

Time: 40 minutes.

Quiz -1

M.M.: 20

Instructions: For the multiple choice type questions, answer with the **correct option only on the provided space in question paper**. **Overwritten/multiple answers** for a question will not be checked. There is no negative marking.

Name: _____ Enr. No.: _____

Part-1

5×1=5

- For a MOSFET in the pinch off region, as the drain voltage is increased, the drain current
 (A) becomes zero (B) abruptly decreases (C) abruptly increases (D) remains constant
- Given the operating point values $I_{DQ} = 1.8 \text{ mA}$ and $V_{DSQ} = 3.1 \text{ V}$ for common-source amplifier circuit operating in edge of saturation region, value of the small signal parameter g_m will be ($V_T = 1.6$, $\lambda = 0$)
 (A) $1.16 \times 10^{-3} \text{ S}$ (B) 0.005 S (C) 0.625×10^{-3} (D) cannot be determined

$$g_m = \frac{2 I_D}{V_{GS} - V_{TH}} = \frac{3.6 \text{ mA}}{3.1 \text{ V}} = 1.16 \times 10^{-3} \text{ S}$$

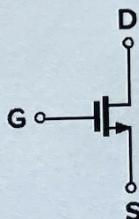


Fig. 1

- For the MOS transistor in Fig. 1, if $V_{GS} > V_T$ and $V_{DS} < V_{GS} - V_T$, the channel voltage _____ along the length of the transistor, and the charge density _____ as we go from the source to the drain.
 (A) remains constant, falls (B) varies, remains unchanged
 (C) remains constant, increases (D) varies, falls

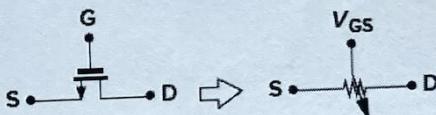
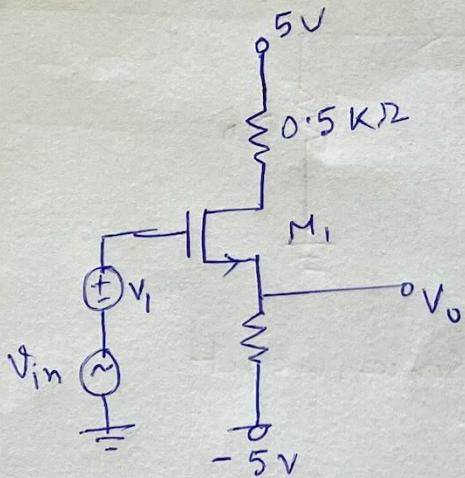


Fig. 2

- $R_{DS(\text{ON})}$ of the MOSFET in Fig. 2 _____ with increasing V_{GS} .
 (A) decreases (B) increases
 (C) remains constant (D) first increases then decreases
- In the CS-stage with source degeneration, if the source resistance R_s is bypassed by a capacitor C_s , then ac voltage gain of the amplifier
 (A) remains the same (B) increases (C) decreases (D) gain is not affected

Answer:	1	2	3	4	5

Q6.



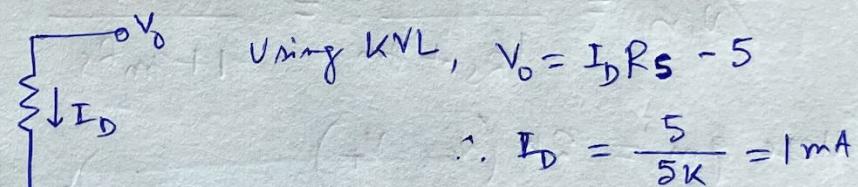
(a) D.C. Analysis: For the gate to source loop, using KVL

$$V_1 - V_{GS} - V_o = 0$$

$$\text{for } V_o = 0, V_1 = V_{GS}$$

Enforcing Saturation condition,

$$\begin{aligned} I_D &= k(V_{GS} - V_T)^2 \\ &= 0.4(V_{GS} - 1)^2 \times 10^{-3} \end{aligned} \quad \text{--- (1)}$$



$$\text{Using KVL, } V_o = I_D R_S - 5$$

$$\therefore I_D = \frac{5}{5k} = 1 \text{ mA}$$

Putting I_D in (1)

$$1 \text{ mA} = 0.4 \text{ mA} (V_{GS} - 1)^2$$

$$\text{or } (V_{GS} - 1)^2 = \frac{1}{0.4} = 2.5$$

$$\text{or } V_{GS} - 1 = \pm \sqrt{2.5} = \pm 1.58$$

Check: Taking $V_{GS} = 2.58 \text{ V}$, $V_{GS} > V_{th}$

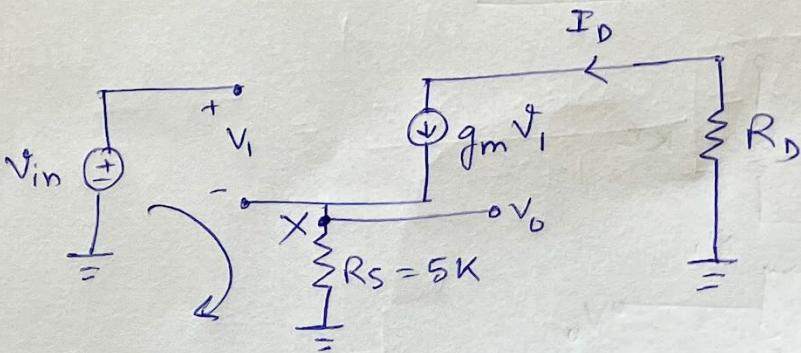
on the outer loop using KVL

$$V_{DD} - I_D R_D - V_{DS} = 0 \quad \text{as } V_o = 0$$

$$\text{or } V_{DS} = 4.5 \text{ V} > V_{GS} - V_{th}$$

$$\text{So } V_1 = 2.58 \text{ V}$$

6. (b)



6. (c)

AC Analysis: Using KVL in loop Gate to Source, we get

$$v_{in} - v_1 = v_o$$

Using KCL at node X

$$\frac{v_o}{R_S} = g_m v_1$$

$$\text{or } \frac{v_o}{R_S} = g_m (v_{in} - v_o)$$

$$\text{or } v_o \left(\frac{1}{R_S} + g_m \right) = v_{in} (g_m)$$

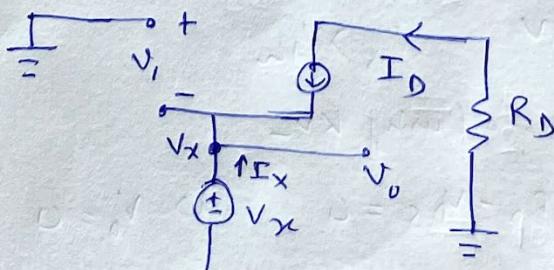
$$\text{or } \frac{v_o}{v_{in}} = \frac{g_m}{1/R_S + g_m} = \frac{g_m R_S}{1 + g_m R_S}$$

$$\begin{aligned} \text{Here } g_m &= 2K(v_{GS} - v_T) \\ &= 2 \times 0.4 \times 10^{-3} (2.58 - 1) \\ &= 1.264 \times 10^{-3} \end{aligned}$$

$$\therefore \frac{v_o}{v_{in}} = A_v = \frac{1.264 \times 10^{-3} \times 5 \times 10^3}{1 + 1.264 \times 10^{-3} \times 5 \times 10^3}$$

$$= 0.863$$

6. (d)



Using KCL, at node X

$$I_x = -g_m v_1$$

$$\frac{v_x}{I_x} = R_o = \frac{1}{g_m} = \frac{10^3}{1.264}$$

$$= 791.13 \Omega$$

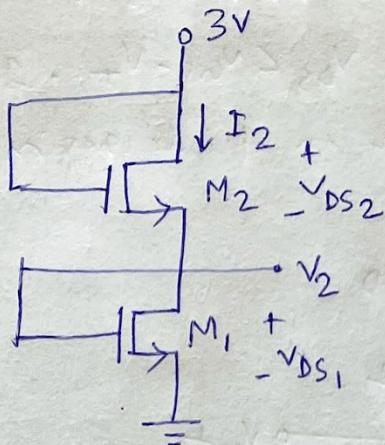
$$\text{on } I_x = g_m v_x$$

(3)

$$\text{Total } R_{\text{out}} = R_0 \| R_S$$

$$= \frac{791.13 \times 5000}{5791.13} = 683.0552$$

Q. (7) (a)



Using KVL on the outer loop

$$3 - V_{DS2} - V_{DS1} = 0 \quad \text{--- (1)}$$

As both transistors are characterized by same device parameters

$$V_{DS2} = V_{DS1}$$

$$\text{From (1), } V_2 = V_{DS1} = \frac{3}{2} \text{ Volt} \\ = 1.5 \text{ Volt}$$

Check for saturation:

$$\text{Here } V_{DS} - V_T = V_{DS} - V_T \quad [\text{As } V_{DS} = V_{DS}]$$

$$\therefore V_{DS} > V_{DS} - V_T$$

∴ The transistors are in saturation.

$$\begin{aligned} \text{Current } I_2 &= \frac{1}{2} \mu n C_{ox} \frac{W}{L} (V_{DS} - V_T)^2 \\ &= \frac{1}{2} 20 \times 10^{-6} (3) (1.5 - 1)^2 \\ &= 10 \times 10^{-6} \times 3 \times 0.25 \\ &= 7.5 \mu A \end{aligned}$$

7(b)

(4)

No, there is no channel-length modulation in triode region.

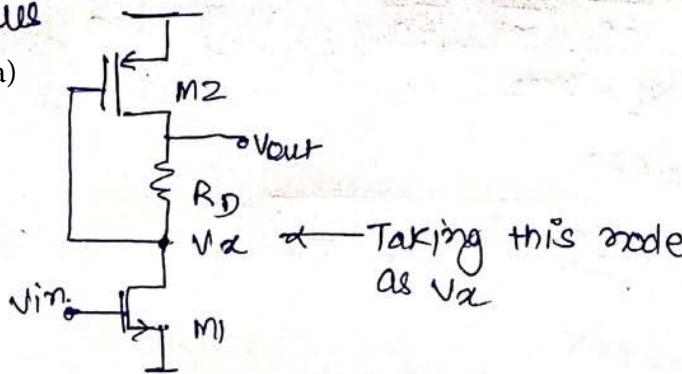
For channel length modulation, pinch off should occur and

$$V_{DS} > V_{GS} - V_T \text{ should be satisfied.}$$

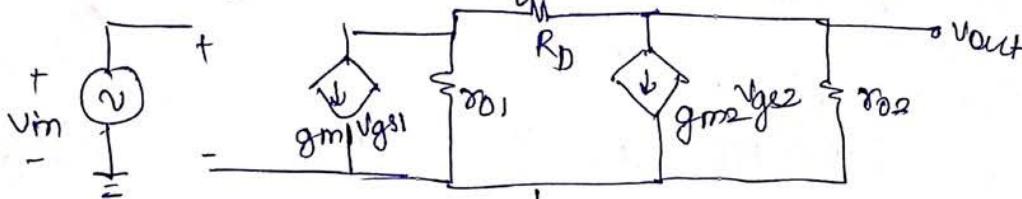
But in triode region $V_{DS} < V_{GS} - V_T$. Therefore channel length modulation should not occur in triode region.

Ques

8(a)



Small signal circuit of above circuit as shown below:



8(b)

Writing KCL at V_x node,

$$g_{m1} V_{g_{m1}} + \frac{V_x}{r_{D1}} + \frac{V_x - V_{out}}{R_D} = 0$$

$V_{g_{m1}}$ (Note: $V_{g_{m2}} = V_x$)
 $V_{g_{m1}} = V_{in}$

$$\frac{V_{out}}{R_D} - g_{m1} V_{in} = V_x \left(\frac{1}{R_D} + \frac{1}{r_{D1}} \right) \quad \textcircled{1}$$

Writing KCL at output node,

$$g_{m2} V_{g_{m2}} + \frac{V_{out}}{r_{D2}} + \frac{V_{out} - V_x}{R_D} = 0$$

$$g_{m2} V_x + \frac{V_{out}}{r_{D2}} + \frac{V_{out}}{R_D} - \frac{V_x}{R_D} = 0$$

$$\frac{V_{out}}{r_{D2}} - V_{out} \left(\frac{1}{r_{D2}} + \frac{1}{R_D} \right) = V_x \left(\frac{1}{R_D} - g_{m2} \right)$$

$$V_x = V_{out} \frac{\left(\frac{1}{r_{D2}} + \frac{1}{R_D} \right)}{\left(\frac{1}{R_D} - g_{m2} \right)} \quad \textcircled{2}$$

Putting eqⁿ ② into eqⁿ ①

$$\frac{V_{out}}{R_D} - g_{m1} V_{in} = \frac{V_{out} \left(\frac{1}{r_{D2}} + \frac{1}{R_D} \right)}{\left(\frac{1}{R_D} - g_{m2} \right)} \times \left(\frac{1}{r_{D1}} + \frac{1}{R_D} \right)$$

$$\frac{V_{out}}{R_D} - \frac{V_{out} \left(\frac{1}{r_{D2}} + \frac{1}{R_D} \right) \left(\frac{1}{r_{D1}} + \frac{1}{R_D} \right)}{\left(\frac{1}{R_D} - g_{m2} \right)} = g_{m1} V_{in}$$

$$V_{out} \left[\frac{\left(\frac{1}{R_D} - g_m^2 \right)}{R_P} - R_D \left(\frac{1}{\infty \omega_2} + \frac{1}{R_P} \right) \left(\frac{1}{\omega_1} + \frac{1}{R_D} \right) \right] = g_m V_{in}$$

$$\frac{V_{out}}{V_{in}} = \frac{g_m (1 - g_m R_D)}{\frac{1}{R_P} - g_m^2 - \left[\left(\frac{R_D}{\infty \omega_2} + 1 \right) \left(\frac{1}{\omega_1} + \frac{1}{R_D} \right) \right]}$$

$$\frac{V_{out}}{V_{in}} = \frac{g_m (1 - g_m R_D)}{\frac{1}{R_P} - g_m^2 - \frac{R_D}{\infty \omega_2 \omega_1} - \frac{1}{\omega_2} - \frac{1}{\omega_1} - \frac{1}{R_D}}$$

$$\frac{V_{out}}{V_{in}} = \frac{g_m (1 - g_m R_D)}{- \left[g_m^2 + \frac{1}{\omega_1} + \frac{1}{\omega_2} \left(1 + \frac{R_D}{\omega_1} \right) \right]}$$

$$\boxed{\frac{V_{out}}{V_{in}} = \frac{g_m (g_m R_D - 1)}{\left[g_m^2 + \frac{1}{\omega_1} + \frac{1}{\omega_2} \left(1 + \frac{R_D}{\omega_1} \right) \right]}}$$