

Measuring charged current neutrino interactions in the Electromagnetic Calorimeters in near detector of T2K

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TODO

A thesis submitted to Imperial College London
for the degree of Doctor of Philosophy

Abstract

To write

Declaration

This dissertation is the result of my own work, except where explicit reference is made to the work of others, and has not been submitted for another qualification to this or any other university. This dissertation does not exceed the word limit for the respective Degree Committee.

Dominic Brailsford

Acknowledgements

Something about my supervisor ...

Preface

This thesis describes my analysis of the ν_μ charged-current cross-section on lead using the T2K near detector electromagnetic calorimeters.

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“These chickens jackin’ my style. ”

— Fergie

Chapter 1

Introduction

“I’ve got that boom boom pow”

— Fergie

Introduce neutrinos here [1–3].

1.1 Neutrino Oscillations

Neutrino oscillations are really kool

Chapter 2

The T2K Experiment

The Tokai-to-Kamioka (T2K) experiment [4] is a long baseline neutrino oscillation experiment located in two sites across Japan which was designed to study the parameters governing the PMNS matrix. The first site is the J-PARC facility in Tokai-mura on Japan's east coast which houses a 30 GeV proton accelerator complex that is used to generate a highly pure ν_μ beam. J-PARC also contains a suite of detectors designed to measure the neutrino beam's unoscillated characteristics. Super-Kamiokande (SK) is located 295 km (see Fig. 2.1) and measures the contents of the neutrino beam post-oscillation.

T2K was the first experiment to observe the $\nu_\mu \rightarrow \nu_e$ appearance channel [5] which excluded $\theta_{13} = 0$ at 7.3σ significance. By comparing this result with precise θ_{13} measurements from reactor experiments, δ_{CP} regions can be excluded at 90% confidence level (see Fig. 2.2). T2K's precision analysis of the ν_μ disappearance channel provide world leading measurements of θ_{23} and Δm_{23}^2 . Independently of the oscillation analyses performed by the experiment, T2K's near detectors, ND280 and INGRID, are used to measure a range of neutrino cross-sections [6,7]. While this is not the primary aim of T2K, such measurements are still extremely important as T2K systematic uncertainties can be constrained with additional cross-section knowledge as well as helping to understand the general neutrino interaction picture.

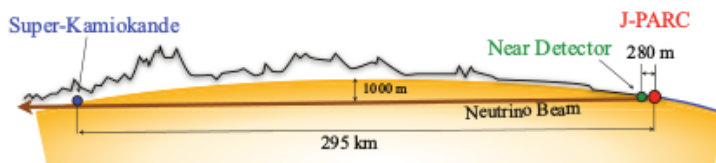


Figure 2.1: The T2K experiment.



Figure 2.2: The 68% and 90% confidence level allowed regions for $\sin^2 2\theta_{13}$ as a function of δ_{CP} for normal hierarchy (top) and inverted hierarchy (bottom). The solid line represents the best fit $\sin^2 2\theta_{13}$ for a given δ_{CP} . The shaded region shows the average θ_{13} provided by the reactor constraint [5].

2.1 T2K beam

The T2K neutrino beam is generated by J-PARC's accelerator complex which produces a 30 GeV proton beam which is fired at a fixed graphite target. The final state particles of interactions with the target are predominately charged pions which decay to produce the neutrino beam. Surrounding and behind the graphite target are a set of magnetic horns which focus the pions into a beam, resulting in a focused neutrino beam after the hadrons have decayed.

2.1.1 Accelerator complex

The J-PARC accelerator complex consists of three sections: the LINnear ACcelerator (LINAC), the Rapid-Cycling Synchrotron (RCS) and the Main Ring synchrotron (MR). Production of the proton beam starts at the LINAC where H^- anions are accelerated to 181 MeV which are subsequently converted to h^+ ions via charge-stripping foils at the RCS injection point. With a 25 Hz cycle, the ions are further accelerated by the RCS



Figure 2.3: A schematic of the T2K neutrino beamline (left) and a side view of the secondary beamline (right).

to 3 GeV with two bunches per cycle. Roughly 5% of the proton bunches are fed into the MR where the final acceleration to 30 GeV occurs in bunches of eight. Extraction of the bunches occurs at two points for different experiments. For T2K, all eight bunches are extracted in a single turn by five kicker magnets and aimed down the neutrino beamline to the graphite target. The extraction of all eight bunches forms a single beam spill with a width of 5 μ sec. The tight structure of the beam spills is vital for background discrimination in the downstream detectors.

2.1.2 Neutrino beamline

The neutrino beamline (NU) is split into a primary and secondary beamline, a schematic of which is shown in Fig. 2.3. The primary beamline consists of a preparation section, an arc section and a focussing section. The preparation section uses 11 normal conducting magnets to tune the proton beam for entry into the arc section where the proton beam is bent to its intended direction. As will be discussed in more detail in section 2.1.3, the axis of the beam is 2.5° away from SK. The final focussing sections then guides the proton beam into the secondary beamline and the graphite target. Sound performance of the proton beam is vital for stability of the T2K neutrino beam. To ensure such performance, the primary beamline is equipped with a suite of monitors to measure the position, profile, loss and intensity of the proton beam. The beam position is measured by 21 electrostatic monitors (ESMs) which consists of four cylindrical electrodes surrounding the beam. The asymmetry of the beam is measured by the induced current in the electrodes is used to infer the position in a non-destructive

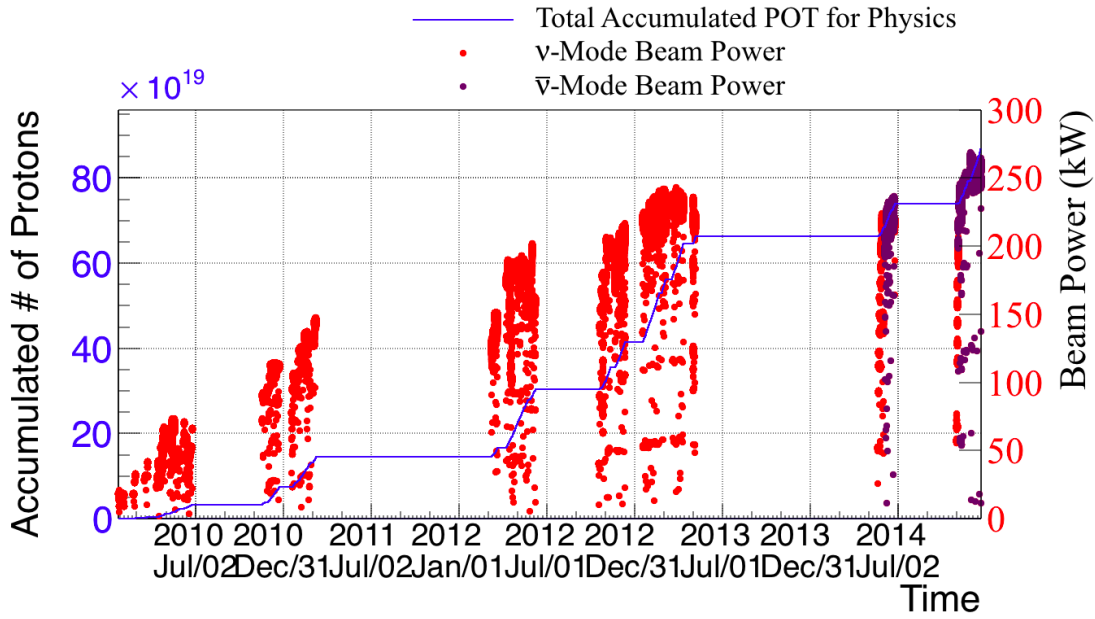


Figure 2.4: The POT recorded by CT5 as a function of time (blue line) and the recorded beam power in ν running mode (red dot) and $\bar{\nu}$ running mode (purple dot).

manner. Segmented secondary emission monitors (SSEMs) are used to measure the beam loss. Each SSEM has an anode foil sandwiched between two titanium foil strips. Protons interact with the strips causing an emission of electrons which electrically drift inducing a current in the strips. The charge distribution is used to reconstruct the profile. The beam loss monitors (BLMs) are Ar-CO₂ filled wire proportional counters and are used to for beam loss. The intensity of the beam is measured by five current transformers (CT) which consist of a 50-turn toroidal coil around a ferromagnetic coil. Passage of the beam induces a current in the coil which is used to infer the number of protons in the spill. The final CT (CT5) is positioned at the end of the focussing section of the primary beamline and is used to count the number of protons incident on the graphite target. The accumulated number of protons on target (POT) is used as a metric for the data collected by T2K. The total POT accumulated so far by T2K is shown in Fig. 2.4.

The secondary beamline consists of the graphite target, a set of magnetic focusing horns, a decay pipe and a beam dump. A schematic for the secondary beamline is shown in Fig. 2.3. The graphite target is a 2.6 cm diameter and 91.4 cm long rod which is surrounded by a 2 mm thick graphite tube and a 0.3 mm titanium case. The proton-graphite interactions produce charged pions and kaons which are focussed by three magnetic horns, one of which surrounds the target. The magnetic horns consist of two coaxial conductors which generate a magnetic field with a strength inversely

proportional to the distance from the beam axis. The current direction in the magnetic horns causes the induced field to focus or deflect particles depending on their charge sign. This simple control allows T2K to operate in ν or $\bar{\nu}$ beam mode. The focused mesons then travel down a decay pipe filled with Helium to reduce pion absorption. It is here that the mesons decay to produce the neutrinos used as the T2K beam. To stop measurement contamination, other decay products must be stopped before reaching the downstream detectors. So, a 75 ton graphite beam dump is positioned at the end of the decay volume. The beam dump stops almost all non-wanted decay products, with only 5 GeV or above muons successfully propagating through. As the muons are generally simultaneously produced with the beam neutrinos, measurements of the muon can be used to monitor the direction of the neutrino beam. To do this, a muon monitor (MUMON) is installed at the downstream end of the beam dump.

2.1.3 Off-axis beam

The kinematics of the pion decays dictate the energy spectrum shape of the neutrinos. Specifically, the peak width of the neutrino energy narrows and shifts as an observer moves off-axis from the pions trajectory. As the pions are the neutrino parents in the T2K beam, the same effect can be seen by moving off-axis from the neutrino beam. This effect is illustrated in Fig. BLAH. By positioning T2K's baseline detectors at 2.5° off-axis, it is possible to align the neutrino beam's peak energy with the first oscillation maximum for the ν_μ disappearance channel. Separately, an off-axis configuration reduces the beam's unwanted high energy tail, improving sensitivity to ν_e appearance and ν_μ disappearance.

2.2 Near detector complex

Stuff about complex

2.2.1 Multi-Pixel Photon Counter

MPPCs

2.2.2 INGRID

Stuff about INGRID

2.2.3 ND280

ND280 time

2.2.3.1 The fine grain detectors

FGDS

2.2.3.2 The time projection chambers

TPCs

2.2.3.3 The π^0 detector

Here is ref for [2.2.3.2](#) pi0

2.2.3.4 The electromagnetic calorimeters

The beasts

2.2.3.5 The side muon range detector

Why bother?

2.2.4 The far detector

I mean SK

Chapter 3

ND280 software and existing ECal event reconstruction

The T2K experiment uses a bespoke software suite for simulation and analysis of ND280 data which is based on the ROOT framework [8]. The vast majority of the ND280 software suite utilises the oaEvent library which provides a unified framework for information manipulation and was specifically designed for this purpose. As ND280 consists of many subdetectors each providing a specific function, the ND280 software suite is designed to reflect this. Not only are there specific software modules for individual subdetectors, there are specific modules for each phase of the subdetector information processing e.g. trip-T calibration, TPC reconstruction etc.

As the software suite handles both production of simulated data and the processing of collected data, there are sections of the software chain which are specific to type of data being processed. While the Monte Carlo simulation and real data do see different areas of the software chain, the general philosophy is to manipulate the Monte Carlo or the real data to a point where they can be treated as equals and then process them in the same manner. So, the description of the software will follow the same path: the Monte Carlo and real data specifics will be discussed first and then the unified treatment will follow.

3.1 Monte Carlo production software

As described above, parts of the software chain are unique to simulated data processing. Specifically, the simulation of the beam and the detector response need to be modelled

before the Monte Carlo can be treated on equal footing with the real data. This special processing is split into several steps, all of which are described below.

3.1.1 Neutrino flux simulation

The neutrino flux simulation uses Fluka2011 [9] and a software set called JNUBEAM to model the J-PARC neutrino beam. The process begins by using Fluka2011 to simulate the 30 GeV protons incident on the graphite target and their subsequent secondary interactions which produce the neutrino parent mesons. The kinematic information of the hadrons is then passed to the JNUBEAM simulation. JNUBEAM is based on GEANT3 [10] and models the J-PARC secondary beamline. The hadrons are tracked through the decay volume and are allowed to interact or decay to produce the simulated neutrino beam. Importantly, all information associated with the daughter neutrinos and their parents are saved at this point. By storing this information, the neutrino flux can be readily re-weighted to include new information associated with beam profile measurements or external data.

The main external tuning source is NA61/SHINE which is a hadron interaction experiment that uses a 31 GeV/c proton beam colliding with changeable targets [11]. For use in the T2K flux simulation, NA61/SHINE has collected data using two graphite targets: one with a 4% nuclear interaction length thickness and a full T2K replica target. The flux simulation used for this analysis is tuned using full replica target data. Observed differences between the fluka2011 simulation and NA61/SHINE data are used to re-weight the simulated neutrino flux.

Additionally to the external data tunings measurements of the T2K beam profile are also used to re-weight the flux. By making such measurements on a run-by-run basis, the simulated flux can be re-weighted to better model variations of the neutrino beam in each data run.

3.1.2 Neutrino interaction simulation

After the neutrino flux has been modelled, simulation of the neutrino interactions with the T2K detectors follows. The NEUT [12] event generator is used to simulate interactions with ND280. The inputs to the interaction simulation are a neutrino vector file produced by the beam simulation and a ROOT based ND280 geometry. The used geometry includes the magnetic field return yoke and everything contained

within. Using the inputs, NEUT tracks the neutrino and calculates the probability of interaction for every material in crosses. To calculate the interaction probability, the potential interaction nucleus must be modelled. For this, NEUT uses two models; the Moniz-Smith Relativistic Fermi Gas (RFG) [13] and the O. Benhar spectral function models [14]. The spectral functions are only implemented for carbon, oxygen and iron so the model used depends on the atomic number of the interaction candidate nucleus. It is important to note at this point that this thesis deals with neutrino interactions on lead, so it is the RFG model that is used for signal interactions.

The main interactions modes at T2K energies are quasi-elastic scattering (CCQE), single pion production ($CC1\pi$) and deep inelastic scattering (DIS) all of which have models in NEUT [15–17].

After the initial interactions, the final step is to simulate the final state interactions within the nucleus. Each particle involved with the interaction is pushed through the nucleus in discrete steps with the probability of a final state interaction being calculated at each step. If an interaction occurs, the final states of that interaction are also included in the subsequent steps. This iterative procedure models the particle cascade until all the final states have reached the nucleus boundary. At this point, all final state particles are recorded along with all information that created those particles. This information is stored in a vector file and passed onto the ND280 detector MC package which handles the detector's response to these final state particles.

3.1.3 ND280 detector simulation

The simulation of the final state particles in ND280 is handled by `nd280mc` which is based on Geant4 [18] and ROOT. The neutrino interaction vector files are taken as input and used as seeds in the detector simulation. The neutrino vector inputs are not organised according to the J-PARC beam bunch structure so the detector simulation first groups the interactions into spills. The beam intensity being simulated is used to define how many interactions occur in a spill with Poisson fluctuations applied to that number. The timing of the beam bunch structure is then used to group the interactions into bunches.

`nd280mc` constructs a ROOT geometry of ND280 based on the design specifications of its subdetectors and then propagates the particles given to it by the neutrino generator through the geometry, simulating energy deposition, scattering and particle decay during propagation.

3.1.4 Detector response simulation

The next and final stage of the MC-only software chain is to model how the detector responds to the simulated particles propagating through it. The detector response software, named `elecSim`, takes the output of `nd280mc` and models how the active regions of the detector would respond given an energy deposition in that region of the detector. In the case of the calorimeters, `elecSim` handles the production of light produced by the constituent scintillator bars, how the light is propagated along the wavelength-shifting fibres and how the MPPCs would respond to the incident photons. For the TPCs, the drift of the ionisation electrons through the gas and the subsequent response of the MicroMEGAS which receive them. In all cases, the readout electronics response is simulated to produce a data-like output format. This step concludes the section of the software chain which is specific to the MC.

3.2 Real data processing software

The real data specific section of the software chain is very short. Physics events deemed worth saving by any of the ND280 triggers are recorded by the detector and then saved for processing. The MIDAS file format is used for storing the saved ND280 events. All of the relevant information needed to process the event is stored in the MIDAS file, so the only unique step to the data processing is the conversion of the MIDAS file to the `oaEvent` format. After the step, the `oaEvent` data files are exposed to the same software as MC files outputted by `elecSim` (see section [3.1.4](#)).

3.3 Main software chain

The aim of the rest of the software chain is to process the readout from the detector, be it simulated or collected signal, and process it so that essential information about the physics of the event can be extracted. This is separated into three steps: calibration, reconstruction and data reduction/summarising.

3.3.1 Detector calibration

The software package responsible for overseeing all aspects of the calibration stage is called oaCalib. This controlling package passes the digitised signal from ND280 to dedicated calibration packages for the various kinds of readout electronics. All of the information which can be extracted from an ECal event relies on the charge read by the MPPCs. Thus, for the Trip-T detectors, like the ECals, the main aim of the calibration is to remove all electronic effects so that an accurate estimation of the charge read by the MPPCs can be made.

Firstly, every MPPC is held at a bias in the absense of any signal to remove the non-linear dependence of the detector response on the lowest ADC channels. This zero signal output is called the pedestal and must be subtracted from the charge readout by the MPPC.

To estimate the number of photo-electrons produced in an MPPC, The readout charge is divided by the MPPC gain. The breakdown voltage of an MPPC linearly varies with temperature (approximately $50 \text{ mV}/^{\circ}\text{C}$). This translates to a percent level variation in the MPPC gain per degree. This means small variations in temperature can cause a significant variation in the MPPC gain. So, the gains for each channel are calculated and stored individually.

The time of the signal read by the MPPC is charge dependent so it relies on the above corrections. However, there are extra steps needed to get an accurate estimate of the timestamp. The MPPC signal is given a timestamp once the charging capacitor exceeds a threshold value. The time it takes to reach this threshold depends on the final collected charge of the MPPC. This means that a lower charge signal would receive a later timestamp than a higher charge signal even if the signals occurred at the same time. This effect is known as the electronic timewalk and is corrected for.

The light emission rate of the WLS fibres follows an exponential decay function which means that the emission rate depends on the total number of photo-electrons. As described above, the Trip-T electronics only assign a timestamp once the collected charge passes a threshold. So, the fibre decay causes a separate timewalk effect, called the fibre timewalk effect which is also corrected for.

3.3.2 Event reconstruction

Once the information has been calibrated it is passed to the ND280 reconstruction software. The reconstruction algorithms are separated into two phases: the local reconstruction and the global reconstruction. The local reconstruction, which is run first, is separated into a set of algorithms specific to each subdetector. Each subdetector reconstruction attempts to form its own picture of the event which passed through it. After this, all of the local reconstruction information is passed to the global reconstruction which attempts to match and refit the subdetector results to maximise the amount of extractable information.

3.3.3 Data reduction and summarising

The final stage of the processing chain is to reduce and summarise all of the previous steps in the chain such that they are in a suitable format for the analyser. A lot of the information, particularly from the reconstruction stage, is stripped out and the physics related objects are extracted. Most importantly, all of the information is summarised in a pure ROOT format, meaning the analyser does not rely on the oaEvent library to analyse ND280 data.

3.4 ECal event reconstruction

As mentioned in section 3.3.2, part of the reconstruction process is to run algorithms specific to the ND280 subdetectors. The ECal is no exception and is equipped with an extensive suite of reconstruction algorithms designed to reconstruct events originating from the tracker region of ND280. The inputs to the reconstruction are the calibrated scintillators bar hits which are used to form 3D objects and attach a topology hypothesis.

3.4.1 Hit preparation

The initial ECal reconstruction stage takes the hits outputted by the calibration stage and prepares them for the downstream algorithms. The ECal hits arrive with timestamps but are not separated according to the bunch structure. So, the hits are ordered

in time and then grouped into buckets where a new bucket starts when a greater than 50 ns gap appears between two time-adjacent hits. A second filter is then applied to arrange the hits according to the sensor they occurred on. For double ended bars with both sensors activated, the time of the hit is re-estimated by averaging the timestamp of the two sensors. The two hits are then merged to form a single hit.

It is then necessary to apply extra calibrations to the charges of the hits. The effect of light attenuation along the WLS fibre is corrected for and a scaling is applied to convert the charge into MIP equivalent units (MEU).

3.4.2 Basic clustering

The time ordered hits are then passed to a set of clustering algorithms which attempts to form an object out of the ECal hits. The first stage of this is called basic clustering which is a nearest neighbour algorithm designed to form 2D clusters of hits for both views of an ECal module. This is initiated by forming a 30 ns window and searching for the highest charge hit contained within it to form a seed. The seed cluster is expanded by searching for and adding candidate hits which pass the following criteria:

- Is located in the 30 ns time window
- Is at most one bar away from a hit in the cluster
- Is at most two layers away from a hit in the cluster

To qualify as a basic cluster, any formed cluster must contain at least three hits. The successfully formed clusters in both views of the ECal modules are then passed to the next stage of the clustering algorithms.

3.4.3 Cluster combination

The second stage of the clustering algorithm takes the basic clusters in a given view and attempts to form merged clusters if a set of conditions are passed. The cluster with the highest number of hits is taken as a seed and compared with all other clusters in the same view. A Principal Components Analysis (PCA) is applied to all 2D clusters as the primary axis is used in one of the merging criteria. A candidate cluster is merged with the seed cluster if:

- The distance of closest approach, taken from the primary axes, of the candidate and seed cluster is less than 80 mm
- The charge weighted average hit times of the candidate cluster is within 40 ns of the seed cluster
- The charge weighted average distance of the candidate cluster to the seed cluster is less than 400 mm

All candidate clusters which pass the conditions are merged with the seed cluster. After all comparisons have been made, a new seed cluster is found and the process is repeated until no more merges take place. All clusters in each ECal view are then passed into the next clustering algorithm.

3.4.4 Cluster expansion

The next and final stage of the 2D clustering attempts to merge any unmatched hits with the already formed clusters if the comparison passes a set of conditions. As before, a PCA is applied to all 2D clusters to calculate the primary and secondary axes as these are used in one of the matching conditions. Let \vec{n}_{pri} and \vec{n}_{sec} be the primary and secondary axes of a cluster found by the PCA. The squared spread of the cluster along the primary or secondary axis is then defined as

$$\sigma_A^2 = \sum_{\alpha=x,y,z} \sigma_\alpha^2 n_{A,\alpha}^2 \quad (3.1)$$

where A refers to either the primary or secondary axis and σ_α refers to the cluster's spread along the cartesian axes. A metric for defining well the hit matches to the cluster can then be defined as

$$w = \sqrt{\left(\frac{\vec{H} \cdot \vec{n}_{\text{pri}}}{\sigma_{\text{pri}}}\right)^2 + \left(\frac{\vec{H} \cdot \vec{n}_{\text{sec}}}{\sigma_{\text{sec}}}\right)^2}, \quad (3.2)$$

where H is the vector joining the charge-weighted centre of the cluster and the centre of the hit. The unmatched hit is merged with the 2D cluster if:

- The unmatched hit is within 6 ns of one of the constituent hits of the 2D cluster

- The difference in bar number of the unmatched hit and at least one of the constituents hits in the 2D cluster is less than 11
- The difference in layer number of the unmatched hit and at least one of the constituents hits in the 2D cluster is less than 21
- The calculate value of w is less than 50

Unlike the previous stage where it is possible to merge every cluster in a view, an unmatched hit can be matched with one, and only one, 2D cluster. So, not only does the hit-cluster comparison have to pass the relevant criteria, the comparison has to be a better match than all other comparisons. In cases where the unmatched hit passes all of the conditions with more than one cluster, the comparison which provides the lowest w is selected as the best match.

The 2D clusters in each view are then passed onto the final stage of the clustering algorithms.

3.4.5 3D cluster formation

The final stage of the clustering algorithm attempts to form full 3D clusters information from both view of an ECal module. To do this, the algorithm takes the 2D clusters from one view and matches them with the 2D clusters in the other view. All 2D clusters from one view are compared to all 2D clusters in the other view and the two that are the best match form a 3D cluster. The metric used for the matching is a simple likelihood based on three input variables. The first variable is the ratio of the total charge in 2D matching candidate clusters, Q_{ratio} . Assuming the two 2D clusters come from the same particle, the amount of charge deposited in each view should be similar, so Q_{ratio} should be ~ 1 . The Q_{ratio} value is then compared with a probability density function generated using ND280 MC to retrieve $\mathcal{L}_{Q_{\text{ratio}}}$. The second input variable to the likelihood compares the first layer used by the two matching candidate clusters which is closest to the ND280 tracker region, $\Delta_{\text{layer, first}}$. If the two candidate clusters are created from the same particle, the difference in starting layer number should ideally be one. As with Q_{ratio} , the $\Delta_{\text{layer, first}}$ found for the matching candidates is compared to a probability density function to retrieve $\mathcal{L}_{\Delta_{\text{layer, first}}}$. The final input to the likelihood is almost identical to the second input. The variable, called $\Delta_{\text{layer, last}}$ compares the difference in layer number furthest away from the ND280 tracker region. Besides this difference, $\Delta_{\text{layer, last}}$ is treated in exactly the same manner as $\Delta_{\text{layer, first}}$

and so will not be described in any more detail.

Once the three inputs for the matching candidates have been calculated, the value of the matching likelihood is then

$$\mathcal{L} = \mathcal{L}_{Q_{\text{ratio}}} \times \mathcal{L}_{\Delta_{\text{layer, first}}} \times \mathcal{L}_{\Delta_{\text{layer, last}}} \quad (3.3)$$

As mentioned above, all 2D clusters in one view are compared with all 2D clusters in the other view. The matching pair which produce the highest value of \mathcal{L} are counted as a match. The matched pair are then removed from the pool and the process is repeated until no more matches can be made or the value of \mathcal{L} falls below e^{-5} . All matched clusters are now counted as 3D objects and are passed onto the rest of the ECal reconstruction algorithms.

3.4.6 3D hit reconstruction

So far in the ECal reconstruction, it has only been possible to reconstruct 2/3 of the hit coordinates have been estimated. However, now that full 3D clusters have been formed, the information from both ECal views can be used to estimate the 3rd hit coordinate which is the coordinate along the length of the bar.

The hits are separated into their respective 2D view and then the charge-weighted average position of each view is calculated. Then, to calculate the final hit coordinate, the nearest four layers from the other view are found and a linear least-squares fit is applied to their 2D coordinates. The line found is then extrapolated into the layer of interest which provides the unknown hit coordinate.

3.4.7 Energy reconstruction

The ECal was designed to catch electromagnetic particles originating from the tracker region of ND280, particularly photons from π^0 decays. An integral part of particle shower reconstruction is estimation of the total energy of the incoming particle. So, the next phase of the reconstruction is particle energy estimation under the assumption that the incident particle created a full contained particle shower upon entering the ECal module. The range of the energy fitter is 25 MeV to 20 GeV which almost fully covers the range of energies seen in the ND280 ECals. The energy fitter works by minimising a likelihood function which takes the total charge, charge RMS and charge

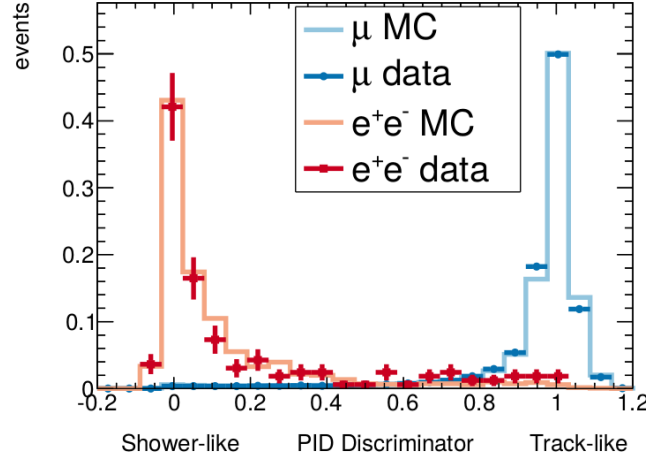


Figure 3.1: The track-like/shower-like discriminator for the DS-ECal. Solid lines show the control sample Monte Carlo and the point show the control sample data.

skew of the 3D cluster as inputs. For each of the three input variables, splines were generated using simple photon particle gun MC which relates the input variables to the true particle energy. The minimizer generates an estimate of the true energy and, via the splines, retrieves the expected values of the input variables. By minimising the distance between the measured input variables and those taken from the splines an accurate estimate of the particle energy is found. This energy estimate, along with the 3D cluster itself is then passed onto the final section of the ECal reconstruction.

3.4.8 Event classification

The final section of the ECal reconstruction is to attach a topology hypothesis to the 3D cluster. The routines currently separate the clusters into two categories: those that are shower-like and those that are track-like using an Artificial Neural Network. This multi-variate analysis object takes multiple pieces of information about the 3D cluster which attempts to measure the energy deposition and shape of the cluster and returns a single number. The value of the returned number suggests whether the reconstructed object is track-like or shower-like. The discriminator was tested using ND280 electron and muon control samples, the results of which are shown for the DS-ECal in Fig. 3.1.

Chapter 4

Enhanced ECal reconstruction

The current implementation of the ECal reconstruction software was designed to reconstruct particles which originate from the ND280 tracker and enter the ECal. As section 3.4 shows, this was realised by only considering ECal hit clusters under the single track-like or shower-like hypothesis. It should be evident that a neutrino interaction occurring within the ECal does not well fit this topology. While it is true that there is some power in the current reconstruction to distinguish a neutrino interaction from an entering track or shower, there is little feature information available. How many final state particles propagated from the interaction? How much visible energy was deposited by each of the particles? Where in the ECal did the interaction occur? These basic questions can not be trivially answered when using the current reconstruction. To maximise the ability of distinguishing ECal neutrino interactions from entering backgrounds, the reconstruction must be revisited.

4.1 The Hough transform

The Hough transform is a popular method of machine pattern recognition used by, but is not limited to, high energy physics experiments. Originally designed for machine track recognition in bubble chamber pictures [19], the version most widely used throughout the world was developed in 1972 [20]. The Hough transform is used to isolate specific features or shapes from a digital image. The simplest implementation, which is of most interest in event reconstruction, allows the extraction of straight, 2D lines from a complex pattern. This is achieved by exploitation of a very simple feature of 2D geometry.



Figure 4.1: Line in 2D cartesian space.

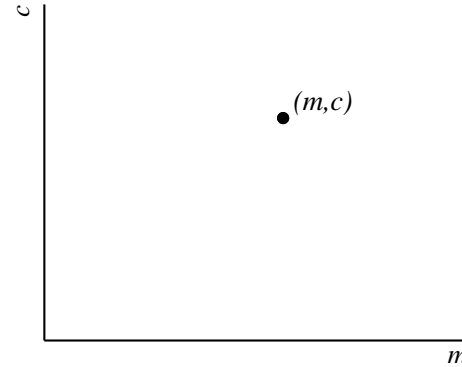


Figure 4.2: Point in 2D parameter space.

4.1.1 Line-point duality

Consider a straight line formed in a 2D cartesian space as shown in Fig. 4.1. The line is usually described by

$$y = mx + c \quad (4.1)$$

where y and x are used as coordinates, m is the gradient of the line and c is the intercept location of the line with the y axis. While it is not necessary to analyse this simple shape in great detail, it is important to note that m and c are the only parameters necessary to completely describe the line.

Now consider a new 2D space where the axes are defined by m and c rather than x and y (here after referred to as the parameter space). As this parameter space is described by the parameters of a general 2D cartesian line, there is an underlying symmetry between the two spaces. The parameters of the 2D line shown in Fig. 4.1 can be used to form a pair of coordinates (m, c) in the parameter space as shown in Fig. 4.2. It is important here to state clearly the general result; a straight line in cartesian space is represented by a single point in parameter space.

Now consider the 2D cartesian space again. Unlike before, we will define a single point rather than a straight line. Such a point is traditionally described by a pair of coordinates (x, y) . However, an alternative description of the point is an infinite number of lines all of which pass through (x, y) . This is highlighted by Fig. 4.3 where three lines of the infinite set are shown along with the point they represent. As the



Figure 4.3: Point in 2D cartesian space.



Figure 4.4: Line in 2D parameter space.

infinite line set are used to describe a single point, all lines in the set must follow a pattern. This relationship is revealed by simple algebraic manipulation of equation 4.1 to give

$$c = -xm + y. \quad (4.2)$$

Despite the manipulation, equation 4.2 still resembles the equation of a 2D line, however the parameters are x and y and the coordinates are m and c . Specifically, equation 4.2 is represented by a line in the parameter space defined above. The gradient of this line is

$$x = \frac{\Delta c}{\Delta m} \quad (4.3)$$

and the intercept of the line with the c axis is y as shown in Fig. 4.4. As before, it is important to clearly state what has been shown; a point in cartesian space is represented by a line in parameter space.

4.1.2 The parameter space

As section 4.1.1 shows, there is a clear relationship between the cartesian space and the parameter space. Specifically, there is a symmetry between lines and points in the two spaces. This relationship between the cartesian and parameter spaces is not only interesting but also very powerful. Consider again the parameter line defined by equation 4.2 and shown in Fig. 4.4. As shown in section 4.1.1, equation 4.2 was derived by considering the infinite set of lines which pass through a cartesian point. As this

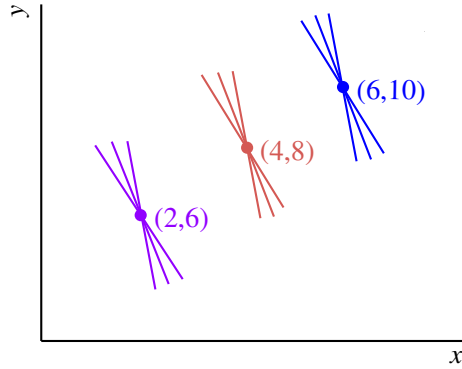


Figure 4.5: The three cartesian points defined in equation 4.4. The colour coding matches that of Fig. 4.6.



Figure 4.6: The three parameter lines defined in equation 4.5. The same colour coding as Fig. 4.5 is used.

infinite set represents the parameter line, it must also be true that the parameter line represents the infinite line set. Using one of the results from section 4.1.1, any point along the parameter line represents one of the lines from our infinite set. This key feature of the parameter space is the central component of the Hough transform.

We will now return to the cartesian space for an example of how the Hough transform works. Let's define three points in this space,

$$\begin{aligned} p_1 &: (2, 6) \\ p_2 &: (4, 8) \\ p_3 &: (6, 10). \end{aligned} \tag{4.4}$$

The three points defined in equation 4.4 are shown in Fig. 4.5. Using one of the results from section 4.1.1 and equation 4.2, the three points can be Hough transformed into the following parameter lines:

$$\begin{aligned} c &= -2m + 6 \\ c &= -4m + 8 \\ c &= -6m + 10. \end{aligned} \tag{4.5}$$

The three parameter lines are shown in Fig. 4.6. From Fig. 4.6, it is clear that the three parameter lines all cross at a common point with parameter space coordinates



Figure 4.7: The line represented by the intersection in Fig. 4.6 with the cartesian points it intercepts.

(2,4). Using the results from section 4.1.1, this common point in parameter space is represented by a line in cartesian space. In addition, as (2,4) is common to all three parameter lines, the cartesian line represented by (2,4) must also pass through all three cartesian points defined by equation 4.4. This new cartesian line is defined by

$$y = 2x + 4 \quad (4.6)$$

and is shown in Fig. 4.7 with the original points used to generate the parameter lines. While this example is relatively simple, it demonstrates the capability of the Hough transform to recognise linear patterns in sets of points.

4.1.3 Redefinition of parameters

Unfortunately, a complication in computation arises when $m \rightarrow \infty$. However, this complication can be removed by redefining the line parameters such that one is bounded. An alternative 2D line parameterisation is to specify a line in terms of the angle it makes with the x axis, θ , and the perpendicular distance of the line from the origin, ρ , as illustrated in Fig. 4.8. The functional form of the cartesian line becomes

$$y = x \tan \theta + \frac{\rho}{\cos \theta}. \quad (4.7)$$

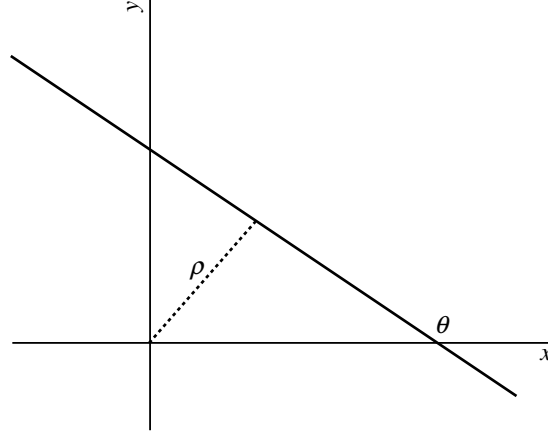


Figure 4.8: $\theta - \rho$ parameterisation of a 2D line.

Using this new parameterisation, we must also define a new parameter space with axes θ and ρ . Using equation 4.7, a line in this new parameter space is defined by

$$\rho = y \cos \theta - x \sin \theta. \quad (4.8)$$

By definition, the θ axis of the parameter space must be bounded to the interval $[0, 2\pi]$. If the directionality of the line is meaningless to the analyser, then the interval can be restricted to $[0, \pi]$.

The disadvantage of this parameterisation is that parameter line generation now involves trigonometric calculations which can be computationally expensive. However, this problem is small when compared to the unbounded complication of the traditional parameterisation.

4.1.4 Discretisation of the parameter space

It must now be considered how the parameter space is analysed. When a large number of parameter lines are generated, it becomes computationally expensive to analyse the resultant parameter space. While approaches exist to analyse the parameter space with very high precision [21], it is often only necessary to extract parameters with finite resolution. In such a case, it is convenient to discretise the parameter space. Under this regime, the parameter space is split into $\theta - \rho$ bins. Then, a parameter line is generated



Figure 4.9: The discrete $\theta - \rho$ space. The plotted lines are those defined in equation 4.5 and reparameterised using equation 4.8.

by incrementing the value of each $\theta - \rho$ bin it passes through. After each line has been added to the parameter space, the crossing locations can be readily found by searching for the $\theta - \rho$ bins with content larger than unity. An example of this discretisation is illustrated in Fig. 4.9, where the parameter lines defined in equation 4.5 have been re-parameterised using equation 4.8 and plotted. The content of each bin in Fig. 4.9 records how many of the three parameter lines pass through each bin. The bin with value 3 is the crossing point of the three parameter lines.

If a discretised approach is acceptable, which is the case in event reconstruction, construction and analysis of the parameter space is reduced to filling a 1D array N times, where N is the number of parameter lines, followed by a 1D grid search of the array to find the bin with the highest content.

4.2 ECal application of the Hough transform

We must now address how the Hough transform can be used as a reconstruction tool in the ECal. To do this, let's consider a neutrino interaction which occurs in the ECal as illustrated in 4.10. While the propagating neutrino is invisible to the ECal, the charged final state are definitely not. To first order, the final state particles propagate in straight lines depositing energy in the scintillator bars as they go. From this, we can infer that

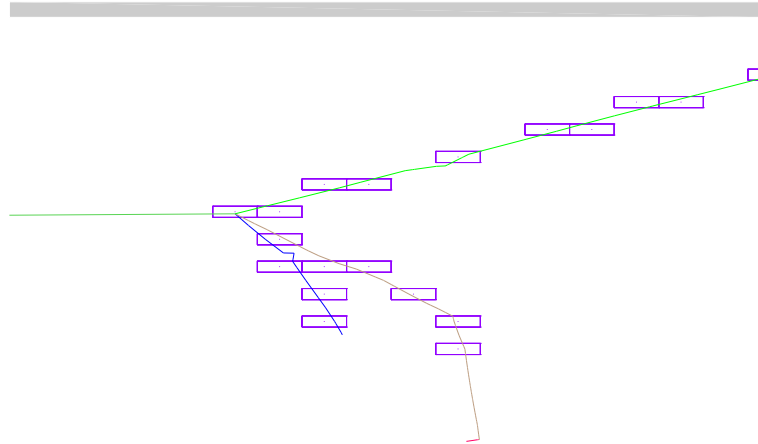


Figure 4.10: Simulated neutrino interaction with 3 final states in the side-right ECal. The green line entering from the left is the ν_μ . The green line exiting to the right is a μ^- , the brown line is a π^+ and the blue line is a proton. The purple rectangles represent the hit ECal bars.

the hit bars arranged in straight lines should reveal the trajectory of the final states. As shown above, the Hough transform is capable of identifying straight lines from a set of coordinates. However, there are two complications in the ECal which the above sections have not addressed. We have only specifically discussed how to extract a single straight line from a pattern. As Fig. 4.10 shows, the number of final states can be, and is often, greater than one. This is merely a problem of computation which will be addressed in section 4.2.3. A much more severe problem is that the above demonstrations only deal with patterns constructed from infinitesimal points. While the centre of a scintillator bar can be used as a point for parameter line generation, it is unlikely that a final state particle will pass through the central point of the scintillator bars that it propagates through. If this is not addressed, the Hough transform will be of little use in trajectory reconstruction.

4.2.1 Modelling the ECal bar

To make the Hough transform viable as a reconstruction tool, the finite dimensions of the ECal bar need to be incorporated into the parameter space generation. This feature of the ECal bars would be very problematic if the parameter space was continuous. However, it is only necessary to know the line parameters with finite resolution and a discrete parameter space can be used. This means that the ECal bar can be modelled



Figure 4.11: Grid representation of an ECal bar.

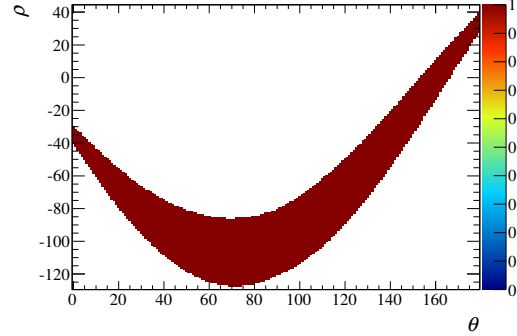


Figure 4.12: Single ECal bar Hough transform using the point configuration shown in Fig. 4.11.

as a set of cartesian points and each of said points can be Hough transformed in turn to build up the parameter line representation of the ECal bar.

There are now two steps to consider. Firstly, how should the points be arranged? Remember that the Hough transform of a point represents all of the lines that pass through that point. So, the points should be arranged in such a fashion that any line which passes through the 2D cross-section of the ECal bar also has to pass through one of the points in the configuration. Secondly, the spacings between the points should be small enough that no gaps appear in the generated parameter line.

Assuming that every bin of the parameter space will have a $1^\circ \times 1$ mm area, an obvious choice would be to use a rectangular grid of points with 1 mm spacing superimposed over the 2D cross-section of an ECal bar. The total number of points used to model the ECal bar is 451. To Hough transform the ECal bar, every point in the grid array can be Hough transformed individually with care taken to ensure that each $\theta - \rho$ bin is filled exactly once. The result is illustrated in Fig. 4.12. The finite size of the ECal bar is evident by the finite size of the resultant parameter line.

While the generated parameter line accurately represents every line which passes through the ECal bar, there are two problems with this approach. Firstly, the large number of points to be Hough transformed is very large which results in a long CPU time. Secondly, there is a very high number of redundant calculations involved in the parameter line generation. Consider an exactly vertical line which passes through one of the points in the grid array. This line also passes through 10 other points in the



Figure 4.13: Cross representation of an ECal bar.



Figure 4.14: Single ECal bar Hough transform using the point configuration shown in Fig. 4.13.

same column of the grid. This means that when the parameter line is being generated, this vertical line is calculated 11 times for each column. Barring this in mind, there are many points along the parameter line which are repeatedly calculated and provide no extra information. This would mean that any algorithm which uses this approach would be very CPU inefficient.

An alternative is to model the ECal bar as a set of points arranged in a cross as shown in Fig. 4.13. Assuming that the spacing between the points on each line of the cross is infinitesimal, any line which passes through the ECal bar would also have to pass through one of the points in the configuration. As the parameter space is discrete, the spacing between the points need not be infinitesimal but only small enough to ensure that no gaps appear in the parameter line. Using 45 points on each line of the cross, the ECal bar can be Hough transformed by Hough transforming each point in the cross. An example of this result is shown in Fig. 4.14 using the same ECal bar used to generate Fig. 4.12. Clearly, Fig. 4.12 and Fig. 4.14 are identical showing that the cross model achieves the same result as the grid model. Comparing the two, the cross model uses a 90 point representation whereas the grid model uses a 451 point representation. This should mean that an algorithm utilising the cross model would be a factor of five faster than one using a grid model.

4.2.2 Parameter space generation

As we have addressed how to Hough transform an ECal bar, we are now in suitable position to generate the full parameter space for an ECal cluster. As described in



Figure 4.15: The full parameter space of the 2D cluster shown in Fig. 4.10.

section 4.1.3, the parameterisation of the 2D lines requires some point in space to act as the origin. It is possible to use the origin defined by the global ND280 geometry, however this is located in TPC 1 which would mean ρ will usually be the order of metres. It is more convenient to define an origin in the vicinity of the ECal cluster being reconstructed. A simple option is to use the charge-weighted centre of the ECal cluster as the origin of the Hough transform. This location is simple to calculate and generally keeps ρ small.

The provided description of the Hough transform in all previous sections is strictly defined in 2D and so the ECal cluster should be split in such a way that this definition can be used. Fortunately, a 3D ECal cluster is built up using the two 2D views that the scintillator layers provide. So, it is relatively easy to split the 3D cluster into a pair of 2D clusters by collecting the cluster's hits into their respective 2D views.

We can now partly answer one of the problems raised in section 4.2 which is how to handle the track multiplicity aspect of the reconstruction? This is partly addressed by generating N parameter spaces with the same $\theta - \rho$ bin configuration where N is the number of hits in the 2D cluster. Each of the N parameter spaces will hold one parameter line generated by one of the 2D hits (in a similar fashion to Fig. 4.14). The final parameter space can then be generated by adding together each of the N parameter spaces. The parameter space of the 2D cluster in Fig 4.10 is shown in Fig. 4.15.

4.2.3 Parameter space analysis

The full parameter space can look arbitrarily complicated. However, it contains a vast amount of trajectory related information about the cluster. Every $\theta - \rho$ bin of the parameter space describes a 2D track and the content value of said bin describes how many 2D ECal hits the track passes through. As described in section 4.2, a particles trajectory should be straight in the ECal which means that the particles path should be revealed by finding the most hits arranged in a line. This hit arrangement can be found by finding the bin in the full parameter space with the highest value. The track candidate parameters can be found by fetching the (θ, ρ) coordinate of the found bin.

While the preferred bin can reveal how many hits the track candidate passed through, it contains no information about which hits were contributors. However, this full parameter space was generated by summing the N parameter spaces discussed in section 4.2.2. So, the contributing hits can be readily found by looking at the same (θ, ρ) bin in each of the N parameter spaces and recording which have a non-zero value. We now have the track candidate's parameters and its contributing hits which is enough to describe the 2D trajectory.

A new search now needs to begin to find any other track candidates. However, repeating the same search of the full parameter space will return the track candidate that has already been found. To find the next track candidate, the presence of the previous track candidate must be removed. So, a reduced parameter space must be generated. The previous step found which of the N parameter lines contributed to the previous track candidate. So, this new parameter space can be formed by subtracting the contributing parameter lines from the full space. An example of this is shown in Fig. 4.16 where the reduced parameter space was formed by subtracting the contributing parameter lines to the highest bin in Fig. 4.15. The next track candidate can then be found by searching for the highest content bin of this reduced parameter space and said bin's contributing parameter lines.

This process can be repeated until some threshold is reached. This threshold is nominally set by demanding that at least three hits are required to form a track candidate.



Figure 4.16: The reduced parameter space of the 2D cluster shown in Fig. 4.10.

4.2.4 3D track reconstruction

Section 4.2.3 describes the track reconstruction of a 2D ECal cluster. However, a 3D cluster consists of two sets of 2D clusters. So, the process described in section 4.2.3 must be performed on each of the 2D clusters. The result of this process is two sets of 2D tracks. To form full 3D tracks, the tracks from each view must now be matched together. This is achieved by making every pairwise comparison of the tracks from each view to find the pair which are most similar to each other. After such a pair is found, the tracks are removed from the pool and the process is repeated to find the next pair until either no tracks are left or one 2D tracks are left. In the latter case the single 2D track is discarded. Every pairwise combination of tracks is used to form a likelihood \mathcal{L} . The pair which produces the highest \mathcal{L} is declared the best match and removed from the pool. Three pieces of information about the matching pair are used to calculate \mathcal{L} , all of which make use of probability density distributions generated using beam Monte Carlo.

As should be expected, a vertex with one visible track will have different characteristics to a vertex with three visible tracks. So, to maximise the ability of the matcher, a different set of probability density distributions are used for the 1, 2 and 3 track cases. If the number of tracks in each view is not identical, the higher number of tracks is used to find the correct probability density distributions. Separately, due to their geometrical differences, the reconstructed shape of vertices in the DS ECal will differ to those in the barrel ECals. This leads to a separate set of probability density

distributions for the barrel and DS ECal modules.

The first input to the likelihood is the ratio of the total deposited charge on each track Q_{ratio} . The denominator is taken as the track which comes from the view with the most hits. Generally speaking, a particle propagating through an ECal module should deposit a similar amount of charge in each of the two views. So, Q_{ratio} should have a value close to 1 if the two 2D tracks are created by the same particle. An example of the Q_{ratio} distribution is shown in Fig. 4.17, taken from beam Monte Carlo in the barrel ECals for cases where the maximum number of tracks found in a given view is 2. In Fig. 4.17, correctly matched (in blue) shows the Q_{ratio} distribution for matching pairs which come from the same particle and incorrectly matched (in red) shows the Q_{ratio} distribution for matching pairs which were created by different particles. As Fig. 4.17 shows, Q_{ratio} well separates the two cases. To generate a probability density distribution for Q_{ratio} , the two distributions shown in Fig. 4.17 are used, but without applying any normalisation. By comparing the bins of each distribution, the probability for correctly matching two tracks in a given bin p_i can be formed by

$$p_i = \frac{s_i}{s_i + b_i}, \quad (4.9)$$

where s_i is the number of correctly matched tracks in bin i and b_i is the number of incorrectly matched tracks in bin i . A discrete probability density distribution for Q_{ratio} can then be formed by calculating p_i for every bin. The discrete probability density distribution is then interpolated with splines to create the final probability distribution. An example of this for the two track, barrel case is shown in Fig. 4.18. When a matching candidate pair is being considered, the value of Q_{ratio} is calculated and used in the spline to retrieve $\mathcal{L}_{Q_{\text{ratio}}}$.

The second input to the likelihood, called $\Delta_{\text{layer, first}}$, is the difference in the starting layer of each 2D track which forms the matching candidate pair, where starting layer refers to the layer closest to the ND280 tracker. For 2D tracks which should be matched together, $\Delta_{\text{layer, first}}$ should be 1. The separation ability of this variable for the two track, barrel is shown in Fig. 4.19. The discrete probability density function was created using eqn. 4.9. It was not necessary to interpolate using splines as $\Delta_{\text{layer, first}}$ is itself discrete. The probability density function for $\Delta_{\text{layer, first}}$ is shown in Fig. 4.20 for the two track, barrel case. For each matching candidate pair, the value of $\Delta_{\text{layer, first}}$ is calculated and the corresponding $\mathcal{L}_{\Delta_{\text{layer, first}}}$ is retrieved from the probability density



Figure 4.17: Q_{ratio} distribution in the barrel ECal for the two track case. The blue distribution refers to matching pairs which were matched to the same true particle. Both distributions are unit normalised.

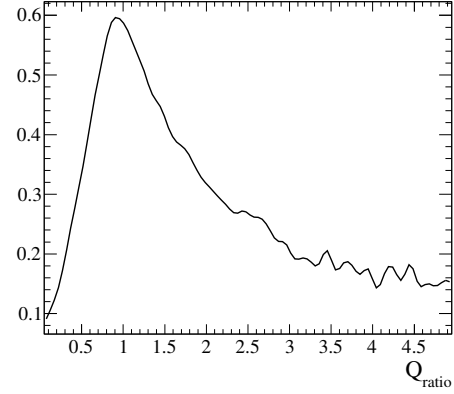


Figure 4.18: Q_{ratio} probability density distribution in the barrel ECal for the two track case.

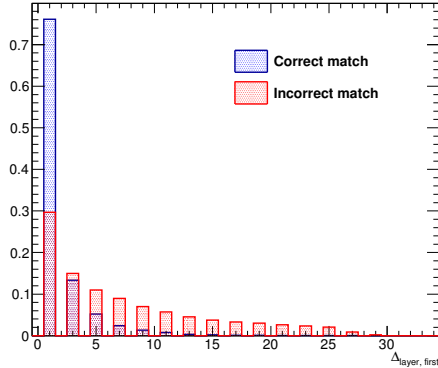


Figure 4.19: $\Delta_{\text{layer,first}}$ distribution in the barrel ECal for the two track case. The blue distribution refers to matching pairs which were matched to the same true particle. Both distributions are unit normalised.

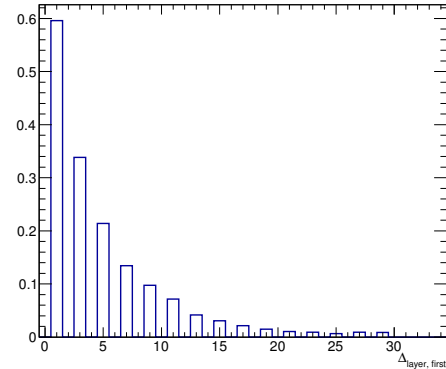


Figure 4.20: $\Delta_{\text{layer,first}}$ probability density distribution in the barrel ECal for the two track case.

function.

The third and final input to the likelihood, called $\Delta_{\text{layer,last}}$, is the difference in the ending layer of each 2D track which forms the matching candidate pair, where the



Figure 4.21: $\Delta_{\text{layer, last}}$ distribution in the barrel ECal for the two track case. The blue distribution refers to matching pairs which were matched to the same true particle. Both distributions are unit normalised.

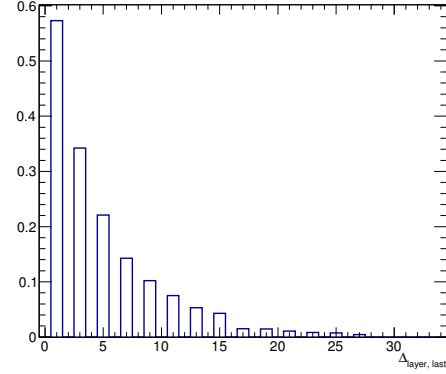


Figure 4.22: $\Delta_{\text{layer, last}}$ probability density distribution in the barrel ECal for the two track case.

ending layer refers to the layer furthest from the ND280 tracker. Functionally, how this function is used is essentially identical to $\Delta_{\text{layer, last}}$ so it will not be described in detail. The separation ability of this variable and its corresponding probability density function for the two track, barrel case are shown in Fig. 4.21 and Fig. 4.22 respectively.

The matching likelihood, \mathcal{L} for a matching candidate pair is then

$$\mathcal{L} = \mathcal{L}_{Q_{\text{ratio}}} \times \mathcal{L}_{\Delta_{\text{layer, first}}} \times \mathcal{L}_{\Delta_{\text{layer, last}}}. \quad (4.10)$$

As described above, \mathcal{L} is calculated for every matching candidate pair and the pair which maximise \mathcal{L} is selected as a match and removed from the pool. The process is then repeated until no more matches can be made.

3D tracks have now been formed, but the associated directions and positions of those tracks still need to be calculated. The track fitting process for the newly formed 3D tracks is very similar to that described in section 3.4.6. The tracks are briefly separated into their constituent 2D views and a charge-weighted average position of each layer is calculated using the track's constituent hits. Then, the hits in the opposing view are used to estimate the 3rd coordinate of a given layer using a least-squares fit. After all of the coordinates have been estimated, a full 3D least-squares fit of the positions in

each layer is performed to estimate the 3D track's direction and position in that ECal layer.

4.2.5 Track pairwise crossing reconstruction

The final step of the reconstruction is to estimate where each of the 3D track's paths cross. As each track is reconstructed as a straight line in 3D, the final step is fairly simple. Using the track direction and position information calculated at the end of section 4.2.4, the position at closest approach for every pairwise combination of 3D tracks is calculated analytically. The distance of closest approach is also calculated. Six hits, the closest three from each 3D track, are then associated to the pairwise crossing.

4.3 Output of the reconstruction

The reconstruction is run over every 3D cluster found in the ECal. By applying the steps outlined above, for each 3D cluster the following output is given:

- A set of 3D tracks
- The pairwise crossings of all 3D tracks found in the cluster

Note that no vertex formation beyond the pairwise crossings is calculated at this stage, nor is any analysis of the 3D tracks performed. While this may seem like an oversight of the reconstruction, this approach was decided as no assumptions are made about what the tracks/crossings represent at this point, making the output more generic. Any analysis which wants to make use of the reconstruction is given enough information to apply more targeted reconstruction downstream.

4.4 Validation of the reconstruction

Someone do this plz

Chapter 5

Magnetic field simulation in ND280

ND280 is housed in the UA1 magnet which provides a 0.2 T magnetic field through the basket. The purpose of this magnetic field is to aid particle identification in ND280's TPCs. This magnetic field is accurately modelled in nd80mc by a constant 0.2 T magnetic field in the basket. The ND280 analyses, which are inputs to the oscillation analyses, search for a TPC track matched to an FGD track so, in a first iteration of these analyses, the magnetic field model is sufficient for its purpose.

However, a significant part of the UA1 magnet is the iron based, magnetic flux return yoke which helps to tightly contain the magnetic field outside of the tracker region. As a result, there is a significant magnetic field contained within the magnetic flux return yoke during operation. This magnetic field in the flux return yoke is not modelled in nd80mc. For the first iterations of the ND280 oscillation input analyses, this approximation was valid. However, as the ND280 analyses become more mature, and non-tracker based analyses are started, this approximation is no longer sufficient. So, the magnetic field model in the simulation needs revising.

5.1 Magnetic field model in the ND280 flux return

A simple model for the magnetic field in the flux return can be found by making two assumptions. Firstly, the flux return yoke consists mostly of iron which has a much higher magnetic permeability than the air surrounding it. So, it can be assumed that any magnetic flux passing through the ND280 basket is solely transported back around



Figure 5.1: Graphical display of the X-Y ND280 cross-section.

by the return yoke (no flux passes through the atmosphere in the pit). It follows that

$$\phi_b = \phi_r, \quad (5.1)$$

where ϕ_b is the magnetic flux passing through the tracker and ϕ_r is the magnetic flux passing through the return yoke. The second assumption regards the shape of the ND280 basket and flux return yoke. The X-Y cross-section of ND280, as shown in Fig. 5.1, can be modelled as two distinct parts: the flux return yoke and everything contained within. It is clear from Fig. 5.1 that both areas are rectangular so the system can be modelled as a smaller rectangle (the basket) contained within a larger rectangle (the return yoke). Using this assumption and Eq. 5.1, the magnetic field strength passing through the return yoke, B_r , is

$$B_r = \frac{B_b A_b}{A_r - A_b}, \quad (5.2)$$

where B_b is the strength of the magnetic field passing through the basket, A_b is the cross-sectional area of the basket region and A_r is the cross-sectional area of the flux return yoke if the flux return yoke was not hollow.



Figure 5.2: Simple model of the magnetic field in the basket and flux return region. The flux return yoke has been separated into ten sections: four vertical B field sections, four corner B field sections and two horizontal B field sections. The height of the basket region, h , is also shown.

Eq. 5.2 is sufficient to model the strength of the magnetic field in the flux return yoke, yet Eq. 5.2 conveys no information about the direction of the magnetic field. However, the direction can be estimated by separating the flux return into ten sections as shown in Fig. 5.2. The sections are: four vertical sections where the magnetic field enters and exits the flux return region, two horizontal sections where the magnetic field in the flux return is anti-parallel to the magnetic field in the basket and four corner sections where the magnetic field transitions between the horizontal and vertical sections. By defining the magnetic field in the basket to be parallel to the x-axis

$$\vec{B}_b = B_b \hat{i}, \quad (5.3)$$

then it follows that the horizontal magnetic field in the flux return is

$$\vec{B}_r^H = -B_r \hat{i}. \quad (5.4)$$

The field model for the vertical section should take into account that the strength of the magnetic field is not constant, but increases in strength until it reaches the corner region. The direction of the field depends on which vertical section is under consideration. For the section where the magnetic field is exiting the tracker and moving upwards, the relevant vector is

$$\vec{B}_r^V = \frac{y}{h/2} B_r \hat{j}, \quad (5.5)$$



Figure 5.3: Comparisons of data and Monte Carlo in the bottom-left barrel ECal for previous software productions. The red and pink histograms are Monte Carlo simulation of T2K beam neutrinos incident on ND280 and the surrounding pit respectively. The blue data points are collected data from run 3C. Both of the plots are POT normalized.

where h is the height of the ND280 basket and y is the height at which the magnetic field is being evaluated in the ND280 coordinate system. In the corner regions, the magnetic field is defined to be straight, constant in strength and at 45° to the horizontal and vertical sections. As with the vertical section, the magnetic field direction is dependent on which corner section is being considered. For the corner section where the magnetic field is exiting the tracker and travelling vertically upwards (as defined in Eq. 5.5), the vector is

$$\vec{B}_r^C = \frac{B_r}{\sqrt{2}}(\hat{j} - \hat{i}). \quad (5.6)$$

The magnetic field in the other corner sections are then 45° rotations of Eq. 5.6.

5.2 Effect of magnetic field on the ECal

It was found in previous iterations of ND280 analyses that there were significant discrepancies between the Monte Carlo and the collected data in the ECal. The dis-

crepancies found had an ECal module dependence where the bottom modules were affected most. The problem appeared in the low level distributions, such as how many scintillator hits were assigned to each reconstructed object. An example of this is shown in Fig. 5.3a which shows a comparison of Monte Carlo with run 3C data for the number of constituent hits in each reconstructed object measured in the bottom-left barrel ECal. For the number of hits region with high population (between roughly 10 and 30) there is a clear excess of collected data events. As the high level variables, such as the ones used for track-shower discrimination, are based on these low level quantities, the discrepancy propagated through causing significant disagreement at all levels. An example of this effect is shown in Fig. 5.3b which shows a data and Monte Carlo comparison, again for the bottom-left barrel ECal, for the Truncated Max Ratio (TMR) of the reconstructed objects. The TMR, which calculates the ratio of the lowest total charge found in an ECal layer to the high total charge in an ECal layer after removing the top and bottom 20% of hits, is an input into the track-shower discriminator described in section 3.4.8. The track-shower discrimination is a key feature of the ECal reconstruction which is used by several ND280 analyses so such a big discrepancy is a serious problem.

As ND280 is off-axis relative to the T2K beam, there is an increase in the neutrino flux in the flux return yoke and surrounding pit regions below the bottom ECals. This means that any charged final states in this region would generally have to propagate through the flux return yoke. If a magnetic field is present in this region, as there would be during data taking, the trajectory of such particles would be bent upwards, towards the ND280 tracker region causing an increase in the event rate in the bottom ECals. If the magnetic field in this region is missing, the above statement does not hold and a relative deficit of events would be seen which describes the situation seen in Fig. 5.3. So, the simple magnetic field model in the flux return yoke described in section 5.1 was implemented in `nd280mc` and a batch of beam and sand Monte Carlo was produced to test its effect. To get an idea of the magnetic field's effect on the rates measured by the ECals, the same variables as shown in Fig. 5.3 are shown in Fig. 5.4, but with the magnetic field activated. The difference is very clear; Fig. 5.4a shows that the excess in the 10 to 30 hits region is now gone. It is also clear that the effect of the magnetic field has propagated through to the high level discriminators, as shown in Fig. 5.4b.

Despite this study only briefly investigating the presence of a magnetic field in the

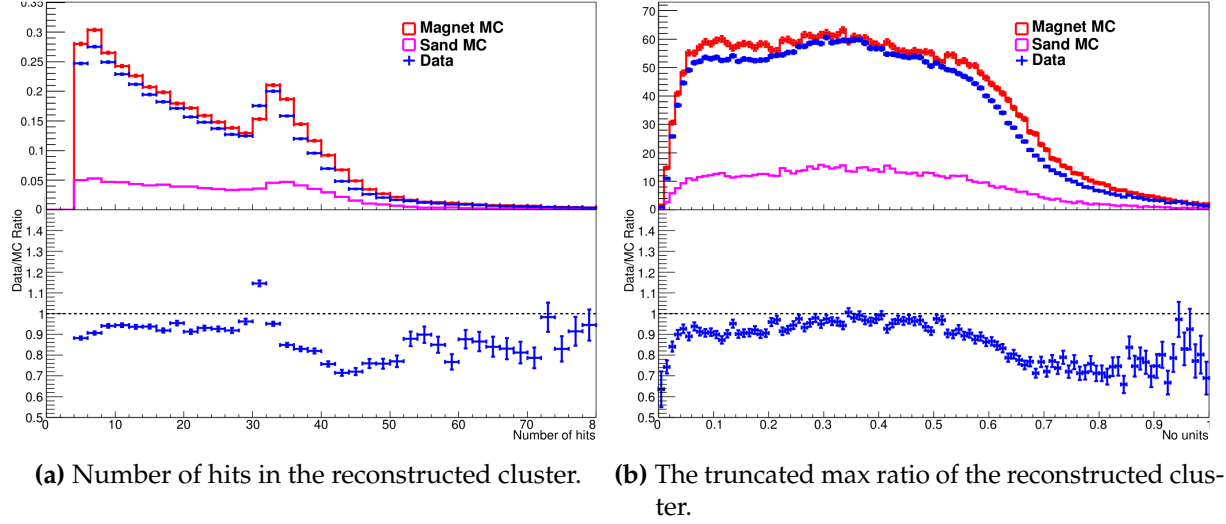


Figure 5.4: Comparisons of data and Monte Carlo in the bottom-left barrel ECal with the magnetic field model described in section 5.1 implemented. The red and pink histograms are Monte Carlo simulation of T2K beam neutrinos incident on ND280 and the surrounding pit respectively. The blue data points are collected data from run 3C. Both of the plots are POT normalized.

UA1 flux return yoke, the improvement provided is undeniable. It was decided that the model would be a permanent feature of the ND280 simulation and is now used in all software productions including the inputs to this analysis.

Chapter 6

Selection of neutrino interactions in the ECal

This analysis presents a measurement of the CC inclusive interaction cross-section of ν_μ with lead nuclei using the ND280 tracker ECals. To make such a measurement, a sample of neutrino interaction vertices within the ECal must be found. The selection of events is based on the enhanced reconstruction outlined in chapter 4, which was specifically designed to introduce track multiplicity. As a result of this method, vertices in the ECal are naturally separated into topologies defined by the number of reconstructed tracks. Any selection development should take advantage of this situation and tailor cuts to be specific to each topology which should result in a higher overall sample purity. The 3D track matching aspect of the reconstruction was only tuned to handle up to 3 tracks simultaneously. However, this analysis aims to measure a CC-inclusive cross-section so should not be biased against any neutrino energy range. Baring this information in mind, the selection should separate out the events into the following topologies:

- 1 prong topology
- 2 prong topology
- 3 prong topology
- 4+ prong topology

The definition of a prong is a reconstructed track associated with a reconstructed vertex.

However, as described in section 4.3, the output of the enhanced reconstruction has been kept generic and is not specifically tailored to this task. The reconstruction outputs a set of clusters which contain a set of 3D tracks and every pairwise crossing that said tracks make. While it is true that in some situations the reconstruction will accurately represent a vertex out of the box, e.g. when only two tracks are reconstructed in the cluster, there will be many situations where extra reconstruction steps are needed before any further selection can take place. So, the structure of this chapter is as follows: the definition of signal is described first along with the sample to develop the selection, followed by a discussion of the vertex reconstruction. After the final reconstruction steps have been discussed, a full discussion of the neutrino selection follows.

6.1 Signal definition

The measurement of this analysis is the CC inclusive interaction cross-section of ν_μ with lead nuclei using the ND280 tracker ECals. The active volume of the ECal consists of layers of plastic scintillator and lead absorbers. Neutrino interactions that occur in the lead absorbers are indistinguishable from those that occur in the plastic scintillator. Because of this fact, the selection does not attempt to separate the two cases out. So, the strict signal definition used by this selection is as follows:

- Interacting neutrino is ν_μ flavour
- Interaction type is charged current
- Interaction occurs within the active volumes of either the barrel ECal or DS ECal

The active volume is defined by the ROOT geometry used in the simulation. Specifically, it is a rectangular box which encompasses all of the lead and scintillator layers for each ECal module. Any target element contained within this volume is a signal target.

6.2 Monte Carlo sample

NEUT was used to generate a neutrino beam sample of Monte Carlo which corresponds to 3.949×10^{20} POT. All of this sample was generated using a simulated beam power of 178 kW which is the average beam power used for Run III. At this intensity,

ECal module	No. signal events
Bottom-right	223042
Side-right	231955
Top-right	135476
Bottom-left	262500
Side-left	293065
Top-left	140539
Downstream	134100
Total	1420677

Table 6.1: The number of signal events in the Monte Carlo sample separated by ECal module.

there are an expected 9.46 neutrino interactions per eight bunch spill in ND280. So, there will be approximately one interaction per bunch across the entire of ND280 meaning the chance of pileup is small.

The sample above only simulated neutrino interactions within ND280 (including the surrounding magnet). However, we expect many interactions in the surrounding pit (referred to as sand interactions from now on) to have final states which enter ND280. So, NEUT was used to generate an additional sample of sand interactions which corresponds to 3.708×10^{20} . There is roughly a 6% difference in the POT of the beam and sand Monte Carlo. As the sand Monte Carlo has a sufficiently high level of statistics, scaling the smaller sample to match the larger is acceptable.

The number of signal interactions from the Monte Carlo sample is shown in table 6.1, separated into the ECal module they occurred in. The number of signal interactions is also shown as a function of neutrino energy for the bottom-left, top-right and DS ECals in Fig. 6.1. Clearly, there are an extremely high number of signal events in the sample, which means this analysis is in no way statistically limited. As an example, consider a selection with a 1% signal efficiency in the DS ECal. Assuming 100% selected sample purity, the number of selected events would be 1341 which correspond to a statistical error of 2.73%. Even in this extreme situation, the statistical error is borderline negligible. It should be clear that any statistical error in this analysis is approximately 0%.



Figure 6.1: The number of signal events as a function of neutrino energy in the bottom-left (red), top-right (blue) and DS (black) ECal.

6.3 Vertex reconstruction

The output of the enhanced reconstruction already supplies most of the necessary information to reconstruct vertices in the ECal. As a reminder, the reconstruction outputs a set of ECal clusters which contain the following:

- A set of 3D reconstructed tracks
- The position at which every pairwise combination of 3D tracks most closely cross (pairwise crossings)

The reconstruction makes no quality checks on the 3D tracks in each cluster. So, the first step is to remove any poorly reconstructed tracks from the cluster. The need for this step is shown in Fig. 6.2a which shows the angular separation of reconstructed tracks with the simulated particle which created them, taken from beam Monte Carlo. While the majority of tracks generally have a small angular separation, Fig. 6.2a clearly shows a build up of tracks which are offset by 90° to the simulated particles.

There are two categories of bad track reconstruction. The first is where the 3D matching matches two 2D tracks which do not have sufficient information to fully model a 3D track. Specifically, one of the 2D tracks involved in the matching only uses one

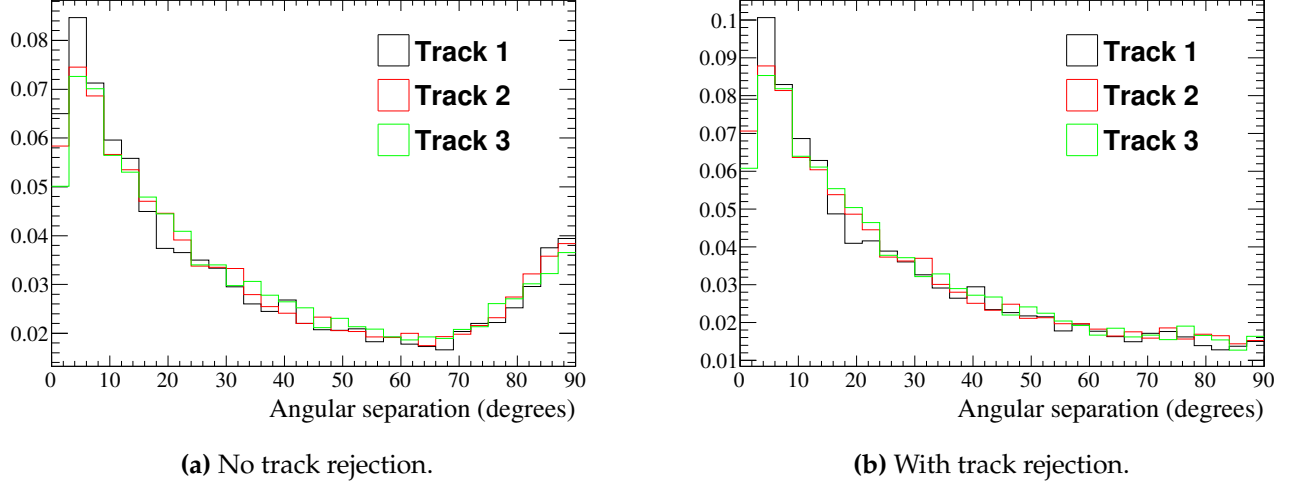


Figure 6.2: Angular separation of the reconstructed tracks in an ECal cluster with the beam-simulated particle that created them. The black, red and green histograms are the tracks that were reconstructed first, second and third respectively. All histograms are area normalized.

ECal layer. As the 3D track reconstruction requires information from both ECal views, tracks which fall into this category do not supply enough information to reconstruct a good quality track. The second category is where the 3D matching produces a grossly incorrect match. The matcher is designed to continually match 2D tracks together until no more 2D tracks are left in the matching pool. So, there are situations where the last possible match made is in no way suitable. This situation is easily identified by matched 2D tracks which do not overlap. For example, one of the 2D tracks uses layers 16, 18 and 20 and the other 2D track uses layers 1 and 3. By removing these two types of tracks from the cluster, the 90° build up in the angular separation distribution is suppressed, as shown in Fig. 6.2b. By removing these categories of tracks, approximately 22% of tracks are rejected.

The final states of a neutrino interaction originate from the same point in space. So, assuming that the reconstructed tracks represent the final states, the reconstructed tracks should most closely cross at the point of interaction. As stated above, one of the outputs of the reconstruction are the pairwise crossings of the constituent tracks in the ECal cluster. Using the above assumptions, the pairwise crossings should be in close proximity to one another when the reconstructed tracks represent the final states of an interaction. This idea promotes a relatively simple method of vertex reconstruction: attempt to cluster the pairwise crossings together if the pairwise crossings are in close

proximity. To quantitatively define this proximity, the quality of the pairwise crossing also has to be considered.

As with the 3D tracks, the reconstruction does not perform any quality checks on the pairwise crossings of the tracks. As the reconstruction will always find a crossing location for a pair of 3D tracks, some of the pairwise crossings will not represent anything physical. The quality definition chosen is simple: pairwise crossings are defined as bad if the crossing location is far away from either of the tracks it is associated with. However, the distance definition is not trivial to define and should be closely correlated with the vertex reconstruction method. For example, a two track vertex would provide very little constraint on the distance which defines a bad crossing, whereas a three track vertex may provide a bad crossing distance constraint which is too strict and destroys the majority two track vertices.

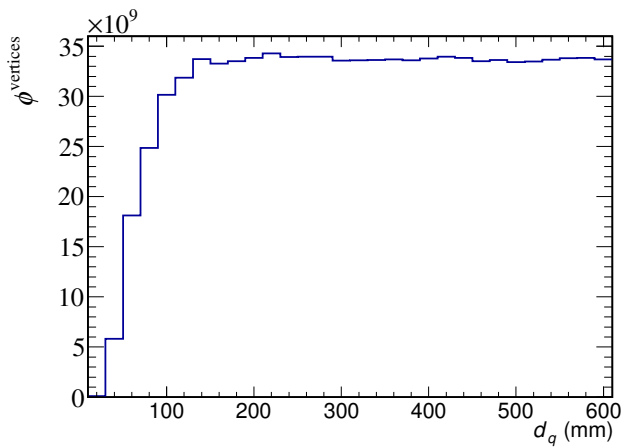
The above discussion promotes two parameters which will govern the vertex reconstruction: the required proximity of two crossings to be clustered together, d_c , and the distance of a crossing from its constituents tracks to be classified as bad quality, d_q . To quantify these values, a sample of reconstructed events matched to interactions in the ECals are used which are taken from beam Monte Carlo. The reconstruction (the pairwise crossing rejection and clustering) is repeatedly run over the sample for different values of the d_c and d_q to find the optimum values. To define the optimum value, a figure of merit is necessary. After running the reconstruction for a given d_c and d_q , the number vertices are separated into one, two and three track vertices and the true neutrino interactions which created the reconstructed vertices are associated. A reconstructed vertex is tagged as correctly reconstructed if it contains the same number of reconstructed tracks as the number of charged final states in the associated neutrino interaction. By defining the number of correctly reconstructed one, two and three track vertices as N_1 , N_2 and N_3 respectively, the figure of merit, ϕ^{vertices} , is

$$\phi^{\text{vertices}} = N_1 N_2 N_3. \quad (6.1)$$

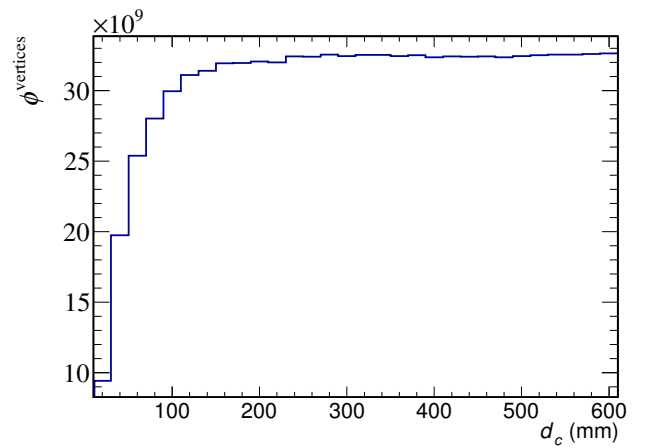
By mapping out ϕ^{vertices} in (d_q, d_c) space, information about the preferred values of d_q and d_c can be found. This space is shown in Fig. 6.3. It is clear from Fig. 6.3 that there is no clear maximum, but rather a plateau of ϕ^{vertices} for d_q and d_c greater than 140 mm. So, marginalized distributions of d_q and d_c can be produced to find where ϕ^{vertices} approaches zero which are shown in Fig. 6.4a and Fig. 6.4b respectively. The



Figure 6.3: Values of ϕ^{vertices} in (d_q, d_c) space. The colour corresponds to the magnitude of ϕ^{vertices} .



(a) d_q



(b) d_c

Figure 6.4: ϕ^{vertices} vs the marginalized vertex reconstruction parameters.

values chosen are shown in table 6.2. The reconstruction now assesses the quality of the crossings and then attempts to cluster the good quality crossings together to form vertex candidates. The final step is to use the constituent tracks of each vertex candidate in a fit to estimate the position of the vertex. The following method was proposed by X. Lu. The position of the vertex, \vec{P} , is defined such that the sum of the squares of the distance of each track to \vec{P} is minimised. An example setup of this is shown in Fig. 6.5 for three constituent tracks. By defining the square of the distance of a line, l_i , to \vec{P} as $|\vec{r}_i|^2$, the function to minimise is

$$D = \sum_i |\vec{r}_i|^2. \quad (6.2)$$

\vec{P} is then defined as the point in space which satisfies

$$\frac{\partial D}{\partial x} = \frac{\partial D}{\partial y} = \frac{\partial D}{\partial z} = 0. \quad (6.3)$$

ϕ_d	ϕ_c
$< 140 \text{ mm}$	$< 200 \text{ mm}$

Table 6.2: Parameters for the vertex reconstruction in the ECal.



Figure 6.5: Example of the vertex position, \vec{P} for three lines: \vec{l}_1 , \vec{l}_2 and \vec{l}_3 . $|\vec{r}_1|$, $|\vec{r}_2|$ and $|\vec{r}_3|$ are the perpendicular distances of \vec{l}_1 , \vec{l}_2 and \vec{l}_3 to \vec{P} respectively.

The value of $|\vec{r}_i|$ is trivially defined by simple vector properties as

$$|\vec{r}_i| = \frac{|(\vec{P} - \vec{a}_i) \times \vec{v}_i|}{|\vec{v}_i|} = |(\vec{P} - \vec{a}_i) \times \hat{v}_i|, \quad (6.4)$$

where \vec{v}_i is the direction vector of \vec{l}_i and \vec{a}_i is a point along \vec{l}_i . By defining \vec{P} mathematically as

$$\vec{P} = x\hat{i} + y\hat{j} + z\hat{k}, \quad (6.5)$$

equation 6.3 can be solved. The following derivation is only for $\partial D / \partial x$ as the method is identical for $\partial D / \partial x$, $\partial D / \partial y$ and $\partial D / \partial z$.

$$\begin{aligned} \frac{\partial D}{\partial x} &= \sum_i 2\vec{r}_i \cdot \frac{\partial \vec{r}_i}{\partial x} \\ &= 2 \sum_i [(\vec{P} - \vec{a}_i) \times \hat{v}_i] \cdot [\hat{i} \times \hat{v}_i] \\ &= 2x \sum_i (\hat{i} \times \hat{v}_i) \cdot (\hat{i} \times \hat{v}_i) + 2y \sum_i (\hat{j} \times \hat{v}_i) \cdot (\hat{i} \times \hat{v}_i) + 2z \sum_i (\hat{k} \times \hat{v}_i) \cdot (\hat{i} \times \hat{v}_i) \\ &\quad - 2(\vec{a}_i \times \hat{v}_i) \cdot (\hat{i} \times \hat{v}_i). \end{aligned} \quad (6.6)$$

By applying the same steps for $\partial D / \partial y$ and $\partial D / \partial z$, the matrix equation

$$\begin{pmatrix} \sum_i [\hat{i} \times \hat{v}_i] \cdot (\hat{i} \times \hat{v}_i) & \sum_i [\hat{j} \times \hat{v}_i] \cdot (\hat{i} \times \hat{v}_i) & \sum_i [\hat{k} \times \hat{v}_i] \cdot (\hat{i} \times \hat{v}_i) \\ \sum_i [\hat{i} \times \hat{v}_i] \cdot (\hat{j} \times \hat{v}_i) & \sum_i [\hat{j} \times \hat{v}_i] \cdot (\hat{j} \times \hat{v}_i) & \sum_i [\hat{k} \times \hat{v}_i] \cdot (\hat{j} \times \hat{v}_i) \\ \sum_i [\hat{i} \times \hat{v}_i] \cdot (\hat{k} \times \hat{v}_i) & \sum_i [\hat{j} \times \hat{v}_i] \cdot (\hat{k} \times \hat{v}_i) & \sum_i [\hat{k} \times \hat{v}_i] \cdot (\hat{k} \times \hat{v}_i) \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} \sum_i [\vec{a}_i \times \hat{v}_i] \cdot (\hat{i} \times \hat{v}_i) \\ \sum_i [\vec{a}_i \times \hat{v}_i] \cdot (\hat{j} \times \hat{v}_i) \\ \sum_i [\vec{a}_i \times \hat{v}_i] \cdot (\hat{k} \times \hat{v}_i) \end{pmatrix} \quad (6.7)$$

can be built up. By defining the equation 6.7 as

$$\underline{\underline{A}}\vec{P} = \vec{B}, \quad (6.8)$$

where $\underline{\underline{A}}$ is the matrix on the left hand side of equation 6.7 and \vec{B} is the vector on the right hand side of equation 6.7. \vec{P} is finally

$$\vec{P} = \underline{\underline{A}}^{-1}\vec{B}. \quad (6.9)$$



Figure 6.6: Example event display showing a set of track merging candidates. The final state μ^- (in green) curves in a complicated way and is reconstructed as four tracks (in light blue). The pairwise crossings of the reconstructed tracks are the red squares. The muon is produced by a charged current interaction in the top left barrel ECal producing two π^+ (in brown) and the curving μ^- .

While the inversion of \underline{A} is in principle analytically solvable, it was decided that the inversion would be handled numerically. So, to find \vec{P} , the vertex reconstruction builds \underline{A}^{-1} (by building and inverting \underline{A}) and \vec{B} and then applies equation 6.9.

By applying the steps outlined above to every reconstructed ECal cluster, a set of candidate vertices are formed. As the enhanced reconstruction is only capable of reconstructing straight tracks, bending trajectories tend to be reconstructed as two or more tracks. The crossings associated with such tracks can, and do, pass the vertex reconstruction criteria defined in table 6.2. An extreme example of this topology is shown in Fig. 6.6 in which a curving μ^- is reconstructed as four tracks. So, the final step on the reconstruction is to attempt to merge tracks to model the curving trajectory topology. Firstly, the reconstructed crossings associated with a clean curving trajectory should pass the crossing quality cut but should be sufficiently far away from any other crossing that it is not clustered during the vertex clustering stage. Therefore, track merging candidates can be initially identified by searching for reconstructed vertices with exactly two track constituents. As an example, all three of the crossings shown in Fig. 6.6 are correctly identified by this check. The two constituent tracks of the identified vertex will form the merged track, so the reconstruction checks the shape that the merged track would make against a set of conditions to decide if the merging should be performed. To identify and tune the conditions for merging tracks, two metrics are used. The first metric is used for identification of the merging conditions

and uses the truth information provided by the geant4 simulation. For every two track vertex that was formed by the vertex clustering, the simulated particle that produced each of the two constituent tracks was checked. If the sample particle is matched to both tracks, then the merging candidate is tagged as a correct match, otherwise it is tagged as an incorrect match. The second metric is used for tuning the identified merging conditions. As part of this analysis is a search for neutrino interactions using vertex-based reconstruction, there will be an expected loss of signal by track merging which must be minimised. So, the track merging condition tuning should be based on ECal signal interactions. As described above, the only tracks that are proposed as merging candidates are those which are constituents of a two track vertex. So, the track merging tuning attempts to separate signal and background events which are reconstructed as a vertex with two track constituents. It is preferable that the merging chooses quality over quantity so the tuning figure of merit is defined as

$$\phi^{\text{merge}} = \epsilon \eta^2 \quad (6.10)$$

where ϵ is the efficiency of the track merging to keep signal events reconstructed as two track vertices and η is the purity of the events that remain as two track vertices after merging has taken place.

The first merging condition identified is the cosine of the opening angle, $\cos \theta$, subtended by the two constituent tracks bounded between 0 and 1 which is shown in Fig. 6.7. The opening angle is clearly a powerful discriminator. The distribution for incorrect matches is very flat across the full angular range whereas there is a clear build up correct matches as $\cos \theta \rightarrow 1$.

The second merging condition identified, called 'distance ratio', measures the ratio of the distance between the two constituent tracks' closest points, d^{small} to the distance between their furthest points, d^{large} . An example of how d^{small} and d^{large} are calculated is shown in Fig. 6.8. The distance ratio distribution is shown Fig. 6.9. While it may seem that there is very little discrimination power present in the distance ratio distribution, there is an underlying dependency between the distance ratio and the opening angle subtended by the constituent tracks, which has already been identified as a merging condition. To illustrate this dependency, two distributions are shown in Fig. 6.10 which both show the distance ratio vs the cosine of the opening angle. Fig. 6.10a only shows the correct matches and Fig. 6.10b only shows the incorrect

matches. While it is true that there is a pileup of both correct matches and incorrect matches for low values of the distance ratio, the opening angle separates the two categories out. Specifically, the correct matches pileup occurs as $\cos\theta \rightarrow 1$ and the incorrect matches pileup occurs as $\cos\theta \rightarrow 0$. To further illustrate this point, a new distance ratio distribution is shown in Fig. 6.9b, but with a $\cos\theta > 0.8$ guess cut applied. Comparing the distributions shown in Fig. 6.9 and Fig. 6.9b, the effect of the



Figure 6.7: The cosine of the angle subtended by the merging candidates, bounded between 0 and 1. The correct matches and incorrect matches are the blue and red histograms respectively.



Figure 6.8: Example event display showing how the parameters of the distance ratio are calculated. The distance ratio is defined as $d^{\text{small}} / d^{\text{large}}$. The blue lines are the two reconstructed tracks which form the merging candidate and the red square is the crossing location of those tracks.



Figure 6.9: The distance ratio of the merging candidates. The correct and incorrect matches are the blue and red histograms respectively.



Figure 6.10: The distance ratio vs the cosine of the opening angle for track merging candidates.

$\cos \theta$ cut can clearly be seen. The original pileup of incorrect matches seen in Fig. 6.9 is now gone, leaving an essentially flat incorrect matches distribution in Fig. 6.9b while leaving the correct matches structure intact.

By utilising both the distance ratio and $\cos \theta$ simultaneously, a better degree of separation can be found. However care must be taken when tuning the distance ratio and $\cos \theta$ cuts to ensure optimal separation of signal and background is achieved. It is clear from Fig. 6.7 and Fig. 6.9b that the correct matches pileup for low values of the distance

ratio and high values of $\cos \theta$. So events should only be tagged for merging when they have a distance ratio value lower than some threshold and a $\cos \theta$ value higher than some other threshold. To find these cut values, the track merging reconstruction was run multiple times, using different values of the thresholds for each run. To take the dependency shown in Fig. 6.10 into account, a square grid search in distance ratio and $\cos \theta$ space was used to find optimum cut values. The tuning metric, as described in equation 6.10, was used to find the optimum cut values. The tuning metric values in distance ratio cut vs $\cos \theta$ cut space are shown in Fig. 6.11. As was found in the tuning of the vertex clustering parameters, there is no clear maximum value of the tuning metric, but rather a plateau. So, as was done in the vertex clustering tuning, marginalised distributions of tuning metric in distance ratio cut space and $\cos \theta$ cut space can be produced to find the optimum cut values. The marginalised distributions for $\cos \theta$ and the distance ratio cuts are shown in Fig. 6.12a and Fig. 6.12b respectively. In the case of the $\cos \theta$ cut there is a clearly preferred value, merging candidates should only be merged if $\cos \theta > 0.82$. In the case of the distance ratio cut distribution, there is less of a clear maximum. As the reconstruction is striving for quality over quantity, the cut value should be fairly close to the drop in ϕ^{merge} . It was decided that merging candidates should only be merged if the distance ratio is less than 0.32.

While the $\cos \theta$ condition is clearly a powerful discriminator, there is a topology degeneracy which $\cos \theta$ is not capable of separating, which is shown in Fig. 6.13. The diagram on the left of Fig. 6.13 is a representation of a signal event which is recon-



Figure 6.11: Values of the tuning metric, as described in equation 6.10, in distance ratio cut vs $\cos \theta$ cut space.



Figure 6.12: ϕ^{merge} vs the track merging conditions.

structured as two tracks, whereas the diagram on the right of Fig. 6.13 represents a curving trajectory reconstructed as two tracks. Importantly, the same opening angle is measured for both situations which is small enough that both topologies pass the $\cos \theta$ track merging condition. To rectify this, an extra sanity check is needed when considering merging candidates. So, the final merging condition identified, called ‘swing’, measures the rotation of one track relative to the other. Specifically, the swing is the ratio of the longest track length, l^{long} , to d^{large} (the same d^{large} that was used in the distance ratio calculation). An example of how these values are calculated are shown in Fig. 6.14. Provided that the opening angle of a merging candidate is not near 90° , the swing should be less than one for the topology on the left of Fig. 6.13 and should be greater than one for the topology on the right of Fig. 6.13. The separation power of the swing parameter is shown in Fig. 6.15. After applying the merging conditions discussed above, the swing parameter becomes bimodal as shown in Fig. 6.15b. The swing parameter is introduced purely as an extra sanity cut which is physically motivated and requires no tuning. So, merging candidates are only merged if the measured swing is less than one.

$\cos \theta$	Distance ratio	swing
> 0.82	< 0.32	< 1

Table 6.3: Cut values for the track merging in the ECal.

All of the merging conditions have now been identified and the associated cut values are summarised in table 6.3.

6.4 Monte Carlo selection

As briefly described at the start of this chapter, the selection separates the reconstructed ECal events into a set of topologies, where each topology is defined by a number of associated prongs. In addition to this separation, the geometrical differences between the barrel and DS ECals suggest a further event separation. The DS ECal lies perpendicular to the beam face. So, particles from neutrino interactions will typically travel at right angles to the DS ECal face. Conversely, all of the barrel ECals lie parallel to the beam axis which means neutrino interaction products will generally pass along the barrel scintillator planes. This motivates a separate selection for the barrel and DS ECals. This essentially means that there are eight individual selections to be made and tuned (1,2,3 and 4+ prong topologies in the barrel and 1,2,3 and 4+ prong topologies in the DS ECal). Clearly, this approach can very quickly become complicated. To mitigate this, similar discriminators are used for each topology. As the reconstruction was only



Figure 6.13: Schematic showing the degeneracy of two merging candidate topologies which would pass the $\cos \theta$ cut. The arrows represent reconstructed tracks and θ is the opening angle measured between the tracks.

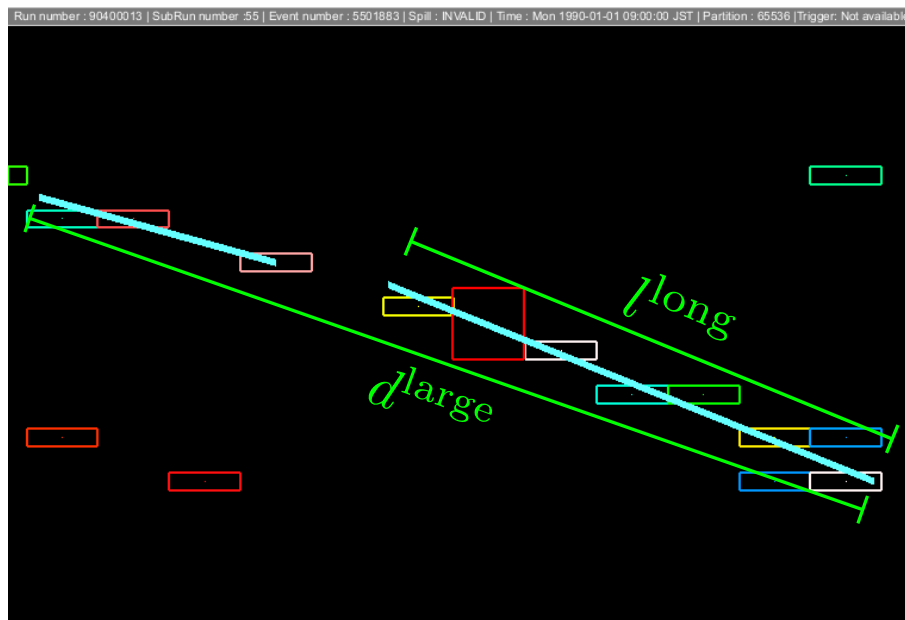
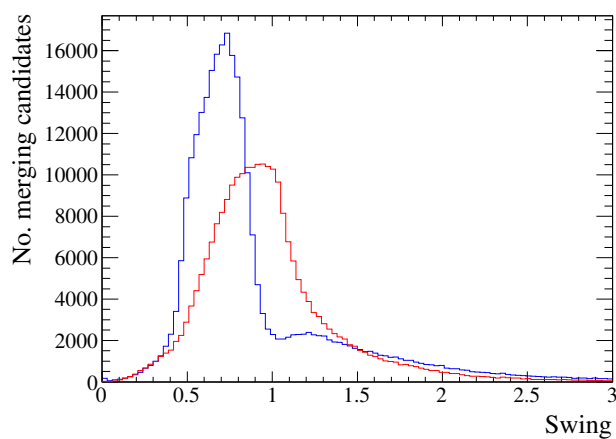
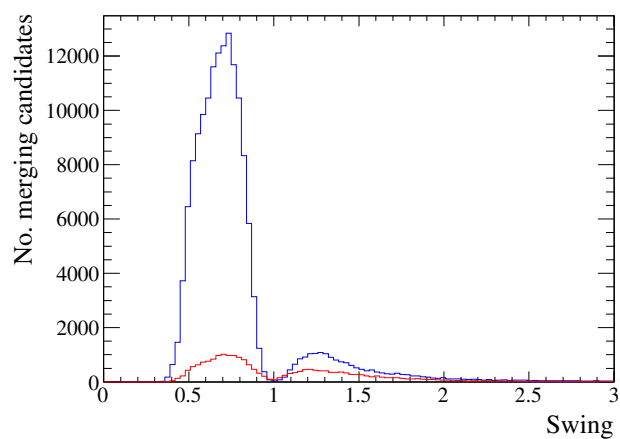


Figure 6.14: Example event display showing how the swing parameters are calculated. Swing is defined as $l^{\text{long}}/d^{\text{large}}$. The blue lines are the two reconstructed tracks which form the merging candidate and the red square is the crossing location of those tracks.



(a) No cuts applied.



(b) For $\cos \theta > 0.82$ and distance ratio < 0.32 .

Figure 6.15: The number of merging candidates as a function of the swing parameter. The correct matches and incorrect matches are the blue and red histograms respectively.

tuned for three reconstructed tracks, the 4+ prong topology will use exactly the same cuts as the 3 prong topology.

Care must be taken when defining what a reconstructed vertex is. For the 2,3 and 4+ prong topologies, it is fairly simple, the reconstructed vertex is as described in section 6.3, but it is not possible to fit for a vertex position when dealing with a single prong. In fact, there is actually little that can be done about this. So, beam kinematics are assumed and the 'vertex' for a single prong is the most upstream end of said prong.

The definition of signal has already been described in section 6.1. However, how the reconstructed events map to the signal interactions also needs discussion. The selection takes place at the reconstructed vertex level but there is not a clear 1:1 map of a reconstructed vertex to a signal interaction. Consider a signal interaction in an ECal module in which the final state particles are involved in one or more secondary interactions. The most likely outcome of this is the reconstruction of two or more vertices: one for the neutrino interaction and one or more for the secondary interactions. By interrogating the associated truth information, each vertex will be matched to the same signal neutrino. It is wholly incorrect to classify each vertex as a reconstruction of a signal event as this will lead to a gross overestimate of the signal rate. To alleviate this, a reconstructed vertex is only tagged as coming from a signal interaction if it obeys the following conditions:

- The reconstructed vertex is matched to a signal interaction
- The reconstructed vertex is the one closest in space to the matched signal interaction

Any reconstructed vertices which pass the first condition but fail the second are tagged as a special case of background events (hereafter referred to as the 'split signal' background).

To illustrate the benefit of separating events into specific prong topologies, Fig. 6.16 shows the truth makeup of events seen in the ECal after applying the reconstruction separation. It is important to note that only the vertex reconstruction and track merging has been applied to the sample at this point. There is a clear difference in the level of backgrounds seen in each topology e.g. the ECal OOFV background is almost exclusively contained in the one prong topology. By applying such a separation and then focusing cuts on each topology, the overall event purity should be higher.

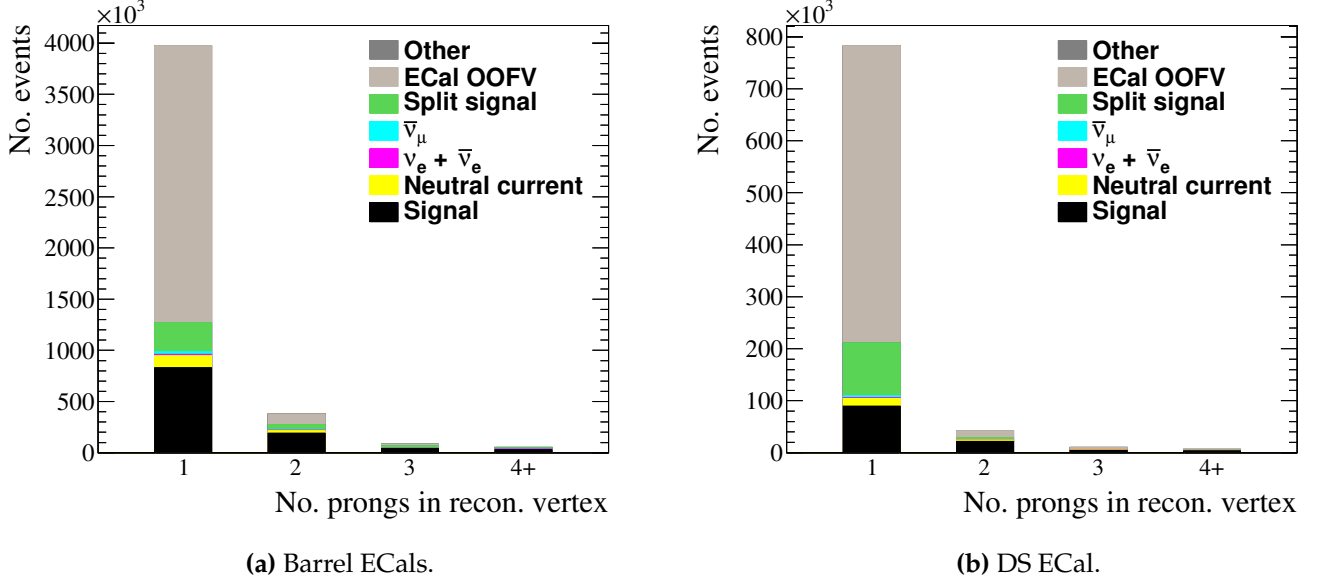


Figure 6.16: The number of reconstructed events in the Monte Carlo sample, separated into the prong topologies. Each event is categorised by the associated truth information from the simulation.

6.4.1 Selection cuts

The enhanced reconstruction was developed with an ECal cross-section analysis in mind. So, most of complex work should already have been handled by the reconstruction aspect of the analysis. In addition, the selection method discussed involves separating events into prong topologies and focusing individual selections on each. These points motivate a simple, cut-based, selection. Some cuts will inevitably require some tuning and a metric is often useful for this purpose. As demonstrated in section 6.2, a high level of stats is seen in each ECal module which means the selection can safely strive for quality over quantity without inflating the final uncertainty. Baring this in mind, the metric used for tuning for prong topology i is

$$\phi_i^{\text{selection}} = \epsilon_i \eta_i^2, \quad (6.11)$$

where ϵ_i and η_i are the selection efficiency and purity of prong topology i . Six selection cuts have been identified which will now be discussed.



Figure 6.17: $\phi_1^{\text{selection}}$ as a function of the distance from the $-y$ face of the bottom-left barrel ECal for the 1 prong topology.

6.4.1.1 Fiducial volume cut

The first cut, the fiducial volume cut, removes most of the ECal OOFV backgrounds in the Monte Carlo sample. This is achieved by defining some outer veto region in which occurring vertices are rejected. There are two items to bare in mind when defining what the fiducial volumes are. Firstly, the off-axis configuration causes each ECal to be exposed to a different energy and particle rate. A good example of this was shown in Fig. 6.1 which shows a higher event rate, but also a higher peak energy of interactions, in the bottom-left ECal than in the top-right ECal. So, the optimised fiducial volume of one ECal need not be the same as another ECal module. Separately to this, Fig. 6.16 shows that the ECal OOFV is almost completely contained in the 1 prong topology bin. This means that a separate fiducial volume definition should be used for the 1 prong topology (it is sufficient for the 2,3 and 4+ prong topologies to use the same fiducial volume definition).

The fiducial volume for a prong topology/ECal module is defined in terms of the distance from each face of the module. So, there are six numbers which define the fiducial volume: the distance from the $\pm x, \pm y$ and $\pm z$ faces of a module. If the distance of a vertex from each ECal face is further than what the fiducial volume defines, the event passes the cut, otherwise it is rejected. To tune these values, each

	$-x$ (mm)	$+x$ (mm)	$-y$ (mm)	$+y$ (mm)	$-z$ (mm)	$+z$ (mm)
Bottom-right	36	36	31	29	206	28
Side-right	31	29	46	44	206	28
Top-right	39	27	29	31	172	28
Bottom-left	25	50	31	29	205	28
Side-left	29	31	50	25	207	28
Top-left	21	34	29	31	207	28
Downstream	29	29	29	30	41	43

Table 6.4: The fiducial volume definitions for each ECal module for the 1 prong topology.

fiducial volume value was systematically increased from 0 mm to 600 mm in mm increments. At each increment the number of passing/rejected events was recorded and $\phi_i^{\text{selection}}$ calculated. The fiducial volume value which maximises $\phi_i^{\text{selection}}$ is accepted as the optimised value. An example of the variation in $\phi_i^{\text{selection}}$ is shown in Fig. 6.17 which shows $\phi_i^{\text{selection}}$ as a function of the distance from the $-y$ face of the bottom-left barrel ECal for the 1 prong topology. There is a clear maximum found which shows the process is effective in finding an optimum distance from the ECal face.

The found fiducial volumes for each ECal module for the 1 prong topology are shown in table 6.4. While all of the ECal face cuts have some discriminatory power, those which cut out according to layer number reject the most background events. Those cuts are the $\pm y$ cuts for the bottom/top barrel ECals, the $\pm x$ cuts for the side ECals and the $\pm z$ cuts for the DS ECal. In the barrel ECals, the inner and outer two layers are removed by the fiducial volume cut and in the DS ECal, the inner and outer three layers are removed. As described above the same fiducial volumes are used for the

2,3 and 4+ prong topologies. So, to tune the fiducial volume cuts, the topologies are temporarily combined and the combined sample is used to tune the cuts. Those fiducial volume cuts are shown in table 6.5. There are clear differences between the fiducial volumes shown in table 6.4 and table 6.5. The cuts suggested by the 2,3 and 4+ prong topology tunings are not as strict as those suggested by the 1 prong topology. This should be expected, as ECal OOFV backgrounds reconstructed as 2,3 or 4+ prong vertices will most likely not have their vertex reconstructed near the faces of an ECal module. The one exception to this is the downstream face of each ECal module. It is clear from table 6.4, that the 2,3 and 4+ prong topologies suggest a stricter downstream

	$-x$ (mm)	$+x$ (mm)	$-y$ (mm)	$+y$ (mm)	$-z$ (mm)	$+z$ (mm)
Bottom-right	19	9	16	0	3	39
Side-right	20	0	6	9	7	65
Top-right	15	9	4	3	5	38
Bottom-left	11	1	34	0	9	69
Side-left	1	4	13	1	3	67
Top-left	11	0	0	7	4	45
Downstream	13	9	13	4	0	64

Table 6.5: The fiducial volume definitions for each ECal module for the 2,3 and 4+ prong topologies.

face cut ($+z$ cut) than the 1 prong topology. The reason for this strict cut is due to the nature of the neutrino beam. J-PARC's neutrino beam is (almost) parallel with the $+z$ axis defined by the ND280 coordinate system. Because of the very forward nature of the beam, any final state particles from ECal neutrino interactions are most likely to travel downstream. So, any subsequent secondary interactions, which are tagged as background, will also occur downstream. The $+z$ face cut attempts to remove these.

6.4.1.2 Visible energy cut

The second cut removes background based on the amount of deposited charge is associated to the constituent prongs. The focus of this cut is to remove particle showers (typically e^\pm and γ) which have been reconstructed as a vertex. For the one prong topology, this information is trivial to evaluate: find which scintillator hits are associated to the single prong and sum their respective charge deposit. The situation is not as clear for a vertex with multiple prongs associated. The variable chosen in this case is the total charge associated to all of the constituent prongs. To further increase the power of this variable as a discriminator, the total prong charge is compared to the total number of scintillator hits associated to the prongs. The aim is to find a 2 dimensional cut which rejects events based on their associated charge and hit information.

The signal and background distributions for the barrel ECal, 1 prong topology are shown in Fig. 6.18a and Fig. 6.18b respectively. To illuminate the separation power, the background/signal ratio is shown in Fig. 6.18c, with the ratio truncated at 2. By

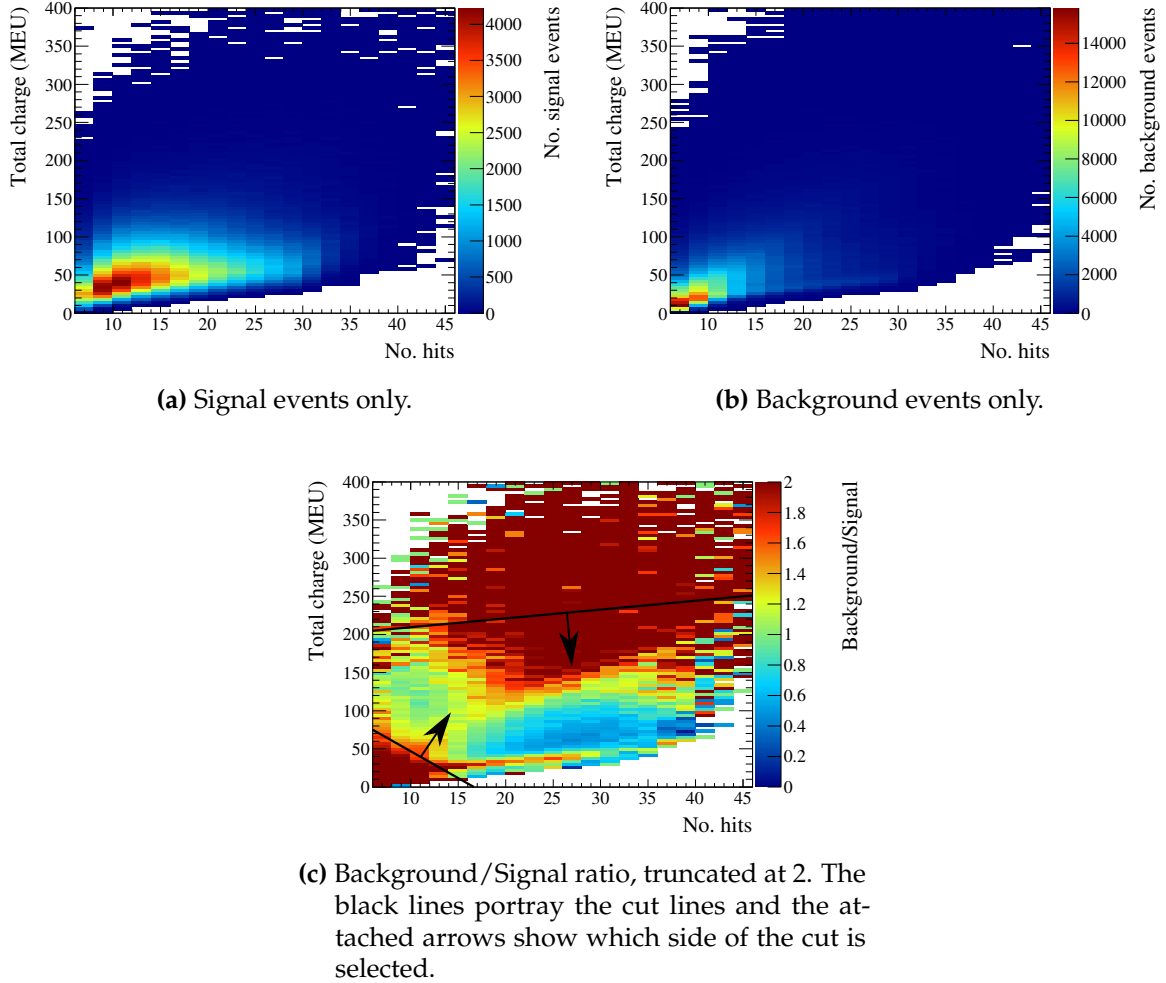


Figure 6.18: Total prong charge vs the number of prong scintillators hits for barrel ECal events in the 1 prong topology.

applying the truncation, areas where the background contamination is at least two times as large as the signal population is easily found. To develop the 2 dimensional cuts, a test line is drawn which appears to roughly cut out the highly contaminated (red) areas in Fig. 6.18c. Then, to tune the cut line, the parameters of said line are varied in a grid search. At each point in the grid, $\phi_i^{\text{selection}}$ is recorded. The maximum value in this grid corresponds to the optimised parameters of the cut line. As is evident from Fig. 6.18c, there are two areas of high background contamination which motivated the development two cut lines which are both overlayed on Fig. 6.18c.

Fig. 6.19 and Fig. 6.20 show similar distributions for the 2 and 3 prong topology in the barrel ECal. The ratio distributions also have the cut lines overlayed. An identical process was used to generate and tune the cut lines. By using a definition for the

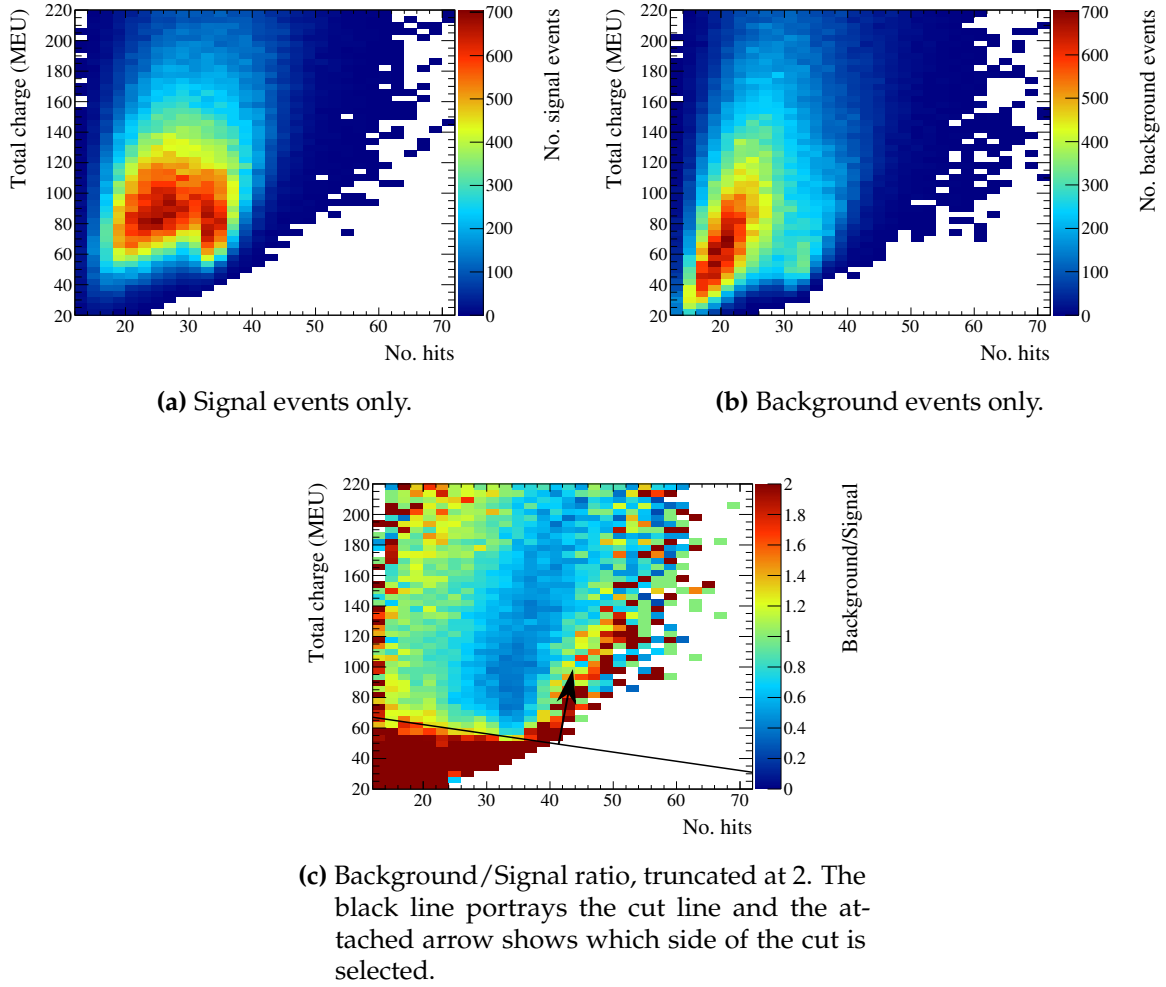


Figure 6.19: Total prong charge vs the number of prong scintillators hits for barrel ECal events in the 2 prong topology.

Prong topology	Barrel cuts (MEU)	DS cuts (MEU)
1	$> -4.5N + 75$ $< N + 205$	$> -3.4N + 62$
2	$> -0.5N + 67$	$> 0.2N + 51$
3	$> 0.7N + 103$	$> -1.1N + 117$

Table 6.6: The definitions of the 2 dimensional cut lines involving the total prong charge and the number of associated scintillator hits. N refers to the total number of scintillator hits associated to the constituent prongs in the vertex.

total number of scintillator hits associated to all constituent prongs in a vertex, N , the definition of the cut lines are shown in table 6.6.



(a) Signal events only.

(b) Background events only.



(c) Background/Signal ratio, truncated at 2. The black line portrays the cut line and the attached arrow shows which side of the cut is selected.

Figure 6.20: Total prong charge vs the number of prong scintillators hits for barrel ECal events in the 3 prong topology.

Prong topology	Barrel cuts (no units)	DS cuts (no units)
1	$< -0.2N + 16$	$< 1.2N + 3$
2	$< 1.5N - 16$	$< 0.7N - 4$
3	$< 1.7N + 7$	$< 0.8N + 1$

Table 6.7: The definitions of the 2 dimensional cut lines involving ΔN and the number of scintillator hits associated with the constituent prongs. N refers to the total number of scintillator hits associated to the constituent prongs in the vertex.

6.4.1.3 Unused hits cut

The output of the enhanced reconstruction is a set of reconstructed clusters. Within those clusters are a set of tracks and their pairwise crossings which are used to reconstruct the ECal vertices used by this analysis. The clusters which contain the tracks and crossing can also be utilised as a discriminator. Particle showers should generally produce a lot of hits and those hits are not necessarily arranged in a linear fashion. So, the third cut implemented assesses how many hits are associated with a cluster but not associated with the vertex. The vertex is defined by its prong constituents so this is really a measure of how many scintillator hits were not associated with the reconstructed prongs. By defining the number of hits in the cluster as N^{Cluster} and the number of hits associated with the i^{th} constituent prong as N_i^{prong} , the discriminator is

$$\Delta N = N^{\text{cluster}} - \sum_i N_i^{\text{prong}}. \quad (6.12)$$

The cut value really should depend on how many hits are associated to the constituent prongs. So, as was done in section 6.4.1.2, the ΔN cut should be 2 dimensional. Specifically, the ΔN cut should depend on the number of scintillator hits associated to the constituent prongs.

So, an identical approach is used to define and tune the cut lines as was used in section 6.4.1.2. The signal, background and background/signal ratio distributions for the 1, 2 and 3 prong topologies in the barrel ECal are shown in Fig. 6.21, Fig. 6.22 and Fig. 6.23 respectively. The layout of the figures is the same as was shown for the visible energy cut. In a similar manner to table 6.6, the ΔN cut definitions are shown in table

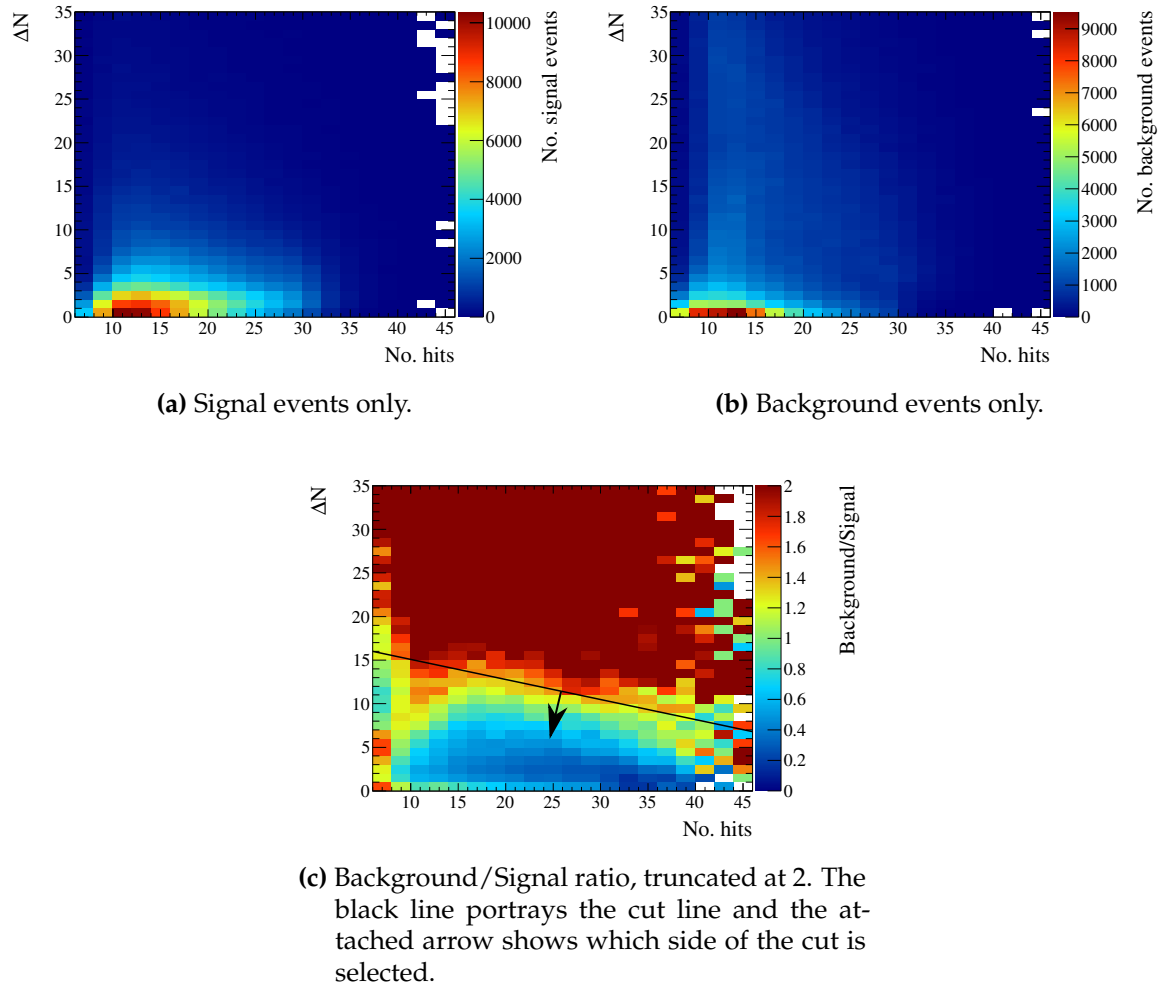
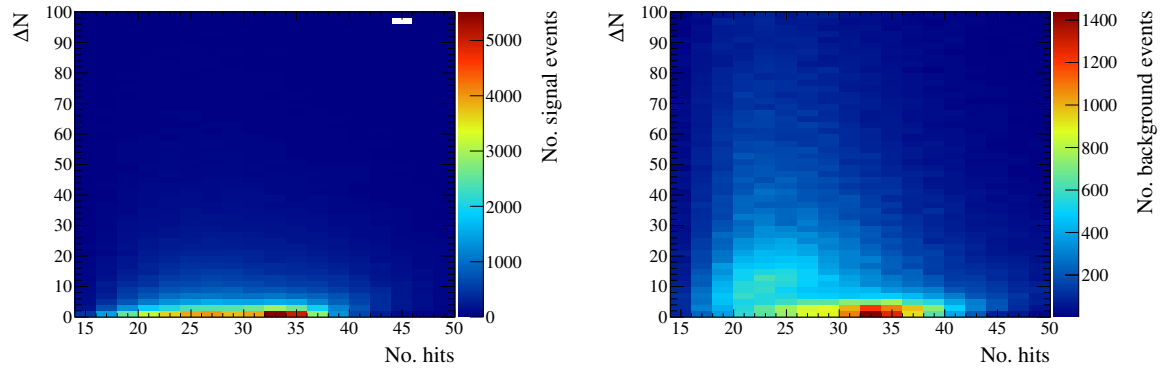
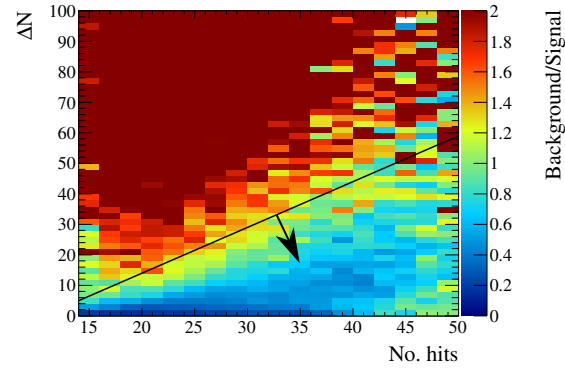


Figure 6.21: ΔN vs the number of prong scintillators hits for barrel ECal events in the 1 prong topology.



(a) Signal events only.

(b) Background events only.



(c) Background/Signal ratio, truncated at 2. The black line portrays the cut line and the attached arrow shows which side of the cut is selected.

Figure 6.22: ΔN vs the number of prong scintillators hits for barrel ECal events in the 2 prong topology.

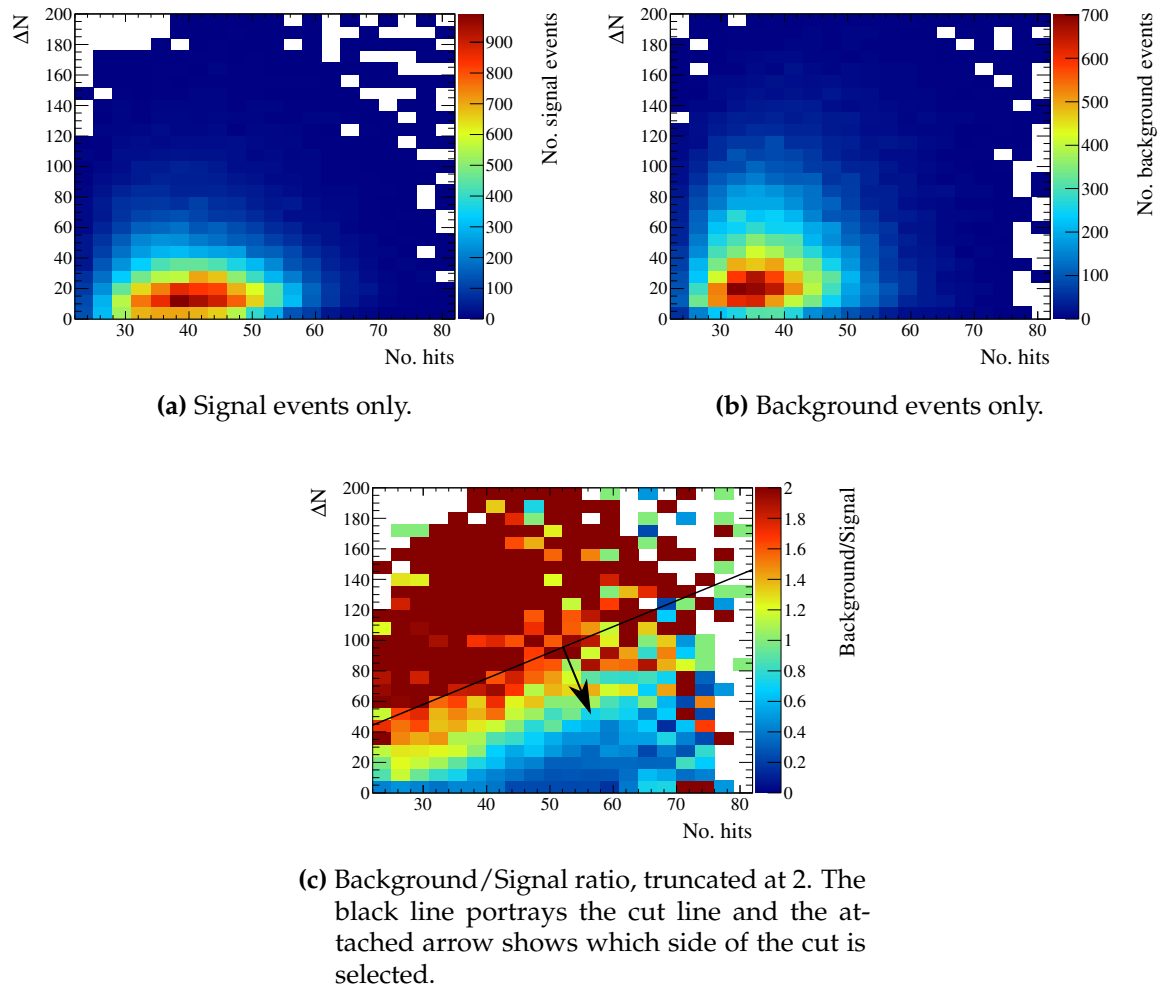


Figure 6.23: ΔN vs the number of prong scintillators hits for barrel ECal events in the 3 prong topology.

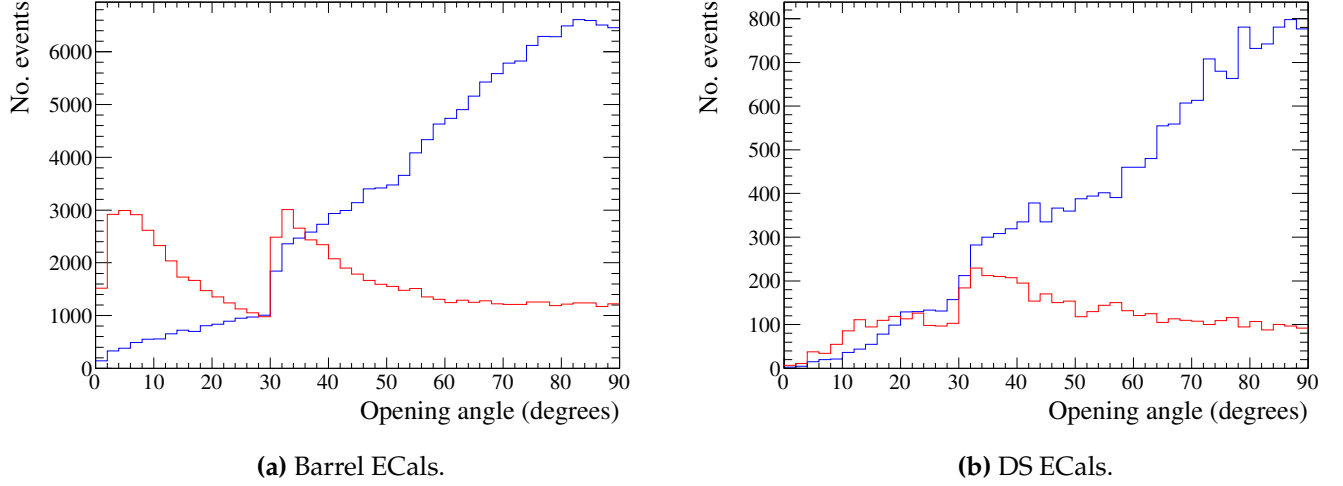


Figure 6.24: The opening angle subtended by the constituents prongs for the 2 prong topology. Signal and background events are the blue and red histograms respectively.

6.4.1.4 Opening angle

Despite the best efforts of the track merging, not all curving trajectories have reconstructed tracks which are successfully merged. So, there will be an inherent ECal OOFV contamination of the 2,3 and 4+ prong topologies where the reconstruction has failed. While future iterations of the analysis should revisit the reconstruction to combat this, it is sufficient to cut these background events out in the selection. As was described in section 6.3, a key signature of a curving trajectory is two prongs with a small opening angle. This means that the opening angle can be used as a cut to remove such background events. To define an opening angle, at least two tracks are required so, unfortunately, such a method can not be implemented for the 1 prong topology.

The signal and background separation provided by the subtended opening angle for the 2 prong topology is shown in Fig. 6.24. While the barrel ECal sees more separation power in the opening angle, it should be clear from Fig. 6.24a and Fig. 6.24b that events should only be selected if their opening angle is bigger than some threshold. To find this threshold, a test cut was systematically varied between 0° and 90° in 1° increments. At each increment, the number of events with an opening angle larger than the test cut was recorded and $\phi_2^{\text{selection}}$ subsequently calculated. An example of the variation in $\phi_2^{\text{selection}}$ is shown in Fig. 6.25 for the barrel ECal. A maximum in $\phi_2^{\text{selection}}$ is clearly found which shows that the opening angle is a good discriminator and that the method works. By applying this method to 2 prong events, events are

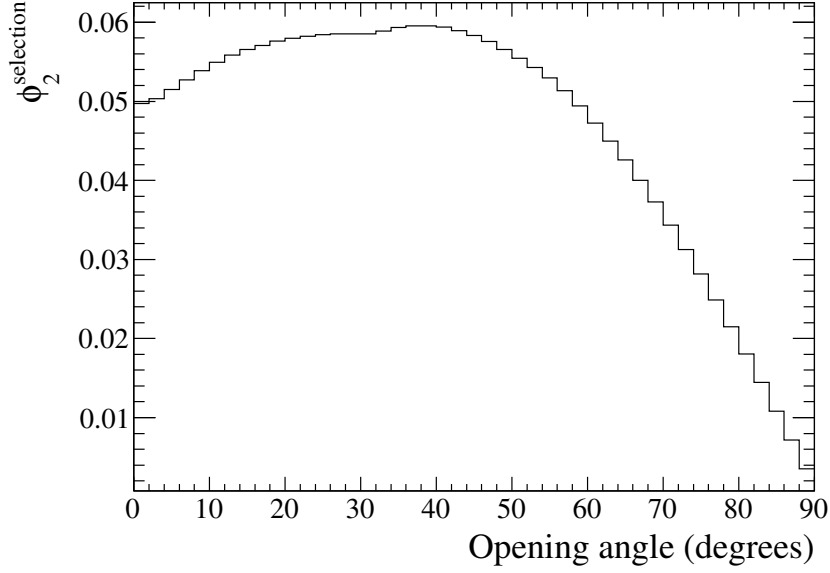


Figure 6.25: $\phi_2^{\text{selection}}$ as a function of the opening angle cut for the 2 prong topology in the barrel ECal.

Prong topology	Barrel cuts (degrees)	DS cuts (degrees)
2	> 34	> 21
3	> 81	> 49

Table 6.8: The definitions of the opening angle cuts.

only selected if the subtended opening angle is greater than 34° for the barrel ECal or greater than 21° for the DS ECal. Similar information should be available for the higher prong topologies. However it is not as trivial to define an opening angle in such situations. The chosen variable in for the 3 prong topology is the summed opening angle for every pairwise combination of the constituent prongs. The signal and background separation for this summed opening angle is shown in Fig. 6.26b. The cut development process used here was identical to the one used for the 2 prong topology. The study suggested that events should only be selected if their summed opening angle is greater than 81° for the barrel ECal and 49° for the DS ECal. The cuts found by this study are summarised in table

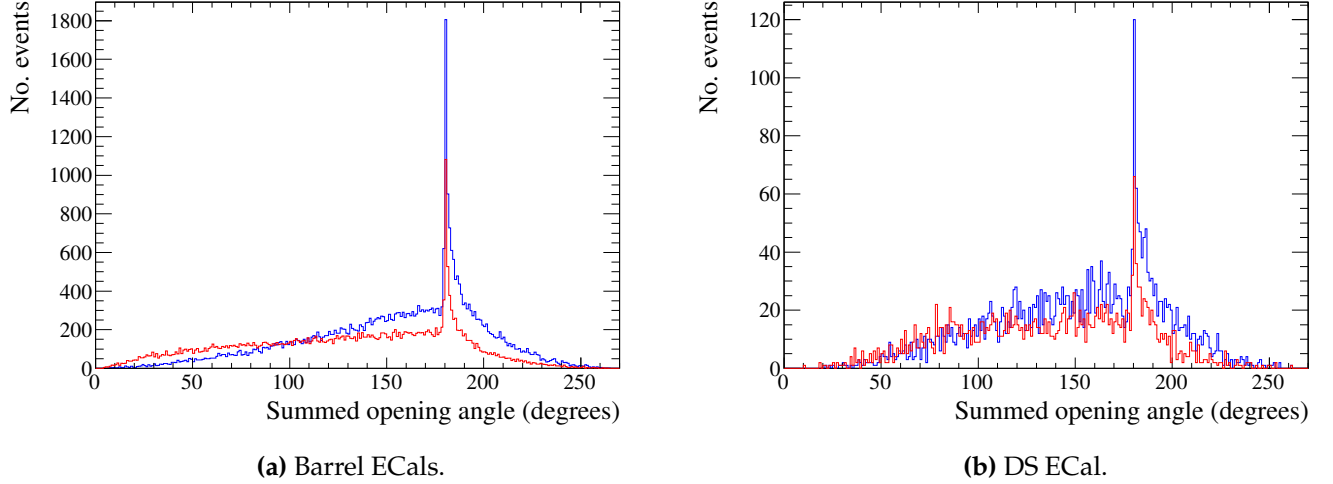


Figure 6.26: The summed opening angle subtended by every pairwise combination of the constituents prongs for the 3 prong topology. Signal and background events are the blue and red histograms respectively.

6.4.1.5 Entering background cut

The fifth cut, simply called the ‘entering background’ cut, uses the prong multiplicity aspect of a vertex to reject events that enter the ECal and then mimic a signal vertex. The cut requires at least two constituent prongs to work, so the 1 prong topology is unaffected by this. The idea is fairly simple, for each vertex, check if any of the prongs have an end which is upstream of the reconstructed vertex position. If so, it may be an entering background and could need rejecting. The position of the upstream prong end is key, as the cut should not reject every event which has an apparent backwards going track. So, the cut checks whether the upstream prong end is outside of the host ECal fiducial volume. As described in section 6.4.1.1, each ECal module uses two fiducial volumes. The 2+ prong fiducial volume would be of little use in this situation as the only strict face definition is for the downstream end of each ECal module. This motivates the use of the 1 prong fiducial volume for this cut. This cut is physically motivated and relies on parameters which have already been tuned. So, this cut requires no tuning to operate.

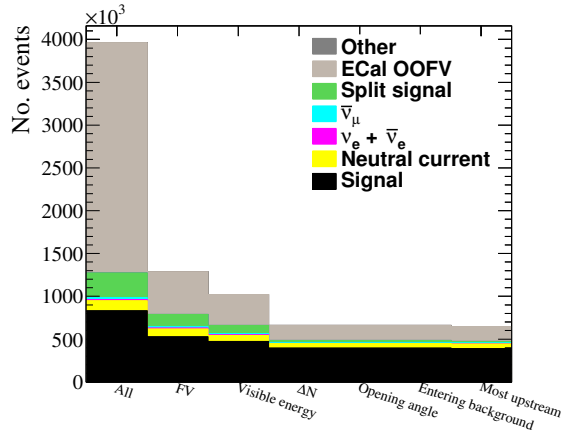
6.4.1.6 Most upstream vertex

The sixth, and final, cut implemented is motivated by the beam kinematics. As discussed in section 6.2, the expected pileup per beam bunch is small. As the reconstruction outputs events in buckets, the same philosophy can be used here: there should only be one signal events per bucket. The assumption used for this cut is any secondary interactions are likely to happen downstream of the interaction. So, the cut selects the most upstream remaining vertex in the beam bucket. As with the ‘entering background’ cut, the selection of the most upstream vertex requires no tuning to operate.

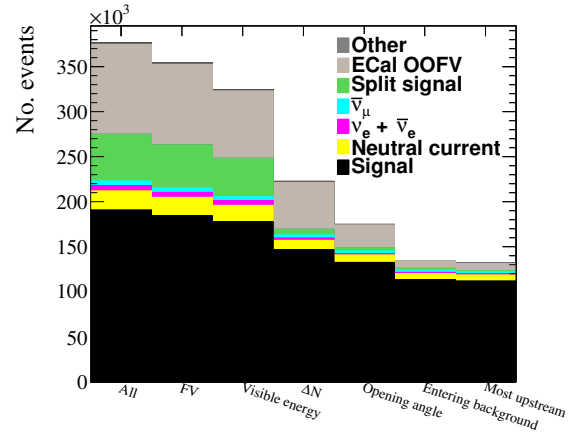
6.4.2 Performance of selection

Now that the cuts have been identified, their performance can be assessed. To do this, the Monte Carlo sample was processed through the selection and the event composition assessed at each stage. As each cut was focused on a specific topology, it is important to check the effect of the cuts on each topology. The first check is to see the event survival as a function of the cuts for each topology. These checks are shown in Fig. 6.27 and Fig. 6.28 for the barrel and DS ECals respectively. Each bin in both figures shows how many events survive after the cut has been supplied. For example, the FV bin in all of the figures shows how many events remain after applying the fiducial volume cut. As the ‘most upstream’ cut is the final cut in the selection, the final bin shows how many events remain after the full selection has been applied. The main piece of information shown is that the backgrounds are being rejected at a much higher rate than the signal, resulting in a sample that is mostly signal.

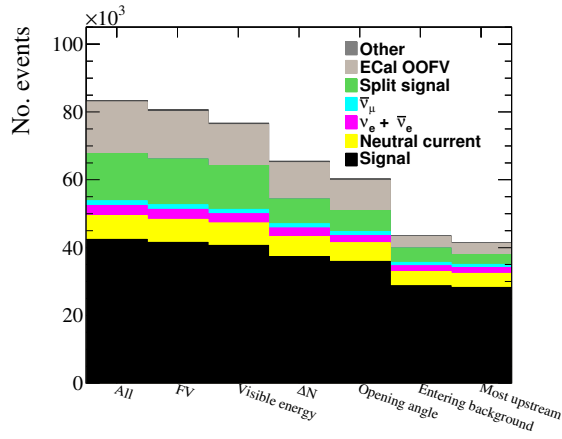
While Fig. 6.27 and Fig. 6.28 shows that the cuts are successfully rejecting background while retaining signal, it is not clear what particle species are rejected. It is important to check this so that the developed selection is understood. The background type which is rejected at the highest rate is the ECal OOFV background so it is sufficient to study the particle composition of this to understand the selection’s ability to reject particles. The particle type is defined by looking at which simulated particles contributed to the ECal cluster as whole. The particle which deposited the highest amount of energy is accepted as the one which created the ECal cluster. The ECal OOFV event survival as a function of the cuts is shown in Fig. 6.29 and Fig. 6.30 for the barrel and DS ECal



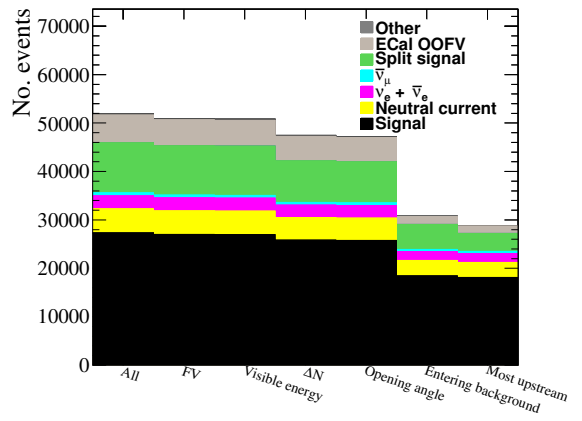
(a) 1 prong topology.



(b) 2 prong topology.

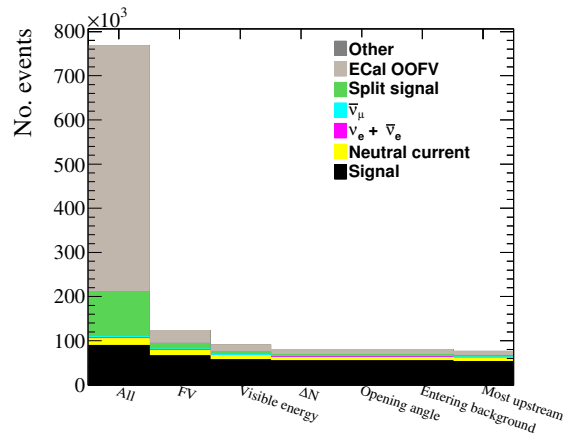


(c) 3 prong topology.

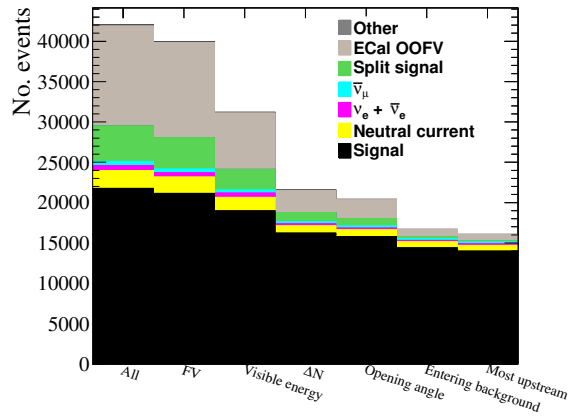


(d) 4+ prong topology.

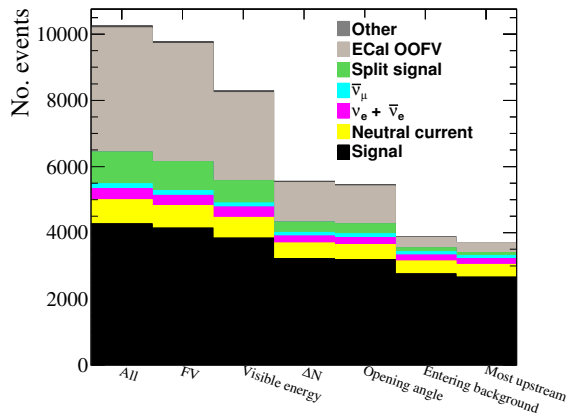
Figure 6.27: Event survival as a function of the cuts for all topologies in the barrel ECal. Each bin refers to the number of events after a cut has been applied.



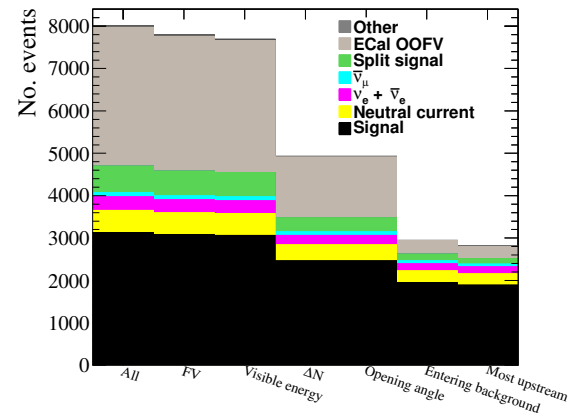
(a) 1 prong topology.



(b) 2 prong topology.



(c) 3 prong topology.

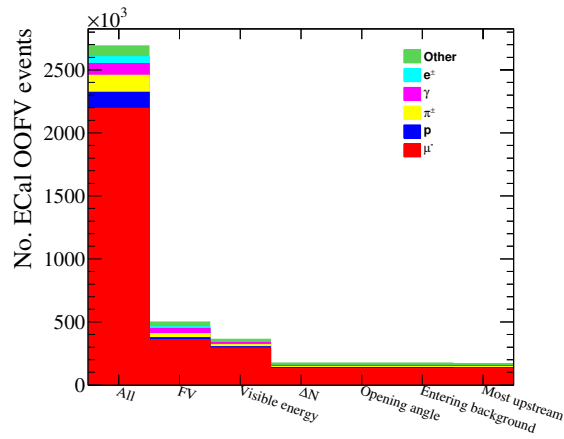


(d) 4+ prong topology.

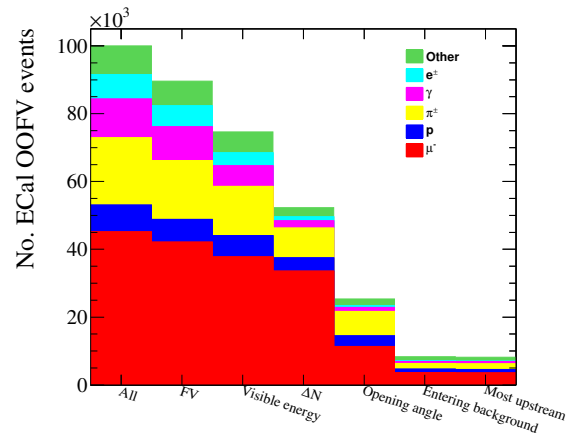
Figure 6.28: Event survival as a function of the cuts for all topologies in the DS ECal. Each bin refers to the number of events after a cut has been applied.

respectively. For each prong topology, the ECal OOFV events are separated into the main particle types which constitute the ECal OOFV background. It is clear that the cuts are rejecting the particle species that one would expect them to reject. For example, the fiducial volume cut in the 1 prong topology almost exclusively rejects entering MIPs. The visible energy and ΔN cuts work together as an effective particle shower tagger to reject e^\pm and γ particles. The opening angle and entering background cuts work as an additional MIP rejectory in cases where the track merging was unsuccessful. The composition of the ECal OOFV background has interesting features, regardless of the cuts applied. Specifically, the particle species varies to a great degree between each prong topology. For example, the 1 prong and 2 prong topologies in the barrel ECal (Fig. 6.29a and Fig. 6.29b) see a muon dominated ECal OOFV background. Whereas, the 3 prong and 4+ prong topologies see a very different background which is π^\pm dominated. The natural separation provided by the topologies should allow investigation of a specific particle species if required by any future analyser.

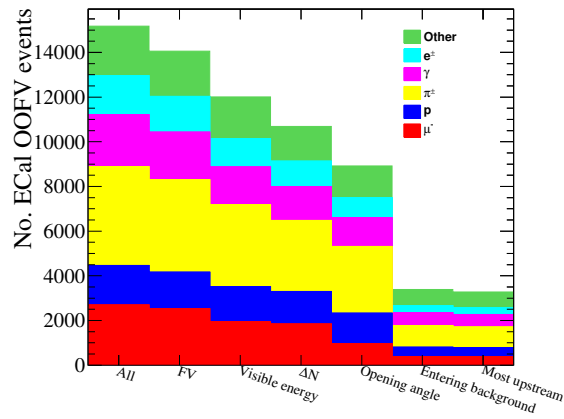
The selection efficiency and purity as a function of the cuts are shown for the barrel ECal and DS ECal in Fig. 6.31 and Fig. 6.32 respectively. Every cut which is relevant to a prong topology has an expected effect, the purity of the sample increases while the efficiency decreases. What is not so clear from the distributions is whether the tuning metric, $\phi^{\text{selection}}$, increases as a function of the cuts. So, $\phi^{\text{selection}}$ is shown in a similar manner for the barrel and DS ECal in Fig. 6.33 and Fig. 6.34 respectively. The tuning metric optimisation in both the barrel and DS ECal shows some interesting features. Firstly, in the barrel, it is clear that for the 1 prong and 2 prong topologies, every applied cut shows a clearly increasing $\phi^{\text{selection}}$. Unfortunately, this is not the case for the 3 prong and 4+ prong topologies. Specifically, the entering background cut degrades the value of $\phi^{\text{selection}}$. This is most obvious in the 4+ prong topology, however it has already been stated that this topology is effectively an overflow bin and is being included more for completeness. What is perhaps more concerning is the degradation of $\phi^{\text{selection}}$ in the 3 prong topology. Fortunately, the decrease in $\phi^{\text{selection}}$ is small when the entering background cut is applied and the change is well within error. It is important to bear in mind that $\phi^{\text{selection}}$ is used as a tuning guide and small deviations from the optimisation process are allowed. It was decided that the entering background cut would remain in place for both the 3 prong and 4+ prong topologies. The $\phi^{\text{selection}}$ distribution in the DS ECal shows some similar and different features to that of the barrel. As with the barrel ECal case, $\phi^{\text{selection}}$ clearly increases as a function of the cuts for the 1 prong and 2 prong topologies. Unlike the barrel ECal, there is



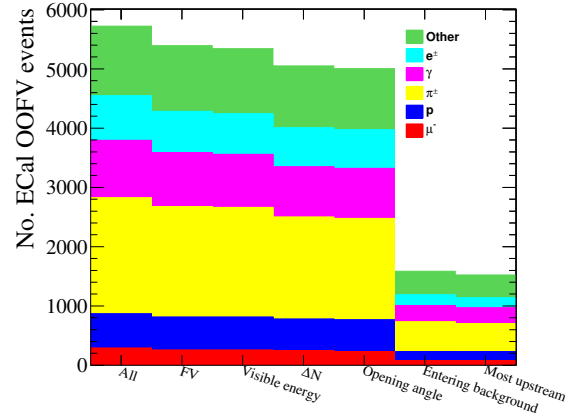
(a) 1 prong topology.



(b) 2 prong topology.

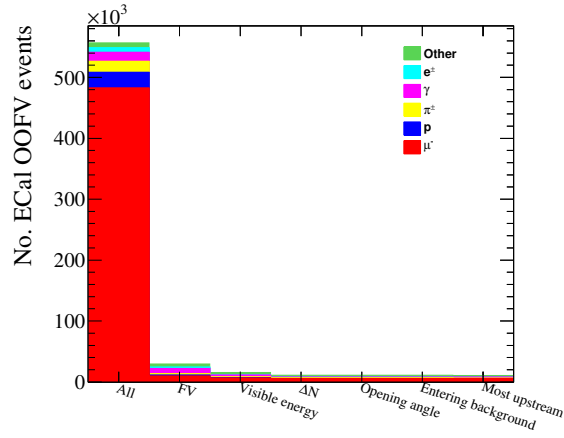


(c) 3 prong topology.

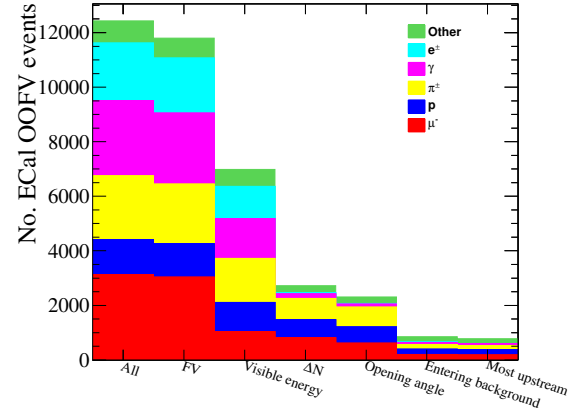


(d) 4+ prong topology.

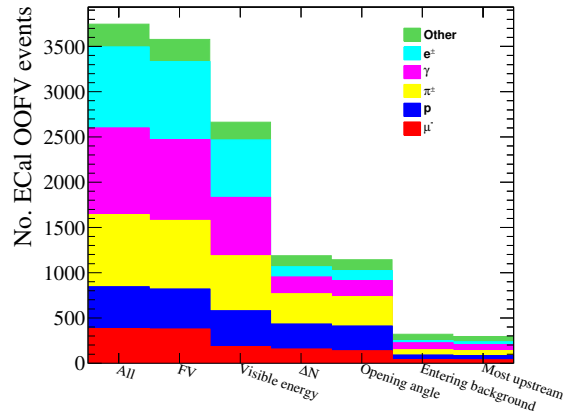
Figure 6.29: ECal OOFV event survival as a function of the cuts for all topologies in the barrel ECal. Each bin refers to the number of events after a cut has been applied.



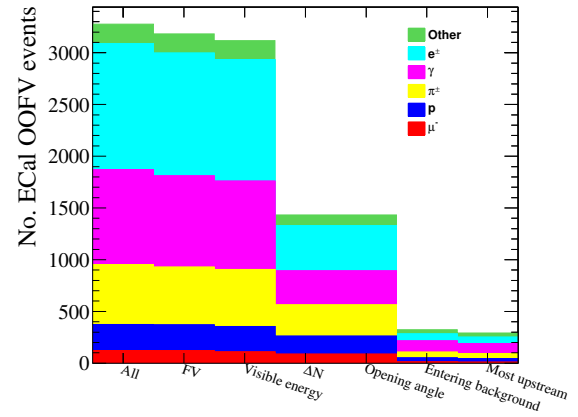
(a) 1 prong topology.



(b) 2 prong topology.



(c) 3 prong topology.



(d) 4+ prong topology.

Figure 6.30: ECal OOFV event survival as a function of the cuts for all topologies in the DS ECal. Each bin refers to the number of events after a cut has been applied.

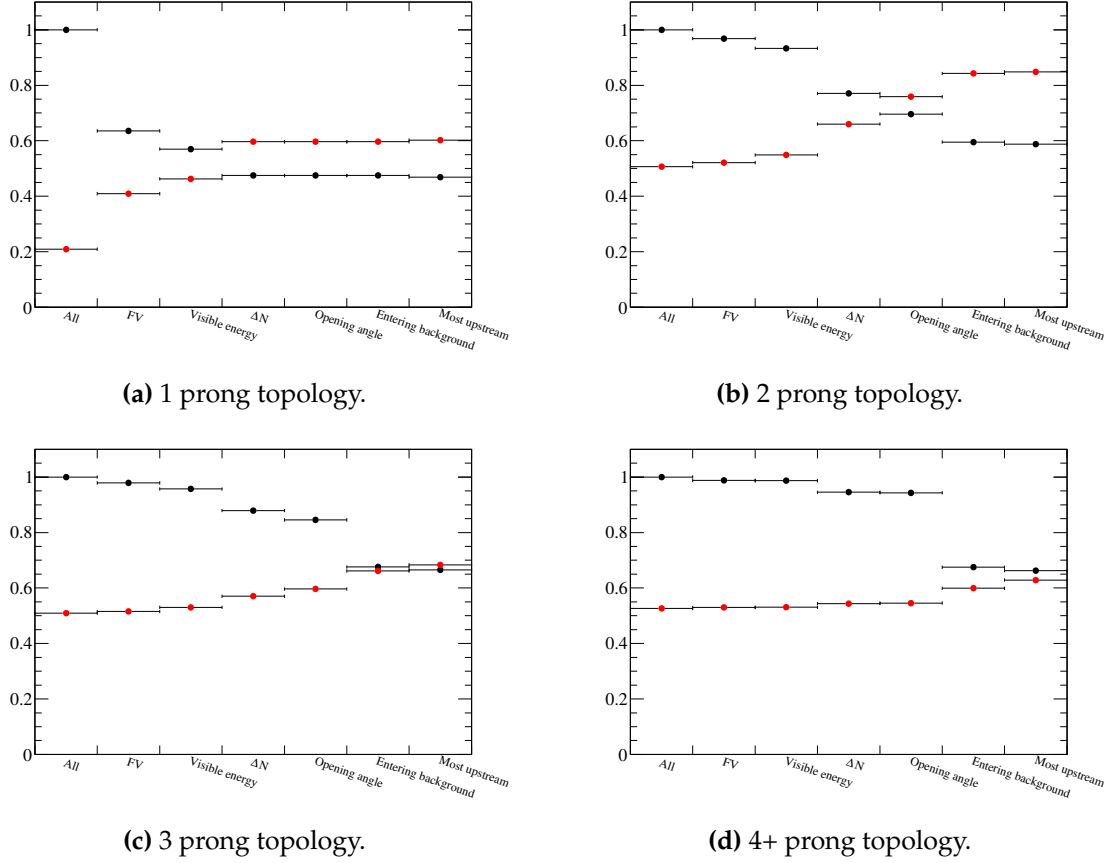
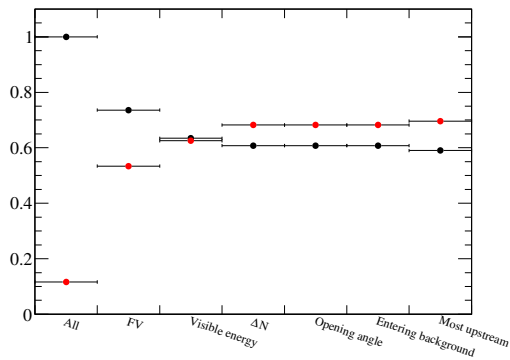


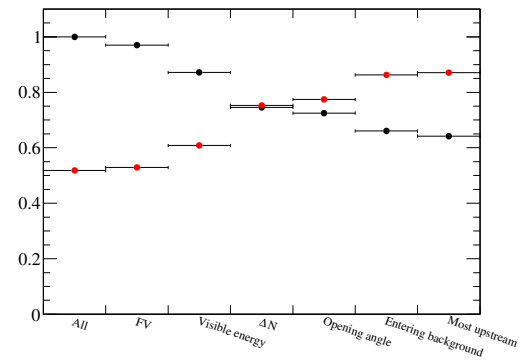
Figure 6.31: The selection efficiency (black) and purity (red) as a function of the cuts in the barrel ECal. Each bin refers to the efficiency and purity after a cut has been applied.

also an increase in $\phi^{\text{selection}}$ when applying the entering background cut. However, there is a minor decrease in $\phi^{\text{selection}}$ when selecting the most upstream vertex. It is not wholly surprising that this is the case as the DS ECal is the most downstream detector in ND280. Such a cut can easily cause a bias where events in the barrel are generally preferred because of their extent in the global Z direction. Fortunately, this effect is very minor and also well within error.

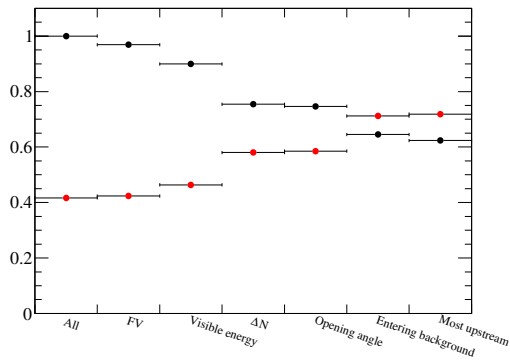
The cross-section measurement presented in this analysis is an inclusive measurement. This means that the neutrino interaction cross-section needs to be measured without bias across the J-PARC beam energy range. All of the performance checks presented so far have only assessed each prong topology individually. So, the final check is to assess how the selection performs after combining the topologies together. The selection efficiency and purity after combining the topologies is shown in Fig. 6.35. For both



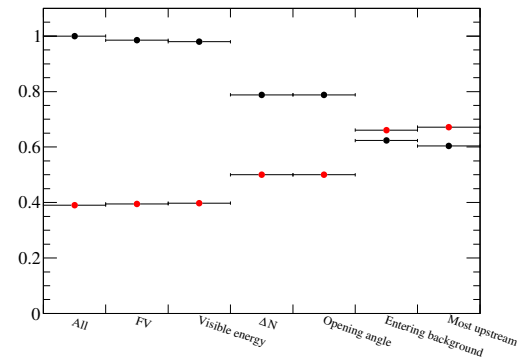
(a) 1 prong topology.



(b) 2 prong topology.

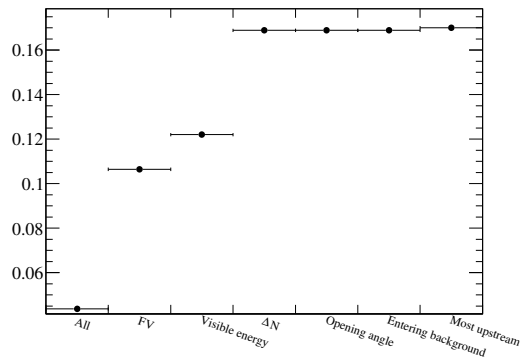


(c) 3 prong topology.

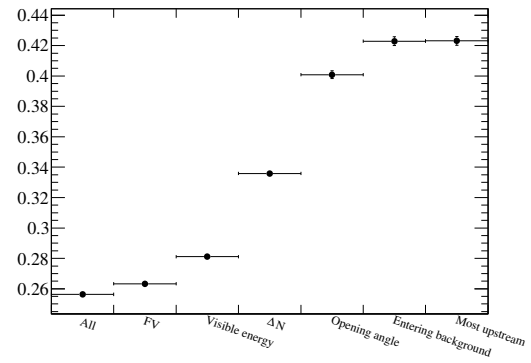


(d) 4+ prong topology.

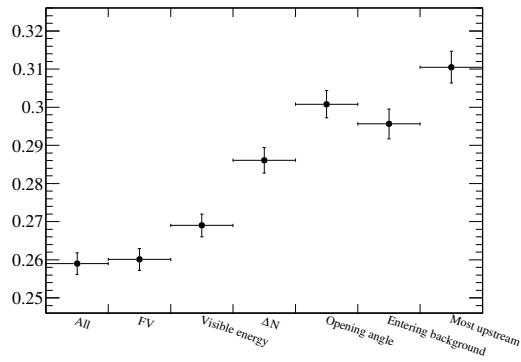
Figure 6.32: The selection efficiency (black) and purity (red) as a function of the cuts in the DS ECal. Each bin refers to the efficiency and purity after a cut has been applied.



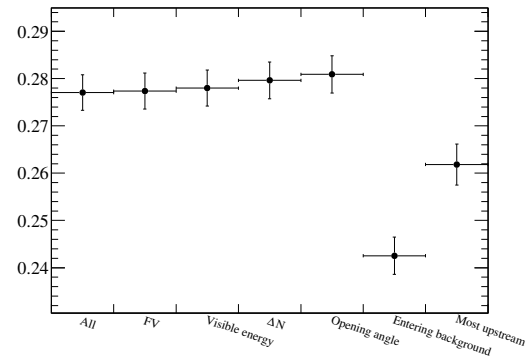
(a) 1 prong topology.



(b) 2 prong topology.

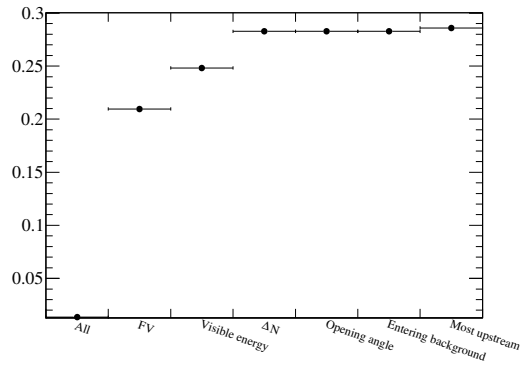


(c) 3 prong topology.

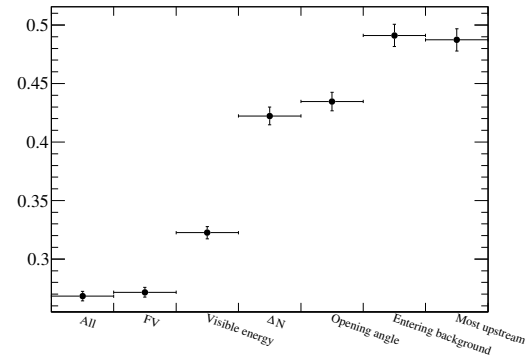


(d) 4+ prong topology.

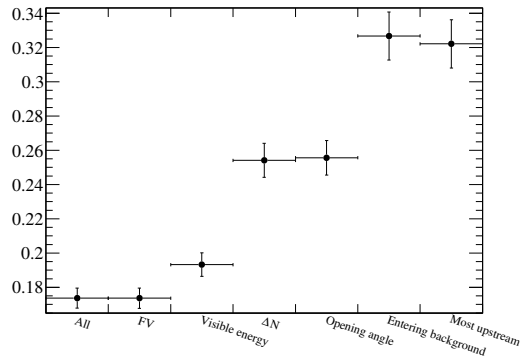
Figure 6.33: $\phi^{\text{selection}}$ as a function of the cuts in the barrel ECal. Each bin refers to the value of $\phi^{\text{selection}}$ after a cut has been applied.



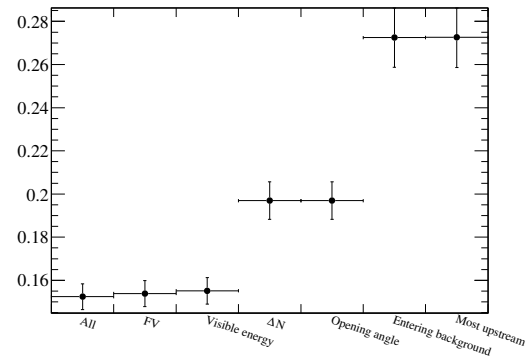
(a) 1 prong topology.



(b) 2 prong topology.



(c) 3 prong topology.



(d) 4+ prong topology.

Figure 6.34: $\phi^{\text{selection}}$ as a function of the cuts in the DS ECal. Each bin refers to the value of $\phi^{\text{selection}}$ after a cut has been applied.

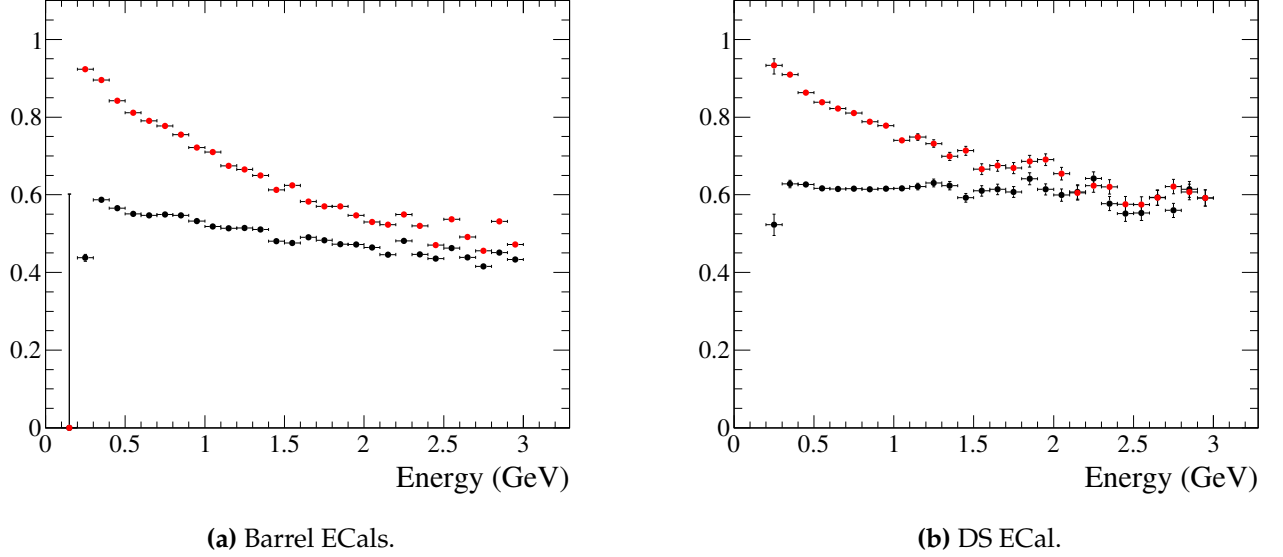


Figure 6.35: The selection efficiency (black) and purity (red) for the combined prong topologies as a function of neutrino energy.

the barrel ECal and DS ECal, there is a clear dependence of the purity on the neutrino energy. However, this should be expected. It is clear that the purity decreases as the neutrino energy increases which can be explained by the self-shielding effect of the ECal. In the low energy regime, the ECal OOFV background is suppressed because there is insufficient energy to either penetrate the ECal or deposit enough energy to allow cluster reconstruction. As the background energy increases, the suppression is lifted, resulting in a decrease in the selection purity. The key piece of information shown in Fig. 6.35 is the selection efficiency. As described above, it is of vital importance that the selection does not introduce a bias which measures one energy regime more than another. The flatness of the efficiency distributions for both the barrel ECal and DS ECal shows this is not the case which means the selection presented here would be suitable for a CC-inclusive measurement.

The number of selected events for each prong topology is shown in Fig. 6.36, with each topology broken down by event categories. For both the barrel and DS, signal events dominate each prong topology. The most impure topology for both detectors is the 1 prong topology. This is primarily due to having an insufficient number of prongs to really benefit from what the reconstruction can provide. Despite this, it is clear that the selection results in a pure sample of events.

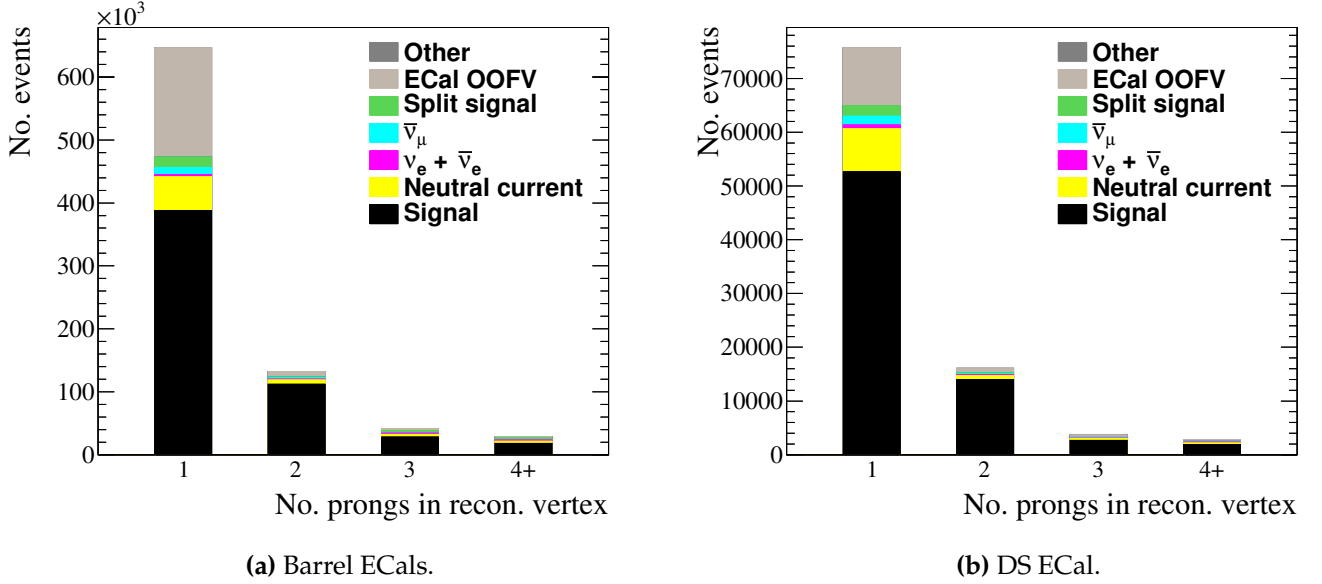


Figure 6.36: The number of selected events in the Monte Carlo sample, separated out into the prong topologies. Each event is categorised by the associated truth information from the simulation.

ECal module	1 prong topology efficiency (%)	2 prong topology efficiency (%)	3 prong topology efficiency (%)	4+ prong topology efficiency (%)
Barrel	46.8	58.7	66.5	66.3
DS	59.0	64.2	62.3	60.4

Table 6.9: The selection efficiencies for each prong topology and ECal module.

The selection and efficiencies for each prong topology are shown in table 6.9 and table 6.10 respectively. The final purities and efficiencies are generally very good. The only concern is the 1 prong topology efficiency in the barrel ECal which is notably lower than all other efficiencies. The main reason for the low efficiency is the strict fiducial volumes defined for each ECal module. Generally speaking, this low efficiency may cause a problem if there is a significant amount of signal migration from the 2 prong topology which is more efficient. It is important to address this when assessing systematic uncertainties for the analysis.

The selection efficiency is defined to be 100% when no cuts have been made. There are inevitably signal events which are not reconstructed, primarily because the energy

ECal module	1 prong topology purity (%)	2 prong topology purity (%)	3 prong topology purity (%)	4+ prong topology purity (%)
Barrel	60.3	85.0	68.5	63.0
DS	69.6	87.2	72.0	67.3

Table 6.10: The selection purities for each prong topology and ECal module.

ECal module	Efficiency (%)	Purity (%)
Barrel	42.4	64.4
DS	53.0	72.4

Table 6.11: The topology combined efficiency and purity.

is below reconstruction threshold. It is non-trivial to include these events in specific prong topology calculation, but it is also unnecessary to do this as the prong topologies are to be summed for the CC-inclusive cross-section measurement. So, the topology combined efficiency and purity are presented in table 6.11. It is these numbers, along with the sample itself, which are the final output of the Monte Carlo selection.

Chapter 7

Measurement of the ν_μ charged current inclusive cross-section on Pb

This chapter presents the measurement of the ν_μ CC inclusive cross-section on Pb using the ND280 ECals. This chapter details the measurement method, the samples used in the measurement, the assessment of the systematic uncertainties, validation of the measurement method and finally the measurement itself.

7.1 Measurement method

The chosen method [22, 23] fits a prediction to measured data using multiple data samples. The core of the analysis method is a χ^2 fit which tries to minimise the difference between the prediction and the data. The χ^2 is defined as

$$\chi^2 = \Delta\vec{N}^T (\underline{\underline{V}}^{\text{syst}} + \underline{\underline{V}}^{\text{stat}})^{-1} \Delta\vec{N}, \quad (7.1)$$

where $\underline{\underline{V}}^{\text{syst}}$ and $\underline{\underline{V}}^{\text{stat}}$ are the systematic and statistical covariance matrices for the sample and $\Delta\vec{N}$ contains the difference between the data and the prediction for each sample. If the number of samples used is M , $\Delta\vec{N}$ is defined as

$$\Delta\vec{N} = \begin{pmatrix} N_1^{\text{data}} - N_1^{\text{pred}} \\ \vdots \\ N_M^{\text{data}} - N_M^{\text{pred}} \end{pmatrix}. \quad (7.2)$$

For sample j of the sample set M , N_j^{data} and N_j^{pred} are the number of measured data events and number of predicted events. The extractable information from the fit is located in N_j^{pred} which can be subdivided into a set of templates, each of which are assigned a normalisation parameter, namely

$$N_j^{\text{pred}} = \sum_i R_i n_{ij}, \quad (7.3)$$

where n_{ij} is the number of events in template i of sample j and R_i is the normalisation assigned to that template. The normalisation parameters are free to float in the fit and so it is in the normalisation parameters that the desired physical information is located.

7.2 Input samples to the fit

The DS ECal provides the main signal sample which will be used to extract the cross-section. As shown in table 6.11, the selected sample in the DS ECal has the highest purity and efficiency in the whole selection making the sample the natural choice to extract the cross-section.

The method outlined above allows for the simultaneous constraint of a physical parameter and the background contamination of a set of input samples. The method works particularly well when the input samples do not share the same sensitivity to a particular background type. For example, in ND280, each ECal module is exposed to a different beam intensity and energy spectrum and so is exposed to a unique amount of beam induced background. Each ECal module can be thought of as a separate input sample which fits well with the method outlined above. So, while the DS ECal will provide the target in which the cross-section will be extracted, the barrel ECals are to also be included in the fit as a background constraint. To further allow the barrel ECals to achieve this, an additional sample of barrel ECal events are to be included. This additional sample set, called the 'reverse' sample set, comes from the same data set as the selected sample described in chapter 6. However, the events in the reverse sample set are events which pass the fiducial volume cuts but fail any other cut. An example of a selected sample compared with a reverse sample is shown in Fig. 7.1. There are clear differences in the shape of the energy spectrum between Fig. 7.1a and Fig. 7.1b which suggests that the selection is biased towards lower energy neutrino interactions, despite the flat efficiency curves shown in Fig. 6.35a. The apparent bias

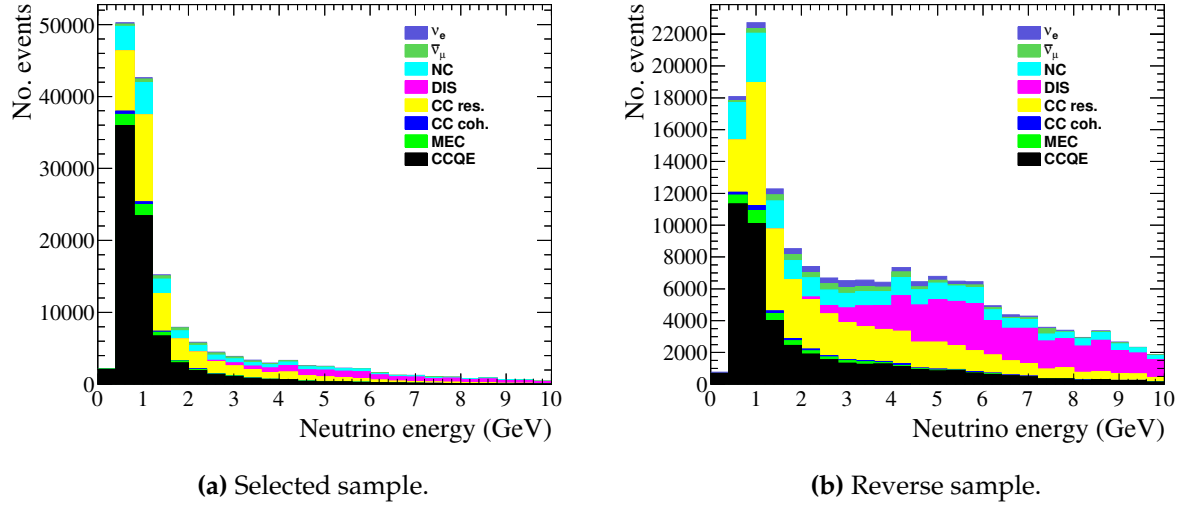


Figure 7.1: The neutrino energy of events seen in the bottom-left ECal module broken down by the neutrino interaction mode.

is actually an effect of higher energy interactions creating a surplus of reconstructed events, most of which are cut away by the selection. The shape of the true neutrino energy spectrum (see Fig. 6.1 for an example) is actually more like the selected sample shown in Fig. 7.1a.

As described in chapter 6, the developed selection does not distinguish between lead and carbon interactions, partly because such events are indistinguishable from one another. It is however desirable to separate the two categories out as the presented measurement purely involves lead. As the ECal is not capable of separating the events by itself, an additional constraint is needed. So, a sample of CC interactions on carbon occurring in the FGD are also included, which are taken from the official ND280 oscillation input analysis [INSERT TECHNOET REFERENCE!!!!].

To summarise, there are many inputs samples to the measurement. Specifically, there are 12 barrel ECal samples (6 selected and 6 reverse), the DS ECal sample and the FGD sample which totals to 12 input samples.

7.3 The ECal rate fit

Now that the general method and the input samples have been introduced, the fit used by the analysis can be introduced. The fit itself is a data-driven constraint of the event rate in each ECal module where the Monte Carlo prediction is separated into templates whose normalisation is allowed to vary. The machinery outlined in section 7.1 almost completely describes what is required to understand the fit, however two specific definitions are needed. The first is that there are 12 input samples to the fit. The second is the definition of N_i^{pred} . To constrain the lead event rate, three Monte Carlo templates are needed: a lead template which contains any reconstructed event associated with a ν_μ CC interaction on lead, a carbon template which contains any reconstructed event associated with a ν_μ CC interaction on carbon and an 'other' template which contains any reconstructed event which does not fall into the above two categories. N_i^{pred} is then defined as

$$N_i^{\text{pred}} = R^{\text{Pb}} n_i^{\text{Pb}} + R^{\text{C}} n_i^{\text{C}} + R^{\text{other}} n_i^{\text{other}}, \quad (7.4)$$

where n_i^{X} is the number of events in template X of sample i and R_i^{X} is the variable normalisation of that template.

The rate fit allows R_i^{Pb} , R_i^{C} and R_i^{other} to vary with no prior constraint in an attempt to minimise the χ^2 as defined in equation 7.1. Once the minimum has been found, the fitted R_i^{Pb} can then be used to extract the cross-section using the selected events in the DS ECal.

The number of events in each input sample, broken down by the template contribution, is shown in Fig. 7.2. As should be expected, the relative background contribution varies between each ECal module.

The underlying fit machinery uses the Minuit2 algorithm provided by the ROOT TFitter framework, chosen primarily because of its ease of use.

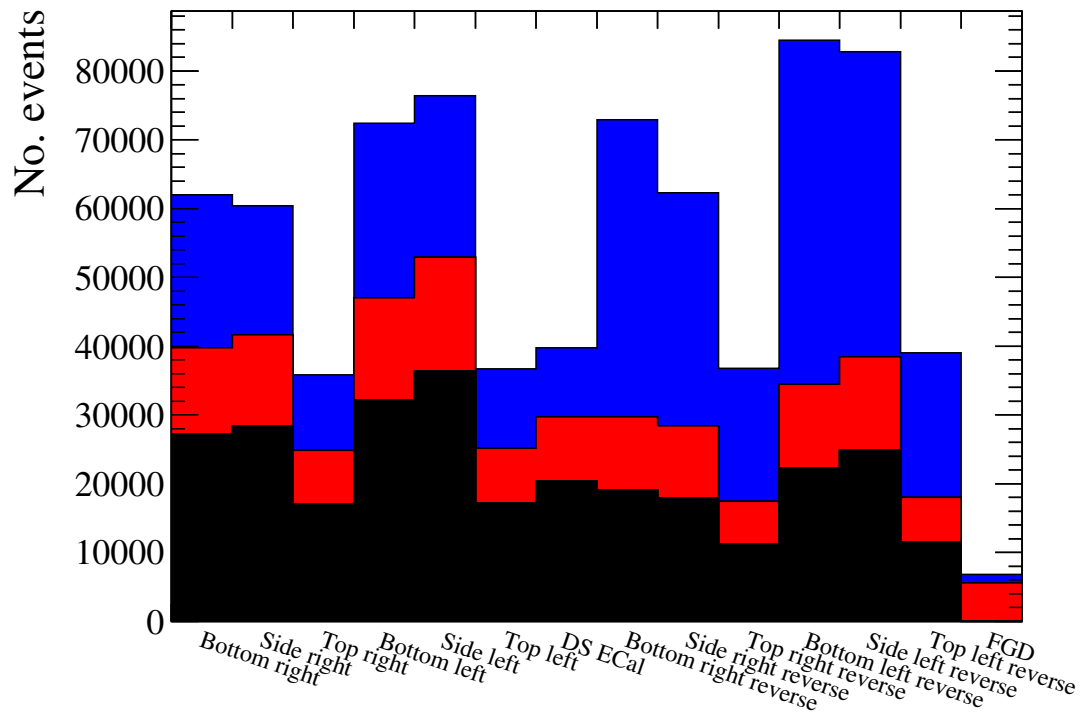


Figure 7.2: The number of events in each input sample separated into the lead (black), carbon (red) and other (blue) templates.

7.4 Systematic uncertainties

The χ^2 definition shown in equation 7.1 allows for systematic uncertainties to be directly included in the fit. As the systematic uncertainty implementation takes the form of a covariance matrix for the input samples, a good understanding of not only the systematic uncertainties, but how the samples correlate with one another is needed.

As stated above, there are 12 input samples so the covariance matrix will be a 12×12 symmetric matrix. While it may be obvious that the contents of the matrix will be the covariances of each input sample, it may not be immediately clear what type of covariances are needed. As described in section 7.3, the algorithm attempts to fit a set of predictions, separated into templates, to a set of measured data samples simultaneously. The variation comes from the normalisations assigned to each template. This means that the overall normalisation of the Monte Carlo prediction is free to vary without prior constraint and so it is the shape information between the prediction and data that constrains the parameters. Therefore the covariance matrix used in the fit should only contain uncertainties which account for the differences in the shape of the samples which the systematic sources introduce.

The ND280 event simulation is essentially broken down into three areas: Simulation of the neutrino flux, simulation of the neutrino interactions and simulation of the detector response. No matter how complicated a simulation can become, it is unlikely to ever simulate reality with 100% accuracy. The differences between what is simulated (be it flux, interaction or detector) and what happens in nature causes a systematic difference to be seen between collected data and Monte Carlo which must be accounted for. As the simulation can be broken down into three key areas, the systematic assessment can be broken down into the same key areas, each of which are presented. The actual assessment of a systematic uncertainty can be broken down into two areas: identification of a systematic error source and the propagation of that systematic error source through the analysis. The identification stage is typically handled by a respective working group or by an analyser with external sources (e.g. control samples). The propagation of the systematic error source has no strict recipe but it typically involves variation of the identified systematic uncertainty and then either a reweighting of events is applied or the analysis chain is re-run. The systematic treatment used in this analysis uses a mixture of the above.

To propagate the systematic uncertainty effect, a Monte Carlo sample akin to the prediction sample set used in the fit is required. So, a 2.5×10^{19} POT sub sample of beam and sand Monte Carlo is used for this purpose. All sample systematic covariance matrices are presented as fractional covariance matrices between each of the different detector samples. For the barrel samples, the selected samples are labelled by their respective module name and the reverse barrel samples (background enriched samples) are labelled with their module name and 'reverse'. The assessment of each systematic source is presented individually, resulting in a fractional covariance matrix for that source. The final systematic covariance matrix is then found by summing all of the individual covariance matrices.

7.4.1 Flux systematic evaluation

The neutrino flux is one of the core components of the ND280 event simulation and any uncertainties associated with the flux have a direct impact on the measured ND280 event rate. The associated flux uncertainties can be broken down into four categories:

- Properties of the proton beam such as profile and alignment
- Alignment of the target and focusing horns
- The current in the focusing horns and the magnetic field it generates
- Hadron production induced by beam interactions with the target

As the neutrino flux prediction is so important for all T2K analyses, the flux uncertainties are constrained using a range of measurements. These include external measurements from the NA61/SHINE collaboration, from the proton beam monitors, measurements of a spare magnetic horn and from the INGRID detector. Measured uncertainties from each source are used to vary the flux in JNUBEAM which produces a covariance matrix for each source. The covariance matrix then used by analyser is the sum of each covariance matrix which is shown in Fig. 7.3. The covariance matrix is split into two detector sections: ND280 and SK. Each detector section is then separated into two beam running modes (ν and $\bar{\nu}$ runnings) which are also separated into four neutrino flavours (ν_μ , $\bar{\nu}_\mu$, ν_e and $\bar{\nu}_e$). Finally, each neutrino flavour is separated into a set of energy bins. The presented analysis is a ν_μ cross-section measurement using ND280, so only the ND280, ν -running mode section of the covariance matrix needs consideration. The provided flux covariance matrix is a fractional covariance matrix,

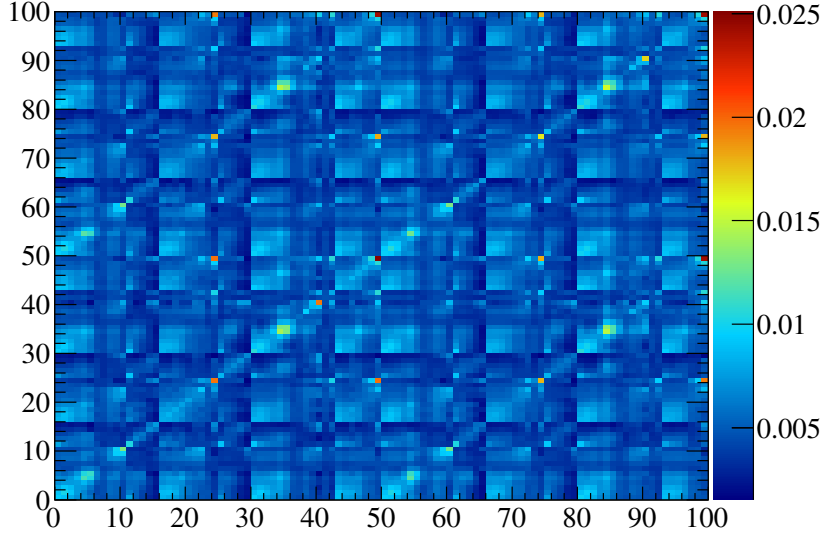


Figure 7.3: The flux prediction covariance matrix. The matrix is binned in detector (SK and ND280), neutrino flavour and energy.

binned in neutrino energy and flavour. As the neutrino energy and flavour information of events seen in this analysis is readily available, the flux covariance matrix can be used to reweight the events in the Monte Carlo sample to propagate the effect of the systematic uncertainty through the analysis. To do this, the flux covariance matrix is Cholesky decomposed and the resulting matrix multiplied by a vector filled with random throws from a Gaussian of mean 0 and width 1. Each element in this multiplied vector constitutes a fractional change in the number of a specific neutrino flavour and energy seen in the analysis. So, the event weightings are generated by adding 1 to each element of this vector. Every event selected in the sample is then weighted by the correct event weight (in this case defined by the neutrino flavour and energy) and this number of reweighted events is then recorded. The above description describes a single throw of the flux systematic propagation. This process is repeated 1000 times to build up the covariance matrix for the sample. The sample covariance matrix elements are calculated as

$$V_{ab} = \frac{1}{N^{\text{throws}}} \sum_{i=1}^{N^{\text{throws}}} \frac{(N_a^i - N_a^{\text{nom}})(N_b^i - N_b^{\text{nom}})}{N_a^{\text{nom}} N_b^{\text{nom}}}, \quad (7.5)$$

where N_a^{nom} is the number of events seen in the nominal Monte Carlo for sample a and N_a^i is generically the number of events seen in sample a for systematic throw

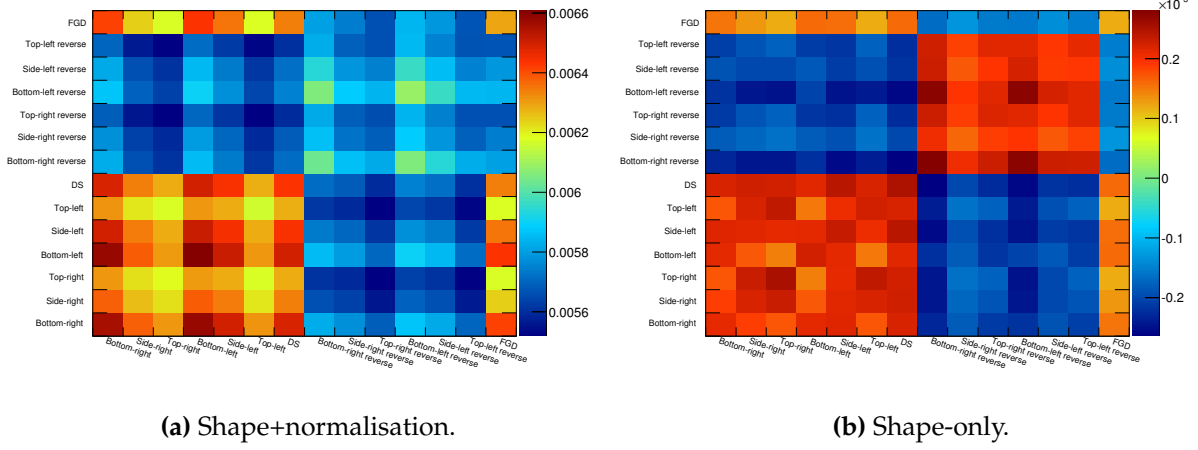


Figure 7.4: The sample covariance induced by the flux uncertainties.

i , but its definition depends on which kind of covariance matrix is being calculated. For a shape+normalisation covariance matrix, N_a^i is defined as

$$N_a^i = N_a^{i'}, \quad (7.6)$$

where $N_a^{i'}$ is simply the number of events in sample a for throw i after applying the systematic variation. In the above example, this after applying the event reweighting based on the flux covariance matrix. When considering a shape-only covariance matrix, N_a^i is

$$N_a^i = N_a^{i'} \frac{\sum_{j=1}^{12} N_j^{\text{nom}}}{\sum_{j=1}^{12} N_j^{i'}}. \quad (7.7)$$

The extra factor on the RHS of equation 7.7 convserves the total number of events seen such that there are an equal total number of events before and after applying the systematic variation. The sample covariance matrices found by applying the above process are shown in Fig. 7.4.

The effect of the flux systematic on the selection efficiency of lead interactions was also evaluated. As the main target used in this analysis is the DS ECal, the efficiency variation was evaluated for this detector only. For each systematic throw described above, the selection efficiency was calculated and recorded. By plotting the efficiency

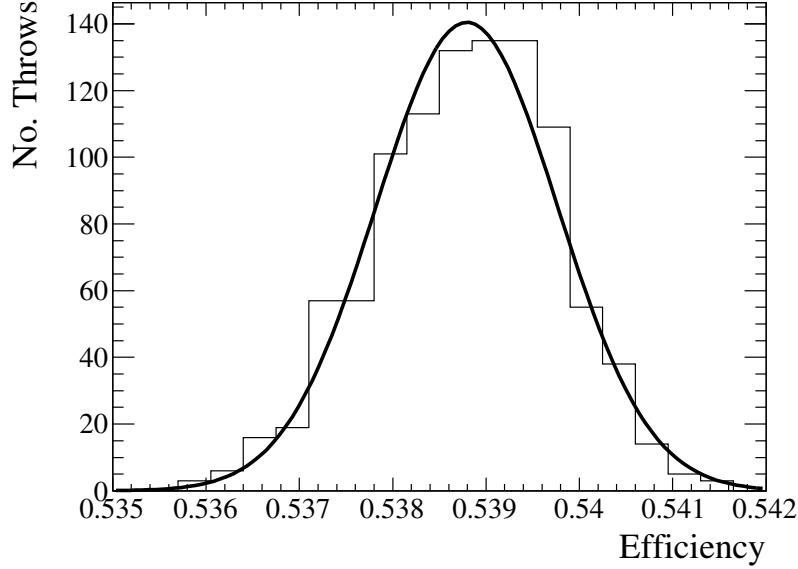


Figure 7.5: The variation in the selection efficiency of lead interactions in the DS ECal caused by the flux systematic.

for each throw, the width of the efficiency distribution can be found which gives the efficiency uncertainty induced by the flux systematic. This efficiency uncertainty was found to be 0.00097. The lead selection efficiency in the DS ECal is nominally 0.539, which implies a fractional change of 0.18%, which is essentially negligible.

7.4.2 Cross-section systematic evaluation

The neutrino cross-section picture is still a very much open area of research. The interaction model used by current neutrino interaction generators use a set of empirical parameters which are tuned on experimental results. Uncertainties on any one of these empirical parameters will alter the simulated cross-section and thus the event rate seen in the ND280 simulation. A dedicated working group handles the assessment of the empirical parameters and their corresponding uncertainties. The parameter uncertainties are given as a covariance matrix along with the known correlations which is shown in Fig. 7.6. The interaction parameter assessment is chiefly undertaken with the T2K oscillation analyses in mind which means that the nuclear model parameters are only considered for carbon and oxygen. In the presented analysis, iron and aluminium are two major sources of background interactions which must also be treated in the systematic assessment. The chosen treatment is to assign a data-motivated,

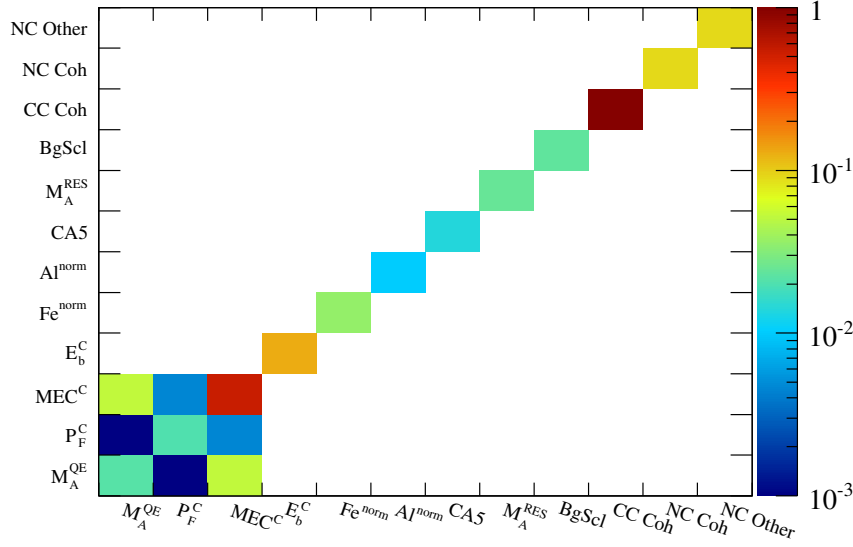


Figure 7.6: The neutrino cross-section model covariance matrix.

normalisation uncertainty to such backgrounds. The iron uncertainty is taken from the iron cross-section measurement using INGRID. The aluminium uncertainty is taken from [INSERT DETAILS HERE]. As element specific parameters for lead do not appear in Fig. 7.6, such parameters are additionally assessed separately using NEUT.

To propagate the effect of the cross-section systematic through the analysis, the covariance matrix shown in Fig. 7.6 was Cholesky decomposed and the resultant matrix multiplied by a vector of random numbers thrown from a gaussian (the same approach as described in section 7.4.1). However, the re-weighting in this case is more complicated. The T2KReWeight [INSERT REFERENCE] software takes the parameters errors from the throw along with the simulated NEUT vertex which is matched to the event. T2KReWeight then calculates a weight based on the inputted errors and the NEUT vertex in question. Using the T2KReWeight machinery, 1000 systematic throws from the covariance matrix shown in Fig. 7.6 were made and sample covariance matrices were calculated, which are shown in Fig. 7.7.

As with the flux systematic, the uncertainty in the selection efficiency for lead interactions in the DS ECal due to the cross-section model systematic was found by recording the efficiency for each throw. The variation in the efficiency is shown in Fig. 7.8. The efficiency uncertainty was found to be 0.001 which corresponds to a 0.2%

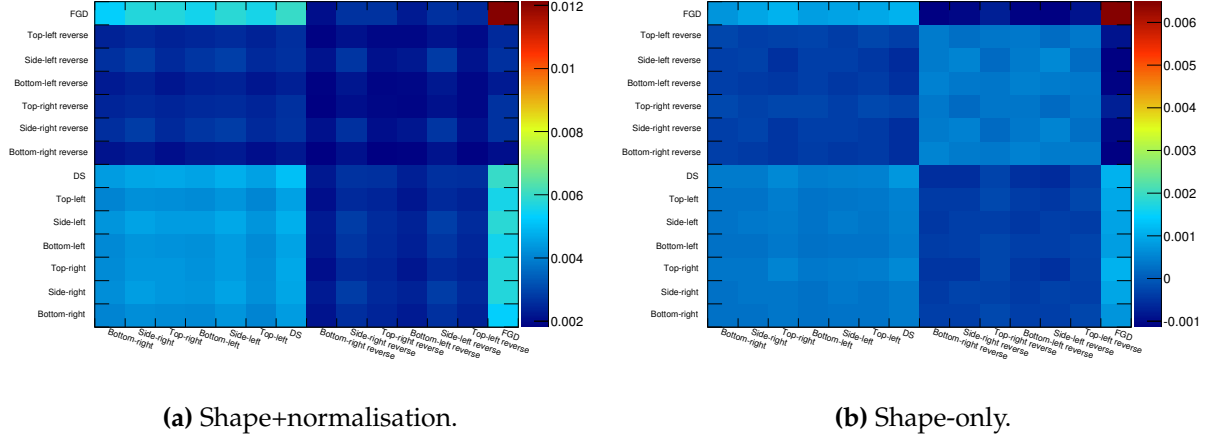


Figure 7.7: The sample covariance induced by the cross-section model uncertainties.

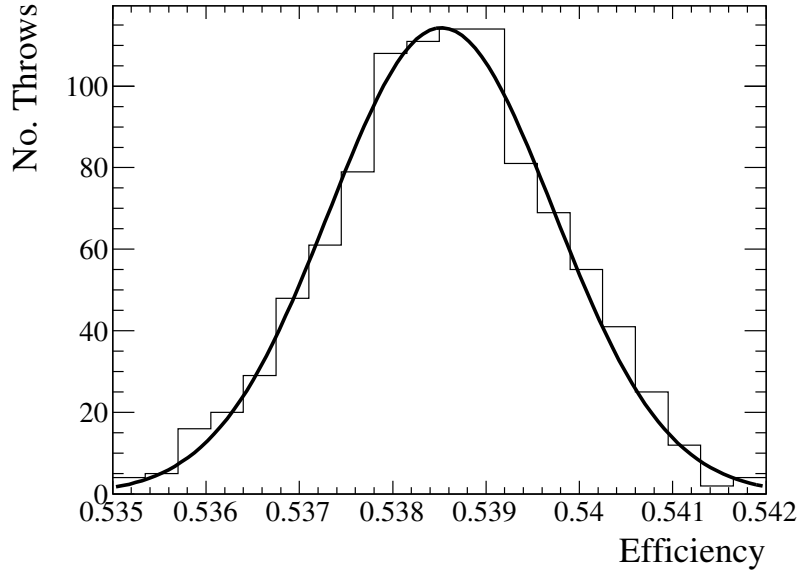


Figure 7.8: The variation in the selection efficiency of lead interactions in the DS ECal caused by the cross-section model systematic.

error which is, again, negligible.

As discussed above, the re-weighting of element specific parameters for events matched to a lead interactions was not possible using T2KReWeight. As meson-exchange current interactions for lead interactions are not implemented in NEUT, the only parameters necessary to vary are P_F^{Pb} and E_b^{Pb} which are the Fermi-momentum and binding energy for lead respectively. So, NEUT was used to produce 10,000 neutrino

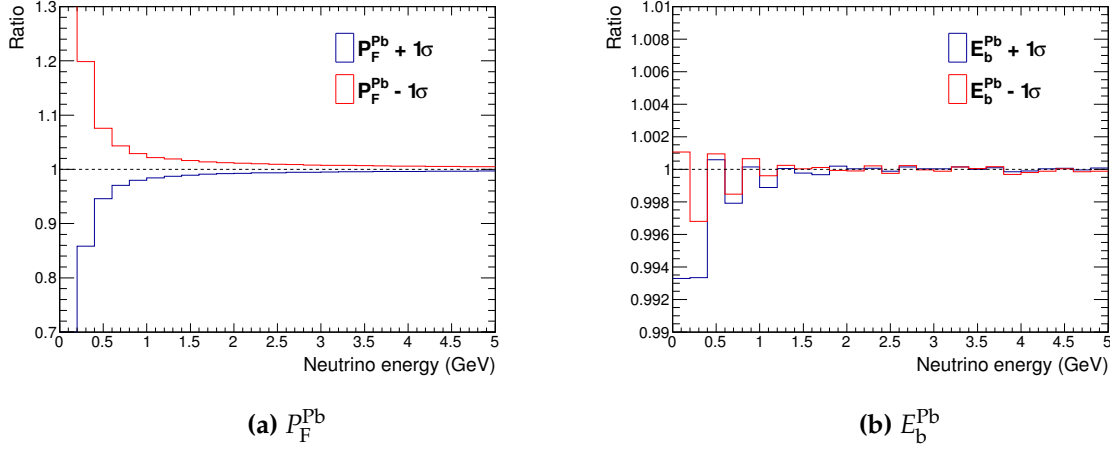


Figure 7.9: The ratio of the $\pm \sigma$ cross-section to the nominal cross-section for lead as a function of neutrino energy.

interactions on lead with uniform energy between 0 GeV and 10 GeV for the nominal parameters and $\pm \sigma$ variations of the parameters. The associated uncertainties were not readily available in the literature so $1.5 \times$ the carbon parameters uncertainties were used as a conservative estimate. The NEUT events were used to plot the ratio of the varied cross-section to the nominal cross-section as a function of energy. The ratios for P_F^{Pb} and E_b^{Pb} are shown in Fig. 7.9a and Fig. 7.9b respectively. The variation in the cross-section caused by variation in E_b^{Pb} is sub-percent so there should be a negligible variation in the event rate which means this can be ignored. However, there is significant variation in the cross-section at low energy due to variations in P_F^{Pb} so this effect must be propagated through the analysis. To do this, the ratio distributions shown in Fig. 7.9a were treated as a set of events weights. The $+\sigma$ and $-\sigma$ weights were applied to the sample separately, creating two systematics throws. The results of the systematic throws were used to generate the sample covariances, which are shown in Fig. 7.10.

Final state interactions (FSI) within the nucleus after a neutrino interaction has occurred could also cause a variation in the event rate. While the selection used in this analysis is CC inclusive, the method used separates events out into prong topologies. Any uncertainty in the FSI could cause migration of events from one prong topology to another. The Neutrino Interaction Working Group (NIWG) assesses these uncertainties and provides a set of parameters for an analyser to vary, all of which are associated with π^\pm interactions. There are six parameters associated with FSI:

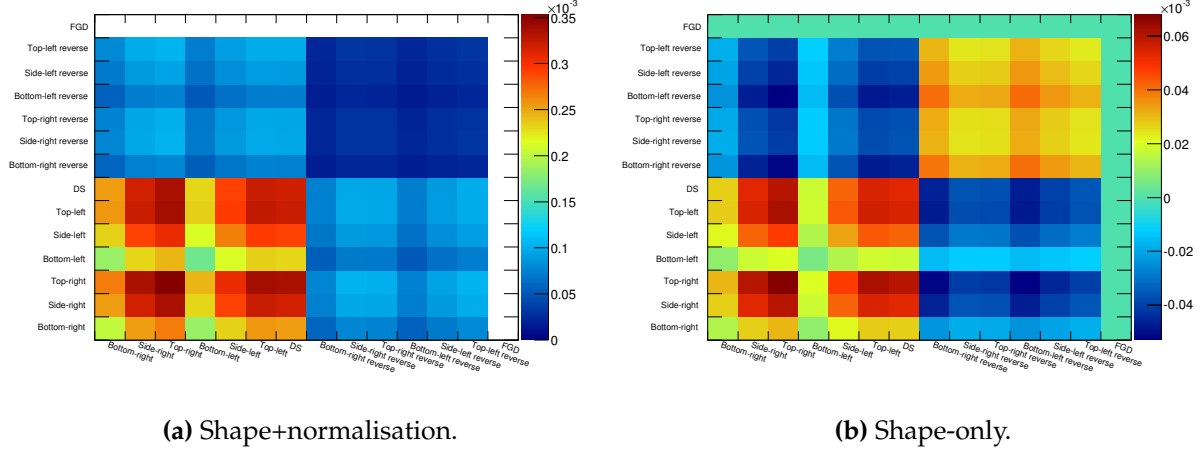


Figure 7.10: The sample covariance induced by variation of P_F^{Pb} .

- Low energy quasi-elastic scattering (FSIQEL)
- High energy quasi-elastic scattering (FSIQEH)
- Pion production (FSIINEL)
- Pion absorption (FSIABS)
- Low energy single charge exchange (FSICXL)
- High energy single charge exchange (FSICXH)

The NIWG provides combinations of the 1σ errors for the parameters highlighted above which span the whole FSI parameter space. The errors are provided in 16 parameters sets which represent the 1σ contour for the FSI parameter space and are shown in table 7.1. Each parameter set can be used to generate one systematic throw, by passing the parameters to T2KReWeight and subsequently re-weighting the events. As with the cross-section model systematics described above, the parameter variations only affect carbon and oxygen. The FSI systematic throws were used to generate the sample covariance matrices which are shown in Fig. 7.11.

7.4.3 ECal detector systematic evaluation

The analysis presented makes heavy use of a computational model of the ND280 ECal. Any differences between this model and the real ND280 ECal could cause a

Parameter set	FSIQEL	FSIQEH	FSIINEL	FSIABS	FSICXL	FSICXH
Nominal	1.0	1.8	1.0	1.1	1.0	1.8
15	0.6	1.1	1.5	0.7	0.5	2.3
16	0.6	1.1	1.5	0.7	1.6	2.3
17	0.7	1.1	1.5	1.6	0.4	2.3
18	0.7	1.1	1.5	1.6	1.6	2.3
19	1.4	1.1	1.5	0.6	0.6	2.3
20	1.3	1.1	1.5	0.7	1.6	2.3
21	1.5	1.1	1.5	1.5	0.4	2.3
22	1.6	1.1	1.5	1.6	1.6	2.3
23	0.6	2.3	0.5	0.7	0.5	1.3
24	0.6	2.3	0.5	0.7	1.6	1.3
25	0.7	2.3	0.5	1.6	0.4	1.3
26	0.7	2.3	0.5	1.6	1.6	1.3
27	1.4	2.3	0.5	0.6	0.6	1.3
28	1.3	2.3	0.5	0.7	1.6	1.3
29	1.5	2.3	0.5	1.5	0.4	1.3
30	1.6	2.3	0.5	1.6	1.6	1.3

Table 7.1: FSI parameters, provided by the NIWG, representing the 1σ contour in the FSI parameter space. Taken from [INSERT REFERENCE].

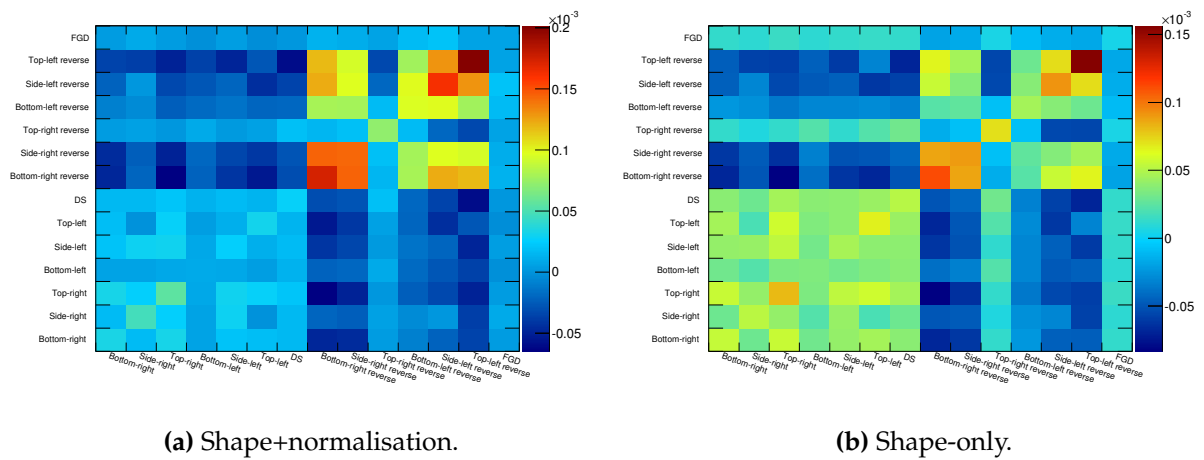


Figure 7.11: The sample covariance induced by variation of of the FSI parameters outlined in table 7.1.

systematic difference between the analysed Monte Carlo and the collected data used in this study. So, several key areas have been identified which could cause such a systematic discrepancy, under the assumption that the differences exist.

The implemented selections uses the enhanced reconstruction, outlined in chapter 4. The enhanced reconstruction, depends on a set of clustering algorithms which are outlined in section 3.4 and the clustering algorithms depend on the hit scintillator bars themselves. Following this trail back, it can be argued that the vast majority of the ECal detector systematics can be covered by assessing the ability of the ECal to reconstruct individual hits.

DISCUSS THE HIT EFFICIENCY SYSTEMATIC (7.8)

The ECal model used in the simulation was based on the as built drawings and so should be an accurate model. However, the components of each ECal module do have associated uncertainties which are not, and can not easily be, taken into account in the simulation, but could easily cause a systematic difference between data and Monte Carlo. For example, if the DS ECal lead absorbers were thicker in the simulated model, one should expect to see a relative deficit of beam triggered events in the DS ECal collected data. Provided that the component dimensions, compositions and uncertainties are known, toy Monte Carlo can be used to construct a set of toy ECal modules which model the variation in the module mass. This can be expanded further, to construct a covariance matrix for the mass of each contributing element. This covariance matrix can then be used to re-weight the events, based on target element, in the Monte Carlo sample to model the effect of the ECal mass systematic. The ECal module designs are split into three types: side, top/bottom and DS. It is only necessary to generate a mass covariance matrix for each of the three types. All values used for the component dimensions/uncertainties are taken from [INSERT JINST REFERENCE]. Precise component dimensions are only quoted for the components in the active regions of each module, namely the lead absorbers, the scintillator bars and the wavelength-shifting fibres, so only these components are considered in the toy Monte Carlo study. A summary of the components are shown in table ??, table ?? and table 7.4 for the side, top/bottom and DS ECal designs respectively.

	Top/Bottom	Side	DS
No. per layer	2	4	2
Length (mm)	3858 ± 4	964.5 ± 4	2016 ± 1
Width (mm)	765 ± 4	2330 ± 4	1008 ± 4
Height (mm)	1.75 ± 0.1	1.75 ± 0.1	1.75 ± 0.1
Sb doping	$2.0 \pm 0.2\%$	$2.0 \pm 0.2\%$	$2.0 \pm 0.2\%$

Table 7.2: Summary of the lead absorbers for the ND280 tracker ECals [24].

	Top/Bottom	Side	DS
No. per layer (para)	38	57	-
No. per layer (perp)	96	96	50
Length (para) (mm)	3840 ± 0.1	3840 ± 0.1	-
Length (perp) (mm)	1520 ± 0.1	2280 ± 0.1	2000 ± 0.1
Width (mm)	$40^{+0.0}_{-0.4}$	$40^{+0.0}_{-0.4}$	$40^{+0.0}_{-0.4}$
Height (mm)	$10^{+0.0}_{-0.4}$	$10^{+0.0}_{-0.4}$	$10^{+0.0}_{-0.4}$
Hole diameter (mm)	1.75 ± 0.1	1.75 ± 0.1	1.75 ± 0.1
Composition (CH:PPO)	99:1	99:1	99:1
Coating thickness (mm)	0.25 ± 0.13	0.25 ± 0.13	0.25 ± 0.13
Coating composition (CH:TiO ₂)	85:15	85:15	85:15

Table 7.3: Summary of the scintillator bars for the ND280 tracker ECals [24].

Parameter set	FSIQEL	FSIQEH	FSIINEL	FSIABS	FSICXL	FSICXH
---------------	--------	--------	---------	--------	--------	--------

Table 7.4: Summary of the DS ECal components.

7.4.3.1 The lead absorbers

Reference [24] provided a clear description of the composition of the lead absorbers for the ECal module designs, which are summarised in table 7.2. All component uncertainties (both dimension and composition) were given as symmetric errors. To construct an ECal lead layer, each layer dimension was systematically varied using a throw from a gaussian of mean 0 and a width of the dimension uncertainty. After the layer volume was defined, the Sb contamination was calculated, also using a gaussian throw, but using a width of the Sb contamination uncertainty. The described information could then be used to retrieve the mass of the Pb and Sb in an ECal lead layer.

7.4.3.2 The scintillator bars

The information used to construct the toy scintillator bars is summarised in table 7.3, most of which was found in reference [24]. The dimensions of the bars were quoted with symmetric uncertainties (like the lead absorbers), so the dimensions were also systematically varied using a throw from a gaussian of mean 0 and a width of the dimension uncertainty. The hole and coating dimensions were also treated in the same manner. The bar composition was reported as polystyrene doped with 1% PPO ($C_{15}H_{11}NO$) and 0.03% POPOP. For the toy bar construction, the POPOP was considered negligible and so was not included. The result is that the toy bar composition (excluding the coating) is 99% CH and 1% $C_{15}H_{11}NO$ by mass. Unfortunately, the full composition of the TiO_2 coating was extensively described. However, a similar systematic study has already been undertaken for the FGD [FGD TN NOTE REFERENCE HERE] which included an investigation of the coating composition. A representative for the Fermilab facility which extruded the scintillator bars reported that the final composition of the coating was 15% rutile-form TiO_2 and 85% CH with other contributing compounds considered negligible. The collected information could then be used to retrieve the contributing mass of each element in a scintillator bar.

7.5 Validation of method

TESTTESTTEST Does it work?

7.6 Applying the fit to ND280 data

Run it

Chapter 8

Discussion and conclusions

Discuss and conclude

8.1 Discussion

Discuss

8.2 Conclusions

Conclusions

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