CH365 Chemical Engineering Thermodynamics

Lesson 13
Cubic Equations of State

Corresponding States

Reduced T:
$$T_r \equiv \frac{T}{T_C}$$
 Reduced P: $P_r \equiv \frac{P}{P_C}$

Reduced P:
$$P_r = \frac{P}{P_0}$$

All fluids, when compared at the same reduced temperature and reduced pressure, have approximately the same compressibility factor, and all deviate from ideal-gas behavior to about the same degree.

Two-parameter models in terms of T_C and P_C works for simple fluids (Ar, Kr, Xe)

Three-parameter models are greatly improved: use T_C and P_C , and " ω "

"acentric factor"

$$\omega \equiv -1.0 - log(P_r^{sat})_{T_r = 0.7}$$

Eq. 3.52

Tables in App. B.1

- Introduced by Pitzer and coworkers
- Related to molecular structure
- Defined with respect to vapor pressure
- Difference between log of reduced vapor pressure of "simple" fluid and more complex fluids at T_r of 0.7

Example: n-Octane

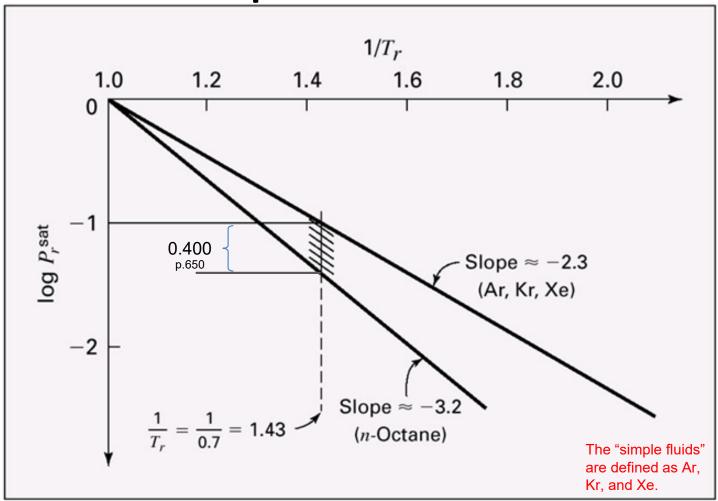


Figure 3.10: Approximate temperature dependence of the reduced vapor pressure.

3-Parameter Theorem of Corresponding States

Characteristic Properties of Pure Species, Table B.1, pages 663-665

	Molar Mass	ω	T _C K	P _c bar	Z _C	V _C cm³mol ⁻¹	T _n K
Methane	16.043	0.012	190.6	45.99	0.286	98.6	111.4
Ethane	30.070	0.100	305.3	48.72	0.279	145.5	184.6
Propane	44.097	0.152	369.8	42.48	0.276	200.0	231.1
n-Butane	58.123	0.200	425.1	37.96	0.274	255.	272.7
	-	÷	į	i	i	į	i
n-Octane	114.231	0.400	568.7	24.90	0.256	486.	398.8
	-	<u> </u>	į	į		į	į
Nitric Acid	63.013	0.714	520.0	68.90	0.231	145.	356.2
Sulfuric Acid	98.080		924.0	64.00	0.147	177.0	610.0

All fluids having the same value of ω , when compared at the same T_r and P_r , have about the same value of Z, and all deviate from ideal-gas behavior to about the same degree.

Pitzer Correlations

For next lesson; needed for Problem 3.44(b)

2nd Virial Coefficient

$$Z = 1 + \frac{BP}{RT} = 1 + \hat{B}\frac{P_r}{T_r}$$
 (Eq. 3.57 and 3.36) where $\hat{B} = \frac{BP_C}{RT_C}$ (Eq. 3.58)

Pitzer and coworkers

$$\mathbf{\hat{B}} = \mathbf{B}^0 + \omega \mathbf{B}^1$$
(Eq. 3.59)

$$B^0 = 0.083 - \frac{0.422}{T_r^{1.6}}$$
 (Eq. 3.61)

$$B^1 = 0.139 - \frac{0.172}{T_r^{4.2}} \tag{Eq. 3.62}$$

3rd Virial Coefficient

$$Z = 1 + B\rho + C\rho^{2} = 1 + \hat{B}\frac{P_{r}}{T_{r}Z} + \hat{C}\left(\frac{P_{r}}{T_{r}Z}\right)^{2} \text{ where } \hat{C} \equiv \frac{CP_{C}^{2}}{R^{2}T_{C}^{2}}$$
(Eq. 3.63 and 3.38)

$$\hat{\mathbf{C}} = \mathbf{C}^0 + \omega \mathbf{C}^1$$
(Eq. 3.65)

$$C^0 = 0.01407 + \frac{0.02432}{T_r} - \frac{0.00313}{T_r^{10.5}} \tag{Eq. 3.66}$$

$$C^1 = -0.02676 + \frac{0.05539}{T_r^{2.7}} - \frac{0.00242}{T_r^{10.5}} \tag{Eq. 3.67}$$

General Cubic Equations of State

$$P = \frac{RT}{V - b} - \frac{a}{(V + \varepsilon b)(V + \sigma b)}$$
(Page 97 Eq. 3.41)

Problem 3.44

$$\mathbf{a} = \Psi \frac{\alpha R^2 T_C^2}{P_C} \quad \text{(Eq. 3.45)}$$

$$\alpha = \alpha \left(\mathsf{T}, \mathsf{T}_C, \omega \right)$$

 α , Ψ , ϵ , σ , and Ω are defined in Table 3.1

$$T_r = \frac{T}{T_C}$$
 (reduced temperature)

T_c is the critical temperature, Table B.1

P_c is the critical pressure, Table B.1

R is the gas constant, Table A.2

$$b = \Omega \frac{RT_C}{P_C}$$
 (Eq. 3.44)

van der Waals

$$\alpha = 1$$
, $\epsilon = 0$ and $\sigma = 0$, T3.1

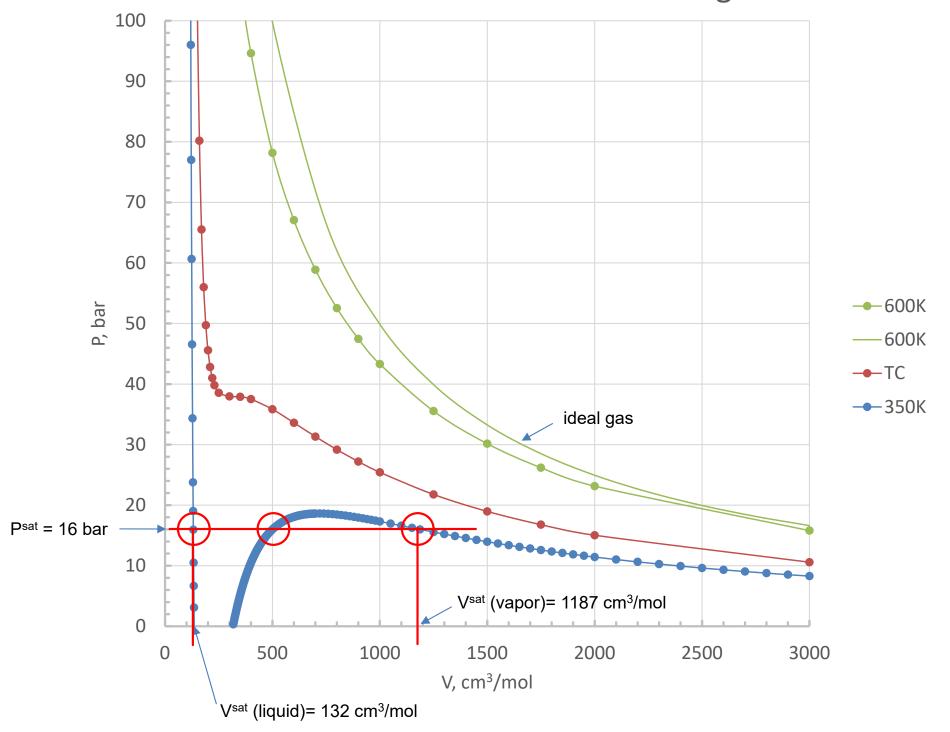
$$\Psi = \frac{27}{64}, \ \Omega = \frac{1}{8}, \ \alpha = 1, \ T3.1$$

$$P = \frac{RT}{V - b} - \frac{a}{V^2}$$

$$a = \frac{27}{64} \frac{R^2 T_C^2}{P_C}$$

$$b = \frac{RT_C}{8P_C}$$

n-Butane Isotherms from Redlich-Kwong EOS



Parameters for Cubic Equations

RK, SRK and PR equations of state were specifically developed for vapor-liquid calculations

Equation of State	α	σ	3	Ω	Ψ	Z _c
vdW	1	0	0	0.12500	0.42188	0.37500
RK	α_{RK}	1	0	0.08664	0.42748	0.33333
SRK	α_{SRK}	1	0	0.08664	0.42748	0.33333
PR	α_{PR}	$1+\sqrt{2}$	$1-\sqrt{2}$	0.07780	0.45724	0.30740

Smith, van Ness, Abbott, and Swihart, Table 3.1, page 100

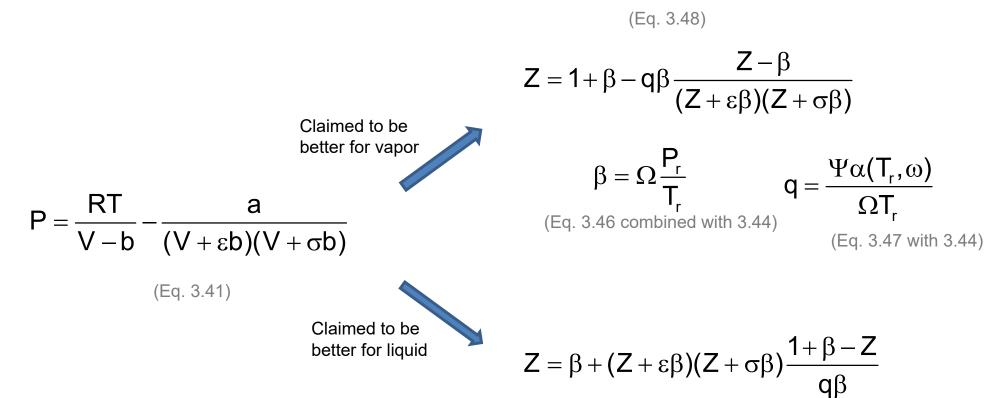
$$\begin{split} \alpha_{\text{RK}} = & 1 \! \! \left/ \sqrt{T_r} = \! T_r^{-1/2} \\ \alpha_{\text{SRK}} = & \left[1 \! + \! \left(0.480 + 1.574 \; \omega \! - \! 0.176 \; \omega^2 \right) \! \! \left(1 \! - \! \sqrt{T_r} \right) \right]^2 \\ \alpha_{\text{PR}} = & \left[1 \! + \! \! \left(0.37464 + 1.54226 \; \omega \! - \! 0.26992 \; \omega^2 \right) \! \! \left(1 \! - \! \sqrt{T_r} \right) \right]^2 \end{split}$$

vdW – van der Walls – 1873 RK – Redlich-Kwong – 1949 SRK – Soave-Redlich-Kwong – 1972 PR – Peng-Robinson – 1976

Example 3.9

Given that the vapor pressure of n-butane at 350 K is 9.4573 bar, find the molar volumes of (a) saturated vapor and (b) saturated liquid n-butane at these conditions as given by the Redlich-Kwong equation.

Eq. 3.41 gives three roots. Largest is vapor. Smallest is liquid.



Easy to demonstrate with "FindRoot" in Mathematica (numerical; requires initial guess)

(Ea. 3.49)

better for liquid

Questions