## **McMaster University Final Exam**

Name	
Student Number	

## MECH ENG 4K03/6K03 ROBOTICS

INSTRUCTOR NAME: Fengjun Yan

**DURATION OF EXAMINATION: 2.5 HRS** 

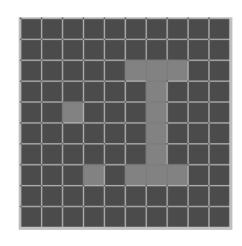
December 2020

THIS EXAMINATION PAPER INCLUDES <u>5</u> PAGES (3 PAGES FOR QUESTIONS AND 2 PAGES FOR FORMULAS) AND <u>5</u> QUESTIONS.

Use of Casio FX-991 MS or MS Plus calculator.

## Questions:

- 1. (8 points) Give the definitions of the following terms in robotics.
- 1) Hard automation
- 2) Flexible automation
- 3) Planar robot
- 4) Dextrous workspace
- 2. Short Answer Questions
- 1) (5 points) If the transformation matrices,  ${}^{C}T_{D}$ ,  ${}^{A}T_{B}$ ,  ${}^{A}T_{E}$  and  ${}^{E}T_{D}$ , are known, derive the transformation equation for  ${}^{B}T_{C}$  in terms of these matrices.
- 2) (5 points) Given the grayscale input image of the letter "I" from an optical character recognition application:

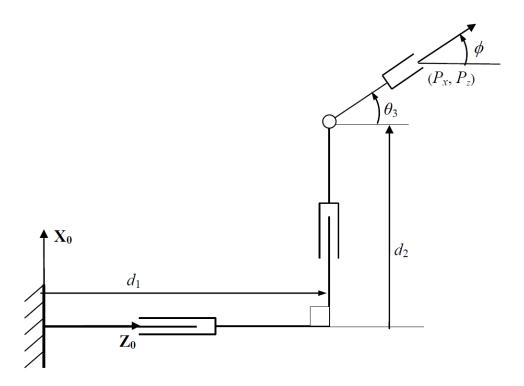


Show a sample calculation for the row=8, col=5 pixel, if we apply a Laplacian 1 filter to the input image.

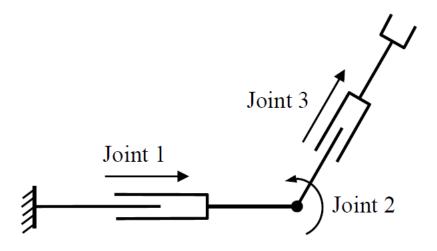
3) (5 points) Which of the following matrices is a valid representation for a frame? Explain your answer.

$$A = \begin{bmatrix} 0.77 & -0.64 & 0 & 3 \\ 0.64 & 0.77 & 0 & 3 \\ 0 & 0 & 1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}; B = \begin{bmatrix} 0 & \sqrt{3}/2 & 0 & 3 \\ -1 & 0 & 0 & 0.5 \\ 0 & 1/2 & 1 & 2 \\ 0 & 0 & 0 & 1 \end{bmatrix}; C = \begin{bmatrix} 0 & \sqrt{3}/2 & -1/2 & 3 \\ -1 & 0 & 0 & 0.5 \\ 0 & 1/2 & -\sqrt{3}/2 & 15 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

- 3. (25 points) For the PPR planar robot shown in the following Figure:
- a) Assign the frames using the D-H method.
- b) Determine the D-H parameters and put them in the standard table form. Identify the joint variables.
- c) Draw a diagram of the robot that properly shows the D-H frames, the joint variables, and any *d* or *a* parameters that are non-zero.
- d) Calculate the A matrices and  ${}^{0}T_{3}$
- e) Its joint variables are  $d_1$ ,  $d_2$ , and  $\theta_3$ . Its end-effector position and orientation are given by  $P_x$ ,  $P_z$  and  $\emptyset$ . Derive its inverse kinematics.

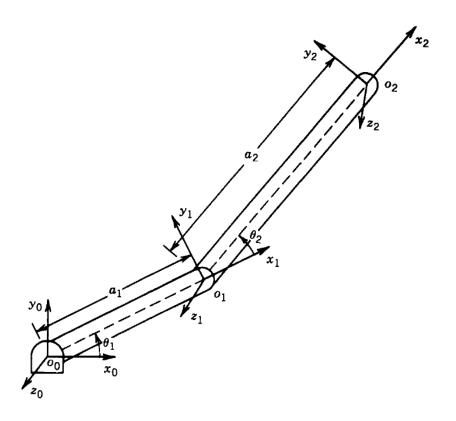


- 4. (25 points) For the planar PRP robot shown in the following Figure:
- a) Derive the 3x3 manipulator Jacobian matrix. (The form used for calculating the linear velocity and angular velocity of the tool).
- b) Determine the singular configuration(s) for this robot by examining the determinant of the Jacobian.
- c) Draw the robot in a singular configuration and indicate which degree (s) of freedom have been lost.



5. (27 points) For the RR planar robot in the following figure, if  $a_1 = 0.4$ m and  $a_2 = 0.3$ m; (a) Assuming the robot operates in the horizontal plane, calculate the joint torques such that the static force at the end-effector is  $F_x = 20$ N and  $F_y = -15$ N for the configuration  $\theta_1 = 35^\circ$  and  $\theta_2 = -75^\circ$ 

(b)Assuming the robot operates in the horizontal plane, calculate the static force applied by the end effector when  $\tau_1 = 10$ Nm,  $\tau_2 = 5$ Nm,  $\theta_1 = 35^{\circ}$  and  $\theta_2 = -75^{\circ}$ .



## **Formulas**

$$Rot(X,\theta) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\theta & -S\theta & 0 \\ 0 & S\theta & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

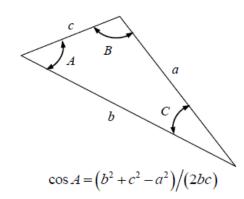
$$Rot(Y,\theta) = \begin{bmatrix} C\theta & 0 & S\theta & 0\\ 0 & 1 & 0 & 0\\ -S\theta & 0 & C\theta & 0\\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$Rot(Z,\theta) = \begin{bmatrix} C\theta & -S\theta & 0 & 0 \\ S\theta & C\theta & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\operatorname{Trans}(a,b,c) = \begin{bmatrix} 1 & 0 & 0 & a \\ 0 & 1 & 0 & b \\ 0 & 0 & 1 & c \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T^{-1} = \begin{bmatrix} n_x & n_y & n_z & -\vec{P} \bullet \vec{n} \\ o_x & o_y & o_z & -\vec{P} \bullet \vec{o} \\ a_x & a_y & a_z & -\vec{P} \bullet \vec{a} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_{n+1} = {}^{n}T_{n+1} = \begin{bmatrix} \mathbf{C}\,\theta_{n+1} & -\mathbf{S}\,\theta_{n+1}\mathbf{C}\,\alpha_{n+1} & \mathbf{S}\,\theta_{n+1}\mathbf{S}\,\alpha_{n+1} & a_{n+1}\mathbf{C}\,\theta_{n+1} \\ \mathbf{S}\,\theta_{n+1} & \mathbf{C}\,\theta_{n+1}\mathbf{C}\,\alpha_{n+1} & -\mathbf{C}\,\theta_{n+1}\mathbf{S}\,\alpha_{n+1} & a_{n+1}\mathbf{S}\,\theta_{n+1} \\ \mathbf{0} & \mathbf{S}\,\alpha_{n+1} & \mathbf{C}\,\alpha_{n+1} & d_{n+1} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix}$$



$$S\theta_1C\theta_2 + C\theta_1S\theta_2 = S(\theta_1 + \theta_2) = S\theta_{12}$$
 
$$C\theta_1C\theta_2 - S\theta_1S\theta_2 = C(\theta_1 + \theta_2) = C\theta_{12}$$

if  $a = \sin \theta$  and  $b = \cos \theta$  then  $\theta = \operatorname{atan2}(a, b)$ 

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} & \frac{\partial p_x(q)}{\partial q_3} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} & \frac{\partial p_y(q)}{\partial q_3} \\ \zeta_1 t_1 & \zeta_2 t_2 & \zeta_3 t_3 \end{bmatrix}$$

$$J(q) = \begin{bmatrix} \frac{\partial p_x(q)}{\partial q_1} & \frac{\partial p_x(q)}{\partial q_2} & \frac{\partial p_x(q)}{\partial q_3} \\ \frac{\partial p_y(q)}{\partial q_1} & \frac{\partial p_y(q)}{\partial q_2} & \frac{\partial p_y(q)}{\partial q_3} \\ \frac{\partial p_z(q)}{\partial q_1} & \frac{\partial p_z(q)}{\partial q_2} & \frac{\partial p_z(q)}{\partial q_3} \end{bmatrix}$$

$$A_{n+1} = {}^{n}T_{n+1} = \begin{bmatrix} C\theta_{n+1} & -S\theta_{n+1}C\alpha_{n+1} & S\theta_{n+1}S\alpha_{n+1} & a_{n+1}C\theta_{n+1} \\ S\theta_{n+1} & C\theta_{n+1}C\alpha_{n+1} & -C\theta_{n+1}S\alpha_{n+1} & a_{n+1}S\theta_{n+1} \\ 0 & S\alpha_{n+1} & C\alpha_{n+1} & d_{n+1} \\ 0 & 0 & 0 & 1 \end{bmatrix} \qquad J(q) = \begin{bmatrix} \frac{\partial p_{x}(q)}{\partial q_{1}} & \frac{\partial p_{x}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{x}(q)}{\partial q_{n}} \\ \frac{\partial p_{y}(q)}{\partial q_{1}} & \frac{\partial p_{y}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{y}(q)}{\partial q_{n}} \\ \frac{\partial p_{y}(q)}{\partial q_{n}} & \frac{\partial p_{y}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{y}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{2}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}} & \cdots & \frac{\partial p_{z}(q)}{\partial q_{n}} \\ \frac{\partial p_{z}(q)}{\partial q_{n}$$

$$Z_i = {}^{0}R_i \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \text{where } {}^{0}R_i = \prod_{k=1}^{i} {}^{k-1}R_k$$

if 
$$A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}$$
 then 
$$A^{-1} = \frac{1}{a_{11}a_{22} - a_{12}a_{21}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

$$\det(J) = j_{11}(j_{33}j_{22} - j_{32}j_{23}) - j_{21}(j_{33}j_{12} - j_{32}j_{13}) + j_{31}(j_{23}j_{12} - j_{22}j_{13})$$

$$\begin{bmatrix} v_x \\ v_y \\ v_z \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = J(q) \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

$$\tau = J(q)^T F$$

$$\tau = J(q)^T H$$

$$F_{i} = \frac{\partial}{\partial t} \left( \frac{\partial L}{\partial \dot{x}_{i}} \right) - \frac{\partial L}{\partial x_{i}}$$

$$\tau_i = \frac{\partial}{\partial t} \left( \frac{\partial L}{\partial \dot{\theta_i}} \right) - \frac{\partial L}{\partial \theta_i}$$

$$K_j = \frac{1}{2} m_j v_{ej}^2 + \frac{1}{2} I_j \omega_j^2$$

$$P_j = -m_j G^T p_{cj}$$

$$\dot{\theta}_{\text{max}} = \frac{\theta_h - \theta_b}{t_h - t_h} = \ddot{\theta}_d t_b$$

$$t_b = \frac{t_f}{2} - \frac{\sqrt{\ddot{\theta_d}^2 t_f^2 - 4\ddot{\theta_d}(\theta_f - \theta_i)}}{2\left|\ddot{\theta_d}\right|}$$

$$\begin{split} \theta(t) &= \theta_i + \tfrac{1}{2} \ddot{\theta}_d t^2, \ \ \dot{\theta}(t) = \ddot{\theta}_d t, \\ \text{and } \ddot{\theta}(t) &= \ddot{\theta}_d \end{split}$$

$$\begin{split} \theta(t) &= \theta_i + \tfrac{1}{2} \ddot{\theta_d} t_b^{\ 2} + \ddot{\theta_d} t_b (t - t_b), \ \dot{\theta}(t) = \ddot{\theta_d} t_b, \\ \text{and } \ddot{\theta}(t) &= 0 \end{split}$$

$$\begin{split} \theta(t) &= \theta_f - \tfrac{1}{2} \ddot{\theta}_d \left( t_f - t \right)^2, \ \ \dot{\theta}(t) = \ddot{\theta}_d \left( t_f - t \right), \\ \text{and } \ddot{\theta}(t) &= -\ddot{\theta}_d \end{split}$$
 The End

Gaussian 
$$M = \begin{bmatrix} 1 & 2 & 1 \\ 2 & 4 & 2 \\ 1 & 2 & 1 \end{bmatrix}$$
, Mean  $M = \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$ 
$$\begin{bmatrix} 0 & -1 & 0 \end{bmatrix}$$
 
$$\begin{bmatrix} 1 & -2 & 1 \end{bmatrix}$$

Lap1 
$$M = \begin{bmatrix} 0 & -1 & 0 \\ -1 & 5 & -1 \\ 0 & -1 & 0 \end{bmatrix}$$
, Lap2  $M = \begin{bmatrix} 1 & -2 & 1 \\ -2 & 5 & -2 \\ 1 & -2 & 1 \end{bmatrix}$ 

Sobel 
$$M_h = \begin{bmatrix} -1 & -2 & -1 \\ 0 & 0 & 0 \\ 1 & 2 & 1 \end{bmatrix}$$
 and  $M_v = \begin{bmatrix} -1 & 0 & 1 \\ -2 & 0 & 2 \\ -1 & 0 & 1 \end{bmatrix}$ 

Prewitt 
$$M_h = \begin{bmatrix} -1 & -1 & -1 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$
 and  $M_v = \begin{bmatrix} -1 & 0 & 1 \\ -1 & 0 & 1 \\ -1 & 0 & 1 \end{bmatrix}$ 

$$F = A + c(A - F_{smooth})$$