CH365 Chemical Engineering Thermodynamics

Lesson 18 Temperature Dependence of $\Delta {\rm H}^{\rm o}$

BLUF: Need T instead of T_{ref}

Chemical Reactions

$$N_2 + 3H_2 \rightarrow 2NH_3$$

$$\nu_{N_2} \, = -1 \qquad \nu_{H_2} \, = -3 \qquad \quad \nu_{NH_3} \, = +2$$

$$|v_1|A_1 + |v_2|A_2 + \dots \rightarrow |v_3|A_3 + |v_4|A_4 + \dots$$

 A_i = chemical formula

 $|v_i|$ = stoichiometric coefficient

positive (+) for products negative (-) for reactants

$$\Delta H^o = \sum_i \nu_i H^o_i \qquad \text{Eq. 4.15} \qquad \Delta H^o = \sum_i \nu_i H^o_{f_i} \quad \text{Eq. 4.16}$$

$$4HCl(g) + O2(g) \rightarrow 2H2O(g) + 2Cl2(g)$$

$$\Delta H^o = \sum_i \nu_i H^o_{f_i} = 2\Delta H^o_{f,H_2O} - 4\Delta H^o_{f,HCI}$$

$$\Delta H_{298}^{\circ} = (2)(-241,818) - (4)(-92307) = -114,408 \text{ J}$$

BLUF: Need T instead of T_{ref}

Standard Reactions

$$dH_i^o = C_{p_i}^o dT \qquad \text{Eq. 2.20}$$

Standard reactions are always at P = 1 bar

multiply by v_i and sum over all i:

$$\sum_i \nu_i dH^o_i = \sum_i \nu_i C^o_{p_i} dT$$

$$\sum_i d \big(\nu_i H_i^o \big) = \sum_i \nu_i C_{p_i}^o dT$$

$$d\left(\sum_{i} \left(\nu_{i} H_{i}^{o}\right)\right) = \sum_{i} \nu_{i} C_{p_{i}}^{o} dT \qquad \Delta H^{o} = \sum_{i} \nu_{i} H_{i}^{o}$$
Eq. 4.15

$$\Delta H^o = \sum_i v_i H^o_i$$
 Eq. (

$$d\Delta H^o = \sum_i \nu_i C^o_{p_i} dT$$

$$d\Delta H^o = \sum_i \nu_i C^o_{p_i} dT \qquad \qquad \Delta C^o_{P} \equiv \sum_i \nu_i C^o_{P_i} \qquad \qquad \qquad \\ Eq. \, 4.17 \qquad \qquad \label{eq:delta_Ho}$$

$$d\Delta H^{o} = \Delta C_{p}^{o} dT$$
Eq. 4.18

$$\Delta H^{o} = \Delta H_{0}^{o} + R \int_{T_{0}}^{T} \frac{\Delta C_{p}^{o}}{R} dT$$
Eq. 4.19

Next step: derive convenient integrated forms for integral (IDCPH, MDCPH)

Eq. 4.20

Integrated Forms

$$\begin{split} \int\limits_{T_0}^T \frac{\Delta C_p^o}{R} dT &= \Delta A \cdot \left(T - T_0\right) + \frac{\Delta B}{2} \cdot \left(T^2 - T_0^2\right) + \frac{\Delta C}{3} \cdot \left(T^3 - T_0^3\right) + \Delta D \cdot \left(\frac{T - T_0}{T \cdot T_0}\right) \\ \Delta A &= \sum_i \nu_i \cdot A_i \text{, etc.} \end{split}$$

 $\frac{\left\langle \Delta C_{p}^{o} \right\rangle_{H}}{R} = \Delta A + \frac{\Delta B}{2} \cdot \left(T + T_{0} \right) + \frac{\Delta C}{3} \cdot \left(T^{2} + T_{0}^{2} + T \cdot T_{0} \right) + \frac{\Delta D}{T \cdot T}$

$$\Delta \mathsf{H}^{\mathsf{o}} = \Delta \mathsf{H}^{\mathsf{o}}_{\mathsf{0}} + \left\langle \Delta \mathsf{C}^{\mathsf{o}}_{\mathsf{p}} \right\rangle_{\mathsf{H}} \left(\mathsf{T} - \mathsf{T}_{\mathsf{0}} \right)$$

 $(T-T_0)$ factored out

Ea. 4.22

$$\frac{\left\langle \Delta C_{p}^{o} \right\rangle_{H}}{R} = \text{MDCPH}$$
In book: MDCPH(T₀,T,DA,DB,DC,DD)

Looks like MCPH from lesson 16

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Derived on next slide

$$\int_{T_0}^{T} \frac{\Delta C_p^o}{R} dT = IDCPH \quad \text{In book: IDCPH}(T_0, T, DA, DB, DC, DD)$$

Looks like ICPH from lesson 16

Derivation of Integrated Forms at T

CO (g) + 2 H₂ (g) = CH₃OH (g)
$$\longrightarrow$$
 C + 2 H = M $\nu_{CO} = -1 = \nu_{C}$ $\nu_{H_{2}} = -2 = \nu_{H}$ $\nu_{CH_{3}OH} = +1 = \nu_{M}$

Important derivation (not in book)

Bring reactants from T to T_0 , react at T_0 , then bring products from T_0 to T

Method: write Cp integrals for each species, add standard heat, reverse order of integration on reactants, replace coefficients with v's, group integrals together, and collect terms:

$$\Delta H = R \int\limits_{T_0}^{T_0} \frac{C_P^C}{R} dT + R \int\limits_{T_0}^{T_0} 2 \frac{C_P^H}{R} dT + \Delta H_R^o + R \int\limits_{T_0}^{T} \frac{C_P^M}{R} dT = R \int\limits_{T_0}^{T} - \frac{C_P^C}{R} dT + R \int\limits_{T_0}^{T} - 2 \frac{C_P^H}{R} dT + R \int\limits_{T_0}^{T} \frac{C_P^M}{R} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ v_C \frac{C_P^C}{R} + v_H \frac{C_P^H}{R} + v_M \frac{C_P^M}{R} \right\} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ v_C \left(A_C + B_C T + C_C T^2 + D_C T^{-2} \right) + v_H \left(A_H + B_H T + C_H T^2 + D_H T^{-2} \right) + v_M \left(A_M + B_M T + C_M T^2 + D_M T^{-2} \right) \right\} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ v_C A_C + v_C B_C T + v_C C_C T^2 + v_C D_C T^{-2} + v_H A_H + v_H B_H T + v_H C_H T^2 + v_H D_H T^{-2} + v_M A_M + v_M B_M T + v_M C_M T^2 + v_M D_M T^{-2} \right\} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ v_C A_C + v_H A_H + v_M A_M + v_C B_C T + v_H B_H T + v_M B_M T + v_C C_C T^2 + v_M C_M T^2 + v_H C_H T^2 + v_C D_C T^{-2} + v_H D_H T^{-2} + v_M D_M T^{-2} \right\} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ \Delta A + \Delta B \cdot T + \Delta C \cdot T^2 + \Delta D \cdot T^{-2} \right\} dT + \Delta H_R^o$$

$$= R \int\limits_{T_0}^{T} \left\{ \Delta A + \Delta B \cdot T + \Delta C \cdot T^2 + \Delta D \cdot T^{-2} \right\} dT + \Delta H_R^o$$
(BLUF: This derivation shows that this equation for calculating the products of the prod

that this equation for calculating same for reactants and products.)

Example 4.6

Calculate the standard heat of formation of the methanol synthesis reaction at 800 °C.

$$\Delta H_{298}^o = \sum_i \nu_i H_{f_i}^o = (1) \cdot (-200,660) + (-1) \cdot (-110,525) = -90,135 \, J$$

Eq. 4.16

i	ν_{i}	A -	Bx10 ³	Cx10 ⁶	Dx10 ⁻⁵
CH ₃ OH	1	2.211	12.216	-3.450	0.000
СО	- 1	3.376	0.557	0.000	-0.031
H ₂	- 2	3.249	0.422	0.000	0.083

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$$\Delta A = (1) \cdot (2.211) + (-1) \cdot (3.376) + (-2) \cdot (3.249) = -7.663$$

$$\Delta B = (1) \cdot (12.216) + (-1) \cdot (0.557) + (-2) \cdot (0.422) = 10.815 \times 10^{-3}$$

$$\Delta C = (1) \cdot (-3.450) + (-1) \cdot (0.000) + (-2) \cdot (0.000) = -3.450 \times 10^{-6}$$

$$\Delta D = (1) \cdot (0.000) + (-1) \cdot (0.031) + (-2) \cdot (0.083) = -0.135 \times 10^{5}$$

$$T = 800 \, ^{\circ}C = 1073 \, \text{K}$$

$$T_0 = 25 \, ^{\circ}C = 298 \, K$$

$$IDCPH = \int_{T_0}^{T} \frac{\Delta C_p^o}{R} dT = \Delta A \cdot \left(T - T_0\right) + \frac{\Delta B}{2} \cdot \left(T^2 - T_0^2\right) + \frac{\Delta C}{3} \cdot \left(T^3 - T_0^3\right) + \Delta D \cdot \left(\frac{T - T_0}{T \cdot T_0}\right) = -1615.46 \, \text{K}$$

Eq. 4.20

$$\Delta H^{o} = \Delta H^{o}_{298} + R \cdot \int\limits_{T_{0}}^{T} \frac{\Delta C^{o}_{P}}{R} dT = \Delta H^{o}_{298} + R \cdot IDCPH = -90,135 + 8.314 \cdot \left(-1615.46\right) = -103,566 \, J$$

Eq. 4.19

Example (4.20 from PS6)

Calculate the standard heat of combustion of 6 moles of methanol at 800 °C with CO₂ and H₂O (g) as products.

$$6 \text{ CH}_3 \text{OH } (g) + 9 \text{ O}_2 (g) = 6 \text{ CO}_2 (g) + 12 \text{ H}_2 \text{O}(g)$$

$$\Delta H_{298}^o = \sum_i \nu_i H_{f_i}^o = (6) \cdot (-393,509) + (12) \cdot (-241,818) + (-6) \cdot (-200,660) + (-9) \cdot (0) = -4,058,910 \, \text{J} \quad \text{Eq. 4.15}$$

i	ν_{i}	Α	Bx10 ³	Cx10 ⁶	Dx10 ⁻⁵
CO ₂	6	5.457	1.045	0.000	-1.157
H ₂ O	12	3.470	1.450	0.000	0.121
CH₃OH	-6	2.211	12.216	-3.450	0.000
O ₂	-9	3.639	0.506	0.000	-0.227

$$\Delta A = (6) \cdot (5.547) + (12) \cdot (3.470) + (-6) \cdot (2.211) + (-9) \cdot (3.639) = 28.365$$

$$T_1 = 800 \, ^{\circ}C = 1073 \, K$$

$$\Delta B = (6) \cdot (1.045) + (12) \cdot (1.450) + (-6) \cdot (12.216) + (-9) \cdot (0.506) = -54.180 \times 10^{-3}$$

$$T_0 = 25 \, ^{\circ}\text{C} = 298 \, \text{K}$$

$$\Delta C = (6) \cdot (0.000) + (12) \cdot (0.000) + (-6) \cdot (3.450) + (-9) \cdot (0.000) = 20.700 \times 10^{-6}$$

$$\Delta D = (6) \cdot (-1.157) + (12) \cdot (0.121) + (-6) \cdot (0.000) + (-9) \cdot (-0.227) = -0.345 \times 10^5$$

$$IDCPH = \int\limits_{T_0}^T \frac{\Delta C_p^o}{R} dT = \Delta A \cdot \left(T - T_0\right) + \frac{\Delta B}{2} \cdot \left(T^2 - T_0^2\right) + \frac{\Delta C}{3} \cdot \left(T^3 - T_0^3\right) + \Delta D \cdot \left(\frac{T - T_0}{T \cdot T_0}\right) = 702.64 \, \text{K}$$

$$\Delta H^{\circ} = \Delta H^{\circ}_{298} + R \cdot \int \frac{\Delta C^{\circ}_{P}}{R} dT = \Delta H^{\circ}_{298} + R \cdot IDCPH = -4,058,910 + 8.314 \cdot \left(702.64\right) = -4,053,068 J$$

Eq. 4.20

Questions?

Homework

What is the standard heat of combustion of n-pentane gas at 25 °C if the combustion products are $H_2O(I)$ and $CO_2(g)$?

Natural gas (assume pure methane) is delivered to a city via pipeline at a volumetric flow rate of 150 million standard cubic feet per day. If the selling price of the gas is \$5.00 per GJ of higher heating value, what is the expected revenue in dollars per day? Standard conditions are 60 °F and 1 atm.

Saturated water vapor, i.e., *steam*, is commonly used as a heat source in heat exchanger applications. Why *saturated* water vapor? Why saturated *water* vapor?

In a plant of any reasonable size, several varieties of saturated steam are commonly available. For example, saturated steam may be available at 4.5, 9, 17, and 33 bar. But the higher the pressure, the lower the useful energy content and the greater the cost. Why is the energy content lower at higher pressure? Why then is higher-pressure steam used?

The oxidation of glucose provides the principal source of energy for animal cells. Assuming the reactants are glucose [$C_6 H_{12}O_6(s)$] and oxygen [$O_2(g)$] and the products are $CO_2(g)$ and $H_2O(I)$, answer the following:

- (a) Write a balanced equation for glucose oxidation, and determine the standard heat of reaction at 298 K.
- (b) During a day, an average person consumes about 150 kJ of energy per kg of body mass. Assuming glucose is the only source of energy, estimate the mass (grams) of glucose required daily to sustain a person of 57 kg.
- (c) For a population of 275 million people, what mass of CO_2 (a greenhouse gas) is produced daily by mere respiration? Data: for glucose, $\Delta H_{f,298}^0 = -1,274,4$ kJ/mol. Ignore the effect of temperature on the heat of reaction.