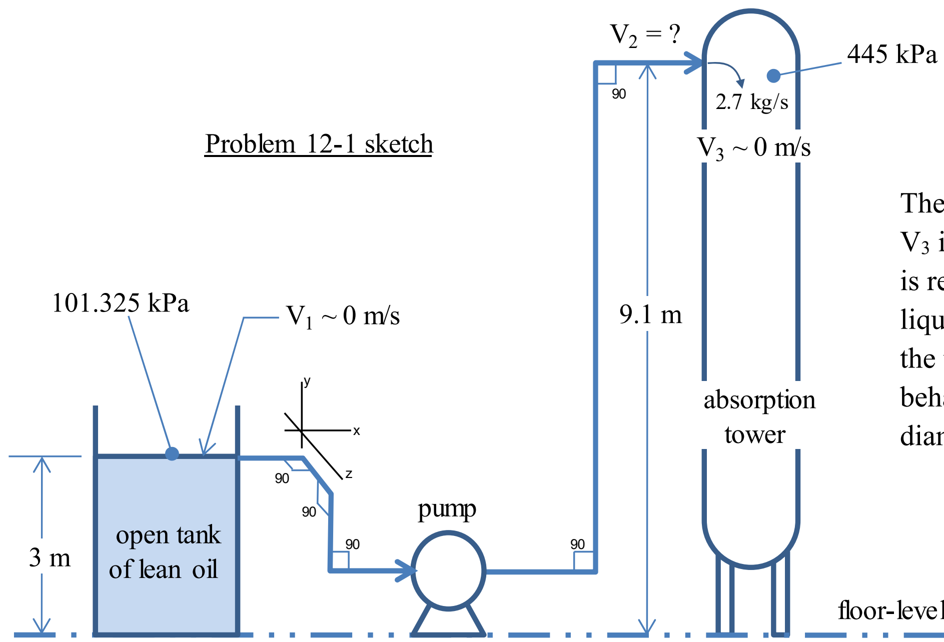
Problem 12-1

Estimate the size of the motor necessary to pump a lean oil to the top of an absorption tower operating at a pressure of 445 kPa. The oil is to be pumped from an open tank with a liquid level 3 m above the floor through 46 m of pipe with an inside diameter of 0.078 m. There are five 90° elbows in the line, and the top of the tower is 9.1 m above the floor level. A flow of 2.7 kg/s of lean oil is required. The viscosity of the oil is 15 cP, and its density is 857 kg/m^3. Assume that the efficiency of the pumping system including the motor is 40%.

Solution:

Start by making a sketch of the system such as the one shown below, and then apply the mechanical energy balance.



The assumption that V_3 is about equal to 0 is reasonable since the liquid is held up on the top tray, which behaves like a large-diameter vessel.

Assuming that the fluid is incompressible, Equation 12-12 on page 492 is the most convenient and appropriate form of the mechanical energy balance:

$$W_o = g\Delta z + \Delta\left(\frac{V^2}{2\alpha}\right) + \Delta(pv) + \Sigma F = g(z_2 - z_1) + \frac{V_2}{2} + \frac{p_2 - p_1}{\rho} + \Sigma F$$

The correction factor α is assumed to be 1 (assuming turbulent flow). Also assume that the velocity of the fluid entering the pipeline is zero, so that V_1=0, and that the velocity in the tower is zero, so that V_3=0. The velocity of the fluid inside the pipe is given by

$$V_2 = \frac{\left(2.7\,\frac{kg}{s}\right)/\left(857\,\frac{kg}{m^3}\right)}{\pi(0.078\text{m})^2/4} = 0.659\,\frac{m}{s}$$

The Reynolds number is needed to calculate the frictional losses, and is given by

$$\mathrm{Rn} = \frac{D V_2 \rho}{\mu} = \frac{0.078\mathrm{m} \cdot 0.659\,\frac{\mathrm{m}}{\mathrm{s}} \cdot 857\,\frac{\mathrm{kg}}{\mathrm{m}^3}}{0.015\,\frac{\mathrm{kg}}{\mathrm{m \cdot s}}} = 2938.25$$

Use this value of Reynolds number to read the friction factor from Figure 12-1 on page 487, getting f=0.011.

To calculate the frictional losses, we must use Equation 12-7 on page 488. However, we must first determine the *total equivalent length* to account for the elbow, using Table 12-1:

$$L = 46\mathrm{m} + 5 \cdot 32 \cdot 0.078\mathrm{m} = 58.48\mathrm{m}$$

$$F = \frac{2 \cdot f \cdot V^2 \cdot L}{D} = \frac{2 \cdot 0.011 \cdot \left(0.659\,\frac{\mathrm{m}}{\mathrm{s}}\right)^2 \cdot 58.48\mathrm{m}}{0.078\mathrm{m}} = 7.163\,\frac{\mathrm{m}^2}{\mathrm{s}^2}$$

There are also frictional losses F_C due to the sudden constriction where the fluid enters the pipe. F_C for sudden constriction is given by the equation in Table 12-1 on page 490:

$$F_C = \frac{K_C \cdot V^2}{2 \cdot \alpha} = \frac{0.4 \cdot 1.25 \cdot \left(0.659\,\frac{\mathrm{m}}{\mathrm{s}}\right)^2}{2} = 0.109\,\frac{\mathrm{m}^2}{\mathrm{s}^2}$$

Note that K_C is really a function of the big and small areas of the constriction (A_1 and A_2 in the sketch), but the maximum value is 0.4·1.25.

There are also frictional losses F_E due at the end of the pipe due to the sudden expansion where the fluid enters the column. F_E for sudden expansion is given in Table 12-1 on page 490:

$$F_e = \frac{\left(V_2 - V_3\right)^2}{2 \cdot \alpha} = \frac{\left(\sim 0 - 0.659\,\frac{\mathrm{m}}{\mathrm{s}}\right)^2}{2} = 0.217\,\frac{\mathrm{m}^2}{\mathrm{s}^2}$$

Now, go back and apply the mechanical energy balance:

$$W_o = 9.8\,\frac{\mathrm{m}}{\mathrm{s}^2} \cdot (9.1\mathrm{m} - 3.0\mathrm{m}) + \frac{445000\mathrm{Pa} - 101325\mathrm{Pa}}{857\,\frac{\mathrm{kg}}{\mathrm{m}^3}} + \frac{\left(0.659\,\frac{\mathrm{m}}{\mathrm{s}}\right)^2}{2} + (0.109 + 7.170 + 0.217)\,\frac{\mathrm{m}^2}{\mathrm{s}^2} = 468.5\,\frac{\mathrm{m}^2}{\mathrm{s}^2}$$

To convert this answer to Watts, multiply by the mass flow rate:

$$W_o = 468.5\,\frac{\mathrm{m}^2}{\mathrm{s}^2} \cdot 2.7\,\frac{\mathrm{kg}}{\mathrm{s}} = 1\underline{2}65.0 \text{ Watts}$$

To calculate the power input to the pump-motor system, divide by the efficiency:

$$W_{in} = \frac{1\underline{2}65.0 \text{ Watts}}{0.4} = \underline{\underline{3\underline{1}62.5 \text{ Watts}}}_{\text{ANS}}$$

PROBLEM SET 1

Design tool for incompressible flow in pipes

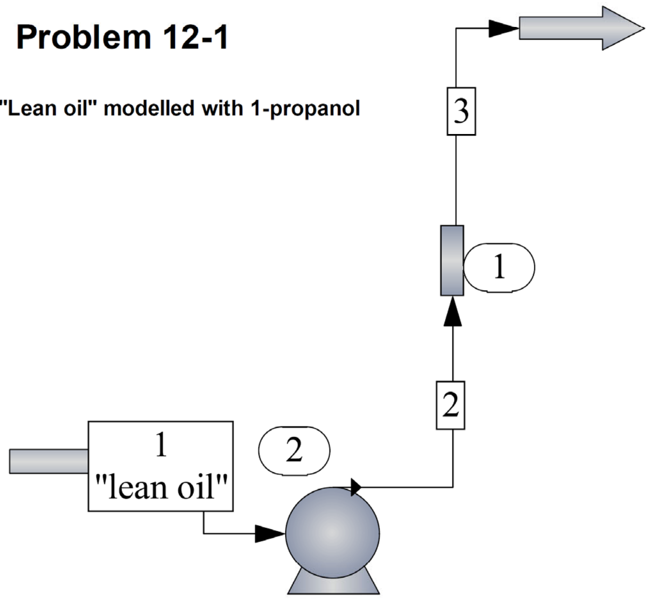
PTW, Problem 12-1.
Yellow highlighting designates required **user** input.

	QUANTITY	Symbol	Units	Specs	Cell Name	Formulae and notes
	viscosity	μ	kg/m·s	0.015	mu	u/s (user specified)
	density	ρ	kg/m^3	857	rho	u/s
	flow rate, specified	m_v	m^3/s	0.00315	mv	u/s
	diameter, specified	D	m	0.07800	D	u/s
	pipe cross-sectional area	A	m^2	0.00478	A	s/c (spreadsheet calculation), $\pi D^2/d$
	velocity	v	m/s	0.65933	v	s/c, volumetric flow rate divided by cross-sectional area
	Reynolds number	Re	dimensionless	2938	Re	s/c, $Dv\rho/\mu$
	Optimal Diameter Section					
	diameter, optimal, SI	D_{opt}	m	0.0589	Dopt	s/c, nested IF statements using eqns 9-76 to 9-79, PTW, p. 404
	area, optimal	A_{opt}	m^2	0.0027	Aopt	s/c, $\pi D_{opt}^2/4$
	velocity, optimal	v_{opt}	m/s	1.1576	vopt	s/c, volumetric flow divided by A_{opt}
	Reynolds number, optimal	Re_{opt}	dimensionless	3893	Reopt	s/c, $D_{opt}v_{opt}\rho/\mu$
Static Head (Gravitation)	**Potential Energy Section**					
	elevation 1	h_1	m	3	hinit	u/s
	elevation 2	h_2	m	9.1	hfinal	u/s
	gravitational acceleration constant	g	m/s^2	9.8	g	u/s
	gravitational potential head	$g\cdot\Delta h$	m^2/s^2 or N·m/kg	59.78	not named	s/c
Static Head (Pressure)	**External Pressure Section**					
	pressure 1	p_1	Pa	101325	pinit	u/s
	pressure 2	p_2	Pa	445000	pfinal	u/s
	pressure head	$\Delta(p\nu)$	m^2/s^2 or N·m/kg	401.0210035	not named	s/c
Dynamic Head (Kinetic E)	**Kinetic Energy Section**					
	initial fluid velocity	v_1	m/s	0.00000	Vinit	s/c, from cell E10
	final fluid velocity	v_2	m/s	0.65933	Vfinal	s/c, from cell E10
	velocity correction	α	dimensionless	1	alpha	n/a
	kinetic energy head	$\Delta(v^2/2\alpha)$	m^2/s^2 or N·m/kg	0.217359032	not named	s/c
Dynamic Head (Friction)	**Pipe Friction Section**					
	Colebrook relation for f			-0.000278739	not named	s/c, eq. 12-6, p. 487
	pipe length	L	m	46	L	u/s
	pipe roughness	ε	m	0.0000457	eps	u/s, fig. 12-1, p. 487
	fanning friction factor, turbulent	f	dimensionless	0.01108	not named	s/c; run solver to minimize blue cell with respect to cell E40
	fanning friction factor, laminar	f	dimensionless	0.00545	not named	s/c, eq. 12-4, p. 487
	fanning friction factor	f	dimensionless	0.01108	f	s/c, IF statement to choose laminar or turbulent
	frictional loss due to straight pipe	F_{pipe}	m^2/s^2 or N·m/kg	5.7	not named	s/c, eq. 12-7, p. 488
	losses due to straight pipe + fittings	$F_{pipe+fittings}$	m^2/s^2 or N·m/kg	7.2	not named	s/c, eq. 12-7, p. 488, with equivalent length L+Le
	total friction head	$F_{pipe+fittings+ec}$	m^2/s^2 or N·m/kg	7.5	not named	s/c, eq. 12-7, p. 488, with expansions and constrictions
	Pump Work Section					
	total head (pump work @ 100% efficiency)	P_o	m^2/s^2 or N·m/kg	469	not named	Energy balance; summation of all gray cells
	total head in Watts	P_o	W	1265	not named	s/c, m^2/s^2·kg/s
	efficiency	η	dimensionless	0.4	eta	u/s
	pump work at specified efficiency	P	m^2/s^2 or N·m/kg	1171	not named	s/c, divide by efficiency
	pump work at specified efficiency	P	W	3163	not named	s/c, divide by efficiency
	Frictional Losses Due to Fittings and Valves					
	Description of fittings	Le/D		number		
	45° elbows	15	dimensionless		not named	u/s, Table 12-1, p. 490, fittings, vavles, etc.
	90° elbows, standard radius	32	dimensionless	5	not named	u/s
	90° elbows, medium radius	26	dimensionless		not named	u/s
	90° elbows, long sweep	20	dimensionless		not named	u/s
	90° elbows, square	60	dimensionless		not named	u/s
	180° bends, close return	75	dimensionless		not named	u/s
	180° bends, medium radius	50	dimensionless		not named	u/s
	Tee (used as elbow, entering run)	60	dimensionless		not named	u/s
	Tee (used as elbow, entering branch)	90	dimensionless		not named	u/s
	Couplings	0	dimensionless		not named	u/s
	Unions	0	dimensionless		not named	u/s
	Gate valves, open	7	dimensionless		not named	u/s
	Globe valves, open	300	dimensionless		not named	u/s
	Angle valves, open	170	dimensionless		not named	u/s
	Water meters, disk	400	dimensionless		not named	u/s
	Water meters, piston	600	dimensionless		not named	u/s
	Water meters, impulse-wheel	300	dimensionless		not named	u/s
	Equivalent length of fittings	Le	m	12.48	Le	s/c, summation of all losses due to fittings
	Frictional Losses Due to Enlargements and Constrictions					
	Area on narrow side of constriction/expansion	A_{narrow}	m^2	0.00478	not named	s/c, calculated earlier in cell E9
	Area on wide side of constriction/expansion	A_{wide}	m^2	4.77836	not named	u/s, used a ratio of 1000 in this case
	Ratio of narrow area to wide area	A_{narrow}/A_{wide}	dimensionless	0.001	not named	s/c, A_{wide} is not known in this case, so the ratio is made small
	Velocity on narrow side of constriction/expansior	v_{narrow}	m/s	0.65933	not named	s/c, volumetric flow divided by area of narrow side
	Velocity on wide side of constriction/expansion	v_{wide}	m/s	0.00066	not named	s/c, volumetric flow divided by area of wide side
	Losses due to enlargements	F_e	m^2/s^2 or N·m/kg	0.21692	not named	s/c, Table 12-1, p. 490, sudden enlargement
	Losses due to constrictions	F_c	m^2/s^2 or N·m/kg	0.10859	not named	s/c, Table 12-1, p. 490, sudden constriction
	Number of enlargements	---	dimensionless	1	not named	u/s, typical value is 1 for pipe emptying into a vessel
	Number of constrictions	---	dimensionless	1	not named	u/s, typical value is 1 for pipe removing liquid from a vessel
	Losses due to enlargements and constrictions	F_e+F_c	m^2/s^2 or N·m/kg	0.32552	not named	s/c

CHEMCAD Solution

Problem 12-1

"Lean oil" modelled with 1-propanol



Stream No.	1	2	3
Name	"lean oil"		
- - Overall - -			
Mass flow kg/sec	2.7000	2.7000	2.7000
Temp K	231.5000	232.1012	232.1012
Pres Pa	101325.0000	502079.0000	445000.0000
Enth kJ/sec	-13982.	-13978.	-13978.
Entropy kJ/K/sec	-21.96	-21.94	-21.94
GibbsEnergy kJ/sec	-8898.2	-8885.8	-8885.9
- - Liquid only - -			
Actual dens kg/m3	854.4092	853.9491	853.9490
Visc cP	14.98	14.65	14.64
Flow rates in kg/sec			
Ethanol	0.0000	0.0000	0.0000
N-Propanol	2.7000	2.7000	2.7000

Equip. No.	1
Name	
Method	2
Diameter m	0.0780
Calculated ID m	0.0780
Pipe length m	46.0000
Roughness factor m	4.5720e-005
Elevation change m	6.1000
Pressure drop Pa	57079.0039
Reynolds # liq	3008.6821
Fric factr liq	0.0450
Avg density kg/m3	853.9491
Calc. velocity m/sec	0.6617
Min. velocity m/sec	0.4158
DP friction Pa	5995.2720
DP elevation Pa	51083.7344
Output press. Pa	445000.0000
DP/100ft, psi	0.4768
Liquid flow kg/sec	2.7000
Liquid density kg/m3	853.9491
Liq viscosity cP	14.6487
Surface tension N/m	0.0285
EL. fittings m	9.5862
Total ELength m	55.5862
small dia./large dia.	0.0010
Standard elbow 90 de	5
Sudden contraction	1
Sudden expansion	1
Friction fac. model	1
Incl. expansion fac.	1
Pipe wall cond. W/m-	51.2818
Inclination angle	7.6204

Equip. No.	2
Name	
Output pressure Pa	502079.0000
Efficiency	0.4000
Calculated power	3168.3052
(J/sec)	
Calculated Pout Pa	502079.0000
Head m	47.8290
Vol. flow rate m3/h	11.3763
Mass flow rate kg/sec	2.7000

This problem would be fairly easy to solve in ChemCAD if the chemical composition of the lean oil were known. However, this was not given. The key to the problem is therefore to identify a reasonable component that matches the density and viscosity of the lean oil. This is sometimes referred to as using a "psuedo-component."

After some searching, I settled on 1-propanol at 231.5 K, which is a pretty close match. The given density was 857 kg/m3 and the viscosity was given as 15 cP. The corresponding values for 1-propanol at 231.5 K are 854.4 and 14.98.

The calculated pump power of 3168 J/s is in good agreement with the value of 3163 W from the by-hand calculations. The small difference is due to small differences in viscosity and density and the Le/D values used by CHEMCAD.

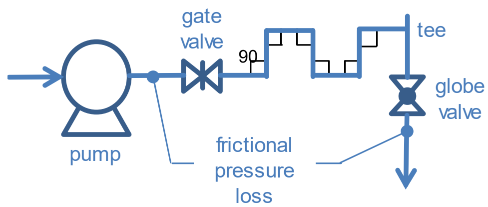
The pipeline tool allows the user to set fluid properties to their own values and then override the CHEMCAD values. Trying this and changing the density and viscosity to the values given in the problem statement, changes the Reynolds number from 3009 to 2938, in excellent agreement with the by-hand calculations. However, this changes the pump power from 3168 W to 3170, or an increase of 2 W. So there is an effect, but it is small and in the wrong direction.

Problem 12-2

What is the pressure loss when 2.14 kg/s of pure benzene at 40 ºC flows through a 21-m length of straight pipe with an inside diameter of 0.0409 m? The pipeline contains six 90º elbows, one tee used as an elbow (equivalent resistance equal to 60 pipe diameters), one globe valve, and one gate valve. The density of benzene is 849 kg/m^3, and its viscosity at 40 ºC is 5×10^{-4} Pa·s.

Solution:

Start by making a sketch of the system, and then apply the frictional loss Equation 12-7, p. 488.



Start with velocity inside the pipe, which is given by

$$V_2 = \frac{\left(2.14\,\frac{kg}{s}\right)/\left(849\,\frac{kg}{m^3}\right)}{\pi\left(0.0409m\right)^2/4} = 1.919\,\frac{m}{s}$$

The Reynolds number is given by

$$Rn = \frac{DV\rho}{\mu} = \frac{0.0409m\cdot 1.919\,\frac{m}{s}\cdot 849\,\frac{kg}{m^3}}{0.0005\,\frac{kg}{m\cdot s}} = 133,271$$

Use the Reynolds number, read the friction factor from Figure 12-1 on page 487, getting f=0.0055. The *total equivalent length* accounts for the elbows, tee, and valves (Table 12-1):

$$L = 21m + \left(6\cdot 32 + 60 + 300 + 7\right)\cdot 0.0409m = 43.86m$$

$$F = \frac{2\cdot f\cdot V^2\cdot L}{D} = \frac{2\cdot 0.0055\cdot\left(1.919\,\frac{m}{s}\right)^2\cdot 43.86m}{0.0409m} = 43.440\,\frac{m^2}{s^2}$$

To convert this answer to Pa, multiply by the density:

CHEMCAD answer is 27.9 kPa
(set roughness correctly!)

ANS may vary slightly depending
on how you read the "Moody Plot"

$$F = 43.440\,\frac{m^2}{s^2}\cdot 849\,\frac{kg}{m^3} = \underline{\underline{36,881\ Pa}}_{\text{ANS}}$$

Excel answer is 27.4 kPa
(essentially the same)

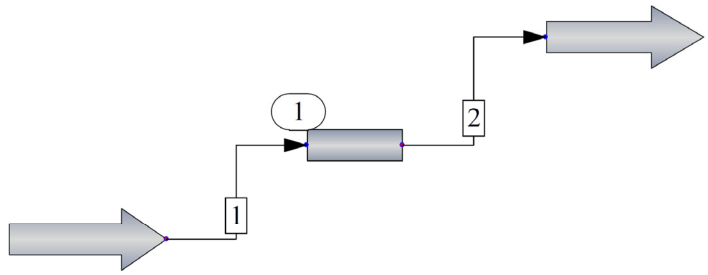
PROBLEM SET 1

Design tool for incompressible flow in pipes

PTW, Problem 12-2.
Yellow highlighting designates required **user** input.

	QUANTITY	Symbol	Units	Specs	Cell Name	Formulae and notes
	viscosity	μ	kg/m·s	0.0005	mu	u/s (user specified)
	density	ρ	kg/m^3	849	rho	u/s
	flow rate, specified	m_v	m^3/s	0.00252	mv	u/s
	diameter, specified	D	m	0.04090	D	u/s
	pipe cross-sectional area	A	m^2	0.00131	A	s/c (spreadsheet calculation), $\pi D^2/d$
	velocity	v	m/s	1.9185	v	s/c, volumetric flow rate divided by cross-sectional area
	Reynolds number	Re	dimensionless	133239	Re	s/c, $Dv\rho/\mu$
	Optimal Diameter Section					
	diameter, optimal, SI	D_{opt}	m	0.0488	Dopt	s/c, nested IF statements using eqns 9-76 to 9-79, PTW, p. 404
	area, optimal	A_{opt}	m^2	0.0019	Aopt	s/c, $\pi D_{opt}^2/4$
	velocity, optimal	v_{opt}	m/s	1.3452	vopt	s/c, volumetric flow divided by A_{opt}
	Reynolds number, optimal	Re_{opt}	dimensionless	111567	Reopt	s/c, $D_{opt}v_{opt}\rho/\mu$
Static Head (Gravitation)	**Potential Energy Section**					
	elevation 1	h_1	m	0	hinit	u/s
	elevation 2	h_2	m	0	hfinal	u/s
	gravitational acceleration constant	g	m/s^2	9.8	g	u/s
	gravitational potential head	$g\cdot\Delta h$	m^2/s^2 or N·m/kg	0	not named	s/c
Static Head (Pressure)	**External Pressure Section**					
	pressure 1	p_1	Pa	101325	pinit	u/s
	pressure 2	p_2	Pa	101325	pfinal	u/s
	pressure head	$\Delta(pv)$	m^2/s^2 or N·m/kg	0	not named	s/c
Dynamic Head (Kinetic E)	**Kinetic Energy Section**					
	initial fluid velocity	v_1	m/s	1.91853	Vinit	s/c, from cell E10
	final fluid velocity	v_2	m/s	1.91853	Vfinal	s/c, from cell E10
	velocity correction	α	dimensionless	1	alpha	n/a
	kinetic energy head	$\Delta(v^2/2\alpha)$	m^2/s^2 or N·m/kg	0	not named	s/c
Dynamic Head (Friction)	**Pipe Friction Section**					
	Colebrook relation for f			4.56869E-07	not named	s/c, eq. 12-6, p. 487
	pipe length	L	m	21	L	u/s
	pipe roughness	ε	m	0.0000457	eps	u/s, fig. 12-1, p. 487
	fanning friction factor, turbulent	f	dimensionless	0.00551	not named	s/c; run solver to minimize blue cell with respect to cell E40
	fanning friction factor, laminar	f	dimensionless	0.00012	not named	s/c, eq. 12-4, p. 487
	fanning friction factor	f	dimensionless	0.00551	f	s/c, IF statement to choose laminar or turbulent
	frictional loss due to straight pipe	F_{pipe}	m^2/s^2 or N·m/kg	20.8	not named	s/c, eq. 12-7, p. 488
	losses due to straight pipe + fittings	$F_{pipe+fittings}$	m^2/s^2 or N·m/kg	43.5101	not named	s/c, eq. 12-7, p. 488, with equivalent length L+Le
	total friction head	$F_{pipe+fittings+ec}$	m^2/s^2 or N·m/kg	43.5	not named	s/c, eq. 12-7, p. 488, with expansions and constrictions
	Pump Work Section					
	total head (pump work @ 100% efficiency)	P_o	m^2/s^2 or N·m/kg	44	not named	Energy balance; summation of all gray cells
	total head in Watts	P_o	W	93	not named	s/c, m^2/s^2·kg/s
	efficiency	η	dimensionless	0.4	eta	u/s
	pump work at specified efficiency	P	m^2/s^2 or N·m/kg	109	not named	s/c, divide by efficiency
	pump work at specified efficiency	P	W	233	not named	s/c, divide by efficiency
	Frictional Losses Due to Fittings and Valves					
	Description of fittings	Le/D		number		
	45° elbows	15	dimensionless		not named	u/s, Table 12-1, p. 490, fittings, vavles, etc.
	90° elbows, standard radius	32	dimensionless	6	not named	u/s
	90° elbows, medium radius	26	dimensionless		not named	u/s
	90° elbows, long sweep	20	dimensionless		not named	u/s
	90° elbows, square	60	dimensionless		not named	u/s
	180° bends, close return	75	dimensionless		not named	u/s
	180° bends, medium radius	50	dimensionless		not named	u/s
	Tee (used as elbow, entering run)	60	dimensionless	1	not named	u/s
	Tee (used as elbow, entering branch)	90	dimensionless		not named	u/s
	Couplings	0	dimensionless		not named	u/s
	Unions	0	dimensionless		not named	u/s
	Gate valves, open	7	dimensionless	1	not named	u/s
	Globe valves, open	300	dimensionless	1	not named	u/s
	Angle valves, open	170	dimensionless		not named	u/s
	Water meters, disk	400	dimensionless		not named	u/s
	Water meters, piston	600	dimensionless		not named	u/s
	Water meters, impulse-wheel	300	dimensionless		not named	u/s
	Equivalent length of fittings	Le	m	22.86	Le	s/c, summation of all losses due to fittings
	Frictional Losses Due to Enlargements and Constrictions					
	Area on narrow side of constriction/expansion	A_{narrow}	m^2	0.00131	not named	s/c, calculated earlier in cell E9
	Area on wide side of constriction/expansion	A_{wide}	m^2	1.31382	not named	u/s, used a ratio of 1000 in this case
	Ratio of narrow area to wide area	A_{narrow}/A_{wide}	dimensionless	0.001	not named	s/c, A_{wide} is not known in this case, so the ratio is made small
	Velocity on narrow side of constriction/expansior	v_{narrow}	m/s	1.91853	not named	s/c, volumetric flow divided by area of narrow side
	Velocity on wide side of constriction/expansion	v_{wide}	m/s	0.00192	not named	s/c, volumetric flow divided by area of wide side
	Losses due to enlargements	F_e	m^2/s^2 or N·m/kg	1.83670	not named	s/c, Table 12-1, p. 490, sudden enlargement
	Losses due to constrictions	F_c	m^2/s^2 or N·m/kg	0.91946	not named	s/c, Table 12-1, p. 490, sudden constriction
	Number of enlargements	---	dimensionless	0	not named	u/s, typical value is 1 for pipe emptying into a vessel
	Number of constrictions	---	dimensionless	0	not named	u/s, typical value is 1 for pipe removing liquid from a vessel
	Losses due to enlargements and constrictions	F_e+F_c	m^2/s^2 or N·m/kg	0.00000	not named	s/c

CHEMCAD Solution



Equip. No.	1
Name	
Method	2
Diameter m	0.0409
Calculated ID m	0.0409
Pipe length m	21.0000
Roughness factor m	457.0000
Pressure drop Pa	35815.1367
Reynolds # liq	133237.8125
Fric factr liq	0.0207
Avg density kg/m3	849.0000
Calc. velocity m/sec	1.9185
DP friction Pa	35815.1367
Output press. Pa	65509.8594
DP/100ft, psi	3.4909
Stream prop. flag	1
Liquid flow kg/sec	2.1400
Liquid density kg/m3	849.0000
Liq viscosity Pa-sec	0.0005
Surface tension N/m	0.0262
EL. fittings m	24.3549
Total ELength m	45.3549
Gate valve	1
Glb seat flatBevelPlug	1
Standard elbow 90 deg.	6
Std T, flow-thr brnch	1
Friction fac. model	1
Incl. expansion fac.	1
Pipe wall cond. W/m-K	51.2818

CHEMCAD gives a pressure drop of 35,815 Pa, compared to 36,881 Pa from the by-hand calculation. The difference is due to rounding error in the properties and probably to differences in the Le/D values used by CHEMCAD for the valves and fittings.