

## McMaster University Final Exam

Name \_\_\_\_\_  
Student Number \_\_\_\_\_

MECH ENG 4K03/6K03 ROBOTICS

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DURATION OF EXAMINATION: 2.5 HRS

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THIS EXAMINATION PAPER INCLUDES 5 PAGES (3 PAGES FOR QUESTIONS AND 2 PAGES FOR FORMULAS) AND 5 QUESTIONS.

Use of Casio FX-991 MS or MS Plus calculator.

Questions:

1. (8 points) Give the definitions of the following terms in robotics.

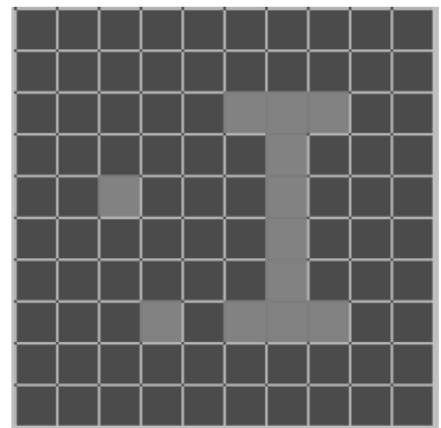
- 1) Hard automation
- 2) Flexible automation
- 3) Planar robot
- 4) Dextrous workspace

2. Short Answer Questions

1) (5 points) If the transformation matrices,  ${}^C T_D$ ,  ${}^A T_B$ ,  ${}^A T_E$  and  ${}^E T_D$ , are known, derive the transformation equation for  ${}^B T_C$  in terms of these matrices.

2) (5 points) Given the grayscale input image of the letter "I" from an optical character recognition application:

$$A = \begin{bmatrix} 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 130 & 130 & 130 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 130 & 75 & 75 & 75 \\ 75 & 75 & 130 & 75 & 75 & 75 & 130 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 130 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 130 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 130 & 75 & 75 & 75 \\ 75 & 75 & 75 & 130 & 75 & 130 & 130 & 130 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 \\ 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 & 75 \end{bmatrix}$$



Show a sample calculation for the row=8, col=5 pixel, if we apply a Laplacian 1 filter to the input image.

- ①
- 1) The use of specialized equipment to create a fixed process for assembly
  - 2) Robots can be reprogrammed without shutdown when task changes
  - 3) A robot whose end-effector motion covers a volume of 3D space
  - 4) The volume of space the end-effector can reach with any desired orientation

② 1)  ${}^B T_C = ({}^A T_B)^{-1} ({}^A T_E) ({}^E T_D) ({}^C T_D)^{-1}$

2) Lap 1  $M = \begin{bmatrix} 0 & -1 & 0 \\ -1 & 5 & -1 \\ 0 & -1 & 0 \end{bmatrix}$

$$S = \sum_{k=1}^3 \sum_{p=1}^3 m_{ij} = 1$$

$$\begin{aligned} f_{85} &= \frac{1}{5} \left( \sum_{k=1}^5 \sum_{p=1}^5 m_{kp} \right) \\ &= \frac{1}{5} (0 \times 75 - 1 \times 75 + 0 \times 75 - 1 \times 130 + 5 \times 75 - 1 \times 130 + 0 \times 75 - 1 \times 75 + 0 \times 75) \\ &= -35 \end{aligned}$$

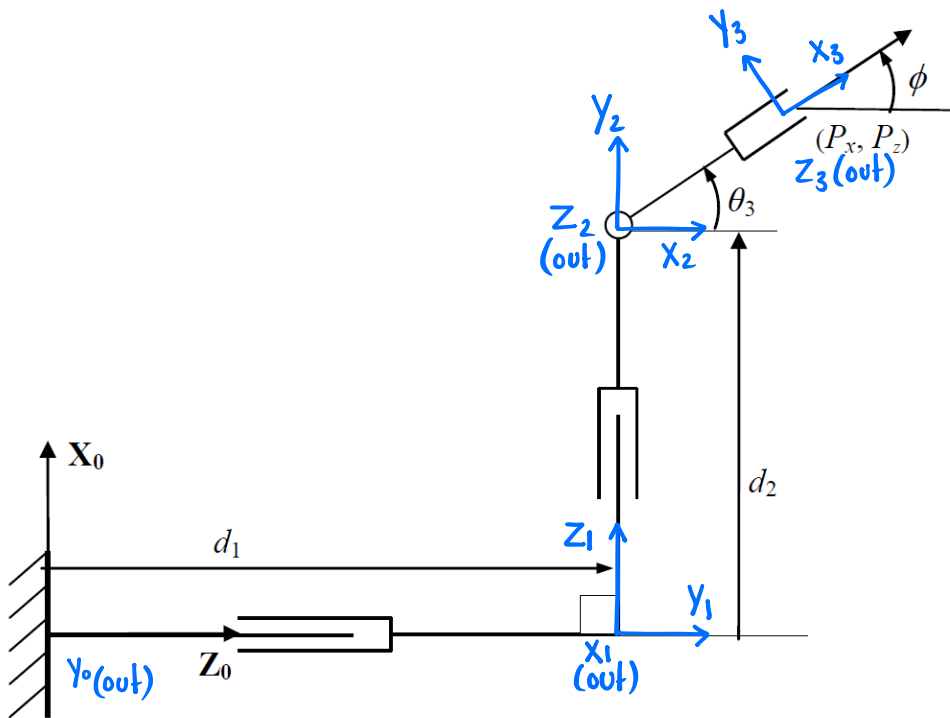
3)  $\vec{n} \cdot \vec{0} = 0 \rightarrow n_x 0_x + n_y 0_y + n_z 0_z = 0$  FRAME A:  $0.77 \times -0.64 + 0.64 \times 0.77 + 0 \times 0 = 0 \checkmark$   
 $\vec{n} \cdot \vec{a} = 0$   $0.77 \times 0 + 0.64 \times 0 + 0 \times 1 = 0 \checkmark$   
 $\vec{a} \cdot \vec{0} = 0$   $0 \times -0.64 + 0 \times 0.77 + 1 \times 0 = 0 \checkmark$

3) (5 points) Which of the following matrices is a valid representation for a frame? Explain your answer.

$$A = \begin{bmatrix} 0.77 & -0.64 & 0 & 3 \\ 0.64 & 0.77 & 0 & 3 \\ 0 & 0 & 1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}; B = \begin{bmatrix} 0 & \sqrt{3}/2 & 0 & 3 \\ -1 & 0 & 0 & 0.5 \\ 0 & 1/2 & 1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}; C = \begin{bmatrix} 0 & \sqrt{3}/2 & -1/2 & 3 \\ -1 & 0 & 0 & 0.5 \\ 0 & 1/2 & -\sqrt{3}/2 & 15 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

3. (25 points) For the PPR planar robot shown in the following Figure:

- Assign the frames using the D-H method.
- Determine the D-H parameters and put them in the standard table form. Identify the joint variables.
- Draw a diagram of the robot that properly shows the D-H frames, the joint variables, and any  $d$  or  $a$  parameters that are non-zero. ( $d_1$  and  $d_2$  are joint variables indicated in the figure;  $a_3$  is the link length after the 3<sup>rd</sup> joint)
- Calculate the  $A$  matrices and  ${}^0T_3$
- Its joint variables are  $d_1$ ,  $d_2$ , and  $\theta_3$ . Its end-effector position and orientation are given by  $P_x$ ,  $P_z$  and  $\phi$ . Derive its inverse kinematics.



4. (25 points) For the planar PRP robot shown in the following Figure:

- Derive the 3x3 manipulator Jacobian matrix. (The form used for calculating the linear velocity and angular velocity of the tool).
- Determine the singular configuration(s) for this robot by examining the determinant of the Jacobian.
- Draw the robot in a singular configuration and indicate which degree (s) of freedom have been lost.

3

b)	n+1	$\Theta_n$	$a_n$	$d_n$	$\alpha_n$
1	1	$90^\circ$	0	$d_1$	$90^\circ$
2	2	$90^\circ$	0	$d_2$	$90^\circ$
3	3	$\Theta_3$	$a_3$	0	0

d)  ${}^0T_3 = A_1 A_2 A_3$

$$A_1 = \begin{bmatrix} c(90^\circ) & -s(90^\circ)c(90^\circ) & s(90^\circ)s(90^\circ) & 0 \\ s(90^\circ) & c(90^\circ)c(90^\circ) & -c(90^\circ)s(90^\circ) & 0 \\ 0 & s(90^\circ) & c(90^\circ) & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} c(90^\circ) & -s(90^\circ)c(90^\circ) & s(90^\circ)s(90^\circ) & 0 \\ s(90^\circ) & c(90^\circ)c(90^\circ) & -c(90^\circ)s(90^\circ) & 0 \\ 0 & s(90^\circ) & c(90^\circ) & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} c\Theta_3 & -s\Theta_3 c(0) & s\Theta_3 s(0) & a_3 c\Theta_3 \\ s\Theta_3 & c\Theta_3 c(0) & -c\Theta_3 s(0) & a_3 s\Theta_3 \\ 0 & s(0) & c(0) & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c\Theta_3 & -s\Theta_3 & 0 & a_3 c\Theta_3 \\ s\Theta_3 & c\Theta_3 & 0 & a_3 s\Theta_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{aligned} {}^0T_3 &= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\Theta_3 & -s\Theta_3 & 0 & a_3 c\Theta_3 \\ s\Theta_3 & c\Theta_3 & 0 & a_3 s\Theta_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} 0 & 1 & 0 & d_2 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\Theta_3 & -s\Theta_3 & 0 & a_3 c\Theta_3 \\ s\Theta_3 & c\Theta_3 & 0 & a_3 s\Theta_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} s\Theta_3 & c\Theta_3 & 0 & a_3 s\Theta_3 + d_2 \\ c\Theta_3 & -s\Theta_3 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

e)  $d_1 = p_x + a_3 \cos \theta$   
 $d_2 = p_y + a_3 \sin \theta$   
 $\theta_3 = \theta$

4

n+1	$\Theta$	d	a	$\alpha$
1	$90^\circ$	$d_1$	0	$90^\circ$
2	$\Theta_2$	0	0	$90^\circ$
3	0	$d_3$	0	0

$${}^nT_{n+1} = A_{n+1} = \begin{bmatrix} c\Theta & -s\Theta c\alpha & s\Theta s\alpha & a c\Theta \\ s\Theta & c\Theta c\alpha & -c\Theta s\alpha & a s\Theta \\ 0 & s\alpha & c\alpha & d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_1 = \begin{bmatrix} c(90^\circ) & -s(90^\circ)c(90^\circ) & s(90^\circ)s(90^\circ) & 0 \\ s(90^\circ) & c(90^\circ)c(90^\circ) & -c(90^\circ)s(90^\circ) & 0 \\ 0 & s(90^\circ) & c(90^\circ) & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} c\Theta_2 & -s\Theta_2 c(90^\circ) & s\Theta_2 s(90^\circ) & a c(90^\circ) \\ s\Theta_2 & c\Theta_2 c(90^\circ) & -c\Theta_2 s(90^\circ) & a s(90^\circ) \\ 0 & s(90^\circ) & c(90^\circ) & d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} c\Theta_2 & 0 & s\Theta_2 & 0 \\ s\Theta_2 & 0 & -c\Theta_2 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} c(0) & -s(0)c(0) & s(0)s(0) & a c(0) \\ s(0) & c(0)c(0) & -c(0)s(0) & a s(0) \\ 0 & s(0) & c(0) & d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

${}^0T_3 = {}^0T_1 \times {}^0T_2 \times {}^0T_3 = A_1 \times A_2 \times A_3$

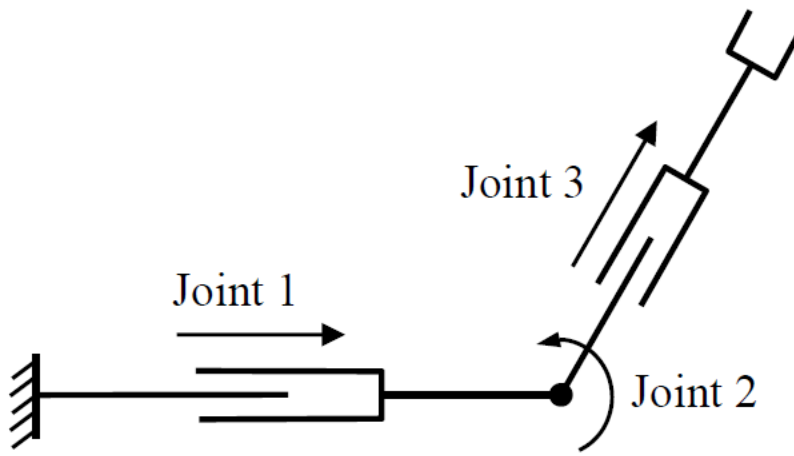
$$= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\Theta_2 & 0 & s\Theta_2 & 0 \\ s\Theta_2 & 0 & -c\Theta_2 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 1 & 0 & 0 \\ c\Theta_2 & 0 & s\Theta_2 & 0 \\ s\Theta_2 & 0 & -c\Theta_2 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

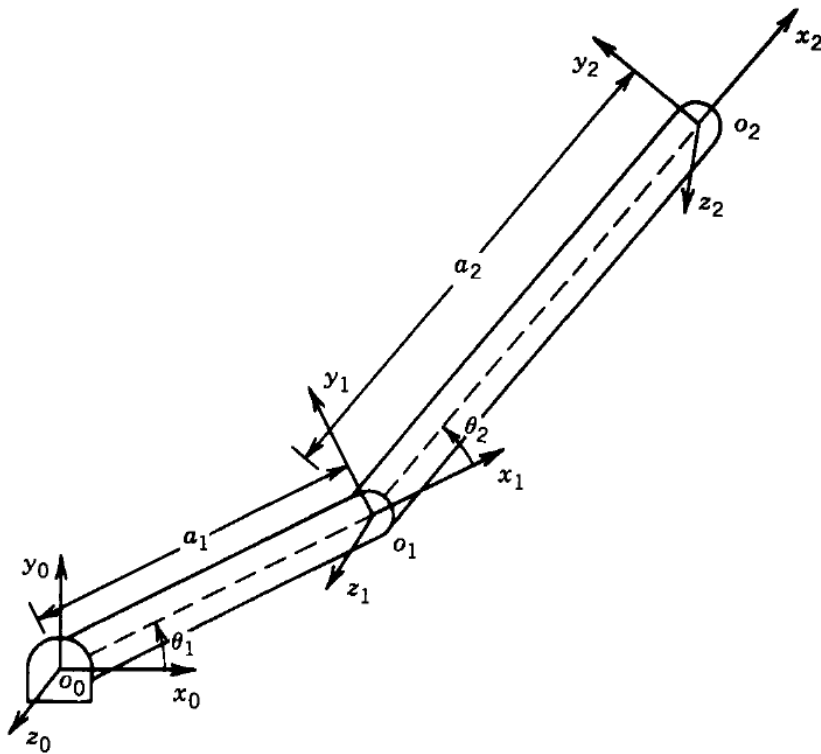
$$= \begin{bmatrix} 0 & 1 & 0 & 0 \\ c\Theta_2 & 0 & s\Theta_2 & s\Theta_2 d_3 \\ s\Theta_2 & 0 & -c\Theta_2 & -c\Theta_2 d_3 + d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

a)  $J(\Theta) = \begin{bmatrix} \frac{dp_x}{dd_1} & \frac{dp_x}{d\Theta_2} & \frac{dp_x}{dd_3} \\ \frac{dp_y}{dd_1} & \frac{dp_y}{d\Theta_2} & \frac{dp_y}{dd_3} \\ \frac{dz}{dz_0} & \frac{dz}{dz_1} & \frac{dz}{dz_2} \end{bmatrix} = \begin{bmatrix} 0 & c\Theta_2 d_3 & s\Theta_2 \\ 1 & s\Theta_2 d_3 & -c\Theta_2 \\ 0 & 1 & 0 \end{bmatrix}$   $ppp \rightarrow \begin{matrix} \varepsilon_1 = 0 \\ \varepsilon_2 = 1 \\ \varepsilon_3 = 0 \end{matrix}$

b)  $\det(J) = (-1)(-s\Theta_2) = s\Theta_2 \rightarrow \text{singularity when } s\Theta_2 = 0$   
 $\hookrightarrow \Theta_2 = 0, 180^\circ$



5. (27 points) For the RR planar robot in the following figure, if  $a_1 = 0.4\text{m}$  and  $a_2 = 0.3\text{m}$ ;
- (a) Assuming the robot operates in the horizontal plane, calculate the joint torques such that the static force at the end-effector is  $F_x = 20\text{N}$  and  $F_y = -15\text{N}$  for the configuration  $\theta_1 = 35^\circ$  and  $\theta_2 = -75^\circ$
- (b) Assuming the robot operates in the horizontal plane, calculate the static force applied by the end effector when  $\tau_1 = 10\text{Nm}$ ,  $\tau_2 = 5\text{Nm}$ ,  $\theta_1 = 35^\circ$  and  $\theta_2 = -75^\circ$ .



$$\textcircled{5} \quad \begin{aligned} O_{2y} &= a_1 \sin \theta_1 + a_2 \sin \theta_{12} \rightarrow \dot{O}_{2y} = \dot{\theta}_1 a_1 \cos \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2) a_2 \cos \theta_{12} \\ O_{2x} &= a_1 \cos \theta_1 + a_2 \cos \theta_{12} \rightarrow \dot{O}_{2x} = -\dot{\theta}_1 a_1 \sin \theta_1 - (\dot{\theta}_1 + \dot{\theta}_2) a_2 \sin \theta_{12} \end{aligned}$$

$$\begin{aligned} v_{01} &= a_1 \dot{\theta}_1 \\ k_1 &= \frac{1}{2} m_1 v_{01}^2 + I_1 \omega_1^2 \\ &= \frac{1}{2} m_1 (a_1 \dot{\theta}_1)^2 \end{aligned}$$

$$\begin{aligned} v_{02} &= \dot{x}_{02}^2 + \dot{y}_{02}^2 \\ k_2 &= \frac{1}{2} m_2 v_{02}^2 + I_2 \omega_2^2 \\ &= \frac{1}{2} m_2 (\dot{x}_{02}^2 + \dot{y}_{02}^2) \end{aligned}$$

$$\begin{aligned} &= \frac{1}{2} m_2 [\dot{\theta}_1^2 a_1^2 \sin^2 \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2) a_2 \sin \theta_{12} \cdot \dot{\theta}_1 a_1 \sin \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2)^2 a_2^2 \sin^2 \theta_{12} \\ &\quad + \dot{\theta}_1^2 a_1^2 \cos^2 \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2) a_2 \cos \theta_{12} \cdot \dot{\theta}_1 a_1 \cos \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2)^2 a_2^2 \cos^2 \theta_{12}] \\ &= \frac{1}{2} m_2 [\dot{\theta}_1^2 a_1^2 + (\dot{\theta}_1 + \dot{\theta}_2) a_2 a_1 \dot{\theta}_1 (\sin \theta_2 + \cos \theta_2) + (\dot{\theta}_1 + \dot{\theta}_2)^2 a_2^2] \\ &= \frac{1}{2} m_2 [\dot{\theta}_1^2 a_1^2 + (\dot{\theta}_1^2 + \dot{\theta}_2 \dot{\theta}_1) a_2 a_1 (\sin \theta_2 + \cos \theta_2) + (\dot{\theta}_1^2 + 2\dot{\theta}_1 \dot{\theta}_2 + \dot{\theta}_2^2) a_2^2] \end{aligned}$$

$$\begin{aligned} p_1 &= -m_1 G^T p_{01} \\ &= -m_{01} [0 \ -g] \begin{bmatrix} x_{01} \\ y_{01} \end{bmatrix} \\ &= -m_{01} (-g) y_{01} \\ &= -m_{01} (-g) a_1 \sin \theta_1 \\ &= m_{01} g a_1 \sin \theta_1 \end{aligned}$$

$$\begin{aligned} p_2 &= m_2 G^T p_{02} \\ &= -m_{02} (-g) y_{02} \\ &= -m_{02} (-g) (a_1 \sin \theta_1 + a_2 \sin \theta_{12}) \\ &= m_{02} g (a_1 \sin \theta_1 + a_2 \sin \theta_{12}) \end{aligned}$$

$$\begin{aligned} L &= k - P = k_1 + k_2 - p_1 - p_2 \\ &= \frac{1}{2} m_1 (a_1 \dot{\theta}_1)^2 + \frac{1}{2} m_2 [\dot{\theta}_1^2 a_1^2 + (\dot{\theta}_1^2 + \dot{\theta}_2 \dot{\theta}_1) a_2 a_1 (\sin \theta_2 + \cos \theta_2) + (\dot{\theta}_1^2 + 2\dot{\theta}_1 \dot{\theta}_2 + \dot{\theta}_2^2) a_2^2] \\ &\quad - m_{01} g a_1 \sin \theta_1 - m_{02} g (a_1 \sin \theta_1 + a_2 \sin \theta_{12}) \\ &= \frac{1}{2} m_1 a_1^2 \dot{\theta}_1^2 + \frac{1}{2} m_2 \dot{\theta}_1^2 a_1^2 + \frac{1}{2} m_2 \dot{\theta}_1^2 + \dot{\theta}_2 \dot{\theta}_1 \end{aligned}$$

$$\textcircled{5} \quad \text{d) } \begin{aligned} a_1 &= 0.4 \text{ m} \\ a_2 &= 0.3 \text{ m} \end{aligned} \quad F = \begin{bmatrix} 20 \\ -15 \end{bmatrix} \text{ N} \quad \begin{aligned} \theta_1 &= 35^\circ \\ \theta_2 &= -75^\circ \end{aligned}$$

$$\text{b) } \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} 10 \\ 5 \end{bmatrix} \text{ Nm}$$

$$F = (J(q)^T)^{-1} \tau$$

$$(J(q)^T)^{-1} = \frac{1}{(-0.0366 \times 0.2298 - 0.557 \times 0.1928)} \begin{bmatrix} -0.0366 & 0.557 \\ 0.1928 & 0.2298 \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial \theta_1} & \frac{\partial p_x(q)}{\partial \theta_2} \\ \frac{\partial p_y(q)}{\partial \theta_1} & \frac{\partial p_y(q)}{\partial \theta_2} \end{bmatrix} = \begin{bmatrix} -a_1 \sin \theta_1 - a_2 \sin \theta_{12} & -a_2 \sin \theta_{12} \\ a_1 \cos \theta_1 + a_2 \cos \theta_{12} & a_2 \cos \theta_{12} \end{bmatrix}$$

$$J(q)^T = \begin{bmatrix} -a_1 \sin \theta_1 - a_2 \sin \theta_{12} & a_1 \cos \theta_1 + a_2 \cos \theta_{12} \\ -a_2 \sin \theta_{12} & a_2 \cos \theta_{12} \end{bmatrix}$$

sub in values

$$\begin{aligned} &= \begin{bmatrix} -0.4 \sin(35^\circ) - 0.3 \sin(35^\circ - 75^\circ) & 0.4 \cos(35^\circ) + 0.3 \cos(35^\circ - 75^\circ) \\ -0.3 \sin(35^\circ - 75^\circ) & 0.3 \cos(35^\circ - 75^\circ) \end{bmatrix} \\ &= \begin{bmatrix} -0.0366 & 0.557 \\ 0.1928 & 0.2298 \end{bmatrix} \end{aligned}$$

$$\begin{aligned} \begin{bmatrix} F_x \\ F_y \end{bmatrix} &= \begin{bmatrix} -1.981 & 4.802 \\ 1.662 & 0.316 \end{bmatrix} \begin{bmatrix} 10 \\ 5 \end{bmatrix} \\ &= \begin{bmatrix} 4.2 \\ 18.2 \end{bmatrix} \text{ N} \end{aligned}$$

$$\begin{aligned} \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} &= \begin{bmatrix} -0.0366 & 0.557 \\ 0.1928 & 0.2298 \end{bmatrix} \begin{bmatrix} 20 \\ -15 \end{bmatrix} \\ &= \begin{bmatrix} -9.081 \\ 0.409 \end{bmatrix} \text{ Nm} \end{aligned}$$



## Formulas

$$\text{Rot}(X, \theta) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\theta & -S\theta & 0 \\ 0 & S\theta & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

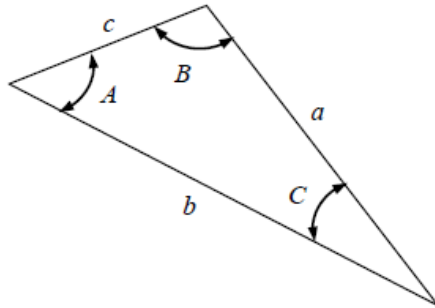
$$\text{Rot}(Y, \theta) = \begin{bmatrix} C\theta & 0 & S\theta & 0 \\ 0 & 1 & 0 & 0 \\ -S\theta & 0 & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\text{Rot}(Z, \theta) = \begin{bmatrix} C\theta & -S\theta & 0 & 0 \\ S\theta & C\theta & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\text{Trans}(a, b, c) = \begin{bmatrix} 1 & 0 & 0 & a \\ 0 & 1 & 0 & b \\ 0 & 0 & 1 & c \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T^{-1} = \begin{bmatrix} n_x & n_y & n_z & -\vec{P} \bullet \vec{n} \\ o_x & o_y & o_z & -\vec{P} \bullet \vec{o} \\ a_x & a_y & a_z & -\vec{P} \bullet \vec{a} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_{n+1} = {}^nT_{n+1} = \begin{bmatrix} C\theta_{n+1} & -S\theta_{n+1}C\alpha_{n+1} & S\theta_{n+1}S\alpha_{n+1} & a_{n+1}C\theta_{n+1} \\ S\theta_{n+1} & C\theta_{n+1}C\alpha_{n+1} & -C\theta_{n+1}S\alpha_{n+1} & a_{n+1}S\theta_{n+1} \\ 0 & S\alpha_{n+1} & C\alpha_{n+1} & d_{n+1} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



$$\cos A = (b^2 + c^2 - a^2) / (2bc)$$

$$S\theta_1 C\theta_2 + C\theta_1 S\theta_2 = S(\theta_1 + \theta_2) = S\theta_{12}$$

$$C\theta_1 C\theta_2 - S\theta_1 S\theta_2 = C(\theta_1 + \theta_2) = C\theta_{12}$$

if  $a = \sin \theta$  and  $b = \cos \theta$  then  $\theta = \text{atan2}(a, b)$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} & \frac{\partial p_x(q)}{\partial q_3} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} & \frac{\partial p_y(q)}{\partial q_3} \\ \zeta_1 t_1 & \zeta_2 t_2 & \zeta_3 t_3 \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} & \frac{\partial p_x(q)}{\partial q_3} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} & \frac{\partial p_y(q)}{\partial q_3} \\ \frac{\partial p_z(q)}{\partial q_1} & \frac{\partial p_z(q)}{\partial q_2} & \frac{\partial p_z(q)}{\partial q_3} \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} & \dots & \frac{\partial p_x(q)}{\partial q_n} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} & \dots & \frac{\partial p_y(q)}{\partial q_n} \\ \frac{\partial p_z(q)}{\partial q_1} & \frac{\partial p_z(q)}{\partial q_2} & \dots & \frac{\partial p_z(q)}{\partial q_n} \\ \hline \zeta_1 z_0(q) & \zeta_2 z_1(q) & \dots & \zeta_n z_{n-1}(q) \end{bmatrix}$$

$$z_i = {}^0R_i \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \text{where } {}^0R_i = \prod_{k=1}^i {}^{k-1}R_k$$



$$\text{if } A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \text{ then}$$

$$A^{-1} = \frac{1}{a_{11}a_{22} - a_{12}a_{21}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

$$\det(J) = j_{11}(j_{33}j_{22} - j_{32}j_{23}) - j_{21}(j_{33}j_{12} - j_{32}j_{13}) + j_{31}(j_{23}j_{12} - j_{22}j_{13})$$

$$\begin{bmatrix} v_x \\ v_y \\ v_z \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = J(q) \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

$$\tau = J(q)^T F$$

$$F_i = \frac{\partial}{\partial t} \left( \frac{\partial L}{\partial \dot{x}_i} \right) - \frac{\partial L}{\partial x_i}$$

$$\tau_i = \frac{\partial}{\partial t} \left( \frac{\partial L}{\partial \dot{\theta}_i} \right) - \frac{\partial L}{\partial \theta_i}$$

$$K_j = \frac{1}{2}m_j v_{\varphi}^2 + \frac{1}{2}I_j \omega_j^2$$

$$P_j = -m_j G^T p_{qj}$$

$$\dot{\theta}_{\max} = \frac{\theta_h - \theta_b}{t_h - t_b} = \ddot{\theta}_d t_b$$

$$t_b = \frac{t_f}{2} - \frac{\sqrt{\ddot{\theta}_d^2 t_f^2 - 4\ddot{\theta}_d(\theta_f - \theta_i)}}{2|\ddot{\theta}_d|}$$

$$\theta(t) = \theta_i + \frac{1}{2}\ddot{\theta}_d t^2, \quad \dot{\theta}(t) = \ddot{\theta}_d t,$$

$$\text{and } \ddot{\theta}(t) = \ddot{\theta}_d$$

$$\theta(t) = \theta_i + \frac{1}{2}\ddot{\theta}_d t_b^2 + \ddot{\theta}_d t_b(t - t_b), \quad \dot{\theta}(t) = \ddot{\theta}_d t_b,$$

$$\text{and } \ddot{\theta}(t) = 0$$

$$\theta(t) = \theta_f - \frac{1}{2}\ddot{\theta}_d (t_f - t)^2, \quad \dot{\theta}(t) = \ddot{\theta}_d (t_f - t),$$

$$\text{and } \ddot{\theta}(t) = -\ddot{\theta}_d$$

**The End**

$$\text{Gaussian } M = \begin{bmatrix} 1 & 2 & 1 \\ 2 & 4 & 2 \\ 1 & 2 & 1 \end{bmatrix}, \text{ Mean } M = \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$$

$$\text{Lap1 } M = \begin{bmatrix} 0 & -1 & 0 \\ -1 & 5 & -1 \\ 0 & -1 & 0 \end{bmatrix}, \text{ Lap2 } M = \begin{bmatrix} 1 & -2 & 1 \\ -2 & 5 & -2 \\ 1 & -2 & 1 \end{bmatrix}$$

$$\text{Sobel } M_h = \begin{bmatrix} -1 & -2 & -1 \\ 0 & 0 & 0 \\ 1 & 2 & 1 \end{bmatrix} \text{ and } M_v = \begin{bmatrix} -1 & 0 & 1 \\ -2 & 0 & 2 \\ -1 & 0 & 1 \end{bmatrix}$$

$$\text{Prewitt } M_h = \begin{bmatrix} -1 & -1 & -1 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix} \text{ and } M_v = \begin{bmatrix} -1 & 0 & 1 \\ -1 & 0 & 1 \\ -1 & 0 & 1 \end{bmatrix}$$

$$F = A + c(A - F_{smooth})$$