

MOLPOP Line Emission Output

Moshe; May 12, 2017

The entire line flux at position τ is

$$F(\tau) = \int_{-\infty}^{\infty} F_{\nu}(\tau) d\nu = \Delta\nu \int_{-\infty}^{\infty} F_{\nu}(\tau) dx \quad (1)$$

We introduced the line cooling rate per unit area ($\text{erg cm}^{-2} \text{ s}^{-1}$) and the cooling factor j via

$$\Lambda = F(\tau_t) - F(0) = 4\pi\Delta\nu j \quad (2)$$

taking account of emission from the two faces of the slab (eq. 4, 2006 CEP paper). As we show in eq. 93 of our CEP notes (where we used \mathcal{E} for Λ), in the case of 1-zone we have

$$j = S\tau_t\beta(\tau_t) = \epsilon\ell\beta(\tau_t) \quad (3)$$

where ϵ is the emission coefficient and ℓ is the slab thickness. Therefore, the $u \rightarrow l$ transition has

$$\Lambda_{u,l} = 4\pi\Delta\nu\epsilon_{u,l}\beta_{u,l}\ell = h\nu_{u,l}A_{u,l}\beta_{u,l}n_u\ell = h\nu_{u,l}A_{u,l}\beta_{u,l}\frac{n_u}{n}N \quad (4)$$

where n_u is the population of the upper level, n is the overall molecular density and N is its column density. Since N is the overall number of molecules per unit area, the cooling rate per molecule (erg s^{-1} per molecule) is

$$\text{cool}_{u,l} = \frac{\Lambda_{u,l}}{N} = h\nu_{u,l}A_{u,l}\beta_{u,l}\frac{n_u}{n} \quad (5)$$

and the flux is

$$F(\tau_t) = -F(0) = \frac{1}{2}\Lambda_{u,l} = \frac{1}{2}\text{cool}_{u,l}N \quad (6)$$

MOLPOP Implementation

We use the variables $\mathbf{x}(i)$ so that

$$\mathbf{n}(i) = \mathbf{nmol} * \mathbf{x}(i) * \mathbf{we}(i) \quad (7)$$

is the population of level i , with $\mathbf{we}(i)$ its weight factor. Therefore

$$\mathbf{n}(i)\mathbf{A}(i, j) = \mathbf{nmol} * \mathbf{x}(i) * [\mathbf{we}(i)\mathbf{A}(i, j)] \quad (8)$$

and in MOLPOP we absorb the weight factor into the A -coefficient. So after that is done,

$$\text{cool}(i, j) = \mathbf{ems}(i, j) * \mathbf{esc}(i, j) * \mathbf{x}(i) \quad (9)$$

(in subroutine `lines`) where

$$\mathbf{ems}(i, j) = h\nu(i, j) * \mathbf{A}(i, j) \quad (10)$$

is defined right after A is scaled with `we(i)` at the end of subroutine `INPUT`. Therefore, the flux should be defined as

$$F(i, j) = \frac{1}{2} \text{cool}(i, j) * \text{nmol} * R \quad (11)$$

This will give the result in $\text{erg cm}^{-2} \text{s}^{-1}$. Switch to MKS: $W = 10^7 \text{ erg s}^{-1}$ and $\text{m}^2 = 10^4 \text{ cm}^2$ so $W \text{ m}^{-2} = 10^{7-4} \text{ erg cm}^{-2} \text{s}^{-1}$ and $\text{erg cm}^{-2} \text{s}^{-1} = 10^{-3} W \text{ m}^{-2}$. Therefore

$$F(i, j) = \text{aux} * \text{cool}(i, j) \quad W \text{ m}^{-2} \quad (12)$$

where

$$\text{aux} = .5 * 10^{-3} \text{nmol} * R \quad (13)$$