{k^2}{r}} = \sqrt{\frac{3.986 \times 10^{14}}{(6.4 + 0.8) \times 10^6}} = 0.789 \times 10^4 \text{ m/sec}$$

The total heat input is given by Eq. (8.155), repeated here:

$$Q_{\text{total}} = \frac{1}{2} \frac{C_f}{C_D} \left( \frac{1}{2} m V_E^2 \right) \quad (8.155)$$

where

$$\frac{1}{2} m V_E^2 = \frac{1}{2} (1800)(0.789 \times 10^4)^2 = 5.60 \times 10^{10} \text{ joule}$$

a. For the cone:

$$C_D = C_{D_p} + C_f = 0.017 + 0.01 = 0.027$$

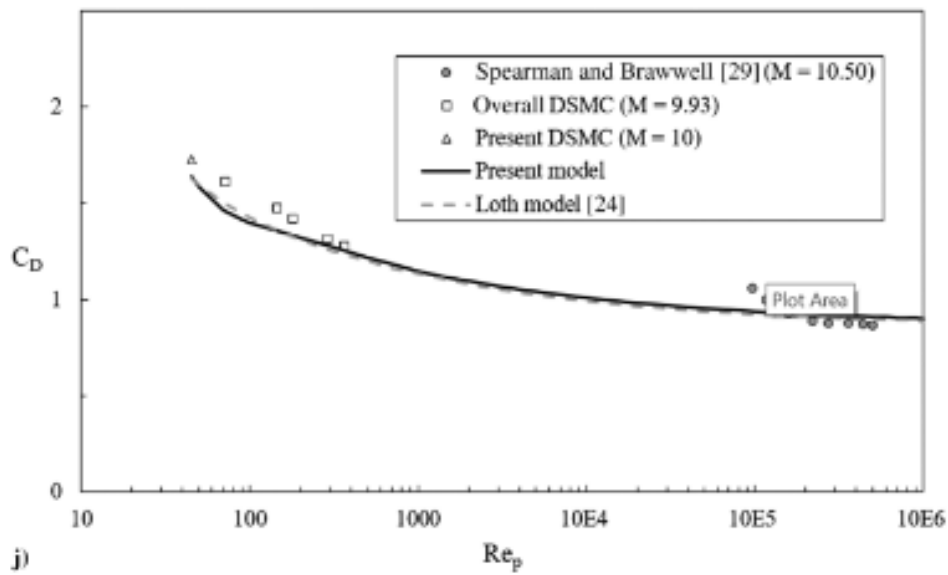
$$\frac{C_f}{C_D} = \frac{0.01}{0.027} = 0.37$$

From Eq. (8.155),

$$Q_{\text{total}} = \frac{1}{2} (0.37)(5.6 \times 10^{10}) = \boxed{1.036 \times 10^{10} \text{ joule}} \text{ (cone)}$$

Info:  $C_d$  vs  $Re$  @ mach 10+ graph. Suggests  $C_d$  approaches 1 like example problem gave. Validation.

Source: Supersonic and Hypersonic Drag Coefficients for a Sphere <https://doi.org/10.2514/1.J060153>



**Fig. 7 (Continued)**

Info: Re range from 800 to 50 km yields  $C_d$  1.5 to 1

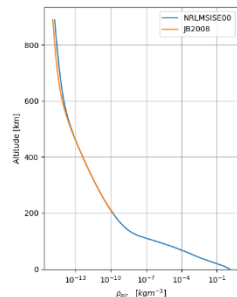
800:  $(10^{-14} \text{ kg/m}^3) \cdot (945 \text{ m/s}) \cdot (3.5 \text{ m}) / (1.825 \cdot 10^{-5} \text{ kg/m-s}) = 1.812\text{E-6}$

50:  $10^{-3} \cdot (945) \cdot (3.5) / (6.63 \cdot 10^{-5}) = 4.989\text{E4}$

Locks in example problem giving 1 as  $C_d$

Source: Google Images Graph for density

[https://www.engineersedge.com/physics/viscosity\\_of\\_air\\_dynamic\\_and\\_kinematic\\_14483.htm](https://www.engineersedge.com/physics/viscosity_of_air_dynamic_and_kinematic_14483.htm)



Info: Heat equation.  $Q = 1.17717\text{E6 J}$

Source: Introduction to Flight

Equating Eqs. (8.153) and (8.151),

$$\frac{dQ}{dV_\infty} \left( -\frac{1}{2m} \rho_\infty V_\infty^2 S C_D \right) = \frac{1}{4} \rho_\infty V_\infty^2 S C_f$$

or 
$$\frac{dQ}{dV_\infty} = -\frac{1}{2} m V_\infty \frac{C_f}{C_D}$$

or 
$$dQ = -\frac{1}{2} m \frac{C_f}{C_D} \frac{dV_\infty^2}{2} \quad (8.154)$$

Integrate Eq. (8.154) from the beginning of entry, where  $Q = 0$  and  $V_\infty = V_E$ , and the end of entry, where  $Q = Q_{\text{total}}$  and  $V_\infty = 0$ :

$$\int_0^{Q_{\text{total}}} dQ = -\frac{1}{2} \frac{C_f}{C_D} \int_{V_E}^0 d \left( m \frac{V_\infty^2}{2} \right)$$

$$\boxed{Q_{\text{total}} = \frac{1}{2} \frac{C_f}{C_D} \left( \frac{1}{2} m V_E^2 \right)} \quad (8.155)$$

Equation (8.155) is the desired result for total heat input to the entry vehicle. It is an important relation—examine it closely. It reflects two vital conclusions:

1. The quantity  $\frac{1}{2} m V_E^2$  is the initial kinetic energy of the vehicle as it first enters

Info: Q to the 6<sup>th</sup> J is a reasonable amount. Validated.

Source: Intro to Flight

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b. For the sphere:

$$C_D = C_{D_p} + C_f = 1.0 + 0.001 = 1.001$$

$$\frac{C_f}{C_D} = \frac{0.001}{1.001} = 0.999 \times 10^{-4}$$

From Eq. (8.155),

$$Q_{\text{total}} = \frac{1}{2} (0.999 \times 10^{-4})(5.6 \times 10^8) = \boxed{2.8 \times 10^4 \text{ joule}} \text{ (sphere)}$$

As expected, the sphere, being a much blunter body, experiences a much smaller total heat input compared to the slender cone.

- Online can find unit of heat per area material can absorb
- Use found Q to calculate thickness and area
- Now you can find gradient of temperature independent of full craft. Check inner layer meets requirements

Dragonfly: <https://ntrs.nasa.gov/api/citations/20190028683/downloads/20190028683.pdf>

$$2.5\text{E}2 \text{ W/cm}^2 = 2.5\text{E}6 \text{ W/m}^2$$

.0366 m thickness

3.75 m diameter

Allowable: <https://ntrs.nasa.gov/api/citations/20160006481/downloads/20160006481.pdf>

$$4\text{E}2 \text{ W/cm}^2$$


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Info: peak heat flux of  $11.3 \text{ MW/m}^2$ ,

heat load of  $209 \text{ MJ/m}^2$

Used those ^ numbers to make relationship with dragonfly

- **Entry heat pulse: 250 sec.**
  - Peak heat flux  $250 \text{ W/cm}^2$  margined

Got dragonfly expected heat load and divided by expected time of descent 250 s to get average heat load of 184,000

Source:

<https://www.tsijournals.com/articles/ablative-heat-shield-design-for-a-sample-return-vehicle.pdf>

<https://ntrs.nasa.gov/api/citations/20190028683/downloads/20190028683.pdf>