

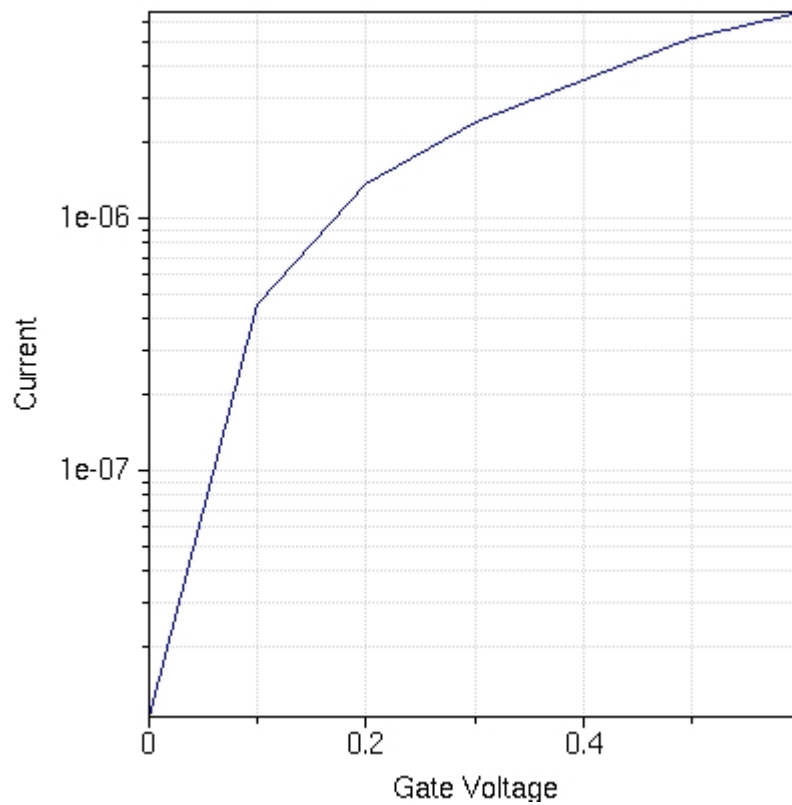
EEE F477- Course Assignment

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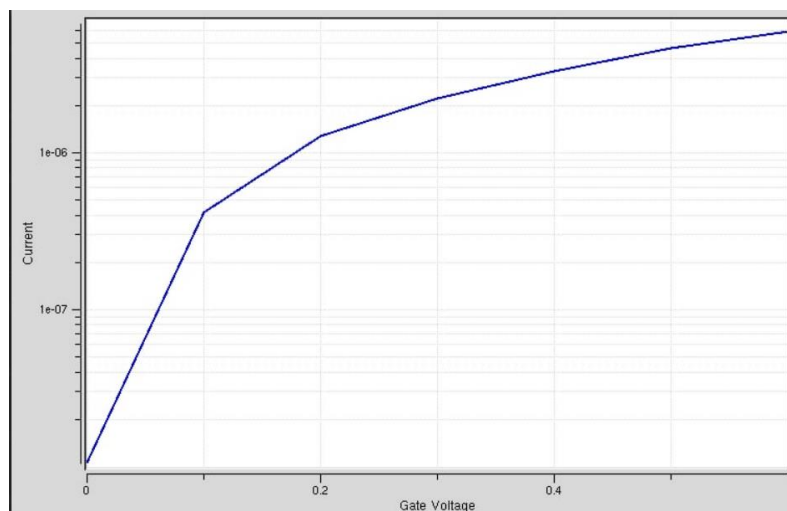
2019A3PS0415H

# Assignment 1

- (i) For effective oxide thickness 1.95 nm:  
 $I_{on} = 6.65668e-06$  A,  $I_{off} = 1.06901e-08$  A



For effective oxide thickness 0.975 nm:  
 $I_{on} = 5.89245e-06$  A,  $I_{off} = 1.0525e-08$  A



The geometric screening for the 1.95nm device is higher because of a larger oxide thickness, hence the effect of DIBL is more (electric field lines from drain will penetrate further into the channel). Because of a larger DIBL effect, the on-state current and the off-state current are higher. A large DIBL effect implies more lowering of the barrier because of drain voltage which in turn implies a larger current.

(ii)

Calculating DIBL

For device with effective oxide thickness 0.975nm:

Assuming current to be 1.28463e-06 A

V<sub>gs</sub> at 0.3V : 0.2V

V<sub>gs</sub> at 0.6V : 0.199943V

DIBL =  $(0.2 - 0.199943)/(0.3) = 0.19 \text{ mV/V}$

For device with effective oxide thickness 1.95nm:

Assuming current to be 1.36048e-06 A

V<sub>gs</sub> at 0.3V : 0.2V

V<sub>gs</sub> at 0.6V : 0.1999V

DIBL =  $(0.2 - 0.1999)/(0.3) = 0.33 \text{ mV/V}$

Therefore, DIBL effect in 1.95nm device is more, which is consistent with my analysis. The geometric screening for the 1.95nm device is higher because of a larger oxide thickness, hence the effect of DIBL is more.

(iii)

The worst DIBL effected device is the one with effective oxide thickness 1.95nm as explained earlier. A device engineering technique to reduce the effect of DIBL could be to increase the oxide Capacitance. This involves decreasing the oxide thickness and using a high-k dielectric as oxide. Another possible technique could be to

carefully control the diameter of the nanowire to reduce the geometric screening length of the Nanowire Transistor.

## Assignment 2

1.

(i) For longitudinal mass = 0.1, transverse mass = 0.1

$$I_{on} = 6.39055e-06 \text{ A}, I_{off} = 9.20773e-12 \text{ A}$$

For longitudinal mass = 0.1, transverse mass = 1

$$I_{on} = 9.65369e-06 \text{ A}, I_{off} = 9.99338e-08 \text{ A}$$

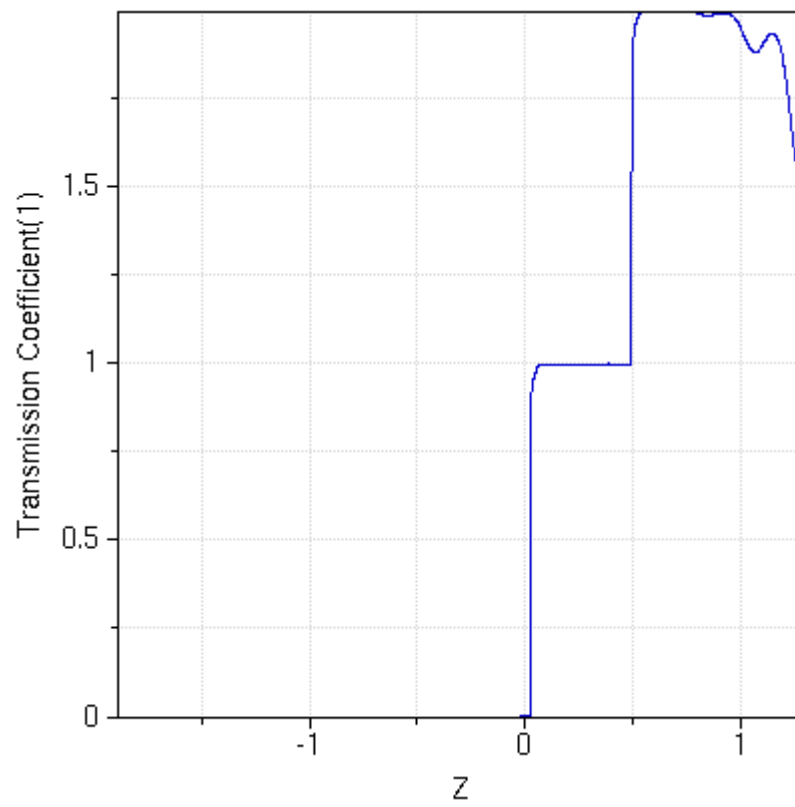
For longitudinal mass = 1, transverse mass = 0.1

$$I_{on} = 8.82744e-06 \text{ A}, I_{off} = 1.09915e-09 \text{ A}$$

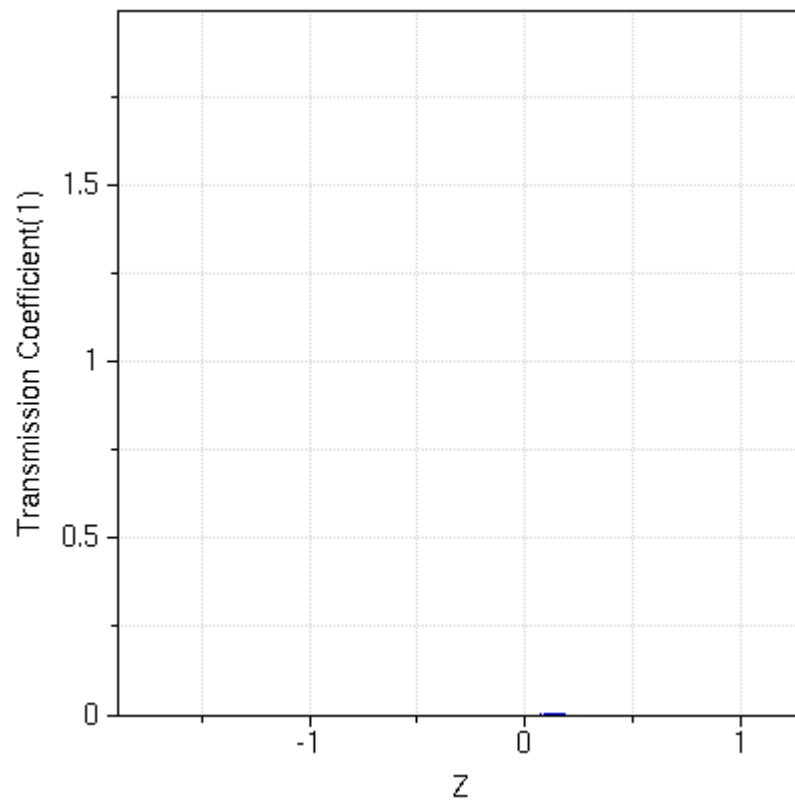
First, it is important to note that, a lower effective mass in a direction implies a higher mobility of carriers in that direction and hence a higher conduction in that direction.

As we can see, on-current is maximum in case (ii) (longitudinal mass = 0.1, transverse mass = 1). This can be reasoned as follows: The channel is in the longitudinal direction, hence a lower effective mass in this direction would result in a higher drain current. A higher effective mass in the transverse direction would result in a lower current in that direction, which means more electrons are available for the longitudinal current (which is the drain current). Therefore, the high currents in case(ii) can be justified by the high transverse mass and low longitudinal mass.

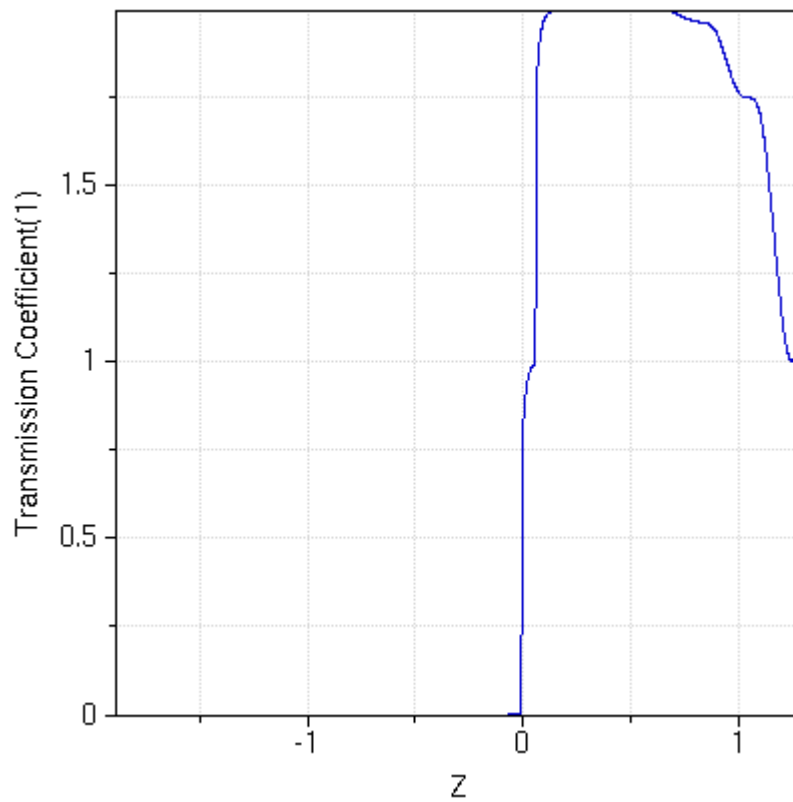
(ii) For longitudinal mass = 0.1, transverse mass = 0.1



For longitudinal mass = 0.1, transverse mass = 1



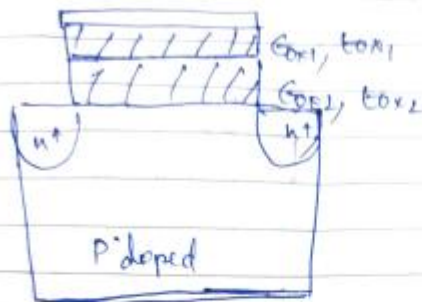
For longitudinal mass = 1, transverse mass = 0.1



Because of the high transverse mass, we can see a low transmission coefficient in the Z direction in case (ii). But there will be a very high transmission coefficient in the longitudinal direction (because of the low longitudinal mass). We can see a high transmission coefficient in the Z direction in case(i) and case(iii) because of a lower effective mass in transverse direction.

2.

## Q2. Level 0 MOSFET model



### 1D Capacitance model

$$\begin{aligned} \frac{1}{C_{ox1}} &= \frac{C_{ox1}}{C_{ox1}} && \text{in inversion} \\ \frac{1}{C_{ox2}} &= \frac{C_{ox2}}{C_{ox2}} && C_G \approx \frac{C_{ox1} \cdot C_{ox2}}{C_{ox1} + C_{ox2}} \\ \frac{1}{C_{dep}} &= \frac{C_{dep}}{C_{dep}} && \end{aligned}$$

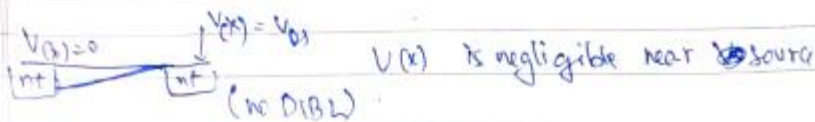
Inversion charge  $Q_n(x)$  : as  $C_{dep} \gg C_{ox1}, C_{ox2}$

$$Q_n(x) = 0 \quad V_{GS} \leq V_T$$

$$Q_n(x) = -C_G (V_{GS} - V_T - V(x)) \quad \text{for } V_{GS} > V_T$$

$$I_D(x) = -w Q_n(x) \langle V_n(x) \rangle$$

$$I_D(0) = -w Q_n(0) \langle V_n(0) \rangle$$



it is safe to assume a constant electric field  
in channel  $= \frac{V_{DS}}{L}$

$$\text{below saturation } \langle v_n(x) \rangle = \mu_n E \\ = \mu_n \frac{V_{DS}}{L}$$

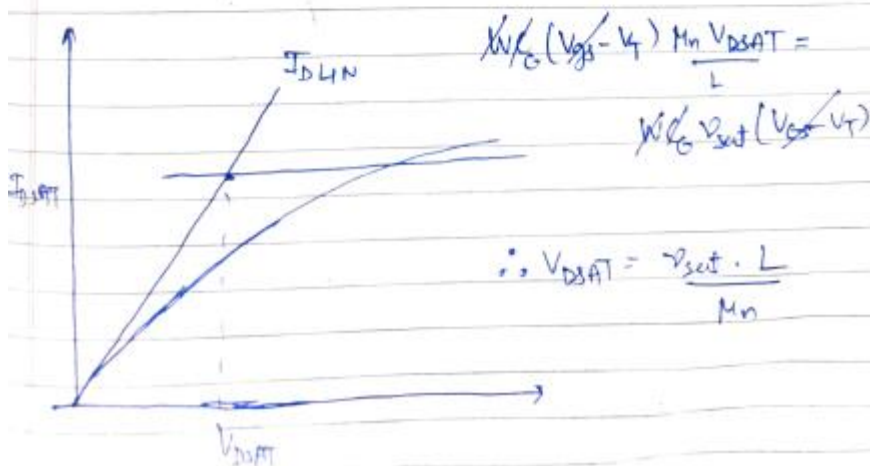
assuming 0 recombination/generation in channel,  $I_D(0) = I_D(L)$

$$\therefore I_D(x) = I_D(0) = I_{D,LIN} \Rightarrow Q_n(0) = -C_G (V_{GS} - V_T)$$

$$I_{D,LIN} = W C_G (V_{GS} - V_T) \frac{\mu_n V_{DS}}{L} \text{ for } V_{DS} \leq V_{DSAT}$$

above saturation:  $\langle v_n(x) \rangle = v_{sat}$

$$I_{D,sat} = W C_G v_{sat} (V_{GS} - V_T) \text{ for } V_{DS} > V_{DSAT}$$





using an empirical model for velocity:

$$\langle v(V_{DS}) \rangle = F_{sat}(V_{DS}) \cdot v_{sat}$$

$$F_{sat}(V_{DS}) = \frac{V_{DS}/V_{DSAT}}{\left[1 + \left(\frac{V_{DS}}{V_{DSAT}}\right)^\beta\right]^{1/\beta}}$$

$$V_{DSAT} = \frac{v_{sat}}{\mu_n}$$

We can finalize the level 0 model as

$$1) \quad I_{DS}/W = \frac{Q_n(V_{GS}) \cdot v(0)}{L} = Q_n(V_{GS}) \langle v(V_{DS}) \rangle$$

$$2) \quad Q_n(V_{GS}) = 0 \quad V_{GS} \leq V_T$$

$$= -C_{ox}(V_{GS} - V_T) \quad V_{GS} > V_T$$

$$C_{ox} = \frac{C_{ox1} \cdot C_{dep1} \cdot C_{dep2}}{C_{ox1} \cdot C_{dep1} + C_{ox1} \cdot C_{dep2} + C_{dep1} \cdot C_{dep2}}$$

$$C_{ox} = \frac{C_{ox1} \cdot C_{ox2}}{C_{ox1} + C_{ox2}}$$

~~W/L~~ ~~W/L~~

device specific parameters

$$3) \quad \langle v(V_{DS}) \rangle = F_{sat}(V_{DS}) \cdot v_{sat}$$

$$4) \quad F_{sat}(V_{DS}) = \frac{V_{DS}/V_{DSAT}}{\left[1 + \left(\frac{V_{DS}}{V_{DSAT}}\right)^\beta\right]^{1/\beta}}$$

$C_{ox1}, C_{ox2}, V_T, v_{sat}, \mu_{eff}, L_{ch}$

empirical parameter

$$5) \quad V_{DSAT} = \frac{v_{sat} L_{ch}}{\mu_{eff}}$$

$\beta$

We can substitute  $K_{ox1} = 20$  and  $t_{ox1} = 1\text{nm}$ ,  $K_{ox2} = 7.5$  and  $t_{ox2} = 2\text{nm}$  as per the specifications given in the question