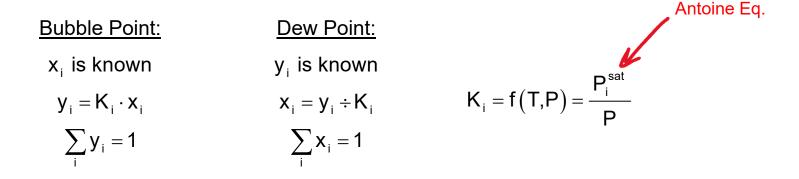
CH365 Chemical Engineering Thermodynamics

Lesson 30
Generalized Property Correlations

CDP - IPR

- Friday 15 November by 2359, pass/fail.
- Keep it short and simple. Answer Questions 1-2. Show progress toward one other problem.
- Signed cover sheet, PDF of Mathematica combined into single signed PDF (with signed cover sheet).
- Question 1 Txy plot in CHEMCAD using NRTL. Suggest you place a screen shot of CHEMCAD plot into Mathematica before bundling pdf.
- Question 2 Txy plot in MMA for ideal case. Suggestion: Txy plot in CHEMCAD using ideal, with screenshot into Mathematica, to show what "right looks like."
- Ideal Txy plot was done in CH362 and CH363. Problem 13.1 is a guide.



WPR3 WARNO

- WPR3 is Wednesday 20 November
- 3 problems, 200 points, from Chapter 5 and 6
 - Calculation of ideal enthalpy and entropy changes
 - Calculation of residual enthalpy and entropy
 - Combining formation, ideal and residual properties to get real properties
 - Lost work (as in heat exchangers)
 - Derivations property relations, Maxwell relations, generating functions
- 55 minutes, during class hour.
- Open note, open book, open computer. Calculator, Mathematica authorized.
- Upload all exam e-work to SharePoint.

Today's Agenda

- Complete discussion of residual properties
- Discussion of generalized methods
- Continue discussion of homework

Residual Properties

 $M^R \equiv M - M^{ig}$

superscript "R" refers to "residual"

(Eq. 6.41)



$$H^{R} = H - H^{ig}$$

$$S^{R} = S - S^{ig}$$

$$G^{R} = G - G^{ig}$$

$$H = H^{ig} + H^{R}$$

$$S = S^{ig} + S^{R}$$

$$G = G^{ig} + G^{R}$$

$$dH^{ig} = C_P^{ig} dT$$
(Eq. 6.23)

$$dS^{ig} = \frac{C_P^{ig}}{T}dT - R \cdot \frac{1}{P} \cdot dP$$
(Eq. 6.24)

$$H^{ig} = H_0^{ig} + \int_{T_0}^{T_2} C_P^{ig} dT$$

$$S^{ig} = S_0^{ig} + \int_{T_0}^{T_2} \frac{C_P^{ig}}{T} dT - R \cdot In \left(\frac{P}{P_0}\right)$$

$$V^{R} = V - V^{ig}$$

$$V^{ig} = \frac{P}{RT}$$

$$P$$

$$-V = \frac{ZRT}{P}$$

$$V^{R} = \frac{ZRT}{P} - \frac{RT}{P} = \frac{RT}{P}(Z-1)$$
(Eq. 6.40)

- The true worth of the equations for ideal gases is now evident.
- They are important because they provide a convenient base for the calculation of real gas properties.

Residual Properties from Cubic EOS

Generic cubic equation of state (in Z-Form)

(WPR3)

$$q = q(x) = \frac{\Psi \alpha(x)}{\Omega \cdot x}$$
 (Eq. 3.51)

 $\alpha = \alpha(\mathbf{X})$

(α is found in Table 3.1)

These are the red equations from L28 slide 8 (cleanup).

Important: α is written as a function of x where x replaces T_r .

q derivatives must be evaluated before process conditions (T_R , P_r) are entered.

Problem 6.141 in PS10

$$\beta = \Omega \frac{P_{r}}{T_{r}} \qquad (3.50)$$

$$Z = 1 + \beta - q\beta \frac{Z - \beta}{(Z + \epsilon\beta)(Z + \sigma\beta)}$$
(3.48)

$$\frac{H^{R}}{RT} = Z - 1 + T_{r} \left(\frac{dq}{dT_{r}} \right) \cdot I$$

(page 497)

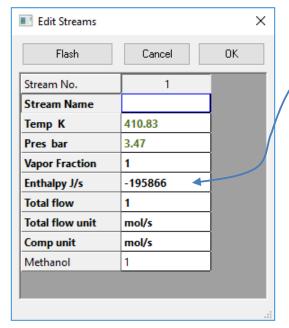
$$\frac{S^{R}}{R} = \ln(Z - \beta) + \left(q + T_{r} \frac{dq}{dT_{r}}\right) \cdot I$$

$$I = \frac{1}{\sigma - \varepsilon} \ln \left(\frac{Z + \sigma \beta}{Z + \varepsilon \beta} \right)$$
 (13.72)

Connection to Total Properties 6

Add ideal gas and residual

CHEMCAD



$$\begin{split} H &= H_0^{ig} + R \int\limits_{T_0}^T C_P^{ig} dT + H^R \\ &= H_0^{ig} + R \int\limits_{T_0}^{T_1} C_P^{ig} dT + H_1^R \\ H_1 &= H_0^{ig} + R \int\limits_{T_0}^{T_2} C_P^{ig} dT + H_1^R \\ &= H_0^{ig} + R \int\limits_{T_0}^{T_2} C_P^{ig} dT + H_2^R \end{split}$$

 $H_0^{ig} = \Delta H_{f298}^{o}$ = standard formation enthalpy, App C, pp 671-672

Difference between streams: residual property at
$$T_2$$

$$\Delta H = H_2 - H_1 = R \int_{T_1}^{T_2} C_P^{ig} dT + H_2^R - H_1^R \qquad \text{(Eq. 6.72)}$$

For CHEMCAD entropy, use Report -> Stream Reports -> Customize Property Sets -> Overall

$$S = S_0^{ig} + \int\limits_{T_0}^T C_P^{ig} \frac{dT}{T} - R ln \frac{P}{P_0} + S^R \\ \text{(Eq. 6.51)} \qquad \Delta S = \int\limits_{T_1}^{T_2} C_P^{ig} \frac{dT}{T} - R ln \frac{P_2}{P_1} + S_2^R - S_1^R \\ \text{(Eq. 6.73)}$$

 $S_0^{ig} = \Delta S_{f298}^{o}$, also from App C, pp 660-662, from ΔH_{f298}^{o} and ΔG_{f298}^{o}

CHEMCAD standard enthalpy and Gibbs energy are in Component Data -> Basic Data

$$\Delta S_{f298}^{ig} = \frac{\Delta H_{f298}^{ig} - \Delta G_{f298}^{ig}}{298.15}$$

Three Methods for Residual Properties

Cubic Equations of States (L28 & L29):

•RK, SRK, PR EOS from Table 3.1

Generalized Methods (New for Today):

- Lee-Kesler Tables
- Virial Equation of State

Lee-Kesler Table Method

Valid for liquids, vapors and gases

$$Z = Z^0 + \omega Z^1$$
 (Pitzer correlation, Eq. 3.53)

$$\frac{\mathsf{H}^{\mathsf{R}}}{\mathsf{R}\mathsf{T}_{\mathsf{c}}} = \frac{\left(\mathsf{H}^{\mathsf{R}}\right)^{0}}{\mathsf{R}\mathsf{T}_{\mathsf{c}}} + \omega \frac{\left(\mathsf{H}^{\mathsf{R}}\right)^{1}}{\mathsf{R}\mathsf{T}_{\mathsf{c}}} \tag{Eq.6.66}$$

$$\frac{S^{R}}{R} = \frac{\left(S^{R}\right)^{0}}{R} + \omega \frac{\left(S^{R}\right)^{1}}{R}$$
 (Eq. 6.67)

$$Z^{0}$$
, Z^{1} , $\frac{\left(H^{R}\right)^{0}}{RT_{c}}$, $\frac{\left(H^{R}\right)^{1}}{RT_{c}}$, $\frac{\left(S^{R}\right)^{0}}{R}$, $\frac{\left(S^{R}\right)^{1}}{R}$, ϕ^{0} , and ϕ^{1} Appendix D pages 676-692

Virial Equation

Truncated

$$Z = 1 + \frac{BP}{RT} = 1 + \hat{B}\frac{P_r}{T_r}$$
 (Eq.3.57)

$$\hat{B} = \frac{BP_c}{RT_c}$$
 (Eq.3.58)

Second virial coefficient

$$\mathbf{\hat{B}} = \mathbf{B}^0 + \omega \mathbf{B}^1$$

 $\hat{B} = B^0 + \omega B^1$ (Pitzer Correlation, Eq. 3.59)

$$\frac{H^{R}}{RT_{c}} = P_{r} \left[B^{0} - T_{r} \frac{dB^{0}}{dT_{r}} + \omega \left(B^{1} - T_{r} \frac{dB^{1}}{dT_{r}} \right) \right]$$
 (Eq. 6.68)

$$\frac{S^{R}}{R} = -P_{r} \left(\frac{dB^{0}}{dT_{r}} + \omega \frac{dB^{1}}{dT_{r}} \right)$$
 (Eq. 6.69)

$$B^{0} = 0.083 - \frac{0.422}{T_{r}^{1.6}} \qquad (Eq. 3.61) \qquad B^{1} = 0.139 - \frac{0.172}{T_{r}^{4.2}} \qquad (Eq. 3.62)$$

$$\frac{dB^{0}}{dT_{r}} = \frac{0.675}{T_{r}^{2.6}} \qquad (Eq. 6.70) \qquad \frac{dB^{1}}{dT_{r}} = \frac{0.722}{T_{r}^{5.2}} \qquad (Eq. 6.71)$$

Mixtures of Gases I - Textbook 10

The critical temperature of a gas is the maximum temperature at which compression can cause liquefaction. The critical pressure of a gas is the minimum pressure at which cooling causes liquefaction. Mixing of gases results in new critical properties for the mixture, and the mixture behaves as a "pseudocritical" pure component.

"pseudocritical" properties

$$\omega \equiv \sum_{i} y_{i} \omega_{i}$$
 (Eq. 6.78)

"pseudocritical acentric factor"

$$T_{pc} \equiv \sum_{i} y_{i} T_{ci}$$
(Eq. 6.79)

"pseudocritical temperature" subscript "p"

$$P_{pc} \equiv \sum_{i} y_{i} P_{ci}$$
(Eq. 6.80)

"pseudocritical pressure"

"pseudoreduced temperature"

$$T_{pr} = \frac{I}{T_{pc}}$$
(Eq. 6.81)

"pseudoreduced pressure"

$$P_{pr} = \frac{P}{P_{pc}}$$
(Eq. 6.82)

Mixtures of Gases II – API - Best 11

API Technical Data Book, T.T. Daubert, ed., 5th Edition, American Petroleum Institute, 1992. Standard method now widely used.

"pseudocritical" properties

worked example is in reference, p. 4-25

"true critical temperature" of mixture
$$T_{cm} = \sum_{i=1}^{11} (\theta_i \cdot T_{ci})$$
 (Eq. 4B1.1-1)

volume fraction of component i
$$\theta_i = \frac{x_i \cdot V_{ci}}{V_{pc}}$$
 (Eq. 4B1.1-2)

molar average critical volume
$$V_{pc} = \sum_{i} x_{i} \cdot V_{ci}$$
 (Eq. 4B1.1-3.79)

"true critical pressure" of mixture

$$P_{cm} = P_{pc} + P_{pc} \left[5.808 + 4.93 \cdot \sum_{i=1}^{n} (x_i \cdot \omega_i) \right] \cdot \left[\frac{T_{cm} - T_{pc}}{T_{pc}} \right]$$

worked example is in reference, pp. 4-28 to 4-29 (Eq. 4B2.1-1)

pseudocritical temperature of mixture
$$T_{pc} = \sum_{i} (x_i \cdot T_{ci})$$
 (Eq. 4B2.1-2)

pseudocritical pressure of mixture
$$P_{pc} = \sum_{i=1}^{n} (x_i \cdot P_{ci})$$
 (Eq. 4B2.1-3)

Questions?