
Problem Set 12 - Solutions

Problem 10.53

The molar volume ($\text{cm}^3 \text{ mol}^{-1}$) of a binary liquid mixture at T and P is given by:

$$V = 120x_1 + 70x_2 + (15x_1 + 8x_2)x_1x_2$$

- (a) Find expressions for the partial molar volumes of species 1 and 2 in terms of x_1 .
- (b) Show that the given equation for V is recovered when these expressions are combined using Eq. 10.11.
- (c) Show that these expressions satisfy Eq. 10.14.
- (d) Show that $(d\bar{V}_1/dx_1)_{x_1=1} = (d\bar{V}_2/dx_1)_{x_1=0} = 0$.
- (e) Make a plot of V, \bar{V}_1 , and \bar{V}_2 versus x_1 .
- (f) Label points V_1 , V_2 , $(\bar{V}_1)_{x_1 \rightarrow 0}$, and $(\bar{V}_2)_{x_2 \rightarrow 0}$ on the plot and show their values.

Common Information

```
In[1]:= Clear["Global`*"]  
In[2]:= x2 = 1 - x1;  
In[3]:= V = 120 x1 + 70 x2 + (15 x1 + 8 x2) x1 x2 // Expand  
Out[3]= 70 + 58 x1 - x1^2 - 7 x1^3
```

Part (a) - Find expressions for the partial molar volumes of species 1 and 2 in terms of x_1

```
In[4]:= V1bar = V + x2 * D[x1, V] // Expand (*Eq. 10.15, L34 Slide 16*)  
Out[4]= 128 - 2 x1 - 20 x1^2 + 14 x1^3
```

The partial molar volume of component 1 is $\bar{V}_1 = 128 - 2x_1 - 20x_1^2 + 14x_1^3$. //ANS

```
In[5]:= V2bar = V - x1 * D[x1, V] // Expand (*Eq. 10.15, L34 slide 16*)  
Out[5]= 70 + x1^2 + 14 x1^3
```

The partial molar volume of component 2 is $\bar{V}_2 = 70 + x_1^2 + 14x_1^3$. //ANS

Part (b) - Show that the given equation for V is recovered when these expressions (for \bar{V}_1 and \bar{V}_2) are combined using Eq. 10.11

```
In[1]:= ansb = x1 * V1bar + x2 * V2bar // Simplify (*Eq. 10.11, L34, slides 15 and 16*)
Out[1]= 70 + 58 x1 - x1^2 - 7 x1^3

In[2]:= ansb == V
Out[2]= True
```

Since $ansb == V$ generates “True” output, $x1 * \bar{V}_1 + x2 * \bar{V}_2$ is equal to V , and the original expression for V is recovered. //ANS

Part (c) - Show that these expressions satisfy Eq. 10.14

```
In[3]:= x1 * ∂x1 V1bar + x2 * ∂x1 V2bar // Simplify (*Eq. 10.14, L34, slides 15 and 16*)
Out[3]= 0
```

Since $x1 * \partial_{x1} \bar{V}_1 + x2 * \partial_{x1} \bar{V}_2 = 0$, Equation 10.14 is satisfied. //ANS

Part (d) - Show that $(d\bar{V}_1/dx_1)_{x_1=1} = (d\bar{V}_2/dx_1)_{x_1=0} = 0$

The ReplaceAll function (/.) is used to substitute $x1 \rightarrow 1$ into $d\bar{V}_1/dx_1$ and $x1 \rightarrow 0$ into $d\bar{V}_2/dx_1$:

```
In[4]:= ∂x1 V1bar /. x1 → 1
Out[4]= 0
```

```
In[5]:= ∂x1 V2bar /. x1 → 0
Out[5]= 0
```

Therefore $(d\bar{V}_1/dx_1)_{x_1=1} = 0$ and $(d\bar{V}_2/dx_1)_{x_1=0} = 0$, as requested. //ANS

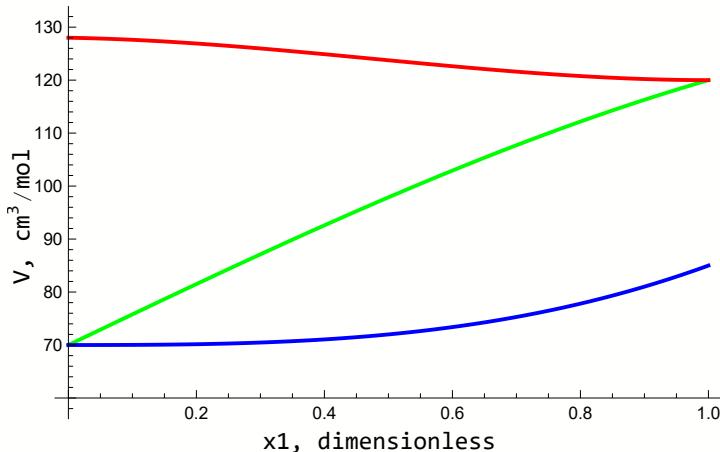
Part (e) - Make a plot of V , \bar{V}_1 , and \bar{V}_2 versus x_1

```
In[6]:= p1 = Plot[V, {x1, 0, 1}, PlotStyle → Blue];
p2 = Plot[V1bar, {x1, 0, 1}, PlotStyle → Red];
p3 = Plot[V2bar, {x1, 0, 1}, PlotStyle → Green];

In[7]:= p10 = Show[p1, p2, p3, PlotRange → {{0, 1}, {60, 130}}, AxesOrigin → {0, 60}];
```

```
In[1]:= Labeled[p10, {"V, cm3/mol", "x1, dimensionless"}, {Left, Bottom}, RotateLabel -> {True, False}]
```

Out[1]=



The required plot is shown above. //ANS

Part (f) - Label the points V_1 , V_2 , $(\bar{V}_1)_{x_1 \rightarrow 0}$, and $(\bar{V}_2)_{x_2 \rightarrow 0}$ on the plot and show their values

Use the provided template.

PLOT FUNCTIONS

```
In[2]:= f = V;
g = V1bar;
h = V2bar;
```

DEFINE THE PARTS OF THE LABELS

```
In[3]:= part1 = "V1";
part2 = f /. x1 -> 1;

part3 = "V2";
part4 = f /. x1 -> 0;

part5 = "(V̄1)x1 → 0";
part6 = g /. x1 -> 0;

part7 = "(V̄2)x2 → 0";
part8 = h /. x1 -> 1;
```

BUILDING THE LABELS

Connect the parts together to form labels.

```
(*label1=StringTemplate["`a` =`b`"] [<|"a"→part1,"b"→part2|>];
label2=StringTemplate["`a` =`b`"] [<|"a"→part3,"b"→part4|>];
label3=StringTemplate["`a` =`b`"] [<|"a"→part5,"b"→part6|>];
label4=StringTemplate["`a` =`b`"] [<|"a"→part7,"b"→part8|>];*)

In[1]:= label1 = StringForm["`1` =`2`", part1, part2];
label2 = StringForm["`1` =`2`", part3, part4];
label3 = StringForm["`1` =`2`", part5, part6];
label4 = StringForm["`1` =`2`", part7, part8];
```

PLOTS

PLOT OF LABELS AND POINTS

```
(*LABEL AND COORDINATE LISTS*)
coordinateList = {{1, part2}, {0, part4}, {0, part6}, {1, part8}};
labelList = {label1, label2, label3, label4};

(*INDIVIDUAL PLOTS*)
p1 = Plot[f, {x1, 0, 1}, PlotStyle → Blue];
p2 = Plot[g, {x1, 0, 1}, PlotStyle → Red];
p3 = Plot[h, {x1, 0, 1}, PlotStyle → Green ];

(*PLOT OPTIONS*)
option1 = PlotStyle → Red;
option2 = PlotMarkers → {Automatic, 9};
option3 = PlotRange → {{0, 1}, {60, 130}};
option4 = AxesOrigin → {0, 60};
option5 = {"V,  $\bar{V}_1$ ,  $\bar{V}_2$ , cm3/mol", "x1, dimensionless"};
option6 = {Left, Bottom};
option7 = RotateLabel → {True, False};

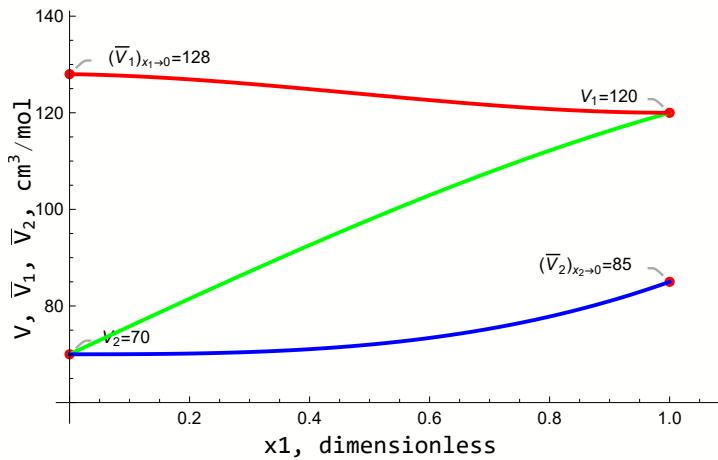
(*POINT/LABEL PLOT*)
p4 = With[
  {pts = coordinateList,
   labels = labelList}, ListPlot[Thread[Callout[pts, labels]], option1, option2]];
```

PLOT OF LABELED FUNCTION CURVES

```
In[]:= (*COMBINED PLOT*)
p11 = Show[p4, p1, p2, p3, option3, option4];
```

```
(*PLOT WITH AXIS LABELS*)
Labeled[p11, option5, option6, option7]
```

Out[]:=



Problem 10.18

Estimate the fugacity of isobutylene gas at 280 °C and

- (a) 1 bar
- (b) 20 bar, and
- (c) 100 bar.

Use the SRK equation of state.

```
In[1]:= Clear["Global`*"]
```

Part (a)

```

In[1]:= (*Temperature and Pressure*)
t = 280 + 273.15; (*K*)
p = 1.; (*bar*)

(*Isobutylene Properties from Table B.1, p.664*)
tc = 417.9; (*K*)
pc = 40.00; (*bar*)
ω = 0.194; (*not used in RK EOS*)

(*Reduced T and P*)
tr = t / tc; (*reduced temperature*)
pr = p / pc; (*reduced pressure*)

(*Equation of state supporting information from Table 3.1 page 100*)
σ = 1;
ε = 0;
Ω = 0.08664;
Ψ = 0.42748;
α[x_] = (1 + (0.480 + 1.574 * ω - 0.176 * ω^2) * (1 - √x))^2; (*Table 3.1*)

(*Equation of state*)
β = Ω * pr / tr; (*eq 3.50*)
q[x_] = (Ψ * α[x]) / (Ω * x); (*eq 3.50*)
eq1 = z = (1 + β - q[tr] * β * (z - β) / ((z + ε * β) * (z + σ * β))); (*Eq. 3.48*)

(*Solve for Z*)
z = z /. Solve[eq1, z, Reals][[1, 1]] // Quiet; (*//ANS*)

(*Solve for the Integral*)
I = 1/(σ - ε) * Log[(z + σ * β) / (z + ε * β)]; (*Eq. 13.72*)

(*Solve for Fugacity Coefficient*)
ϕ = Exp[z - 1 - Log[z - β] - q[tr] * I]; (*Eq. 13.85*)

(*Solve for Fugacity*)
f = ϕ * p

```

Out[1]=
0.996 8878

At P = 1 bar, f = 0.996888 bar. //ANS

Part (b)

Pressure is re-entered and all terms dependent on pressure must be re-calculated.

```
In[0]:= (*Update Pressure*)
p = 20.; (*bar*)

(*Update Reduced Pressure*)
pr = p / pc; (*reduced pressure*)

(*Update equation of state*)
β = Ω * pr / tr; (*eq 3.50*)
q[x_] = (Ω * α[x]) / (Ω * x); (*eq 3.50*)
eq1 = z = 
$$\left(1 + \beta - q[tr] * \beta * \frac{z - \beta}{(z + \epsilon * \beta) * (z + \sigma * \beta)}\right); (*Eq. 3.48*)$$


(*Re-solve for Z*)
Z = z /. Solve[eq1, z, Reals][[1, 1]] // Quiet; (*//ANS*)

(*Re-solve for the Integral*)
I = 
$$\frac{1}{\sigma - \epsilon} * \text{Log}\left[\frac{z + \sigma * \beta}{z + \epsilon * \beta}\right]; (*Eq. 13.72*)$$


(*Re-solve for Fugacity Coefficient*)
ϕ = Exp[Z - 1 - Log[Z - β] - q[tr] * I]; (*Eq. 13.85*)

(*Re-solve for Fugacity*)
f = ϕ * p
```

Out[0]=

18.79554

At P = 20 bar, f = 18.7955 bar. //ANS

Part (c)

```
In[1]:= (*Update Pressure*)
p = 100.; (*bar*)

(*Update Reduced Pressure*)
pr = p / pc; (*reduced pressure*)

(*Update equation of state*)
β = Ω * pr / tr; (*eq 3.50*)
q[x_] = (Ω * α[x]) / (Ω * x); (*eq 3.50*)
eq1 = z = 
$$\left(1 + \beta - q[tr] * \beta * \frac{z - \beta}{(z + \epsilon * \beta) * (z + \sigma * \beta)}\right); (*Eq. 3.48*)$$


(*Re-solve for Z*)
Z = z /. Solve[eq1, z, Reals][[1, 1]] // Quiet; (*//ANS*)

(*Re-solve for the Integral*)
I = 
$$\frac{1}{\sigma - \epsilon} * \text{Log}\left[\frac{z + \sigma * \beta}{z + \epsilon * \beta}\right]; (*Eq. 13.72*)$$


(*Re-solve for Fugacity Coefficient*)
ϕ = Exp[Z - 1 - Log[Z - β] - q[tr] * I]; (*Eq. 13.85*)

(*Re-solve for Fugacity*)
f = ϕ * p
```

Out[1]=

74.8573

At P = 100 bar, f = 74.8573 bar. //ANS

At higher pressure, molecules are forced closer together and thus experience greater IMFs and decreasing the fugacity.

Problem 10.21

From the data in the steam tables, determine a good estimate of f/f^{sat} for liquid water at 150°C and 150 bar, where f^{sat} is the fugacity of saturated liquid at 150°C.

SOLUTION

Use the Poynting factor from Eq. 10.44.

Use Table E.1 (saturated steam) on pages 697-703.

Table E.1 is for saturated steam in SI units (P in bar, T in °C, V in cm^3/g).

The temperature is given as 150°C - lookup in table on page 700.

P^{sat} is 4.76 bar - lookup.

$V^{\text{sat}} = 1.091 \text{ g/cm}^3$ - lookup.

Assume liquid is incompressible so that $V_i^{\text{sat}} = V^{\text{sat}}$.

```
In[°]:= Psat = 4.76; (*bar*)
MW = 18.015; (*g/mol*)
Vil = 1.091 * MW; (*molar volume of liquid; units  $\frac{\text{cm}^3}{\text{mol}} * \frac{\text{g}}{\text{mol}} = \frac{\text{cm}^3}{\text{mol}}$ *)
T = 150 + 273.15 ; (*K*)
P = 150; (*bar, given*)
(*Gas constant in  $\frac{\text{bar}\cdot\text{cm}^3}{\text{mol}\cdot\text{K}}$  from Table A.2*)
R = 83.14;
Poynting factor = f/f^sat;
(*Poynting factor = f/f^sat*)

In[°]:= PoyntingFactor = Exp[ $\frac{Vil * (P - Psat)}{R * T}$ ]
Out[°]= 1.084524
```

The Poynting factor is 1.084524. //ANS