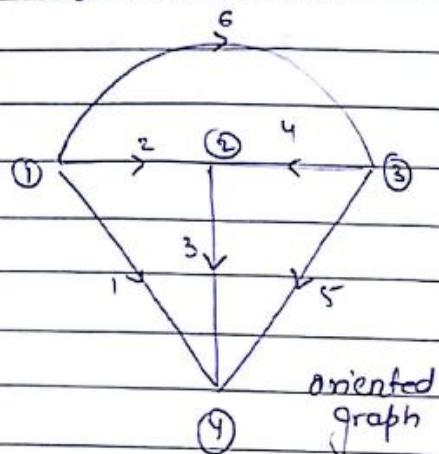


UNIT - 3

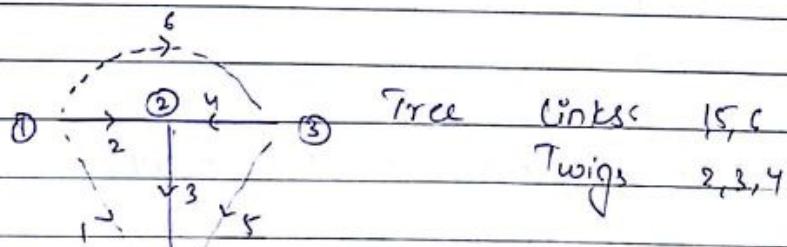
Ques With the help of oriented graph, Find twig and link matrix.



$$[A] = \begin{matrix} & \begin{smallmatrix} 1 & 2 & 3 & 4 & 5 & 6 \end{smallmatrix} \\ \begin{smallmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{smallmatrix} & \begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 1 \\ 0 & -1 & 1 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 1 & -1 \\ -1 & 0 & -1 & 0 & 1 & 0 \end{bmatrix} \end{matrix}$$

If the arrow from node is
 • in = -1
 • out = 1

$$\text{Reduced } [n] = \begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 1 \\ 0 & -1 & 1 & -1 & 0 & 0 \\ -1 & 0 & -1 & 0 & -1 & 0 \end{bmatrix}$$



$$\text{Reduced } [n] = \begin{bmatrix} 2 & 3 & 4 & 5 & 6 & 1 \\ 1 & 0 & 0 & 1 & 0 & 1 \\ -1 & 1 & -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 & -1 & 0 \end{bmatrix}$$

Twigs Links

$$\text{Twig Matrix } [T] = \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & -1 \\ 0 & -1 & 0 \end{bmatrix} \quad \text{Link Matrix } [L] = \begin{bmatrix} 1 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & -1 & 0 \end{bmatrix}$$

The determinant of Link Matrix is 1 or -1

$$\text{Det} [T] = 1(-1) - 0 + 0 \\ = -1$$

* No. of Trees from a Graph

Determinant $| [B] \cdot [B]^T |$

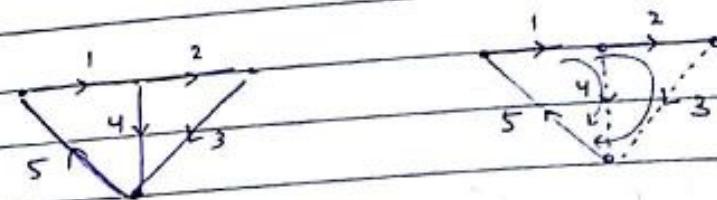
$$= \begin{vmatrix} 1 & 1 & 0 & 0 & 0 & 1 \\ 0 & 1 & 1 & 1 & 0 & 0 \\ -1 & 0 & -1 & 0 & -1 & 0 \end{vmatrix} \begin{vmatrix} 1 & 0 & -1 \\ 1 & -1 & 0 \\ 0 & 1 & -1 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \\ 1 & 0 & 0 \end{vmatrix}$$

$$= \begin{vmatrix} 1+1+1 & -1 & -1 \\ -1 & 1+1+1 & -1 \\ -1 & -1 & 1+1+1 \end{vmatrix}$$

$$= \begin{vmatrix} 3 & -1 & -1 \\ -1 & 3 & -1 \\ -1 & -1 & 3 \end{vmatrix} = 3(9-1) + 1(-3-1) + 1(1+3) \\ = 24 - 4 - 4 \\ = 16$$

* Fundamental Tie-set Matrix

A fundamental loop or tie-set matrix of a graph w.r.t. a tree is a loop for by only one link associated with other twigs



(L₁) loop 1 : (1, 4, 5)

(L₂) loop 2 : (1, 2, 3, 5)

Fundamental
loop matrix

	1	2	3	4	5
L ₁	1	0	0	1	1
L ₂	1	1	1	0	1

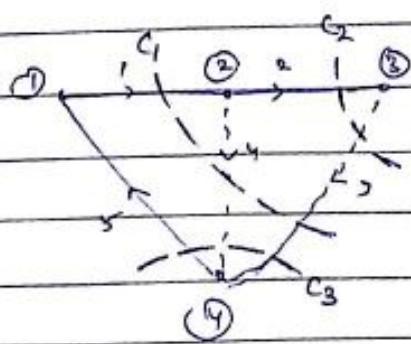
- if the arrows
in the direction
of loop = 1
- opp. to the direction
of loop = -1

* Cut-Set Matrix

It consists of one and only one branch of the network tree together with any links which must be cut to divide the network into two parts.

Assumptions:

1. Cut is always (n-1) in a tree [n: no. of nodes]
2. Cut should be like this only, one node is included
3. Cut should be like this only, one solid line (twig) is included.

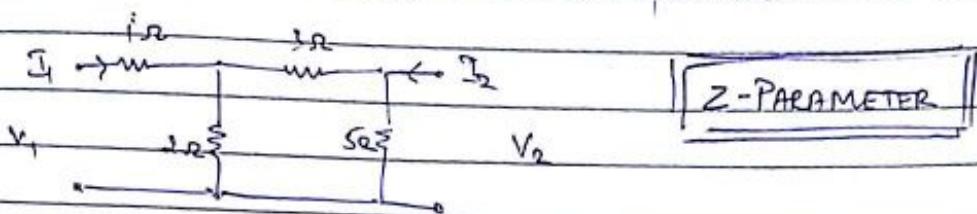


$$[C] = C_1 \begin{bmatrix} 1 & -1 & -1 & 1 & 0 \\ 0 & 1 & -1 & 0 & 0 \\ 0 & 0 & 1 & 1 & -1 \end{bmatrix}$$

if arrow from the arc is
outward = -1
inward = 1

Two Port Network Analysis

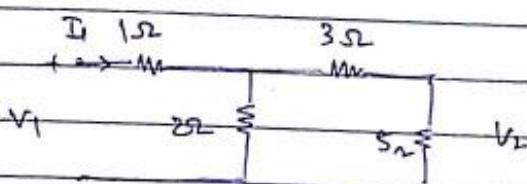
- Z → Parameter
- Y → Parameter
- T (ABCD) - Parameter
- h - Parameter



$$\begin{array}{|c|c|} \hline I_2 = 0 & I_1 = 0 \\ \hline Z_{11} = \frac{V_1}{I_1} & Z_{12} = \frac{V_1}{I_2} \\ \hline \end{array}$$

$$Z_{21} = \frac{V_2}{I_1} \quad Z_{22} = \frac{V_2}{I_2}$$

Case I: $I_2 = 0$



$$R_{11} = \left(\frac{16}{10} + 1 \right) = 2.6 \Omega$$

$$V_1 = R_{11} \cdot I_1$$

$$\Rightarrow V_1 = 2.6 \cdot I_1$$

$$\frac{V_1}{I_1} = Z_{11} = 2.6 \Omega$$

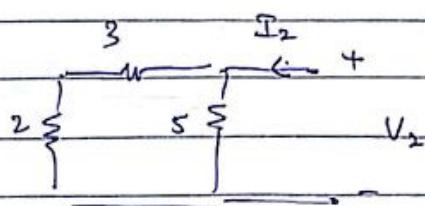
$$V_2 = 5 \cdot I_{2n}$$

$$\Rightarrow 5 \cdot I_{2n} = I_1 \cdot \frac{2}{10}$$

$$\Rightarrow V_2 = I_1$$

$$\Rightarrow \frac{V_2}{I_1} = Z_{21} = \underline{\underline{1\Omega}}$$

Case II : $\Sigma_i = 0$



$$Rev = \frac{5-5}{10} = 0,5 \Omega$$

$$V_2 = Rev \cdot I_2$$

$$\frac{V_2}{I_2} = Z_{22} = \underline{\underline{2,5 \Omega}}$$

$$V_1 = 2 \cdot I_{2n}$$

$$I_{2n} = I_2 \cdot \frac{5}{10}$$

$$V_1 = 2 \cdot \frac{I_2}{2}$$

$$\frac{V_1}{I_2} = Z_{12} = \underline{\underline{1\Omega}}$$

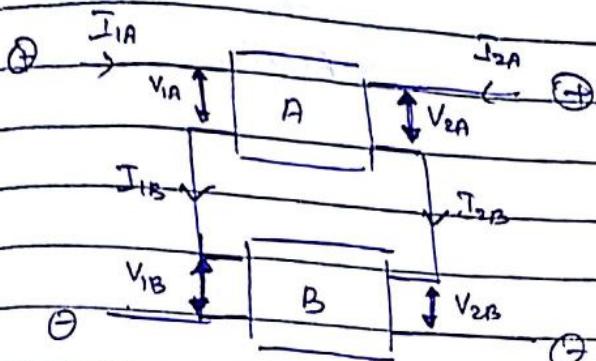
Inter Connection of 2-Port Network

Series - 2

Parallel - 4

Transcads - T

① Series Connection



For Network A

$$V_{1A} = Z_{11A} \cdot I_{1A} + Z_{12A} \cdot I_{2A}$$

$$V_{2A} = Z_{21A} \cdot I_{1A} + Z_{22A} \cdot I_{2A}$$

For Network B

$$V_{1B} = Z_{11B} \cdot I_{1B} + Z_{12B} \cdot I_{2B}$$

$$V_{2B} = Z_{21B} \cdot I_{1B} + Z_{22B} \cdot I_{2B}$$

Refer to given configuration, i.e. series connection

$$I_1 = I_{1A} = I_{1B}$$

$$I_2 = I_{2A} = I_{2B}$$

$$V_1 = V_{1A} + V_{1B}$$

$$V_2 = V_{2A} + V_{2B}$$

$$\begin{aligned} \therefore V_1 &= (Z_{11A} \cdot I_{1A} + Z_{12A} \cdot I_{2A}) + (Z_{11B} \cdot I_{1B} + Z_{12B} \cdot I_{2B}) \\ &= (Z_{11A} + Z_{11B}) I_1 + (Z_{12A} + Z_{12B}) I_2 \end{aligned}$$

Similarly

$$V_2 = (Z_{21A} + Z_{21B}) I_1 + (Z_{22A} + Z_{22B}) I_2$$

~~Addition~~

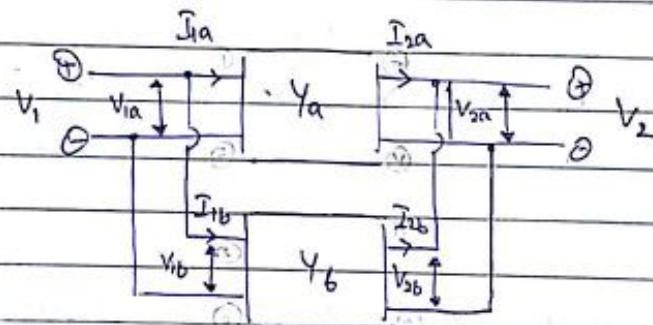
$$\begin{bmatrix} Z \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Z_{11A} + Z_{11B} & Z_{12A} + Z_{12B} \\ Z_{21A} + Z_{21B} & Z_{22A} + Z_{22B} \end{bmatrix}$$

Definitions

- Linear Element
- Active Elements
- Unilateral Ckt.
- Linear ckt.
- Non Linear Element
- Passive Elements
- Bilateral

~~4/10/17~~

② Parallel Connection



$$\begin{bmatrix} I_{1a} \\ I_{2a} \end{bmatrix} = \begin{bmatrix} Y_{11a} & Y_{12a} \\ Y_{21a} & Y_{22a} \end{bmatrix} \begin{bmatrix} V_{1a} \\ V_{2a} \end{bmatrix}$$

$$\begin{bmatrix} I_{1b} \\ I_{2b} \end{bmatrix} = \begin{bmatrix} Y_{11b} & Y_{12b} \\ Y_{21b} & Y_{22b} \end{bmatrix} \begin{bmatrix} V_{1b} \\ V_{2b} \end{bmatrix}$$

$$V_1 = V_{1a} = V_{2b}$$

$$V_2 = V_{2a} = V_{1b}$$

$$I_1 = I_{1a} + I_{1b}$$

$$I_2 = I_{2a} + I_{2b}$$

$$I_{1a} = Y_{11a} \cdot V_{1a} + Y_{12a} \cdot V_{2a} \quad \text{--- (1)}$$

$$I_{2a} = Y_{21a} \cdot V_{1a} + Y_{22a} \cdot V_{2a} \quad \text{--- (2)}$$

$$I_{1b} = Y_{11b} V_{1b} + Y_{12b} V_{2b} \quad \text{--- (2)}$$

$$I_{2b} = Y_{21b} V_{1b} + Y_{22b} V_{2b} \quad \text{--- (4)}$$

Adding (2) & (4)

$$\Rightarrow I_1 = (Y_{11a} + Y_{11b}) V_1 + (Y_{12a} + Y_{12b}) V_2 \quad \text{--- (5)}$$

Adding (2) & (4)

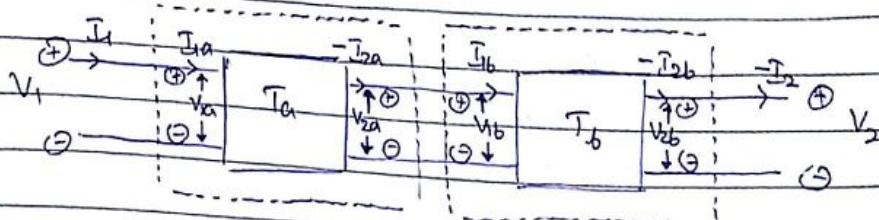
$$\Rightarrow I_2 = (Y_{21a} + Y_{21b}) V_1 + (Y_{22a} + Y_{22b}) V_2 \quad \text{--- (6)}$$

On comparing

$$\begin{bmatrix} (Y_{11a} + Y_{11b}) & (Y_{12a} + Y_{12b}) \\ (Y_{21a} + Y_{21b}) & (Y_{22a} + Y_{22b}) \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = [Y]$$

Imp.

(3) Cascade Connection



$$\begin{bmatrix} V_{1a} \\ I_{1a} \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} V_{2a} \\ -I_{2a} \end{bmatrix} \quad \text{--- (1)}$$

Since $I_2 = 0$
 $V_2 = 0$

$$\begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix} = \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix} \begin{bmatrix} V_{2b} \\ -I_{2b} \end{bmatrix} \quad \text{--- (2)}$$

$$I_1 = I_{1a} \quad T_{1b} = -I_{2b}$$

$$I_2 = I_{2b}$$

$$V_1 = V_{1a} \quad V_{1b} = V_{2a}$$

$$V_2 = V_{2b}$$

Using (1)

$$\Rightarrow \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} = \begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix}$$

Substituting ②

$$\Rightarrow \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

~~$$\Rightarrow \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix}$$~~

~~$$[T] = [E_a][T_b]$$~~

6/10/17 Reciprocity

A two port network is said to be reciprocal if its ratio of excitation to response is invariant to an interchange of the pos. of the excitation and response in the ckt.

Symmetry

A two port network is said to be symmetrical if the ports can be interchanged without changing the port, var. voltages & current

Parameter	Relation b/w V and I	Cond* for symmetry	Cond* for reciprocity
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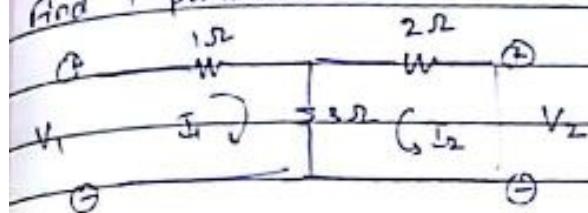
$$Z \quad (V_1, V_2) = F(I_1, I_2) \quad Z_{11} = Z_{22} \quad Z_{12} = Z_{21}$$

$$Y \quad (I_1, I_2) = F(V_1, V_2) \quad Y_{11} = Y_{22} \quad Y_{12} = Y_{21}$$

$$T \quad (V_1, I_2) = F(V_2, I_1) \quad A = D \quad AD - BC = 1$$

$$h \quad (V_1, I_2) = F(V_2, I_1) \quad h_{11}h_{22} - h_{12}h_{21} = 1 \quad h_{12} = -h_{21}$$

Find Y parameter



$$[Y] = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}$$

$$Y_{11} = \frac{I_1}{V_1} \quad Y_{21} = \frac{I_2}{V_1}$$

$$\text{Case I: } V_1 = 0$$

$$Y_{12} = \frac{I_1}{V_2} \quad Y_{22} = \frac{I_2}{V_2}$$

$$V_1 = I_1 + 3(I_1 + I_2)$$

$$0 = 2I_2 + 3(I_1 + I_2)$$

$$\Rightarrow -3I_1 = 5I_2$$

$$\therefore V_1 = Y_{11}I_1 = \frac{1}{5}I_1$$

$$= \frac{11}{5}I_1$$

$$Y_{11} = \frac{I_1}{V_1} = \frac{5}{11} \Omega^{-1}$$

$$V_1 = Y_{11} \left(-\frac{5}{3}I_2 \right) + 3I_2$$

$$\Rightarrow -\frac{11}{3}I_2$$

$$Y_{21} = \frac{I_2}{V_1} = \frac{-3}{11} \Omega^{-1}$$

$$\text{Case II, } V_1 = 0$$

$$0 = I_1 + 3(I_1 + I_2)$$

$$\Rightarrow -4I_1 = 3I_2$$

$$V_2 = 2I_2 + 3(I_1 + I_2)$$

$$= 5I_2 + 3I_1$$

$$\therefore V_2 = 5I_2 + 3\left(-\frac{3}{4}I_2\right)$$

$$= \left(\frac{20-9}{4}\right)I_2$$

$$= \frac{11}{4}I_2$$

$$\Rightarrow \frac{V_2}{I_2} = \frac{40}{11} = Y_{22}$$

$$V_2 = 5\left(-\frac{4}{3}I_1\right) + 3I_1$$

$$= \left(\frac{-20+9}{3}\right)I_1$$

$$= -\frac{11}{3}I_1$$

$$\Rightarrow \frac{I_1}{V_2} = Y_{12} = \frac{-3}{11} \Omega^{-1}$$

$Y_{11} \neq Y_{22} \therefore$ The given port network is not symmetric
 $Y_{21} = Y_{12} \therefore$ It is reciprocal

$\text{ABC}\Delta$ Parameter

Case I $I_2 = 0$

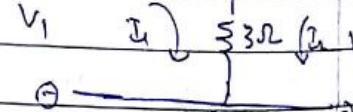
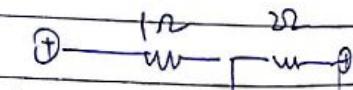
$$A = \frac{V_1}{V_2}$$

$$C = \frac{I_1}{V_2}$$

$\text{Case II } V_2 = 0$

$$B = V_1$$

$$D = \frac{I_1}{-I_2}$$



$$V_1 = \frac{11}{5} \cdot 4 \therefore +1$$

Case II : $I_2 = 0$

$$V_2 = I_2 \cdot 4$$

$$V_2 = 3I_1 \quad +$$

$$\Rightarrow C = \frac{V_1}{V_2} = \frac{1}{3} \text{ } \Omega^{-1}$$

$$V_1 = \frac{V_2}{3} \cdot 4$$

$$\Rightarrow A = \frac{V_1}{V_2} = \frac{4}{3}$$

Case II : $V_2 = 0$

$$V_1 = 4I_1 + 3(I_1 + I_2)$$

$$V_1 = I_1 + 3(I_1 + I_2) \\ = 4I_1 + 3I_2$$

$$0 = 2I_2 + 3(I_1 + I_2)$$

$$5I_2 = -3I_1$$

$$\frac{I_1}{-I_2} \rightarrow D = \frac{5}{3}$$

$$V_1 = 4 \cdot \left(\frac{-5I_2}{3} \right) + 3I_2$$

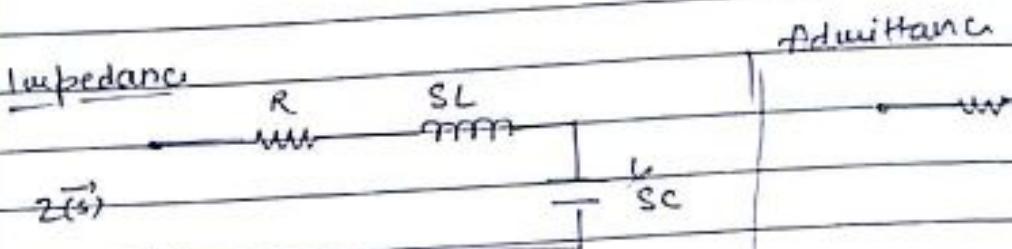
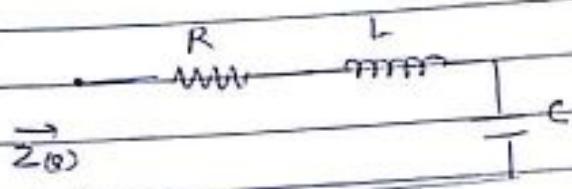
$$= \frac{-11}{3} I_2$$

$$\frac{V_1}{-I_2} = \frac{11}{3} \text{ } \Omega$$

Network Functions

	$Z(s)$	$Y(s)$	Inittance	Impedance → Admittance
R	R	$Y_R = \frac{1}{R}$		
L	sL	$Y_{SL} = \frac{1}{sL}$		
C	$\frac{1}{sC}$	sC		

$Z_{21}(s) = \frac{V_2(s)}{I_1(s)}$	Forward Impedance Transfer Junc ⁿ	$Z_{12}(s) = \frac{V_1(s)}{I_2(s)}$	Reverse Impedance T.F.
$Y_{21}(s) = \frac{I_2(s)}{V_1(s)}$	Fwd. Admittance T.F.	$Y_{12}(s) = \frac{I_1(s)}{V_2(s)}$	Rev. Admittance T.F.
$\beta_{21}(s) = \frac{V_2(s)}{V_1(s)}$	Fwd. Voltage T.F.	$\beta_{12}(s) = \frac{V_1(s)}{V_2(s)}$	Rev. Voltage T.F.
$\alpha_{21}(s) = \frac{I_2(s)}{I_1(s)}$	Fwd. Current T.F.	$\alpha_{12}(s) = \frac{I_1(s)}{I_2(s)}$	Rev. Current T.F.



$$Z(s) = Z_1(s) + Z_2(s) + Z_3(s)$$

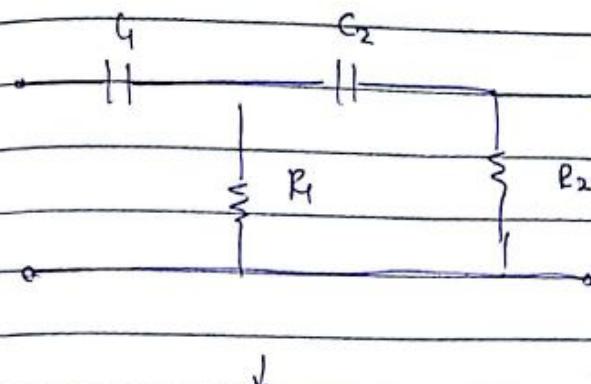
$$= R + sL + \frac{1}{sC}$$

$$= \frac{RSC + s^2 LC + 1}{sC}$$

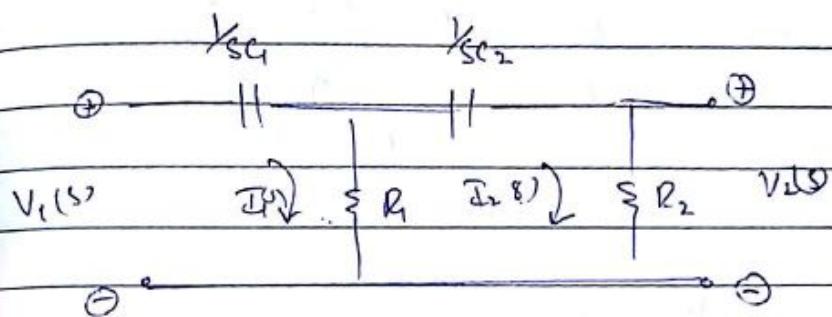
$$= \frac{LC(s^2 + (\frac{R}{L})s + \frac{1}{LC})}{sC}$$

$$= \frac{LC(s^2 + (\frac{R}{L})s + \frac{1}{LC})}{s}$$

Q) Find the exp. for voltage transfer function of given network



↓



loop 1

$$V_1(s) = \frac{I_1}{sC_1} + R_1 [I_1(s) - I_2(s)]$$

$$V_1(s) = I_1(s) \left(R_1 + \frac{1}{sC_1} \right) - I_2(s) R_1 \quad \text{--- (1)}$$

loop 2

$$\frac{I_2(s)}{sC_2} + R_2 \cdot I_2(s) + R_1 [I_2(s) - I_1(s)] = 0$$

$$\Rightarrow I_2(s) \left(R_1 + R_2 + \frac{1}{sC_2} \right) - I_1(s) \cdot R_1 = 0 \quad \text{--- (2)}$$

$$V_2(s) = R_2 \cdot I_2(s) \quad \text{--- (3)}$$

$$\beta_{21}(s) = \frac{V_2(s)}{V_1(s)} = \frac{R_2 I_2(s)}{V_1(s)}$$

CRAMMER RULE

- $a_1x + b_1y = c_1$
- $a_2x + b_2y = c_2$

$$D = \begin{vmatrix} a_1 & b_1 \\ a_2 & b_2 \end{vmatrix}$$

$$D_x = \begin{vmatrix} c_1 & b_1 \\ c_2 & b_2 \end{vmatrix} \quad D_y = \begin{vmatrix} a_1 & c_1 \\ a_2 & c_2 \end{vmatrix}$$

$$x = \frac{D_x}{D} \quad y = \frac{D_y}{D}$$

$$I_2(s) = \frac{\begin{vmatrix} R_1 + \frac{1}{sC_1} & V_1(s) \\ -R_1 & 0 \end{vmatrix}}{\begin{vmatrix} R_1 + \frac{1}{sC_1} & -R_1 \\ -R_1 & R_1 + R_2 + \frac{1}{sC_2} \end{vmatrix}}$$

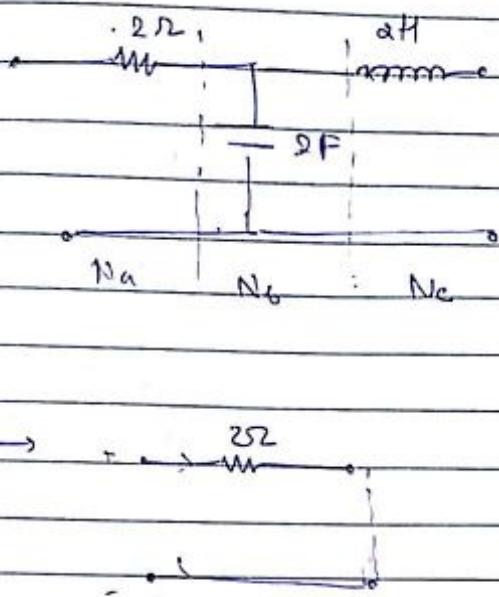
$$= \frac{V_1(s) \cdot R_1}{R_1 R_2 + \frac{R_1}{sC_1} + \frac{R_1 + R_2}{sC_2} + \frac{1}{s^2 C_1 C_2}}$$

$$\therefore \beta_{21}(s) = \frac{\begin{vmatrix} R_1 R_2 & V_1(s) \\ R_1 R_2 + \frac{R_1}{sC_2} + \frac{R_1 + R_2}{sC_1} + \frac{1}{s^2 C_1 C_2} \end{vmatrix}}{V_1(s)}$$

$$\Rightarrow \left[\frac{R_1 R_2}{R_1 R_2 + \frac{R_1}{sC_2} + \frac{R_1 + R_2}{sC_1} + \frac{1}{s^2 C_1 C_2}} \right]$$

↙

Determine the transmission parameter of a T-network considering 3 sections. Assuming connected in cascade manner.



$N_a \rightarrow$

$$\text{Case I: } I_2 = 0$$

$$A = \frac{V_1}{V_2} \quad C = \frac{I_1}{V_2}$$

- $V_1 = V_2$

$$\Rightarrow A = 1$$

- $I_1 = I_2 = 0$ no close loop

$$\Rightarrow C = 0$$

$$\text{Case II: } V_2 = 0$$

$$B = \frac{V_1}{-I_2} \quad D = \frac{I_1}{-I_2}$$

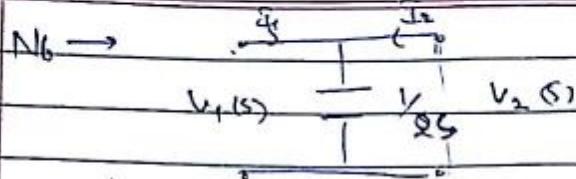
$$V_1 = I_1 \cdot 2$$

$$\text{but } I_1 = -I_2$$

$$\Rightarrow B = \frac{V_1}{-I_2} = 2 \Omega$$

$$D = 1$$

$$\therefore [T_{12}] = \begin{bmatrix} 1 & 2 \\ 0 & 1 \end{bmatrix}$$

Case I: $I_1 = 0$

$$V_1 = \frac{I_1}{2s}, \quad C_1 V_2 = \frac{I_1}{2s}$$

$$\left| \begin{array}{l} C \cdot \frac{I_1}{V_2} = 2s \\ V_2 \end{array} \right| \Rightarrow I_1 = 2s V_2^{-1}$$

$$\left| \begin{array}{l} A = \frac{V_1}{V_2} = 1 \\ V_2 \end{array} \right|$$

case II: $V_2 = 0$

$$V_1(s) = \frac{1}{2s}(I_1 + I_2)$$

$$0 = \frac{1}{2s}(I_1 + I_2) \Rightarrow I_1 = -I_2$$

$$\left| \begin{array}{l} D = \frac{I_1}{-I_2} = 1 \\ -I_2 \end{array} \right| \quad \boxed{B=0}$$

$$[T_B] = \begin{bmatrix} 1 & 0 \\ 2s & 1 \end{bmatrix}$$



$$[T_C] = \begin{bmatrix} 1 & 2s \\ 0 & 1 \end{bmatrix}$$

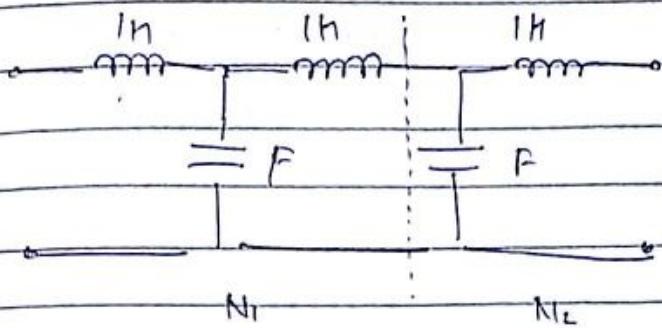
By cascade property

$$[T] = [T_B][T_B][T_C]$$

$$= \begin{bmatrix} 1 & 2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 2s & 1 \end{bmatrix} \begin{bmatrix} 1 & 2s \\ 0 & 1 \end{bmatrix}$$

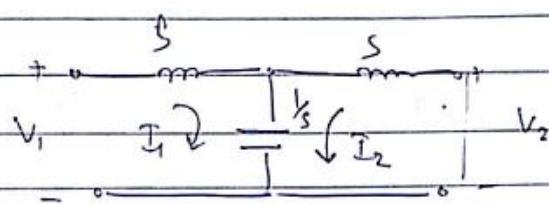
$$= \begin{bmatrix} 1+4s & 2 \\ 2s & 1 \end{bmatrix} \begin{bmatrix} 1 & 2s \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1+4s & 2s(1+4s)+2 \\ 2s & 4s^2+1 \end{bmatrix}$$

Find the T parameters of the network, using the concept of interconnection of two port network in cascade.



$$[T] = [T_1][T_2]$$

For N_1 :



Case I: $I_2 = 0$

$$V_1 = I_1 s + \frac{1}{s} I_1$$

$$V_1 = I_1 \left(s + \frac{1}{s} \right)$$

$$V_2 = I_1 \cdot \frac{1}{s}$$

$$\left| \begin{array}{l} \text{C} \\ \text{C} \end{array} \right. \frac{I_1}{V_2} = s \Omega^{-1}$$

$$\left| \begin{array}{l} A \\ A \end{array} \right. \frac{V_1}{V_2} = s^2 + 1$$

Case II: $V_2 = 0$

$$V_1 = \left(\frac{V_2 + 1}{s} \right)$$

$$V_1 = I_1 s + \frac{1}{s} (I_1 + I_2)$$

$$I_2 \cdot s + \frac{1}{s} (I_2 + I_1) = 0$$

$$\left(\frac{s^2 + 1}{s} \right) I_2 = -\frac{I_1}{s}$$

$$V_1 = -s(s^2 + 1) I_2 + \frac{1}{s} I_2$$

$$V_1 = s(s^2 + 1) - \frac{1}{s} + (s^2 + 1)$$

$$V_1 = \frac{s^4 + s^2 - 1 + s^3 + s}{s}$$

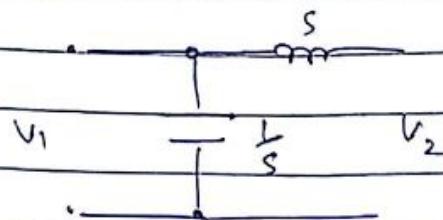
$$V_1 = -(s^2 + 1)(s^2 + 1) I_2 + \frac{I_2}{s}$$

$$V_1 = \frac{s^4 + 2s^2 + 1 - 1}{-I_2 s}$$

$$\boxed{B = \frac{s^3 + 2s}{-I_2}}$$

$$\boxed{D = \frac{I_1}{-I_2} = s^2 + 1}$$

For N₂



Case I: $I_2 = 0$

$$V_1 = \frac{I_1 \cdot L}{s}$$

$$V_2 = \frac{I_1}{s}$$

Case II: $V_2 = 0$

$$V_1 = \left(I_1 + I_2 \right) \frac{1}{s}$$

$$0 = \frac{sI_2}{s} + (I_1 + I_2)$$

$$\boxed{C = \frac{V_2}{V_1} = s = \Omega^{-1}}$$

$$\Rightarrow 0 = \frac{2I_2}{s} + \frac{I_1 + I_2(s^2 + 1)}{s}$$

$$\boxed{A = 1}$$

$$\Rightarrow I_1 = -2I_2$$

$$I_1 = -I_2(s^2 + 1)$$

$$B = \frac{V_1}{-I_2} = \frac{1}{2s}$$

$$\boxed{D = \frac{I_1}{-I_2} = s^2 + 1}$$

$$V_1 = \frac{(-I_2(s^2 + 1) + I_2)}{s}$$

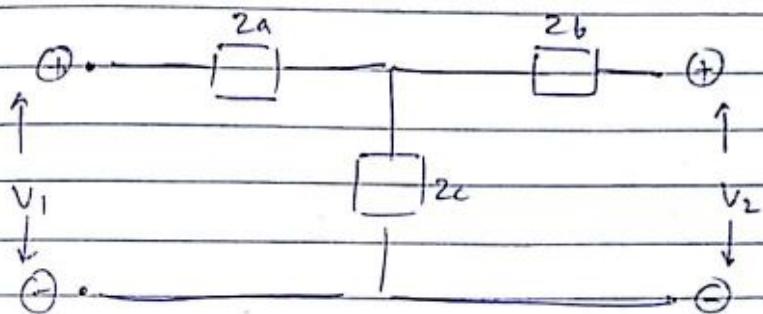
$$\boxed{B = \frac{V_1}{-I_2} = s \Omega}$$

$$\left[T \right] = \left[T_1 \right] \left[T_2 \right]$$

$$= \begin{bmatrix} s^2 + 1 & s^3 + 2s \\ s & s^2 + 1 \end{bmatrix} \begin{bmatrix} 1 & s \\ s & s^2 + 1 \end{bmatrix}$$

$$= \begin{bmatrix} (s^2 + 1 + s^4 + 2s^2) & (s^3 + s + s^5 + 2s^3 + s^3 + 2s) \\ (s + s^3 + s) & (s^2 + s^4 + 2s^2 + 1) \end{bmatrix}$$

T-Configuration 2-Port Network



Z-Parameter

$$\boxed{I_2 = 0}$$

$$Z_{11} = \frac{V_1}{I_1}$$

$$Z_{21} = \frac{V_2}{I_1}$$

$$\boxed{I_1 = 0}$$

$$Z_{12} = \frac{V_1}{I_2}$$

$$Z_{22} = \frac{V_2}{I_2}$$

When $I_2 = 0$

$$V_1 = I_1 (Z_a + Z_c)$$

$$Z_{11} = \frac{V_1}{I_1} = Z_a + Z_c$$

$$V_2 = I_1 \cdot Z_c$$

$$Z_{21} = \frac{V_2}{I_1} = Z_c$$

When $I_1 = 0$

$$V_2 = I_2 (Z_b + Z_c)$$

$$Z_{22} = \frac{V_2}{I_2} = Z_b + Z_c$$

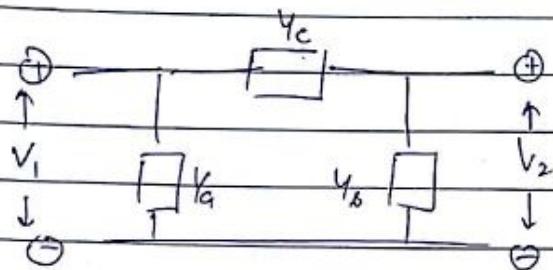
$$V_1 = Z_c \cdot I_2$$

$$Z_{12} = \frac{V_1}{I_2} = Z_c$$

$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \rightarrow \begin{bmatrix} Z_a + Z_c & Z_c \\ Z_c & Z_b + Z_c \end{bmatrix}$$

- $Z_{11} = Z_a + Z_c$
- $Z_{12} = Z_{21} = Z_c$
- $Z_{22} = Z_b + Z_c$
- $Z_a = Z_{11} - Z_{12}$
- $Z_b = Z_{22} - Z_{12}$
- $Z_c = Z_{21} = Z_{12}$

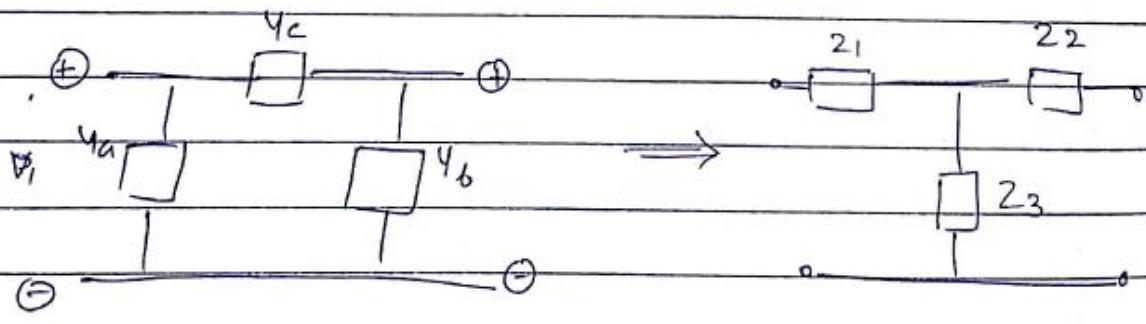
II configuration 2 Port Network



~~Chuilec~~ $\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \rightarrow \begin{bmatrix} Y_a + Y_c & -Y_c \\ -Y_c & Y_b + Y_c \end{bmatrix}$

- $Y_a = Y_{11} + Y_{12}$
- $Y_b = -Y_{12} = -Y_{21}$
- $Y_c = Y_{22} + Y_{12}$

Conversion



$$\Delta Y = Y_a Y_b + Y_b Y_c + Y_c Y_a$$

$$Z_1 = \frac{Y_b}{\Delta Y}$$

$$Z_2 = \frac{Y_a}{\Delta Y}$$

$$Z_3 = \frac{Y_c}{\Delta Y}$$

$$| Z \rightarrow Y \Rightarrow T \rightarrow \Pi |$$

$$Y_a = \frac{Z_2}{\Delta Z}$$

$$\Delta Z = Z_1 Z_2 + Z_2 Z_3$$

$$Y_b = \frac{Z_1}{\Delta Z} + Z_1 Z_3$$

$$Y_c = \frac{Z_3}{\Delta Z}$$

Image Impedance

If we see a two port network from input end and short the o/p end, with load then the virtual load appears at I/P end.

i.e. Z_{i1}

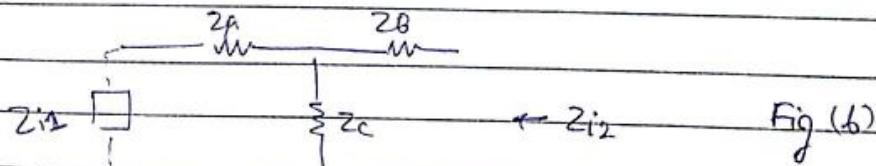
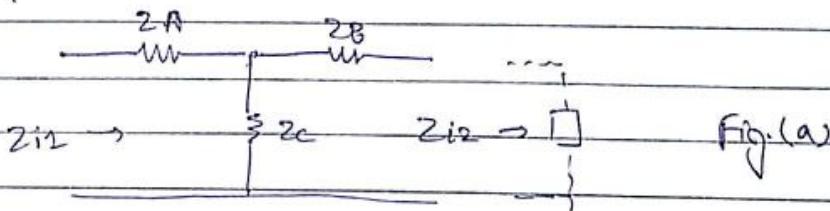
Similarly if load is connected at I/P end then img. of that load appears at o/p end
i.e. Z_{i2}

So Z_{i1} and Z_{i2} is called image / iterative impedance

If $Z_{i1} = Z_{i2}$ then network is symmetrical

$$Z_{img} = \sqrt{Z_{sc} Z_{oc}}$$

Image Impedance



Fig^(a)

$$Z_{i3} = Z_A + [Z_C // (Z_B + Z_{i2})]$$
$$= Z_A + \frac{Z_C (Z_B + Z_{i2})}{Z_B + Z_C + Z_{i2}}$$

$$\Rightarrow Z_{i3} (Z_B + Z_C + Z_{i2}) = Z_A (Z_B + Z_i + Z_{i2}) + Z_C (Z_B + Z_{i2})$$

$$\Rightarrow Z_{i1} \cdot Z_{i2} + Z_{i1} (Z_B + Z_C) - Z_{i2} (Z_A + Z_C) = \underline{\underline{Z_A Z_B + Z_B Z_C + Z_A Z_C}} \\ \sum Z_A \cdot Z_B$$

①

Dt. 11/10/17 Pg. _____ B+

CGB

$$P(s) = 4s^6 + 2s^5 + 17s^4 + 8s^3 + 16s^2 + 6s + 3$$

$$e(x) = 4x^6 + 17x^4 + 16x^2 + 3$$

$$v(s) = 2s^5 + 8s^3 + 6s$$

$$P(8) = 2s^5 + 8s^3 + 6s \quad | \quad 4s^6 + 17s^4 + 16s^2 + 3 \quad | \quad 2s$$

$$O(8) - \underline{4s^2 + 16s^4 + 12s^2}$$

$$* \quad 8^4 + 48^2 + 3 \mid 21^5 + 38^3 + 65 \mid 28$$

$$\underline{2x^8 + 8x^3 + 6x}$$

x

Kauri wood should have
true eq" end terminates abruptly

The continued ^{fract} expansion terminates abruptly.

The last divisor $(x^4 + 4x^2 + 3)$ is therefore one of the factors of given polynomial. [P(5)]

To find another factor for $P(s)$, divide $P(s)$ with last divisor obtained in continued fract" expansion.

$$\begin{array}{r}
 \overline{4x^5 + 2x^4 + 1} \\
 4x^6 + 2x^5 + 17x^4 + 8x^3 + 16x^2 + 6x + 3 \\
 - 4x^6 \qquad \qquad + 16x^4 \qquad \qquad + 12x^2 \\
 \hline
 2x^5 + 8x^4 + 8x^3 + 4x^2 + 6x + 3 \\
 - 2x^5 \qquad \qquad + 8x^3 \qquad \qquad + 6x \\
 \hline
 8x^4 + 4x^2 + 3 \\
 - 8x^4 + 4x^2 + 3 \\
 \hline
 X
 \end{array}$$

$$\therefore P(s) = (s^4 + 4s^2 + 3)(4s + 2s + 1)$$

$$= P_1(s) \cdot P_2(s)$$

$$\rightarrow P_1(s) = s^4 + 4s^2 + 3$$

Condition
 1st all coeff. term should be +ve
 2nd either all odd/even term should be missing
 3rd.

$$P_1(s) = s^4 + 4s^2 + 3$$

$$O_1(s) = \frac{dP_1(s)}{ds}$$

$$\rightarrow 4s^3 + 8s$$

$$\begin{array}{r} O_1(s) = 4s^3 + 8s \\ \hline 0,1s) \end{array} \quad \left| \begin{array}{l} s^4 + 4s^2 + 3 \\ 8s^3 + 2s^2 \end{array} \right| \begin{array}{l} 0 \\ 8/4 \end{array}$$

$$\begin{array}{r} 2s^3 + 3 \\ \hline 2s^3 + 6s \end{array} \quad \left| \begin{array}{l} 4s^3 + 8s \\ 4s^3 + 6s \end{array} \right| \begin{array}{l} 2s \\ \hline 0 \end{array}$$

$$\begin{array}{r} 2s^2 + 3 \\ \hline 2s^2 \end{array} \quad \left| \begin{array}{l} 8 \\ 2s \end{array} \right| \begin{array}{l} 8 \\ 2s \end{array}$$

$$\begin{array}{r} 3 \\ 2s \\ \hline 2s \\ 0 \end{array}$$

X
 ∵ turbidity condition

$$\rightarrow P_2(s) = 4s^2 + 2s + 1$$

$$O_2(s) = 4s^2 + 1$$

$$O_2(s) = 2s$$

$$\begin{array}{r} O_2(s) = 2s^2 | 4s^2 + 1 \\ \hline 0,2s^2) \end{array} \quad \left| \begin{array}{l} 2s^2 | 4s^2 + 1 \\ 4s^2 \end{array} \right| \begin{array}{l} 2s \\ 0 \end{array}$$

X

∴ Herbitz

Premium

Z - Parameters in terms of Y - Parameter

$$\text{We know } Z = \frac{1}{Y}$$

$$\Rightarrow [Z] = [Y]^{-1}$$

$$\Rightarrow \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}^{-1}$$

$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Y_{22} & -Y_{12} \\ -Y_{21} & Y_{11} \end{bmatrix} \cdot \frac{1}{\Delta Y} \rightarrow \text{determinant} \\ = Y_{11} \cdot Y_{22} - Y_{12} \cdot Y_{21}$$

$$\therefore Z_{11} = \frac{Y_{22}}{\Delta Y} \quad Z_{12} = -\frac{Y_{12}}{\Delta Y}$$

$$Z_{21} = -\frac{Y_{21}}{\Delta Y} \quad Z_{22} = \frac{Y_{11}}{\Delta Y}$$

Z - Parameter in terms of T - Parameter

$$V_1 = Z_{11} I_1 + Z_{12} \cdot I_2 \quad (1) \quad V_1 = A V_2 + B (-I_2) \quad (3)$$

$$V_2 = Z_{21} I_1 + Z_{22} \cdot I_2 \quad (2) \quad V_1 = C V_2 + D (-I_2) \quad (4)$$

Using eq (4)

$$C V_2 = I_1 + D I_2$$

$$V_2 = \frac{I_1}{C} + \frac{D}{C} I_2 \quad (5)$$

Comparing (2) & (5)

$$\Rightarrow \boxed{Z_{21} = \frac{I_1}{C}} \quad \boxed{Z_{22} = \frac{D}{C}}$$

• PRF, filter design, numerical based on filter
 passive filter only Dt. _____ Pg. _____ B+

Using (5) & (3)

$$V_1 = \frac{A}{C} I_1 + \frac{AD}{C} I_2 + B(-I_2)$$

$$V_1 = \frac{A}{C} I_1 + I_2 \left(\frac{AD - BC}{D} \right) \quad (6)$$

Comparing (1) and (6)

$$\Rightarrow \boxed{Z_{11} = \frac{A}{C}} \quad \boxed{Z_{12} = \frac{AD - BC}{C}}$$

h parameter in terms of T parameter

$$V_1 = h_{11} I_1 + h_{12} V_2 \quad (1) \quad V_1 = A V_2 + B(-I_2) \quad (3)$$

$$I_2 = h_{21} I_1 + h_{22} V_2 \quad (4) \quad I_2 = C V_2 + D(-I_2) \quad (4)$$

$$D I_2 = C V_2 - I_1$$

$$I_2 = -\frac{I_1}{D} + \frac{C}{D} V_2 \quad (5)$$

$$\boxed{h_{21} = -\frac{1}{D}} \quad \boxed{h_{22} = \frac{C}{D}}$$

$$V_1 = A V_2 - B \left(-\frac{I_1}{D} + \frac{C}{D} V_2 \right)$$

$$= \left(\frac{AD - BC}{D} \right) V_2 + \frac{B}{D} I_1$$

$$\boxed{h_{11} = \frac{B}{D}}$$

$$\boxed{h_{12} = \frac{AD - BC}{D}}$$

Properties of Positive Real Function (PRF)

F

$$F(s) = \frac{P(s)}{Q(s)}$$

$$= a_m s^m + a_{m-1} s^{m-1} + \dots + a_1 s + a_0$$

$$b_m \cdot s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0$$

The necessary & sufficient condⁿ for a rational network $F(s)$ to be real & positive are stated as

- (1) $F(s)$ must not have any pole in the right side of the s -plane, i.e. both $P(s)$ and $Q(s)$ of $F(s)$ are Hurwitz

This condition can be checked by continued fraction expansion of the odd to even part and even to odd part of $P(s)$ and $Q(s)$

- (2) Real part of $F(s)$ must be greater or equal to 0 for all w

$$\operatorname{Re}[F(-jw)] \geq 0 \quad \text{for all } w$$

$$\Leftrightarrow M_1(jw) = M_1(jw) M_2(jw) - N_1(jw) \cdot N_2(jw)$$

where M_1 & M_2 are the even part of $P(s)$ & $Q(s)$

N_1 & N_2 are the odd parts of $P(s)$ & $Q(s)$

- (3) This condⁿ is tested for the poles of $F(s)$ lying on the jw axis. This is done by using the partial fraction expansion of $F(s)$ to check whether the residues of the poles on the jw axis are real

$$\text{Q: } F(s) = \frac{s^2 + 6s + 5}{s^2 + 9s + 14}$$

$$F(s) = \frac{f(s)}{Q_s}$$

$$\therefore P(s) = s^2 + 6s + 5 \quad | \quad Q(s) = s^2 + 9s + 14$$

$$P_p(s) = s^2 + 5$$

$$Q_p(s) = 6s$$

$$P_p(s) = s^2 + 14$$

$$Q_p(s) = 9s$$

$$6s \mid s^2 + 5 \mid s/6$$

$$s^2 +$$

$$s \mid 6s \mid 6/5$$

$$6s$$

$$9s \mid s^2 + 14 \mid s/9$$

$$s^2$$

$$14 \mid 9s \mid 98/14$$

$$9s$$

$$X$$

\therefore Both $P(s) \in Q(s)$ are Hermitz polynomial.
 $\therefore F(s)$ is Hermitz polynomial

$$\operatorname{Re}[F(j\omega)] \geq 0$$

$$A(\omega) = (s^2 + 5)(s^2 + 14) - (6j)A_{ij} \geq 0$$

$$s^4 + 19s^2 + 70 - 34s^2 \geq 0$$

$$s^4 - 35s^2 + 70 \geq 0$$

replace 's' by 'jω'

$$\omega^4 + 35\omega^2 + 70 \geq 0$$

$$A(\omega^2) > 0 \Rightarrow F(s) \text{ is PRF}$$

The 'real' is positive degree

$$\Phi(s) = s^2 + 3s + \frac{1}{4}$$

$$s^2 + s + 4$$

$$P(s) = s^2 + \frac{3s}{4} + \frac{3}{4}$$

$$\Phi(s) = s^2 + s + 4$$

$$\frac{3s}{4} \mid \begin{array}{r|l} s^2 + 3 \\ \hline 4 & s^2 \end{array} \quad \frac{s^2}{3}$$

$$s \mid \begin{array}{r|l} s^2 + 4 \\ \hline s^2 & s \end{array}$$

$$\begin{array}{r|l} s^2 \\ \hline 3 & \mid \begin{array}{r|l} 3s \\ \hline 1 & \end{array} \end{array} \quad \text{R1}$$

$$\begin{array}{r|l} s^2 \\ \hline 4 & \mid \begin{array}{r|l} s & s/4 \\ \hline & x \end{array} \end{array}$$

$$\Delta(w^2) = \left(s^2 + \frac{3}{4}\right)(s^2 + 4) - \frac{3s}{4} \cdot s \geq 0$$

$$4 = \frac{1}{4}$$

$$s^4 + s^2 \frac{19}{4} + \frac{3}{4} - \frac{3s^2}{4} \geq 0$$

$$s^4 + 16s^2 + 3 \geq 0$$

$$w^4 - \frac{14w^2}{4} + 3 \geq 0$$

$$w^4 - 4w^2 + 3 \geq 0$$

Sturm Test

$$w^2 = x$$

$$P_0(x) = x^2 - 4x + 3$$

$$P'_0(x) = 2x - 4$$

$$\frac{P_0(x)}{P'_0(x)}$$

$$\gamma_2 = 1$$

$$2x - 4 \quad | \quad 2^2 - 4x + 3$$

$$x^2 - 2x$$

$$-2x + 3$$

$$-2x + 4$$

$$-1$$

$$= -P_1(x)$$

	Sign of $P_0(x)$	Sign of $P_0'(x)$	Sign of $P_1(x)$	Total Sign of sign of change
$x=0$	+	-	+	0
$x=\infty$	+	+	+	0

$$\text{No. of total sign change} = 2 - 0 = 2$$

\therefore The given function is not physically reliable

Q) $A(\omega^2) = 3\omega^4 - 12\omega^2 + 4$

$$P_0(\omega) = 3\omega^4 - 12\omega^2 + 4$$

$$P_0'(\omega) = 12\omega^3 - 24\omega$$

$$\omega^4 - 4/\omega^2$$

$$12\omega^3 - 24\omega \quad | \quad 3\omega^4 - 12\omega^2 + 4$$

$$\overline{\omega^4 - 6\omega^2}$$

$$-6\omega^2 + 4$$

$$-6\omega^2 + 12$$

$$-8 = -P_1(x)$$

Dt. _____

Pg. _____

B+

	sign of $P_{(s)}$	sign of $P'(s)$	sign of $P''(s)$	Total no. change
$n = 0$	+	+	-	1
$n = \infty$	+	+	-	1

Q) $F(s) = \frac{2s^2 + 2s + 1}{s^3 + 2s^2 + s + 2}$

$$P(s) = 2s^2 + 2s + 1$$

$$\begin{array}{r|rr|l} 2s & | & 2s^2 + 1 & 1 \\ & & 2s^2 & \\ \hline & 1 & 2s & 1s \\ & & & X \end{array}$$

$$Q(s) = s^3 + 2s^2 + s + 2$$

$$\begin{array}{r|rr|l} s^3 + s & | & 2s^2 + 2 & 2 \\ & & 2s^2 & \\ \hline & & & X \end{array}$$

$$1 + \frac{2}{s}$$

$$\begin{array}{r|rr|l} s^3 + s & | & s^3 + 2s^2 + s + 2 & 2 \\ & & s^3 & + s \\ \hline & & 2s^2 & + 2 \\ & & 2s^2 & + 2 \\ & & & X \end{array}$$

$$\therefore Q(s) = (s^3 + s) \left(1 + \frac{2}{s} \right)$$

$$Q_1(s) = s^3 + s$$

$$Q_2(s) = 1 + \frac{2}{s}$$

$$Q_{01}(s) = s^3 + s$$

$$Q_{02}(s) = \frac{2}{s}$$

$$Q_{e1}(s) = 3s^2 + 1$$

$$Q_{e2}(s) = 1$$

$$\begin{array}{r} s^3 + 8 \\ \hline s^2 + 3 \\ -2 \\ \hline s^3 + 8 \end{array}$$

Check whether the given polynomial

$$F_1(s) = s^5 + 2s^3 + s$$

$$F_0(s) = s^5 + 2s^3 + s$$

$$F_r(s) = 3s^4 + 6s^2 + 1$$

stop/11

Filter Designing

1. Foster I } Partial fraction

2. Foster II

3. Cauer I } continued
4. Cauer II } fraction expansion

Coues

$$Z(s) = \frac{s(s+2)(s+5)}{(s+1)(s+4)}$$

$$\Rightarrow Z(s) = \frac{s^2 + 7s + 10}{s^2 + 5s + 4}$$

	$Z(s)$	$Y(s)$
-m-	R	$\frac{1}{R}$
-mm-	sL	$\frac{1}{sL}$
-II-	$\frac{1}{sC}$	∞

$$s^2 + 5s + 4 \mid s^2 + 7s + 10 \mid 1$$

$$s^2 + 5s + 4$$

$$2s + 6$$

Dt.

P_B.

B+

$$\Rightarrow Z(s) = 1 + \frac{8s+6}{s^2+7s+10},$$

$Z^*(s)$

$$Z^*(s) = \frac{8s+6}{(s+1)(s+4)}$$

$$= \frac{A}{s+1} + \frac{B}{s+4}$$

$$A = \frac{4}{3} \quad B = \frac{2}{3}$$

$$Z^*(s) = \frac{4}{3} \frac{1}{(s+1)} + \frac{2}{3} \frac{1}{(s+4)}$$

$$\therefore Z(s) = 1 + \frac{4}{s} + \frac{2}{3(s+1)} + \frac{2}{3(s+4)}$$

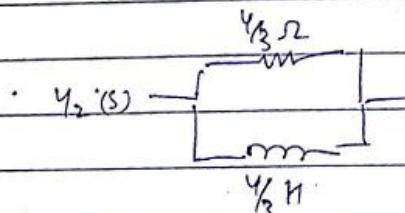
$$Z(s) = s + \frac{4s/3}{(s+1)} + \frac{2s/3}{(s+4)}$$

$$= Z_1(s) + Z_2(s) + Z_3(s)$$

- $Z_1(s) = 1/s \rightarrow \frac{1H}{m}$

- $Z_2(s) = 4s/3 / (s+1)$

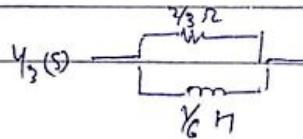
$$Z_2(s) = \frac{s+1}{4s/3} = \frac{1}{4s/3} + \frac{1}{4s/3}$$



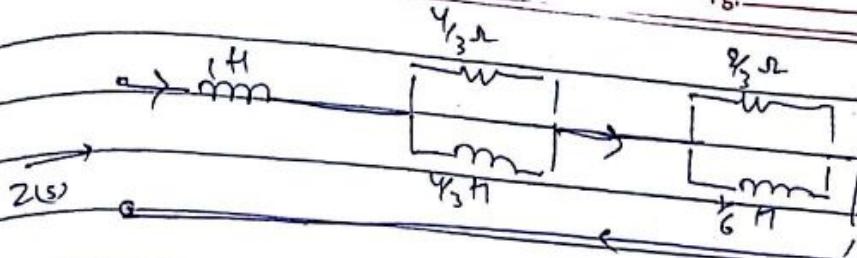
- $Z_3(s) = 2s/3$

$$s+4$$

$$Z_3(s) = \frac{s+4}{2s/3} = \frac{1}{2s/3} + \frac{4}{8/6}$$



Premium



Foster Form II

* For Foster II form we always solve our functⁿ in admittance form using partial fraction

$$Z(s) = \frac{R(s+2)(s+5)}{(s+1)(s+4)}$$

$$\therefore Y(s) = \frac{(s+1)(s+4)}{s(s+2)(s+5)} = \frac{(-1)(-2)}{(-2)(3)}$$

$$= \frac{A}{s} + \frac{B}{s+2} + \frac{C}{s+5}$$

$$A = \frac{4}{10} = \frac{2}{5}$$

$$B = \frac{1}{3}$$

$$C = \frac{(-4)(-1)}{(-5)(-3)} = \frac{4}{15}$$

$$= \frac{2}{5s} + \frac{1}{3(s+2)} + \frac{4}{15(s+5)}$$

↓

$$\begin{array}{c} 1 \\ 3 \\ \hline 5/14 \end{array}$$

$$Y_{(1)}(s) = \frac{1}{3(s+2)}$$

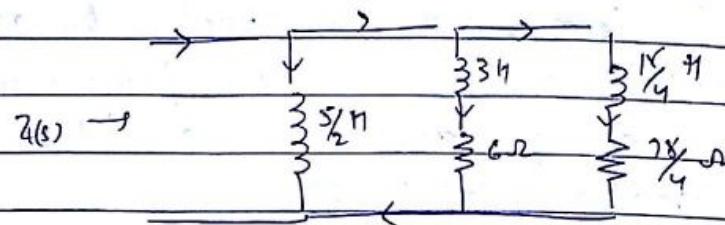
$$\rightarrow Z_2(s) = 3s + 6$$

$\begin{array}{c} 3s \\ -m \\ \hline m \end{array}$

$$Y_{(3)}(s) = \frac{4}{15(s+5)}$$

$$Z_3(s) = \frac{15s}{4} + \frac{75}{4}$$

$\begin{array}{c} 15s \\ -m \\ \hline m \end{array}$ $\begin{array}{c} 75 \\ -m \\ \hline m \end{array}$



Foster's Cossic Form I

* The highest power of s should be at numerator side

$$Z(s) = \frac{s(s+2)(s+5)}{(s+1)(s+4)}$$

$$= \frac{s^3 + 7s^2 + 10s}{s^2 + 5s + 4}$$

$$\begin{array}{r}
 s^2 + 5s + 4 \quad | \quad s^3 + 7s^2 + 10s \quad | \quad s \quad Z_1(s) \\
 -s^3 - 5s^2 - 4s \\
 \hline
 2s^2 + 6s \quad | \quad s^2 + 5s + 4 \quad | \quad s \quad Z_2(s) \\
 -2s^2 - 10s \\
 \hline
 2s + 4 \quad | \quad 2s^2 + 6s \quad | \quad s \quad Z_3(s) \\
 -2s^2 - 4s \\
 \hline
 2s \quad | \quad 2s + 4 \quad | \quad 4 \quad Z_4(s) \\
 -2s \\
 \hline
 4 \quad | \quad 2s \quad | \quad 2s \\
 \hline
 X
 \end{array}$$

$$\begin{array}{ccccccc} & 1H & & 1H & & & \\ \xrightarrow{2m} & m & \rightarrow & m & \rightarrow & \frac{1}{2}m & \\ 2(0) \rightarrow & \frac{2}{3}22 & & \frac{2}{3}12 & & & \end{array}$$

* In case II form realize the functⁿ by rearranging the numerator and denominator polynomial in ascending order of degree & and take continued fraction expansion

$$\begin{aligned} 2(0) = & \frac{8(8+2)(8+5)}{(8+1)(8+4)} \\ & \rightarrow \frac{108 + 78^2 + 8^3}{48 + 58 + 8^2} \end{aligned}$$

$$\begin{array}{r} 4 + 5x + x^2 \quad | \quad 108 + 7x^2 + x^3 \quad | \quad 10x^4 = \frac{5}{2}x \\ - \qquad \qquad \qquad \qquad | \qquad \qquad \qquad \qquad | \\ \hline -11x^2 - 3x^3 \quad | \quad 4 + 5x + x^2 \quad | \quad -\frac{2}{11x^2} \end{array}$$

Since we get -ve quotient term in continued fraction expansion. To avoid this we take reciprocal of our given functⁿ

$$\therefore Y(s) = \frac{4 + 5s + s^2}{10s + 7s^2 + s^3}$$

$$10s + 7s^2 + s^3 \mid 4 + 5s + s^2 \quad | \quad Y(s) = \frac{2}{5s} \cdot Y_1(s)$$

$$= 4 + \frac{14s}{5} + \frac{2s^2}{5}$$

$$11s + 3s^2 \quad | \quad 10s + 7s^2 + s^3 \quad | \quad \begin{matrix} 5 \times 10 \\ 11 \end{matrix} \\ 10s + \frac{30s^2}{11} + \frac{s^3}{11}$$

$$11 \quad | \quad \frac{47}{11} s^2 + s^3 \quad | \quad \frac{11s}{5} + \frac{3s^2}{5} \quad | \quad Y_2$$

$$Y_1(s) = \frac{2}{5s}$$

$$Y_4(s) = \frac{220}{44}$$

$$Y_2(s) = \frac{50}{11}$$

$$Y_3(s) = \frac{4}{47s}$$

$$Y_5(s) = \frac{121}{235s}$$

