### ECEP 480 Solar Energy Engineering Rooftop PV Design

Group 01
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Winter 2021-22

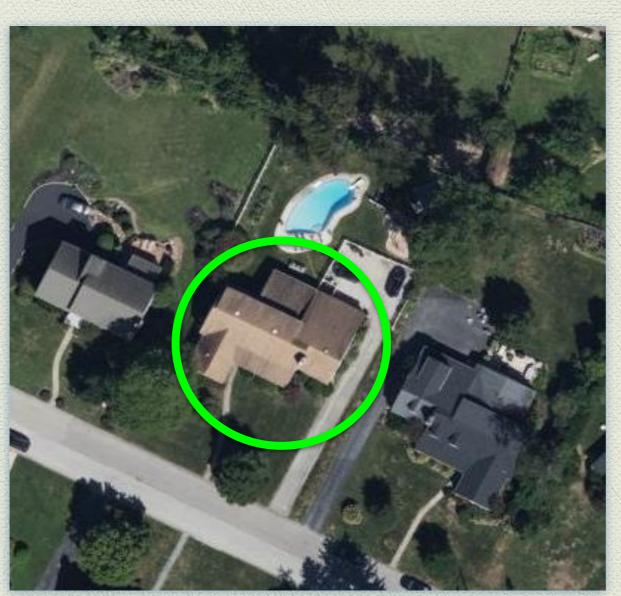
# Mhat is a PV system

- PV stands for photovoltaic
- Includes solar panels along with other components
- Electricity from sunlight



## The Project

3009 Robin Lane, Havertown, PA 19083



• Longitude: -75.34

• Latitude: 40.01

• Elevation: 111 meters

## Installation Overview





Active Surface	Area (m. sq.)	Azimuth (deg)					
1	14.49	116.8					
2	26.76	206.8					
3	37.4	206.8					
4	14.96	206.8					

#### Installation Overview

**Secondary Connection** 

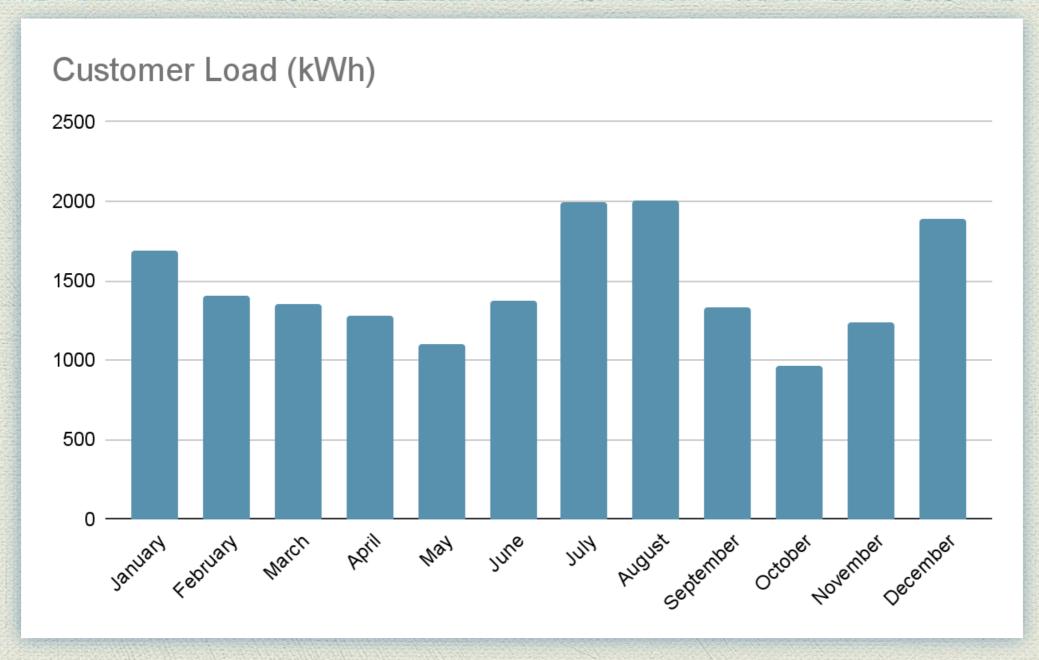


**Array Locations** 

Inverter

Meter

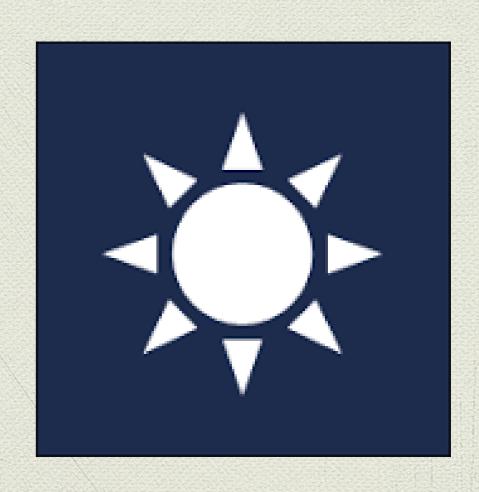
## Customer Load



Total: 17,631 kWh/year

#### What is SAM?

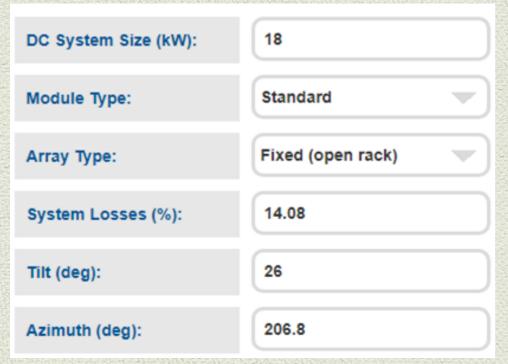
- Model many types of renewable energy systems
- Produce financial models for projects
- Used by
  - Project managers and engineers
  - Policy analysts
  - Technology developers
  - Researchers



# Initial Design

#### Initial PV energy supply goal: 100%

Estimate initially with 18kW gives 23,608kWh... Too much!



 $\left(\frac{17,631\text{kWh}}{23,608\text{kWh}}\right) \times 18\text{kW} = 13.443\text{kW}$ 

After calculating the actual power needed

DC System Size (kW):	13.443
Module Type:	Standard
Array Type:	Fixed (open rack)
System Losses (%):	14.08
Tilt (deg):	26
Azimuth (deg):	206.8

Array size needed: 13.443kWdc

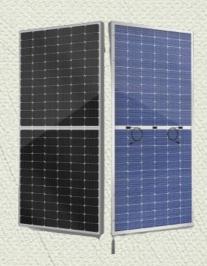
# Design Approach and Component Calculations - Initial Design

- Inverter Fronius USA: Fronius Primo 15.0-1 [240V]
  - o 15000W
  - o MPPT: 320V < V < 800
- Module Seraphim Energy Group Inc. SEG-440-BMA-BG
  - 440W (31 of them gives 13640W)
  - $\circ$  V<sub>OC Max</sub> of 55.48V
  - ∘ V<sub>M Min</sub> of 39.65
  - Operating Temperatures: -40°C < T < 85°C

- Could not fit allotted 31 modules for 100% of the load
- Inverter was oversized

# Design Approach and Component Calculations - Final Design

- Inverter Fronius USA: Fronius Primo 12.5-1 [240V]
  - o 12500W
  - o MPPT: 260V < V < 800
- Module Seraphim Energy Group Inc. SEG-440-BMA-BG
  - 440W (28 of them gives 12320W)
  - $\circ$  V<sub>OC Max</sub> of 55.48V
  - V<sub>M Min</sub> of 39.65
  - Operating Temperatures: -40°C < T < 85°C





## Determine String Size

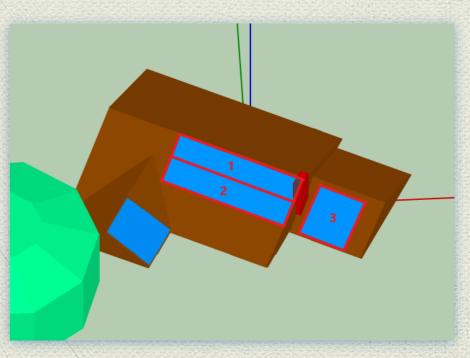
• Step 1: Determine V<sub>OC Max</sub> and V<sub>M Min</sub>

$$V_{m(min)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{max} - 25^{\circ}C\Big) \frac{\Delta V_{m}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min} - 25^{\circ}C\Big) \frac{\Delta V_{oc}}{\Delta T}\Big] \\ V_{oc(max)} = V \Big(25^{\circ}C\Big) \Big[1 + \Big(T_{min}$$

• Step 2: Determine maximum and minimum number of modules

$$\mathit{Modules}_{min} \, = \, \frac{\mathit{MPPT}_{(min)}}{V_{m(min)}} \qquad \mathit{Modules}_{max} \! = \! \frac{\mathit{MPPT}_{(max)}}{V_{oc(max)}}$$

- String size
  - 7 < #modules < 14 per string
  - Need 31 modules to satisfy 100% of the load
  - Can only fit 28 modules in our design



# Balance of System

Calculations Voltage Drop(%VD)	String of Modules	
Open Loop Length	78.6 ft	Total Wiring of System
One Way distance	39.3 ft	Total Wiring of System/2
Isc	11.3 A	Short Circuit Current
Im	10.6 A	Max Rated Current
VM(String)	331.2 V	8 * Vm per module
12 Awg (Ω/kft)	1.93	
%VD	0.485 %	

# Balance of System

- The connection between the junction box and inverter is 60ft and must carry the output of 2 strings.
  - o 18.2 m length (60 ft)
  - Conduit 2" above roof 100 °F (38 °C) ambient temperature
  - $\circ$  Isc = 11.3 A
  - $\circ$  Im = 10.6 A
  - o NEC 690.8(A) NEC 690.8(0.1)
    - 11.3 A x 156% is 17.628 A/string
    - $\blacksquare$  17.628 A x 2 = 35.256 A total

Table 4.13 Ambient Temperature Correction Factors for Conduit Run across Rooftops

Height of conduit above roof (in.)	0-0.5	0.5–3.5	3.5-12	>12
Add to ambient (°C)	33	22	17	14

- $\circ$  Conduit run temperature correction Table 4.13 38 + 22 = 60 °C
- Ambient temp ampacity correction Table 4.12 0.71 for 60 °C
- Derate based on the conduit fill factor of 1.0

$$\frac{(1.25 \times 11.3A)(2)}{(0.71)(1)} = 39.7A$$

with 90 C insulation	Table 4.12	Summary of Ambient Temperature Correction Factors for Wire with 90°C Insulation
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W	ith 90°C insui	ation			
Temp (°C)	21–25	26–30	31–35	36–40	41–45
Correction	1.04	1.00	0.96	0.91	0.87
Temp (°C)	46-50	51-55	56-60	61-65	66-70
Correction	0.82	0.76	0.71	0.58	0.41

# Balance of System

• The 30 °C ampacity must be no less than 39.7 A, or the higher of the two numbers. From Table 4.2, no less than 10 AWG, with a current of 40 A.

Table 4.2 Pro	Table 4.2 Properties of Copper Conductors with 90°C Insulation									
Size (AWG)	18	16	14	12	10	8	6	4		
dc ( $\Omega$ /kft)	7.77	4.89	3.07	1.93	1.21	0.764	0.491	0.308		
I <sub>max</sub> (A)	14	18	25	30	40	55	75	95		
Size	3	2	1	0	00	000	0000	250 kcm		
dc (Ω/kft)	0.245	0.194	0.154	0.122	0.0967	0.0766	0.0608	0.0515		
I <sub>max</sub> (A)	110	130	150	170	195	225	260	290		

At 10 AWG,

$$\% \, \text{VD} = \left[ \frac{0.2 \times (2 \, \text{Strings} \times 10.6 \, \text{A}) \times 60 \text{ft}}{8 \, \text{Modules} \times 41.4 \text{V}} \left( 1.21 \frac{\Omega}{\text{kft}} \right) \right] = 0.929 \, \%$$

• Total %VD = 0.485% + 0.929% = 1.414%

#### SAM Simulation

#### Modules

Seraphim Energy Group Inc. SEG-440-BMA-BG

Cell material Mono-c-Si

Module area 1.87 m<sup>2</sup>

Module capacity 440.08 DC Watts

Quantity 28

Total capacity 12.32 DC kW

Total area 52 m<sup>2</sup>

#### Inverters

Fronius USA: Fronius Primo 12.5-1

Unit capacity 12.5 AC kW

Input voltage 260 - 800 VDC DC V

Quantity 1

Total capacity 12.5 AC kW

DC to AC Capacity Ratio 0.99 AC losses (%) 1.00

Max Power: 440Wd

• V<sub>MP</sub>: 41.4Vdc

• V<sub>OC</sub>: 49.7Vdc

• I<sub>SC</sub>: 11.3Adc

• Efficiency: 23.53%



• AC Power: 12500 Wac

• DC Power: 13000Wdc

• AC Voltage: 240Vac

• MPPT: 260V < V < 800V



## SAM Simulation

#### Shading of Array on Main Roof

Subar	rray 1, S	tring 1	1									S	hade Los	ss (%):	0=no shade,	100=fully	shaded							
	12am	1am	2am	3am	4am	5am	6am	7am	8am	9am	10am	11am	12pm	1pm	2pm	3pm	4pm	5pm	брт	7pm	8pm	9pm	10pm	11pm
Jan	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0	17.9272	79.9065	100	100	100	100	100	100	100
Feb	100	100	100	100	100	100	100	21.1058	0	0	0	0	0	0	0	0	68.1785	100	100	100	100	100	100	100
Mar	100	100	100	100	100	100	100	47.7859	0	0	0	0	0	0	0	0	12.0882	100	100	100	100	100	100	100
Apr	100	100	100	100	100	100	100	27.3071	1.87219	0	0	0	0	0	0	0	0	8.04703	60.2649	100	100	100	100	100
May	100	100	100	100	100	100	21.7145	21.0974	3.67963	0	0	0	0	0	0	0	0	0.686169	13.5131	100	100	100	100	100
Jun	100	100	100	100	100	100	20.3818	20.3841	5.14998	0.119695	0	0	0	0	0	0	0	0.194212	5.92643	100	100	100	100	100
Jul	100	100	100	100	100	100	5.76923	22.3626	5.76721	0.0830392	0	0	0	0	0	0	0	0.152947	6.04519	100	100	100	100	100
Aug	100	100	100	100	100	100	100	26.4745	3.76018	0	0	0	0	0	0	0	0	0.974098	20.9492	100	100	100	100	100
Sep	100	100	100	100	100	100	100	25.8296	0	0	0	0	0	0	0	0	0.0363876	95.5534	100	100	100	100	100	100
Oct	100	100	100	100	100	100	100	6.53675	0	0	0	0	0	0	0	4.1268	100	100	100	100	100	100	100	100
Nov	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0	40.8157	99.9381	100	100	100	100	100	100	100
Dec	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0.00117603	41.2226	83.3976	100	100	100	100	100	100	100

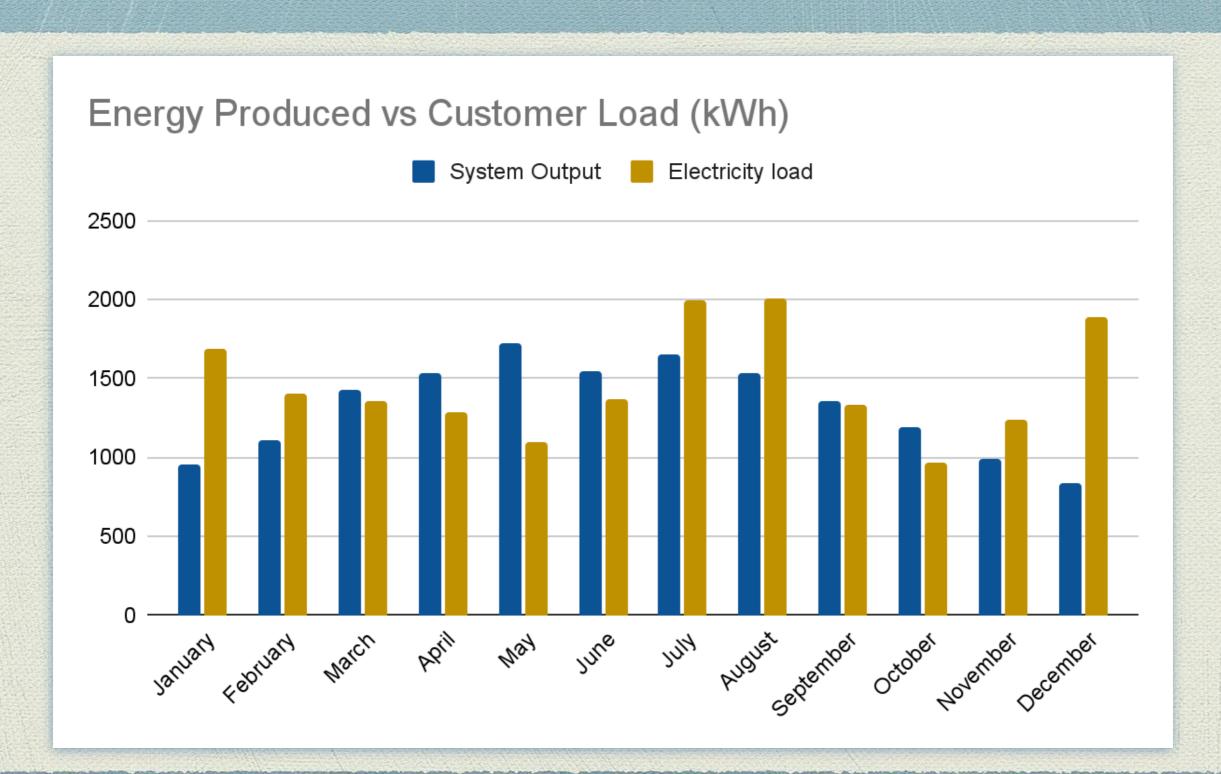
5	ubar	ray 1, S	tring 2	2									Sh	ade Loss	(%): 0=no	shade, 1	00=fully s	haded							
Matthe		12am	1am	2am	3am	4am	5am	6am	7am	8am	9am	10am	11am	12pm	1pm	2pm	3pm	4pm	5pm	6pm	7pm	8pm	9pm	10pm	11pm
	lan	100	100	100	100	100	100	100	78.3495	31.6852	15.8896	10.0708	6.53271	4.71397	2.54548	2.0098	3.49737	86.4112	100	100	100	100	100	100	100
SA-TAN	eb	100	100	100	100	100	100	100	56.2716	35.1073	17.0317	9.89079	6.4482	4.00102	2.31258	1.85157	1.61538	41.6202	99.9311	100	100	100	100	100	100
Month	Mar	100	100	100	100	100	100	100	29.1048	25.8658	15.2276	9.41153	5.90167	3.39398	1.40905	1.48153	1.80925	2.09976	84.6156	100	100	100	100	100	100
	Apr	100	100	100	100	100	100	100	18.0589	18.1542	12.0455	7.7443	4.88971	2.47456	1.11331	1.2013	1.69382	1.17316	1.31826	2.30794	100	100	100	100	100
	May	100	100	100	100	100	100	8.70555	13	13.6113	9.61926	6.23778	3.37078	1.4755	1.37486	1.21952	1.17871	1.38976	0.955026	1.18527	100	100	100	100	100
	lun	100	100	100	100	100	100	8.12898	10.8441	11.9985	9.82846	6.04416	3.98407	1.15014	1.03111	1.20815	1.22793	1.14052	1.54007	0.723337	100	100	100	100	100
2000	lul	100	100	100	100	100	100	21.4162	11.235	12.8491	10.2205	6.7773	3.97994	1.68276	1.0694	1.11859	1.21021	1.36753	1.19354	0.976274	100	100	100	100	100
	Aug	100	100	100	100	100	100	100	14.6717	16.1392	11.1511	7.19818	4.80439	2.05039	0.82807	1.70312	1.23934	1.19383	1.36119	1.75896	100	100	100	100	100
	Бер	100	100	100	100	100	100	100	25.2862	20.6461	12.8443	8.20394	5.40757	2.59148	1.38944	1.70179	1.1973	2.08203	35.084	100	100	100	100	100	100
	Oct	100	100	100	100	100	100	100	48.6042	23.1554	13.068	8.16767	5.05996	3.09535	1.77817	1.87921	1.67651	88.1981	100	100	100	100	100	100	100
No.	VoV	100	100	100	100	100	100	100	69.5814	23.2443	13.0036	8.11265	5.36148	3.39316	1.89715	1.96313	20.0015	100	100	100	100	100	100	100	100
	Dec	100	100	100	100	100	100	100	62.1953	24.4157	13.1591	8.81242	5.77304	3.94217	2.33529	2.08202	24.7504	94.3109	100	100	100	100	100	100	100

## SAM Simulation

#### Shading of Array on Garage Roof

Suba	rray 2, S	tring 1	1											Shade	Loss (%):	0=no sha	ade, 100=1	fully shad	led					
	12am	1am	2am	3am	4am	5am	6am	7am	8am	9am	10am	11am	12pm	1pm	2pm	3pm	4pm	5pm	брт	7pm	8pm	9pm	10pm	11pm
Jan	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0	1.9152	26.5861	100	100	100	100	100	100	100
Feb	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0	3.7487	24.9822	100	100	100	100	100	100	100
Mar	100	100	100	100	100	100	100	0	0	0	0	0	0	0	1.18132	9.19712	30.0749	100	100	100	100	100	100	100
Apr	100	100	100	100	100	100	100	0	0	0	0	0	0	0	5.53689	18.0922	40.1534	90.5798	100	100	100	100	100	100
May	100	100	100	100	100	100	0	0	0	0	0	0	0	0.77507	9.5307	25.3044	50.7883	85.4122	100	100	100	100	100	100
Jun	100	100	100	100	100	100	0	0	0	0	0	0	0	1.1445	10.2262	26.2483	52.449	82.0617	100	100	100	100	100	100
Jul	100	100	100	100	100	100	0	0	0	0	0	0	0	0.191702	8.70424	23.5255	48.0631	79.014	100	100	100	100	100	100
Aug	100	100	100	100	100	100	0	0	0	0	0	0	0	0	6.48571	19.6052	41.5624	78.9364	100	100	100	100	100	100
Sep	100	100	100	100	100	100	100	0	0	0	0	0	0	0	3.72688	15.3708	38.8456	99.8661	100	100	100	100	100	100
Oct	100	100	100	100	100	100	100	0	0	0	0	0	0	0	1.57274	13.3951	79.9331	100	100	100	100	100	100	100
Nov	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0.23021	10.7482	45.1789	100	100	100	100	100	100	100
Dec	100	100	100	100	100	100	100	0	0	0	0	0	0	0	0	5.40911	35.3424	100	100	100	100	100	100	100

#### SAM Results



## SAM Financials

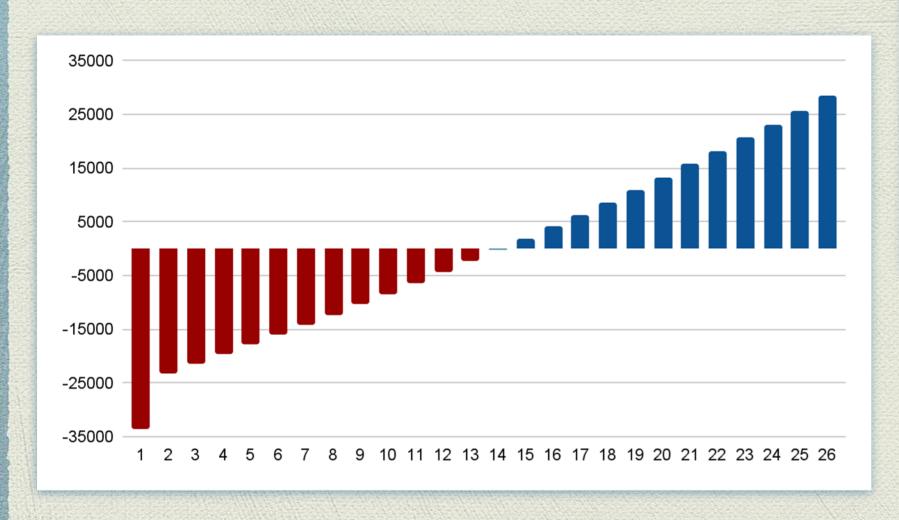
Incentives	
Federal ITC 26%	SRECS

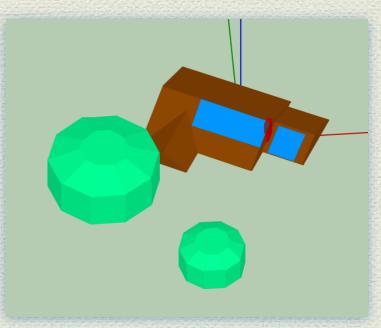
Electricity Demand and Rate Summary											
Fixed charge \$10.02/month											
Monthly excess kWh rollover											
Flat energy buy rate	\$0.13245/kWh										

System Overview	
Annual Energy	15,858kWh
Performance Ratio	0.73
Energy bill without system	\$2,455/year
Energy bill with system	\$414/year
Net Savings	\$2,041/year
Net Present Value	\$8,309
Simple payback period	13.1years
Net capital cost	\$33,535

### Conclusions

#### Payback Cashflow (\$)





Renewable Factor: 89.9%

NPV: \$8,300

**Electricity Bill Savings:** 83.1%

#### References

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https://www.seraphim-energy.com/wp-content/uploads/download/SRP-(430-445)-BMA-BG\_Frame\_166.pdf

https://sam.nrel.gov/

# THANK YOU!

Questions?