Mechatronics 3DX4

Slides 7: Steady-State Errors

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Material based on lecture notes by P. Taylor and M. Lawford, and Control Systems Engineering by N. Nise.

Introduction

- ▶ We now focus on the third design specification, *steady-state error*.
- We define steady-state error to be the difference between input and output as $t \to \infty$.
- We will see that control system design typically means we will have to make trade-offs between the desired transient, steady-state, and stability specifications.

Test Inputs

► Table below shows the standard test inputs typically used for evaluating steady-state error.

Waveform	Name	Physical interpretation	Time function	Laplace transform	
r(t)	Step	Constant position	1	$\frac{1}{s}$	
r(t)	Ramp	Constant velocity	t	$\frac{1}{s^2}$	
(1)	Parabola	Constant acceleration	$\frac{1}{2}t^2$	$\frac{1}{s^3}$	

Table 7.1.

Choosing a Test Inputs

► The test inputs we will choose for our steady-state analysis and design depends on our target application.

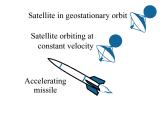




Figure 7.1.

Steady-State Error and Stable Systems

- ► The calculations we will be deriving for steady-state apply only to stable systems.
- Unstable systems represent loss of control in steady-state as the transient response swamps the forced response.
- As we analyze and design a system for steady-state error, we must constantly check the system for stability.

Steady-State Error and Step Inputs

- With step inputs, we can get two types of steady-state errors:
 - 1. Zero error.
 - 2. A constant error value.

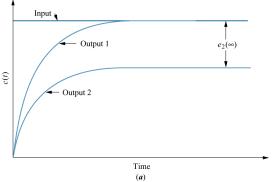


Figure 7.2.

Steady-State Error and Ramp input

- With ramp inputs, we can get three types of steady-state errors:
 - 1. Zero error.
 - 2. A constant error value.
 - 3. Infinite error.

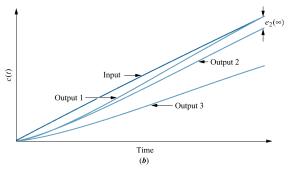


Figure 7.2.

Steady-State Error and Block Diagrams

- If we have a closed-loop transfer function T(s), we can represent our error signal, E(s), as in figure (a).
- We are interested in the time domain signal, $e(t) = \mathcal{L}^{-1}\{E(s)\}$, as $t \to \infty$.
- If we have a unity feedback system, we already have E(s) as part of our diagram, as shown in figure (b).

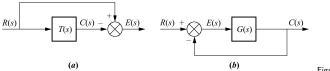


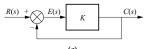
Figure 7.3.

Sources of Steady-State Error

- Steady-state errors can arise from nonlinear sources, such as backlash in gears or motors requiring a minimum input voltage before it starts to move.
- Steady-state errors can also arise from configuration of system and the input we apply.
- Consider a step input applied to the system below which has constant gain.
- ▶ If a unity feedback system has a feedforward transfer function G(s), then we can derive the transfer function $\frac{E(s)}{R(s)}$ as follows:

$$C(s) = E(s)G(s) \tag{1}$$

$$E(s) = R(s) - C(s) \tag{2}$$



)2006-2012 R.J. Leduc (a) Figure 7.4.

Sources of Steady-State Error - II

Substituting equation 1 into equation 2 gives:

$$E(s) = R(s) - E(s)G(s)$$

$$E(s)[1 + G(s)] = R(s)$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G(s)}$$
(3)

ightharpoonup For G(s) = K, we get

$$\frac{E(s)}{R(s)} = \frac{1}{1+K} \tag{4}$$

- ▶ For $R(s) = \frac{1}{s}$ (unit step), we get $E(s) = \frac{1}{s(1+K)}$.
- We thus have $e_{ss} = \lim_{t\to\infty} e(t) = \lim_{s\to 0} sE(s) = \frac{1}{1+K}$

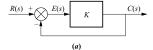


Figure 7.4.

Sources of Steady-State Error - III

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G(s)}$$

▶ If we add an integrator to the forward-path gain, we get $G(s) = \frac{K}{s}$ giving

$$\frac{E(s)}{R(s)} = \frac{1}{1 + \frac{K}{s}} = \frac{s}{s + K} \tag{5}$$

- ▶ For $R(s) = \frac{1}{s}$ (unit step), we get $E(s) = \frac{1}{(s+K)}$.
- We thus have

$$e_{ss} = \lim_{t \to \infty} e(t) = \lim_{s \to 0} sE(s) = \frac{0}{0+K} = 0$$
 (6)

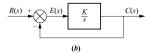


Figure 7.4.

Steady-State Error and T(s)

- ▶ In Diagram below, we have E(s) = R(s) C(s).
- ► We also have:

$$C(s) = R(s)T(s) \tag{7}$$

Combining the two we get

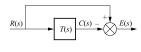
$$E(s) = R(s) - R(s)T(s) = R(s)[1 - T(s)]$$
(8)

We thus have

$$e_{ss} = \lim_{s \to 0} s E(s)$$

= $\lim_{s \to 0} s R(s)[1 - T(s)]$ (9)

Figure 7.3.



(a)

Steady-State Error and G(s)

► From equation 3, we have

$$E(s) = \frac{R(s)}{1 + G(s)}$$
 (10)

▶ We thus have

$$e_{ss} = \lim_{s \to 0} s E(s)$$

$$= \lim_{s \to 0} s \frac{R(s)}{1 + G(s)}$$
(11)

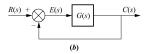


Figure 7.3.

Steady-State Error, G(s), and Step Input

► For input $R(s) = \frac{1}{s}$, we get

$$e_{ss} = \lim_{s \to 0} s \, \frac{1/s}{1 + G(s)} = \frac{1}{1 + \lim_{s \to 0} G(s)}$$
 (12)

- ▶ We refer to the term $\lim_{s\to 0} G(s)$ as dc gain of the forward transfer function.
- ► To have zero steady-state error we need

$$\lim_{s \to 0} G(s) = \infty \tag{13}$$

▶ For G(s) of form below, we thus need $n \ge 1$

$$G(s) \equiv \frac{(s+z_1)(s+z_2)\cdots}{s^n(s+p_1)(s+p_2)\cdots}$$
(14)

▶ If n = 0, we get

$$\lim_{s \to 0} G(s) = \frac{(0+z_1)(0+z_2)\cdots}{(0+p_1)(0+p_2)\cdots} = \frac{z_1 z_2 \cdots}{p_1 p_2 \cdots}$$
(15)

Steady-State Error, G(s), and Ramp Input

For input $R(s) = \frac{1}{s^2}$, we get

$$e_{ss} = \lim_{s \to 0} \frac{s(1/s^2)}{1 + G(s)} = \lim_{s \to 0} \frac{1}{s + sG(s)} = \frac{1}{\lim_{s \to 0} sG(s)}$$
 (16)

▶ To have zero steady-state error for ramp input, we need

$$\lim_{s \to 0} s G(s) = \infty \tag{17}$$

▶ For G(s) of form below, we thus need $n \ge 2$

$$G(s) \equiv \frac{(s+z_1)(s+z_2)\cdots}{s^n(s+p_1)(s+p_2)\cdots}$$
(18)

▶ If n = 1, we get

$$\lim_{s \to 0} s G(s) = \frac{z_1 z_2 \cdots}{p_1 p_2 \cdots} \tag{19}$$

▶ If n = 0, we get

$$\lim_{s \to 0} s G(s) = \frac{s(s+z_1)(s+z_2)\cdots}{(s+p_1)(s+p_2)\cdots} = 0$$
 (20)

Steady-State Error, G(s), and Parabolic Input

▶ For input $R(s) = \frac{1}{s^3}$, we get

$$e_{ss} = \lim_{s \to 0} \frac{s(1/s^3)}{1 + G(s)} = \lim_{s \to 0} \frac{1}{s^2 + s^2 G(s)} = \frac{1}{\lim_{s \to 0} s^2 G(s)}$$
(21)

▶ To have zero steady-state error for a parabolic input, we need

$$\lim_{s \to 0} s^2 G(s) = \infty \tag{22}$$

▶ For G(s) of form below, we thus need $n \ge 3$

$$G(s) \equiv \frac{(s+z_1)(s+z_2)\cdots}{s^n(s+p_1)(s+p_2)\cdots}$$
(23)

▶ If n = 2, we get

$$\lim_{s \to 0} s^2 G(s) = \frac{z_1 z_2 \cdots}{p_1 p_2 \cdots}$$
 (24)

▶ If n = 1, we get

$$\lim_{s \to 0} s^2 G(s) = \frac{s(s+z_1)(s+z_2)\cdots}{(s+p_1)(s+p_2)\cdots} = 0$$
 (25)

Steady-State Error eg.

Find the steady state errors for inputs 5u(t), 5tu(t), and $\frac{5}{2}t^2u(t)$.

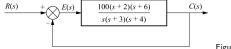


Figure 7.6.

Static Error Constants

- We now define steady state-error performance specifications called static error constants.
 - **1. Position Constant:** $K_p = \lim_{s \to 0} G(s)$, thus

$$e_{step}(\infty) = \frac{1}{1 + K_p}$$

2. Velocity Constant: $K_v = \lim_{s\to 0} sG(s)$, thus

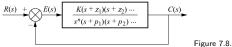
$$e_{ramp}(\infty) = \frac{1}{K_v}$$

3. Aceleration Constant: $K_a = \lim_{s\to 0} s^2 G(s)$, thus

$$e_{parabola}(\infty) = \frac{1}{K_a}$$

System Type

- ▶ The static error constants are determined by the structure of G(s).
- ▶ They are mostly determined by the number of integrators in G(s).
- ► The system type is the number of integrators in the forward path, thus the value of n in figure below.



Steady-State Error Summary

► Table shows relationship between input type, system type, static error constants, and steady-state errors.

		Type 0		Type 1		Type 2	
	Steady-state error formula	Static error constant	Error	Static error constant	Error	Static error constant	Error
Step, $u(t)$	$\frac{1}{1+K_p}$	$K_p =$ Constant	$\frac{1}{1+K_p}$	$K_p = \infty$	0	$K_p = \infty$	0
Ramp, tu(t)	$\frac{1}{K_v}$	$K_{\nu} = 0$	∞	$K_v = $ Constant	$\frac{1}{K_{\nu}}$	$K_v = \infty$	0
Parabola, $\frac{1}{2}t^2u(t)$	$\frac{1}{K_a}$	$K_a = 0$	∞	$K_a = 0$	∞	$K_a =$ Constant	$\frac{1}{K_a}$

able

Tight Steady-State Error Specifications

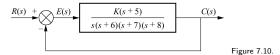
Example of a system requiring tight steady-state error specifications to be useful.



Figure 7.9.

Steady-State Error Specifications eg.

► For system below, find value of *K* such there is 10% error in steady state.



Steady-State Error and Disturbances

- Can use feedback systems to handle unwanted disturbances to the systems.
- By using feedback, we can design systems that follow the input signal with small or zero error, despite these disturbances.
- ightharpoonup Consider feedback system below with disturbance, D(S), added between plant and controller.
- The system output is

$$C(s) = E(s)G_1(s)G_2(s) + D(s)G_2(s)$$
(26)

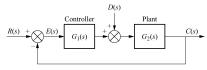


Figure 7.11.

Steady-State Error and Disturbances - II

However

$$E(s) = R(s) - C(s) \Rightarrow C(s) = R(s) - E(s) \tag{27}$$

▶ Using Equations 27 and 26 and solving for E(s) gives

$$E(s) = \frac{R(s)}{1 + G_1(s)G_2(s)} - \frac{D(s)G_2(s)}{1 + G_1(s)G_2(s)}$$
(28)

Using final-value theorem, the steady-state error is

$$e_{ss} = \lim_{s \to 0} sE(s) \tag{29}$$

$$= \lim_{s \to 0} \frac{sR(s)}{1 + G_1(s)G_2(s)} - \lim_{s \to 0} \frac{sD(s)G_2(s)}{1 + G_1(s)G_2(s)}$$
(30)

$$= e_R(\infty) + e_D(\infty) \tag{31}$$

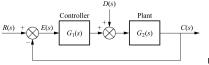


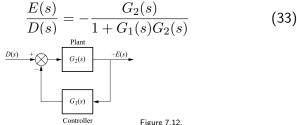
Figure 7.11.

Steady-State Error and Disturbances - III

- ▶ The $e_R(\infty)$ term is the steady-state error due to input R(s)that we have already seen.
- ▶ The $e_D(\infty)$ term is the steady-state error due to D(s).
- ▶ If D(s) = 1/s (step input), we have

$$e_D(\infty) = -\frac{1}{\lim_{s\to 0} \frac{1}{G_2(s)} + \lim_{s\to 0} G_1(s)}$$
 (32)

If we set R(s) = 0, we get from Eqn28 the transfer function:



Steady-State Error and State Space

- We now consider how to evaluate steady-state error for a system represented in state-space.
- ➤ As we saw in Section 3.6 of the text, we can convert a single-input single-ouput state-space representation to an equivalent closed-loop transfer function using

$$T(s) = \frac{Y(s)}{U(s)} = \underline{C}(s\underline{I} - \underline{A})^{-1}\underline{B}$$
 (34)

- ▶ In Diagram below, we have E(s) = R(s) C(s).
- ▶ We also have:

$$C(s) = R(s)T(s)$$

$$(35)$$

$$C(s) = R(s)T(s)$$

$$C(s) = R(s)T(s)$$

Figure 7.3.

Steady-State Error and State Space - II

Combining the two we get

$$E(s) = R(s) - R(s)T(s) = R(s)[1 - T(s)]$$
(36)

▶ We thus have

$$e_{ss} = \lim_{s \to 0} s E(s)$$

= $\lim_{s \to 0} s R(s)[1 - T(s)]$ (37)

▶ Substituting in for T(s) gives

$$e_{ss} = \lim_{s \to 0} s R(s) \left[1 - \underline{C}(s\underline{I} - \underline{A})^{-1}\underline{B}\right]$$
 (38)