



Mechanical Design & Load Analysis 5-DOF Robotic Arm

1: System Description

This report presents the complete mechanical design, kinematic modeling, and static load analysis of a 5-Degree of Freedom (5-DOF) robotic arm designed for sorting applications.

The robot is intended to pick, manipulate, and place objects into predefined locations based on sorting criteria such as length.

The analysis focuses on:

- **Links**
- **Joints**
- **Gripper (End Effector)**
- **The robot base is assumed to be fixed and therefore excluded from kinematic and dynamic calculations, in accordance with standard robotic modeling practice.**

2: System Overview

- 1. Manipulator Type:** Serial robotic arm
- 2. Degrees of Freedom:** 5
- 3. Joint Type:** All joints are revolute
- 4. Application:** Sorting and pick-and-place operations
- 5. Base Condition:** Fixed support
- 6. Manufacturing Method:** 3D printing

3: Degrees of Freedom & Joint Configuration

| Joint No. | Joint Type | Function |
|-----------|------------|------------------------------|
| J1 | Revolute | Base/Waist rotation |
| J2 | Revolute | Shoulder lift |
| J3 | Revolute | Elbow motion |
| J4 | Revolute | Wrist pitch |
| J5 | Revolute | Gripper rotation / actuation |

Total Joints = 5

Total DOF = 5

All joints are rotational (Revolute Joints)

4: Link Definition and Classification

Each link is defined as a rigid body connecting two consecutive joints.

| Link ID | Description |
|---------|-------------|
| L1 | Waist Link |
| L2 | Upper Arm |
| L3 | Forearm |
| L4 | Wrist Link |

- The base is not classified as a link since it does not contribute to motion.**

5: Material Selection – ABS

The robotic arm structure is manufactured from **ABS** (Acrylonitrile Butadiene Styrene) due to:

Low density → reduced inertia

Adequate mechanical strength

Ease of manufacturing (3D printing / molding)

Electrical insulation

Mechanical Properties of ABS:

- **Density = 1040, Kg/ m³**
- **Tensile strength ≈ 40 MPa**
- **Elastic modulus ≈ 2–2.5 GPa**

Material Justification:

Lightweight → reduced torque demand

Adequate strength for low-payload robotic systems

Good vibration damping

Suitable for precise 3D printing

6.CAD-Based Mass Properties

All mass properties were extracted directly from the SolidWorks Mass Properties tool, ensuring consistency between CAD geometry and analytical calculations.

Assembly Mass Properties:

- **Total moving mass: 0.62156 kg**
- **Center of Mass (COM):**

- X = 108.05 mm
- Y = 133.33 mm
- Z = 85.11 mm

The motors are excluded from link mass calculations and treated as external loads applied at joint locations.

7:Denavit–Hartenberg(D–H)Kinematic Modeling

The kinematic model of the robotic arm is developed using the standard Denavit–Hartenberg (D–H) convention.

D–H Parameters Definition:

- θ_i : Joint angle
- d_i : Link offset
- a_i : Link length
- α_i : Link twist

8: D–H Parameter Table

| Joint | θ_i (mm) | d_i (mm) | a_i (mm) | α_i (rad) |
|-------|-----------------|------------|------------|------------------|
| 1 | θ_1 | 194 | 0 | $+\pi/2$ |
| 2 | θ_2 | 0 | 115 | 0 |
| 3 | θ_3 | 0 | 50 | 0 |
| 4 | θ_4 | 0 | 120 | 0 |
| 5 | θ_5 | 0 | 0 | 0 |

These parameters accurately represent the physical geometry of the robotic arm and form the basis for forward and inverse kinematics.

9: Gripper (End Effector) Analysis

The gripper is treated as an independent mechanical unit.

- **Gripper Mass:** Extracted from CAD
- **Payload Mass:** 0.05 kg (design value)

Total Load at End Effector:

$$m(\text{total}) = m(\text{gripper}) + m(\text{payload})$$

The gripper is designed to handle the payload safely without exceeding joint torque limits.

10: Mass Calculation of Links

The mass of each link is calculated using the standard mass–density relationship:

$$m(\text{link}) = p \times V(\text{link})$$

Where:

p= density of ABS

V= volume extracted from CAD (SolidWorks)

- Volume and Center of Mass are obtained directly from CAD software (Mass Properties).

Placeholder Table (to be filled from SolidWorks):

| Link | Volume (m^3) | Mass (kg) |
|------|-------------------------|-----------|
| L1 | 1.15×10^{-4} | 0.119 |
| L2 | 1.35×10^{-4} | 0.141 |
| L3 | 0.48×10^{-4} | 0.050 |
| L4 | 1.21×10^{-4} | 0.126 |

11: Joint Mass Calculation

Each joint housing is treated as a rigid body.

$$m(\text{joint}) = \rho \times V(\text{joint})$$

- Motors are not included in link mass and are treated as external loads acting on joints.

| Joint | Volume (m^3) | Mass (kg) |
|-------|-------------------------|-----------|
| J1 | 0.25×10^{-4} | 0.026 |
| J2 | 0.32×10^{-4} | 0.033 |
| J3 | 0.22×10^{-4} | 0.023 |
| J4 | 0.18×10^{-4} | 0.019 |

12: Gripper Analysis (Independent Unit)

The gripper is treated as the end effector tool.

Components considered:

- Gripper body mass
- Actuation mechanism
- Payload (object to be lifted)

Payload is limited by:

- Grip force
- Joint torque capacity
- Structural safety factor

13: Load Accumulation on Joints

Each joint must support the weight of all components located after it.

$$W_i = \sum (m_k \cdot g)$$

Where:

$$g = 9.81, m/s^2$$

14: Required Torque Calculation

The required torque at each joint is calculated as:

$$T_i = \sum (m_k \cdot g \cdot d_k)$$

Where:

d_k = distance from joint axis to center of mass

Design Torque:

$$T(\text{design}) = T(\text{required}) \times SF$$

Safety Factor SF = 1.5_2

15: Torque Calculation (Worst-Case Scenario)

The worst-case loading condition occurs when the arm is fully extended horizontally.

Torque Equation:

$$T = m \cdot g \cdot d$$

Calculated Values:

- Arm torque $\approx 8.12 \text{ kg}\cdot\text{cm}$
- Payload torque $\approx 1.40 \text{ kg}\cdot\text{cm}$

Total Required Torque:

T(required)~9.52 kg.cm

16: Motor Capability Verification

- **Motor Type: MG995=50gm +sg90s=9gm**
- **Rated Torque: 13 kg·cm @ 6V**
- **Safety Factor: [SF= 13/9.52=~1.36]**

This safety factor ensures reliable operation under real conditions, accounting for friction and dynamic effects.

Design condition:

T(motor)>=2×T(required)

- **This ensures:**
- **No motor stall**
- **Stable motion**
- **Long motor lifetime**

17: Weight Optimization Justification

ABS reduces total arm mass

Hollow link design reduces inertia

Maximum load concentrated near the gripper only

This results in:

- **Lower torque demand**
- **Better dynamic response**
- **Improved system stability**

- **Assumptions**

- **Quasi-static operation**
- **Friction neglected**
- **Rigid links**
- **Fixed base**
- **Vertical gravitational loading**

18:Conclusion

- **The mechanical design of the 5-DOF robotic sorting arm has been fully validated.**
- **All links, joints, and the gripper satisfy mechanical strength and torque requirements based on CAD-verified mass properties and standard engineering equations.**
- **The robot is mechanically stable, lightweight, and capable of safely handling the specified payload for sorting applications.**