

Parámetros estáticos y dinámicos de dispositivos de medición

Mediciones Biomédicas 2024 Ingeniería Civil Biomédica

Alejandro Veloz alejandro.veloz@uv.cl

- Criterios cuantitativos de desempeño de los instrumentos.
 - De especial utilidad para comparar equipos y evaluar nuevas tecnologías y diseños.
- Estos criterios especifican cuán bien un instrumento mide una variable de interés y cuánto la salida depende de señales modificantes y de interferencia.
- Estas características se pueden dividir en dos clases, las cuales dependen de las frecuencias de las señales de entrada.
 - Características estáticas: describe el desempeño de los instrumentos para entradas de baja frecuencia, incluyendo la frecuencia fundamental (dc).
 - Características dinámicas: requiere el uso de ecuaciones diferenciales para describir la calidad de las mediciones.

Parámetros estáticos

Exactitud (accuracy):

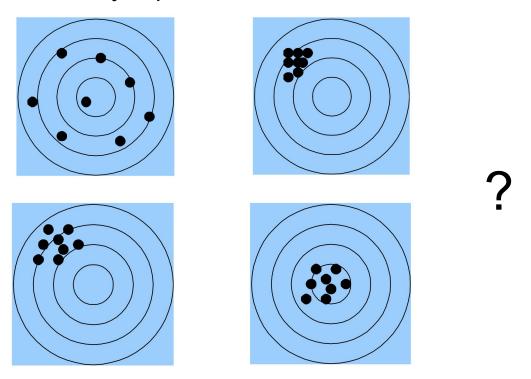
(valor real – valor medido) / valor real

Precisión: número de alternativas distinguibles en un resultado. Por ejemplo, la medición 2.434 V es más precisa que la lectura 2.43 V. Alta precisión no implica alta exactitud.

Resolución: La cantidad incremental más pequeña que puede ser medida.

Reproducibilidad o repetitividad: Mismos valores de salida ante los mismos valores de entrada.

La mayor parte del quehacer en el diseño de equipos de bioinstrumentación está en obtener la mayor exactitud, precisión, resolución y reproducibilidad.



Control (estadístico): asegura que variaciones aleatorias en las condiciones de operación son tolerables.

Sensibilidad estática: medida de la variación de la salida respecto de la variación de la entrada.

Deriva (drift) del origen: Traslado del origen.

Deriva (drift) de sensibilidad: La pendiente de la curva de calibración cambia de manera proporcional a la magnitud de la entrada.



Sensor de presión sanguínea Merit BP series

SPECIFICATIONS

Parameter	Minimum	Typical	Maximum	Units	Notes
Performance 1					I
Offset	-25	0	25	mmHg	Zero
Sensitivity	4.95	5	5.05	μV/V/mmHg	
Calibration	97.5	100	102.5	mmHg	2
Symmetry	-5		5	%	
Accuracy (-30 to 50 mmHg)	-1 mmHg - 1% of Reading	0	+1 mmHg + 1% of Reading		6 - Per AAMI BP22
Accuracy (50 to 300 mmHg)	-3	0	3	% of Reading	6 - Per AAMI BP22
Temp Coeff – Zero	-0.3	0	0.3	mmHg/°C	3, 5
Temp Coeff – Sensitivity	-0.1	0	0.1	%/°C	3, 5
Frequency Response	1,200			Hz	5
Phase Shift			5	degrees	5
Offset Drift			1	mmHg/8 hrs	4, 5

$$m = \frac{n \sum x_{d}y - (\sum x_{d})(\sum y)}{n \sum x_{d}^{2} - (\sum x_{d})^{2}}$$

$$b = \frac{(\sum y)(\sum x_{\mathrm{d}}^2) - (\sum x_{\mathrm{d}}y)(\sum x_{\mathrm{d}})}{n\sum x_{\mathrm{d}}^2 - (\sum x_{\mathrm{d}})^2}$$

$$y = mx_d + b$$

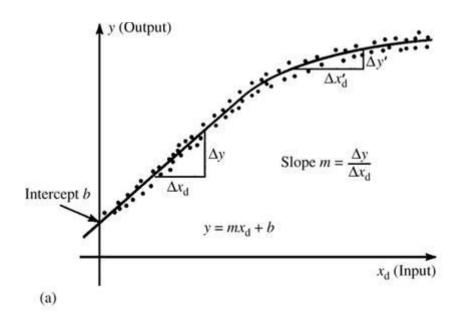
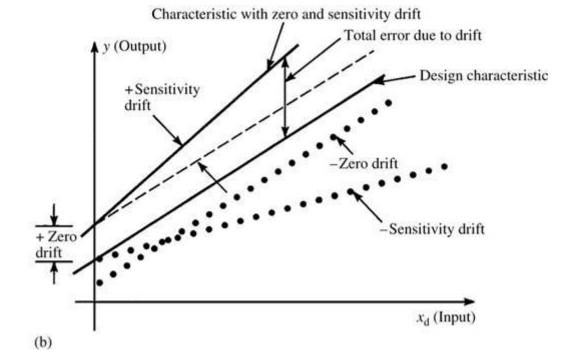


Figure 1.3 (a)

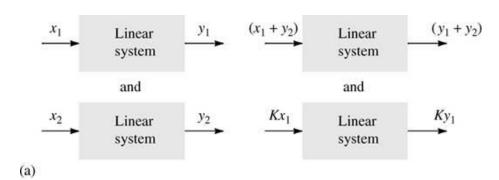
Static-sensitivity curve that relates desired input x_d to output y. Static sensitivity may be constant for only a limited range of inputs, (b) Static sensitivity: zero drift and sensitivity drift. Dotted lines indicate that zero drift and sensitivity drift can be negative.

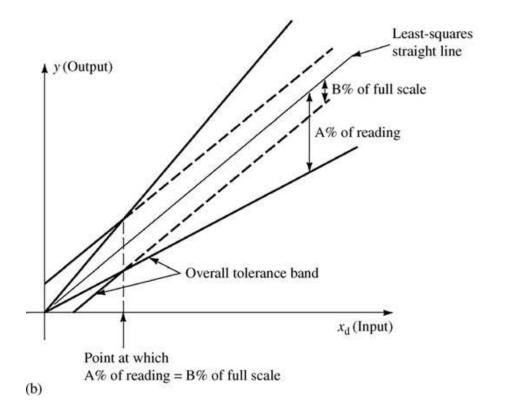


Linealidad: propiedad de un sistema que satisface la homogeneidad y superposición.

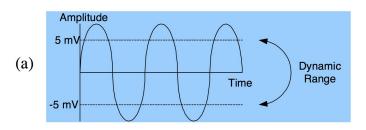
Figure 1.4 (a) Basic definition of linearity for a system.

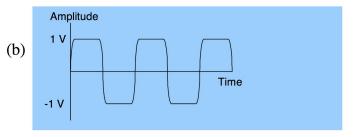
The same linear system or element is shown four times for different inputs, (b) A graphical illustration of independent nonlinearity equals ±A% of the reading, or ±B% of full scale, whichever is greater (that is, whichever permits the larger error).





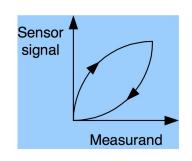
Rangos de entrada: rango de operación máximo es el rango de valores de entrada que no produce daños en el sensor, el rango de operación lineal es aquel que produce una relación lineal entrada-salida. Rango dinámico.





Impedancia de entrada: permite evaluar el grado en el cual el instrumento de medición influye en la cantidad medida.

Histéresis: La curva de salida es diferente cuando la cantidad medida aumenta y cuando disminuye.



Parámetros dinámicos

Características dinámicas

La mayoría de los instrumentos médicos miden y/o procesan cantidades que varían con el tiempo, por lo tanto, estudiar las características dinámicas de estos instrumentos es relevante.

Se requieren ecuaciones que den cuenta de estas variaciones: ecuaciones diferenciales y sus múltiples herramientas y representaciones.

$$a_n \frac{d^n y}{dt^n} + \dots + a_1 \frac{dy}{dt} + a_0 y(t) = b_m \frac{d^m x}{dt^m} + \dots + b_1 \frac{dx}{dt} + b_0 x(t)$$

$$a_n \frac{d^n y}{dt^n} + \dots + a_1 \frac{dy}{dt} + a_0 y(t) = b_m \frac{d^m x}{dt^m} + \dots + b_1 \frac{dx}{dt} + b_0 x(t)$$
$$(a_n D^n + \dots + a_1 D + a_0) y(t) = (b_m D^m + \dots + b_1 D + b_0) x(t)$$

$$a_n \frac{d^n y}{dt^n} + \dots + a_1 \frac{dy}{dt} + a_0 y(t) = b_m \frac{d^m x}{dt^m} + \dots + b_1 \frac{dx}{dt} + b_0 x(t)$$
$$(a_n D^n + \dots + a_1 D + a_0) y(t) = (b_m D^m + \dots + b_1 D + b_0) x(t)$$

$$\frac{y(D)}{x(D)} = \frac{b_m D^m + \dots + b_1 D + b_0}{a_n D^n + \dots + a_1 D + a_0}$$

$$\frac{Y(j\omega)}{X(j\omega)} = \frac{b_m (j\omega)^m + \dots + b_1 (j\omega) + b_0}{a_n (j\omega)^n + \dots + a_1 (j\omega) + a_0}$$

Instrumentos de orden 0, 1, 2, ...

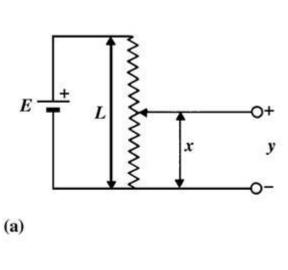
Instrumento de orden cero

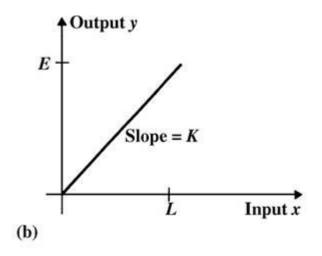
$$a_0 y(t) = b_0 x(t)$$

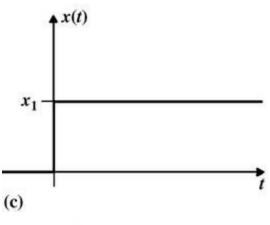
$$\frac{y(D)}{x(D)} = \frac{Y(j\omega)}{X(j\omega)} = \frac{b_0}{a_0} = K = \text{static sensitivity}$$

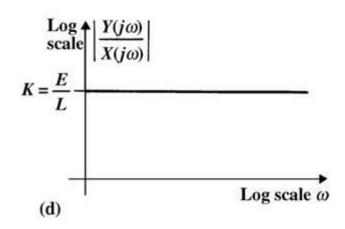
La salida es proporcional a la entrada para todas las frecuencias, por lo tanto, no hay distorsión de amplitud o fase.

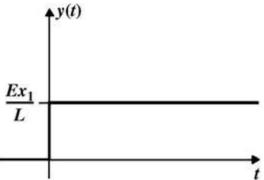
Figure 1.5 (a) A linear potentiometer, an example of a zero-order system, (b) Linear static characteristic for this system, (c) Step response is proportional to input, (d) Sinusoidal frequency response is constant with zero phase shift.

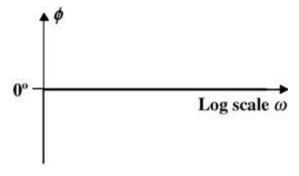












Instrumento de primer orden

$$a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

Instrumento de primer orden

$$a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$
$$(\tau D + 1)y(t) = Kx(t)$$

donde
$$\tau = a_1/a_0$$
,
 $K = b_0/a_0$.

Instrumento de primer orden

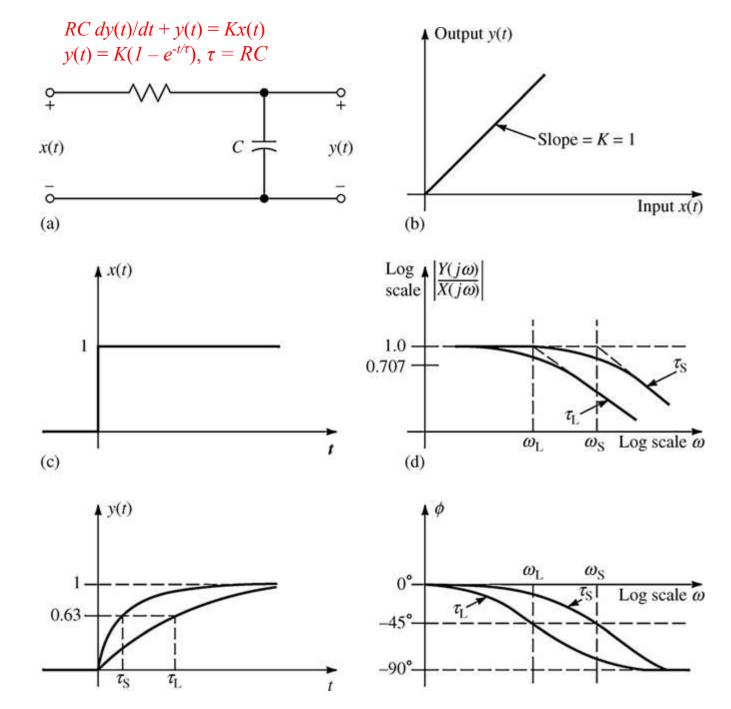
$$a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$
$$(\tau D + 1)y(t) = Kx(t)$$

donde
$$\tau = a_1/a_0$$
,
 $K = b_0/a_0$.

$$\frac{y(D)}{x(D)} = \frac{K}{1 + \tau D}$$

$$\frac{Y(j\omega)}{X(j\omega)} = \frac{K}{1+j\omega\tau} = \frac{K}{\sqrt{1+\omega^2\tau^2}} / \phi = \arctan(-\omega\tau/1)$$

Figure 1.6 (a) A low-pass RC filter, an example of a first-order instrument, (b) Static sensitivity for constant inputs, (c) Step response for large time constants $(\tau_{_{\rm I}})$ and small time constants (τ_s) . (d) Sinusoidal frequency response for large and small time constants.



EXAMPLE 1.2 A first-order low-pass instrument has a time constant of 20 ms. Find the maximal sinusoidal input frequency that will keep output error due to frequency response less than 5%. Find the phase angle at this frequency.

EXAMPLE 1.2 A first-order low-pass instrument has a time constant of 20 ms. Find the maximal sinusoidal input frequency that will keep output error due to frequency response less than 5%. Find the phase angle at this frequency.

$$rac{Y(j\omega)}{X(j\omega)} = rac{K}{1+j\omega au}$$

$$\left| \frac{K}{1 + j\omega \tau} \right| = \frac{K}{\sqrt{1 + \omega^2 \tau^2}} = 0.95K$$

EXAMPLE 1.2 A first-order low-pass instrument has a time constant of 20 ms. Find the maximal sinusoidal input frequency that will keep output error due to frequency response less than 5%. Find the phase angle at this frequency.

$$\frac{Y(j\omega)}{X(j\omega)} = \frac{K}{1+j\omega\tau}$$

$$\left|\frac{K}{1+j\omega\tau}\right| = \frac{K}{\sqrt{1+\omega^2\tau^2}} = 0.95K$$

$$(\omega^2\tau^2 + 1)(0.95)^2 = 1$$

$$\omega^{2} = \frac{1 - (0.95)^{2}}{(0.95)^{2}(20 \times 10^{-3})^{2}}$$

$$\omega = 16.4 \text{ rad/s}$$

$$f = \frac{\omega}{2\pi} = 2.62 \text{ Hz}$$

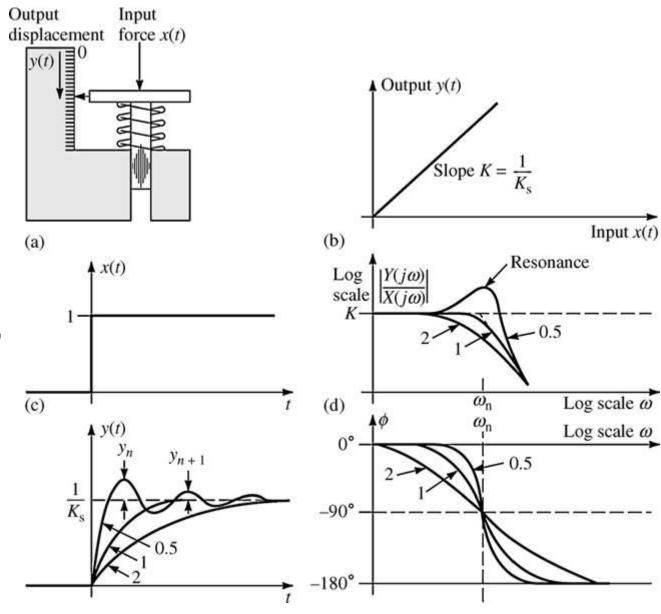
$$\phi = \tan^{-1}\left(\frac{-\omega\tau}{1}\right) = -18.2^{\circ}$$

¿Qué pasa si intercambiamos las posiciones de R y C en el circuito anterior?

$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

Figure 1.7 (a) Force-measuring spring scale, an example of a second-order instrument, (b) Static sensitivity, (c) Step response for overdamped case $\zeta = 2$, critically damped case ζ = 1, underdamped case $\zeta = 0.5$. (d) Sinusoidal steady-state frequency response, ζ = 2, ζ = 1, ζ

= 0.5.



$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

$$\left[\frac{D^2}{\omega_n^2} + \frac{2\zeta D}{\omega_n} + 1\right] y(t) = Kx(t)$$

$$K=b_0/a_0$$
 Sensibilidad estática

$$\omega_n = \sqrt{a_0/a_2}$$
 Frecuencia natural no amortiguada

$$\zeta = a_1/2\sqrt{a_0a_1}\,$$
 Factor de amortiguamiento

$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

$$\left[\frac{D^2}{\omega_n^2} + \frac{2\zeta D}{\omega_n} + 1\right] y(t) = Kx(t)$$

$$\frac{y(D)}{x(D)} = \frac{K}{\frac{D^2}{\omega_n^2} + \frac{2\zeta D}{\omega_n} + 1}$$

$$K=b_0/a_0$$
 Sensibilidad estática $\omega_n=\sqrt{a_0/a_2}$ Frecuencia natural no amortiguada $\zeta=a_1/2\sqrt{a_0a_1}$ Factor de amortiguamiento

$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b_0 x(t)$$

$$\left[\frac{D^2}{\omega_n^2} + \frac{2\zeta D}{\omega_n} + 1\right] y(t) = Kx(t)$$

$$K=b_0/a_0$$
 Sensibilidad estática $\omega_n=\sqrt{a_0/a_2}$ Frecuencia natural no amortiguada

 $\zeta = a_1/2\sqrt{a_0a_1}\,$ Factor de amortiguamiento

$$\frac{y(D)}{x(D)} = \frac{K}{\frac{D^2}{\omega^2} + \frac{2\zeta D}{\omega_n} + 1}$$

$$\frac{Y(j\omega)}{X(j\omega)} = \frac{K}{(j\omega/\omega_n)^2 + (2\zeta j\omega/\omega_n) + 1}$$

$$= \frac{K}{\sqrt{[1 - (\omega/\omega_0)^2]^2 + 4\zeta^2\omega^2/\omega_n^2}} / \phi = \arctan \frac{2\zeta}{\omega/\omega_n - \omega_n/\omega}$$

$$x(t) - B\frac{dy(t)}{dt} - K_s y(t) = M\frac{d^2 y(t)}{dt^2}$$

$$K = \frac{1}{K_s}$$
 $\omega_{\rm n} = \sqrt{K_s/M}$ $\zeta = \frac{B}{2\sqrt{K_{\rm m}M}}$

Caso sobreamortiguado, ζ >1

$$y(t) = -\frac{\zeta + \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}} K e^{\left(-\zeta + \sqrt{\zeta^2 - 1}\right)\omega_n t} + \frac{\zeta - \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}} K e^{\left(-\zeta - \sqrt{\zeta^2 - 1}\right)\omega_n t} + K$$

Caso sobreamortiguado, ζ=1

$$y(t) = -(1 + \omega_{\rm n}t)Ke^{-\omega_{\rm n}t} + K$$

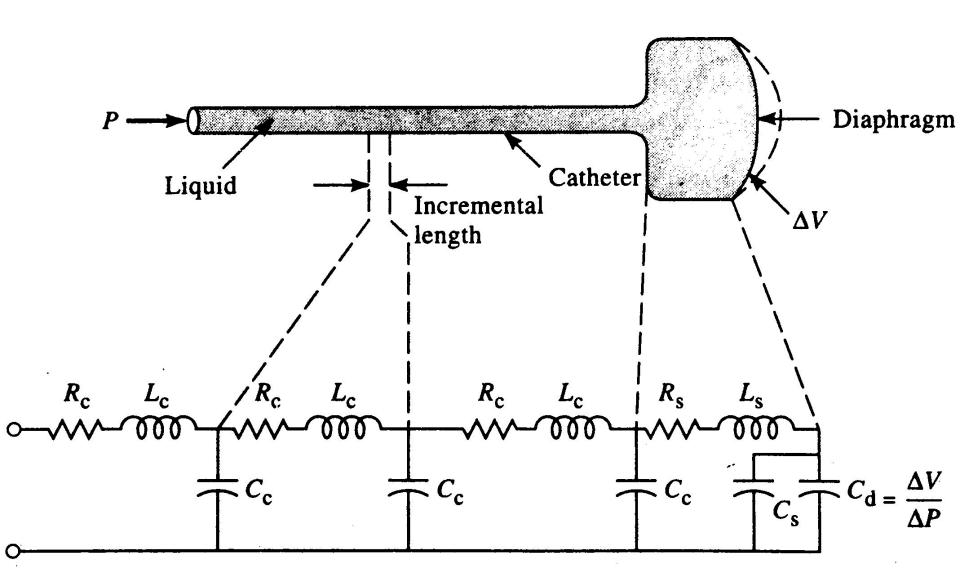
Caso subamortiguado, 0<ζ≤1

$$y(t) = -\frac{e^{-\zeta\omega_{n}t}}{\sqrt{1-\zeta^{2}}}K\sin\left(\sqrt{1-\zeta^{2}}\omega_{n}t + \phi\right) + K$$
$$\phi = \arcsin\sqrt{1-\zeta^{2}}$$

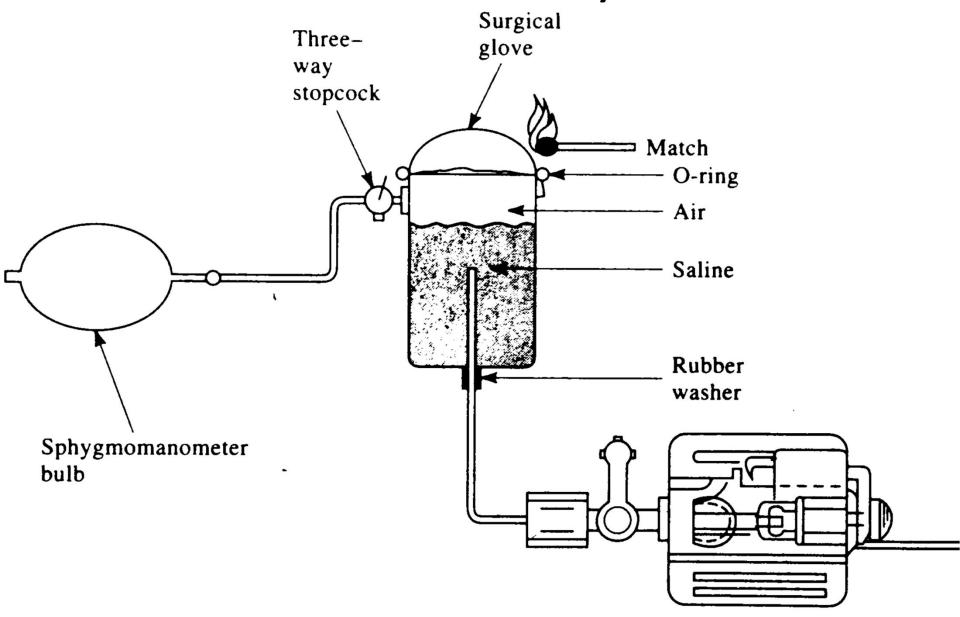
Control package in Python

```
import matplotlib.pyplot as plt
import numpy as np
import control
fig, ax = plt.subplots()
sys = control.tf([1],[1,1,1])
T, yout = control.impulse_response(sys, np.linspace(0,20,num=1000), 0)
ax.plot(T,yout)
```

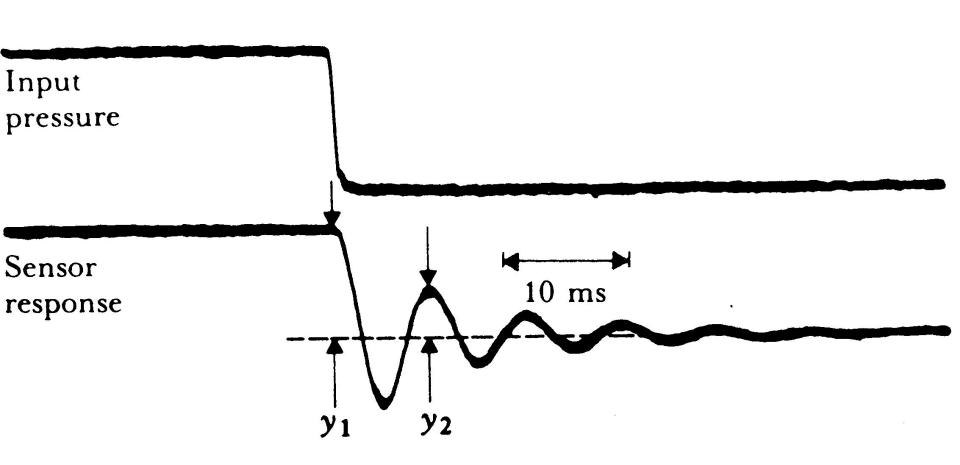
Electrical Model of Catheter-Sensor system



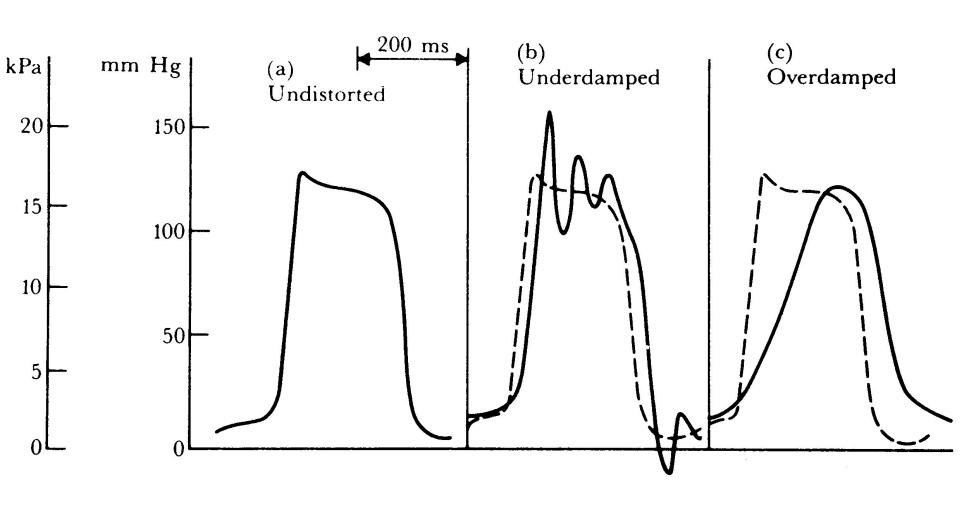
Testing technique for measuring the transient response of the catheter-sensor system



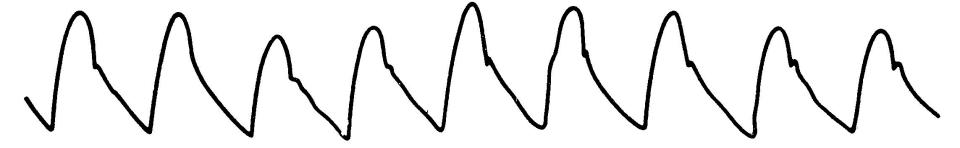
Transient response of the catheter-sensor system



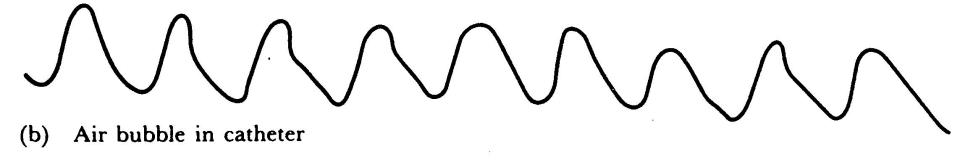
Pressure-waveform distortion



Distortion during the recording of arterial pressure



(a) Undistorted pressure waveform





Stethoscope Frequency response

