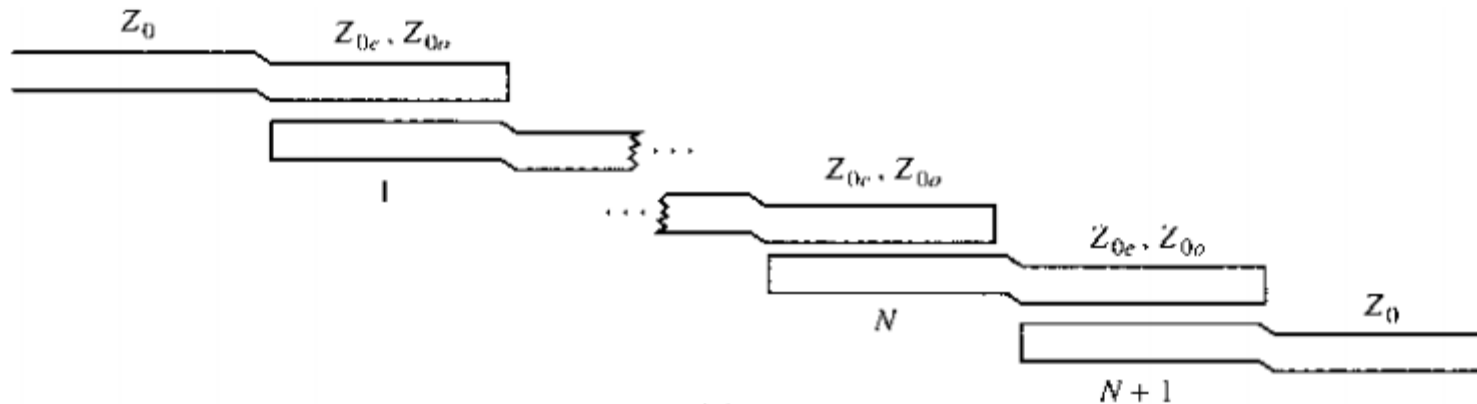
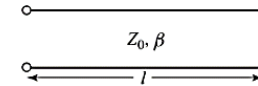


# Design of Coupled Line Bandpass Filters



# Design of a Coupled Line BPF

TX line ABCD Matrix



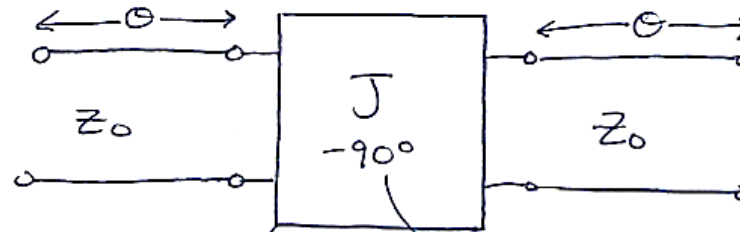
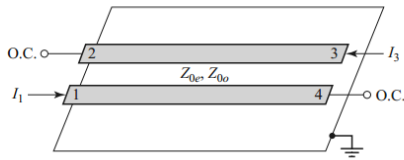
$$A = \cos \beta \ell$$

$$C = jY_0 \sin \beta \ell$$

$$B = jZ_0 \sin \beta \ell$$

$$D = \cos \beta \ell$$

□ A single coupled line is approximated as:



$$Z_0 = \frac{1}{j}$$

Admittance Inverter

$90^\circ$  phase shift due to  $\frac{\lambda}{4}$  length

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} \cos \theta & jZ_0 \sin \theta \\ \frac{j \sin \theta}{Z_0} & \cos \theta \end{bmatrix} \begin{bmatrix} 0 & -\frac{j}{j} \\ -jj & 0 \end{bmatrix} \begin{bmatrix} \cos \theta & jZ_0 \sin \theta \\ \frac{j \sin \theta}{Z_0} & \cos \theta \end{bmatrix}$$

Transmission line

Admittance inverter: A quarter – wave length of transmission of characteristic impedance,  $\frac{1}{j} = Z_0$

# Design of a Coupled Line BPF

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} \left( JZ_0 + \frac{1}{JZ_0} \right) \sin \theta \cos \theta & j \left( JZ_0^2 \sin^2 \theta - \frac{\cos^2 \theta}{J} \right) \\ j \left( \frac{1}{JZ_0^2} \sin^2 \theta - J \cos^2 \theta \right) & \left( JZ_0 + \frac{1}{JZ_0} \right) \sin \theta \cos \theta \end{bmatrix}. \quad (8.104)$$

The image impedance  $Z_i$  at the center frequency ( $\theta = \frac{\pi}{2}$ )

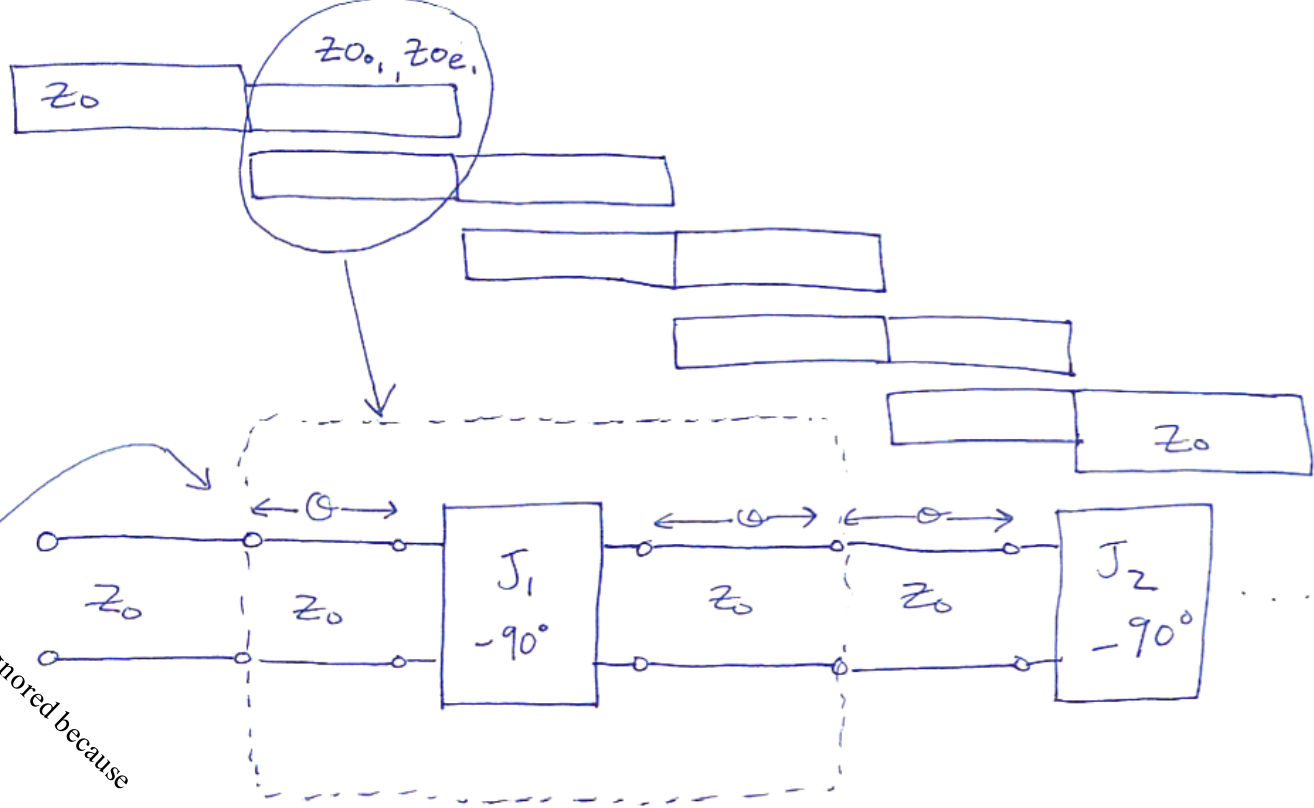
$$\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow\downarrow \quad \left(\text{from } Z_i = \sqrt{\frac{AB}{CD}} \text{ and } \theta = \frac{\pi}{2}\right)$$

## The propagation constant:

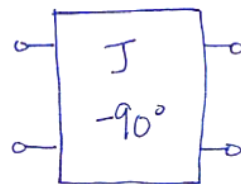
$$\cos \beta = A = \downarrow$$

(from  $e^\gamma = \sqrt{AD} - \sqrt{BC}$ )

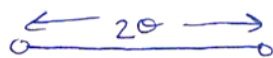
Now consider a BPF composed of a cascade of  $N+1$  coupled line sections:



Equivalent Ckts:



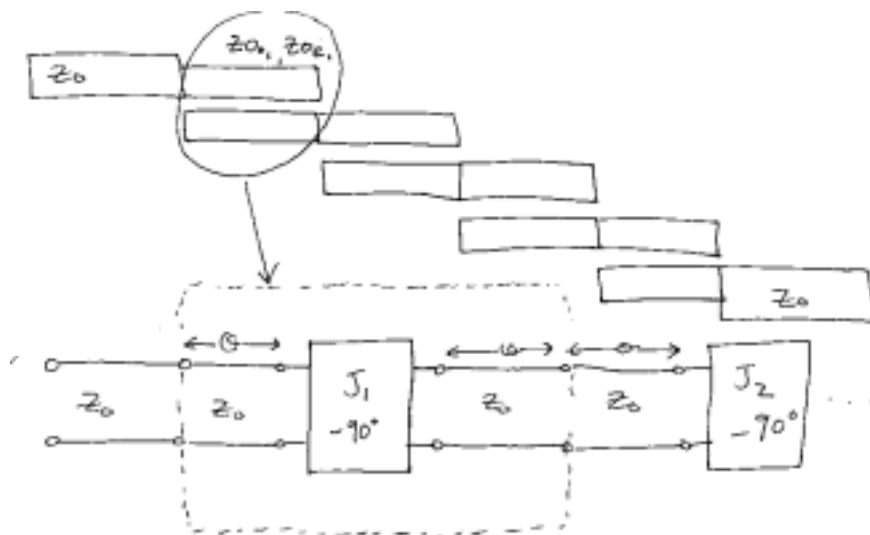
=



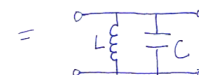
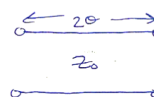
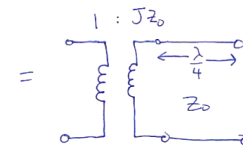
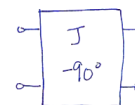
$z_0$

=





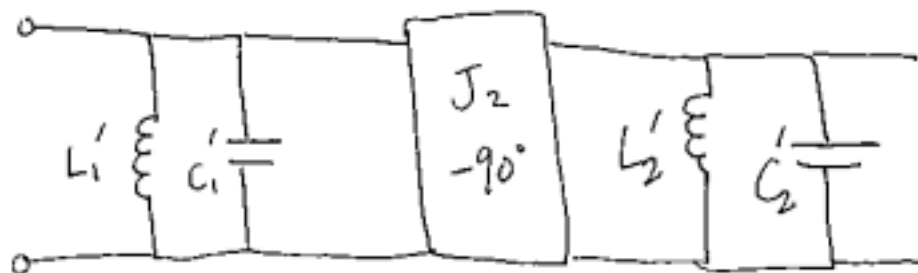
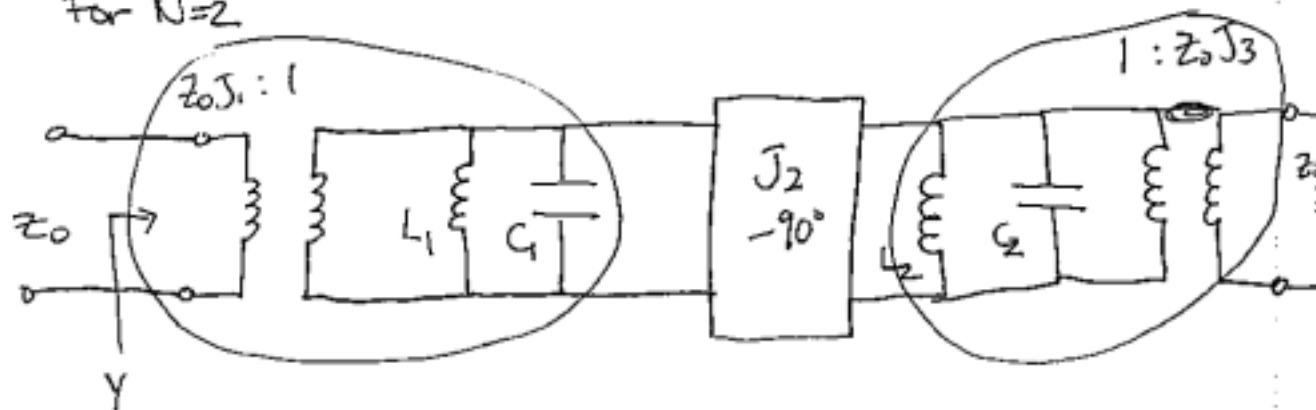
Equivalent Ckts:



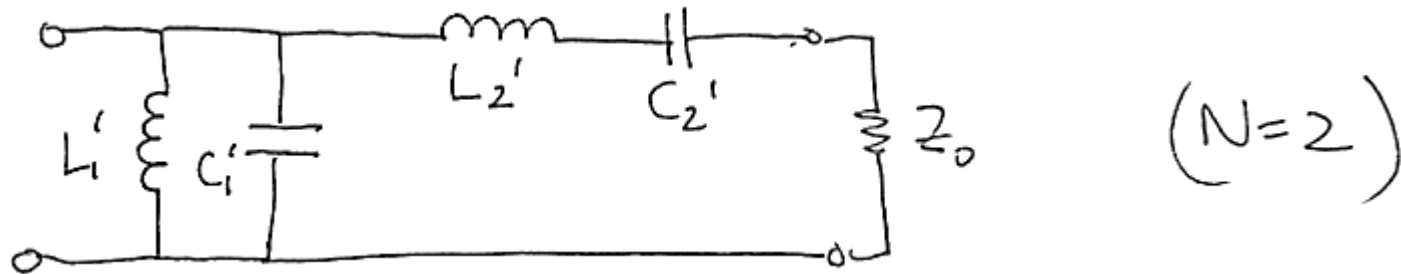
$$L = \frac{2z_0}{\pi\omega_0}$$

$$C = \frac{1}{\omega_0^2 L} = \frac{\pi}{2z_0\omega_0}$$

For  $N=2$



An admittance inverter will transform a shunt LC circuit to a series LC circuit



From here we can use the lumped element Lowpass prototype to determine values.

$$L'_1 = \Delta$$

$$L'_2 = \Delta$$

$$C'_1 = \Delta$$

$$C'_2 = \Delta$$

where  $\Delta = \Delta$

(i.e. fractional bandwidth)



General Formulas are:

$$z_0 J_1 = \sqrt{\frac{\pi \Delta}{2g_1}}$$

$$z_0 J_n = \frac{\pi \Delta}{2\sqrt{g_{n-1}g_n}}$$

$$z_0 J_{N+1} = \sqrt{\frac{\pi \Delta}{2g_N g_{N+1}}}$$

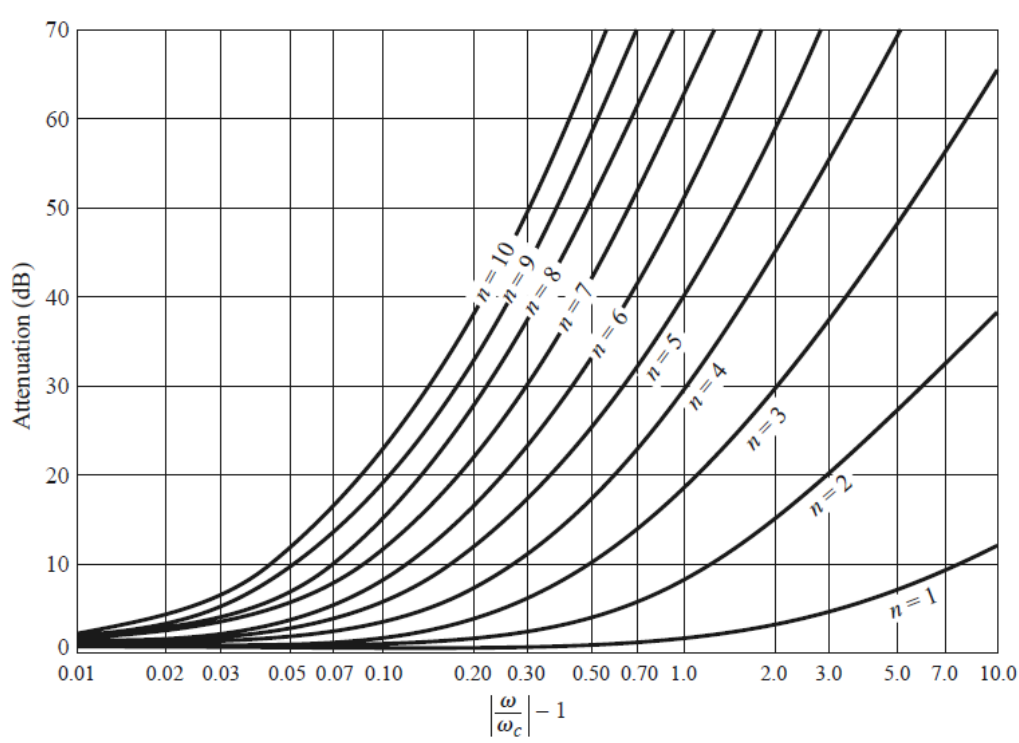
$$z_{0_e} = z_0 [1 + Jz_0 + (Jz_0)^2]$$

$$z_{0_0} = z_0 [1 - Jz_0 + (Jz_0)^2]$$



TABLE 8.4 Element Values for Equal-Ripple Low-Pass Filter Prototypes ( $g_0 = 1, \omega_c = 1, N = 1$  to 10, 0.5 dB and 3.0 dB ripple)

$N$	0.5 dB Ripple										
	$g_1$	$g_2$	$g_3$	$g_4$	$g_5$	$g_6$	$g_7$	$g_8$	$g_9$	$g_{10}$	$g_{11}$
1	0.6986	1.0000									
2	1.4029	0.7071	1.9841								
3	1.5963	1.0967	1.5963	1.0000							
4	1.6703	1.1926	2.3661	0.8419	1.9841						
5	1.7058	1.2296	2.5408	1.2296	1.7058	1.0000					
6	1.7254	1.2479	2.6064	1.3137	2.4758	0.8696	1.9841				
7	1.7372	1.2583	2.6381	1.3444	2.6381	1.2583	1.7372	1.0000			
8	1.7451	1.2647	2.6564	1.3590	2.6964	1.3389	2.5093	0.8796	1.9841		
9	1.7504	1.2690	2.6678	1.3673	2.7239	1.3673	2.6678	1.2690	1.7504	1.0000	
10	1.7543	1.2721	2.6754	1.3725	2.7392	1.3806	2.7231	1.3485	2.5239	0.8842	1.9841







x) Design a coupled line BPF with  $N=3$  and 0.5 dB equal response. The center frequency is 2.0 GHz, the bandwidth is 10 % and  $Z_o = 50 \Omega$ .  $\Delta = 0.1$  (given)

TABLE 8.4 Element Values for Equal-Ripple Low-Pass Filter Prototypes ( $g_0 = 1$ ,  $\omega_c = 1$ ,  $N = 1$  to 10, 0.5 dB and 3.0 dB ripple)

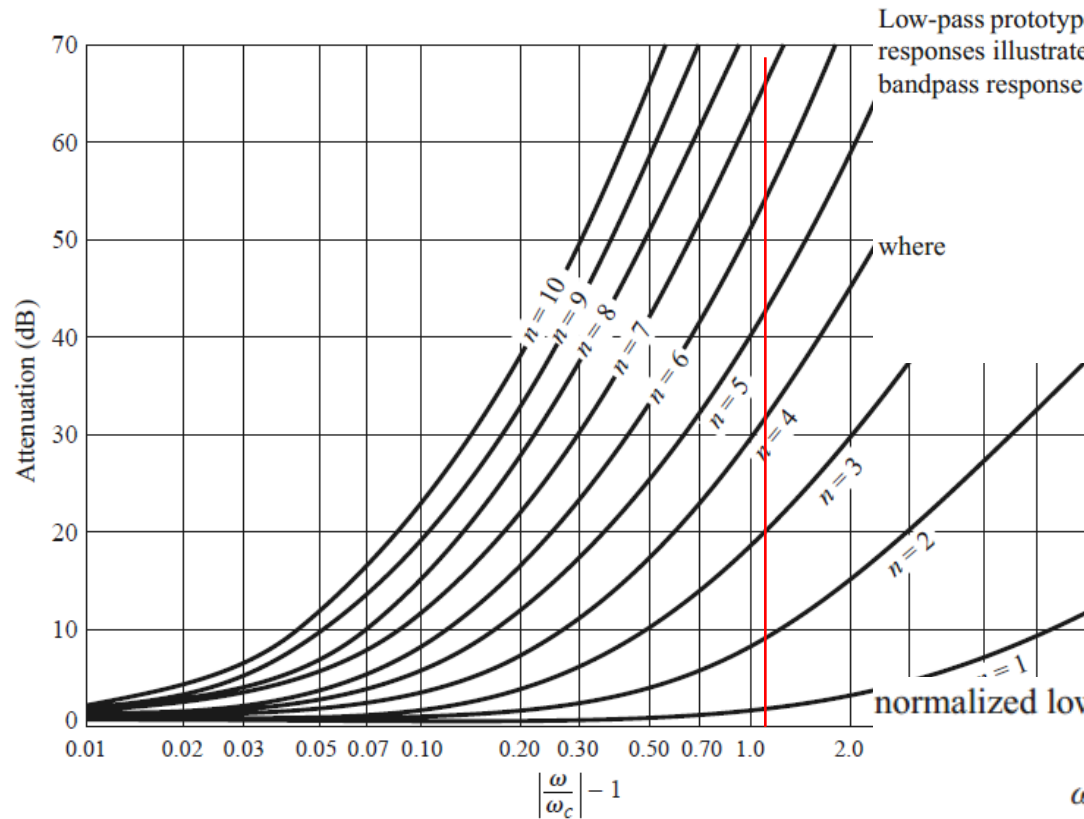
$N$	0.5 dB Ripple										
	$g_1$	$g_2$	$g_3$	$g_4$	$g_5$	$g_6$	$g_7$	$g_8$	$g_9$	$g_{10}$	$g_{11}$
1	0.6986	1.0000									
2	1.4029	0.7071	1.9841								
3	1.5963	1.0967	1.5963	1.0000							
4	1.6703	1.1926	2.3661	0.8419	1.9841						
5	1.7058	1.2296	2.5408	1.2296	1.7058	1.0000					
6	1.7254	1.2479	2.6064	1.3137	2.4758	0.8696	1.9841				
7	1.7372	1.2583	2.6381	1.3444	2.6381	1.2583	1.7372	1.0000			
8	1.7451	1.2647	2.6564	1.3590	2.6964	1.3389	2.5093	0.8796	1.9841		
9	1.7504	1.2690	2.6678	1.3673	2.7239	1.3673	2.6678	1.2690	1.7504	1.0000	
10	1.7543	1.2721	2.6754	1.3725	2.7392	1.3806	2.7231	1.3485	2.5239	0.8842	1.9841



Ex) Design a coupled line BPF with  $N=3$  and 0.5 dB equal response. The center frequency is 2.0 GHz, the bandwidth is 10 % and  $Z_o = 50 \Omega$ .  $\Delta = 0.1$  (given)

x) Design a coupled line BPF with  $N=3$  and 0.5 dB equal response. The center frequency is 2.0 GHz, the bandwidth is 10 % and  $Z_o = 50 \Omega$ .  $\Delta = 0.1$  (given)

What is the attenuation at 1.8 GHz?



Low-pass prototype filter designs can also be transformed to have the bandpass or bandstop responses illustrated in Figure 8.31. If  $\omega_1$  and  $\omega_2$  denote the edges of the passband, then a bandpass response can be obtained using the following frequency substitution:

$$\omega \leftarrow \frac{\omega_0}{\omega_2 - \omega_1} \left( \frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right) = \frac{1}{\Delta} \left( \frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right), \quad (8.71)$$

$$\Delta = \frac{\omega_2 - \omega_1}{\omega_0} \quad (8.72)$$

$$\omega \leftarrow \frac{1}{\Delta} \left( \frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right) = \frac{1}{0.1} \left( \frac{1.8}{2.0} - \frac{2.0}{1.8} \right) = -2.11.$$

Attenuation versus normalized frequency for equal-ripple (a) 0.5 dB ripple level.

Then the value on the horizontal scale of Figure 8.27a is

$$\left| \frac{\omega}{\omega_c} \right| - 1 = |-2.11| - 1 = 1.11,$$

which indicates an attenuation of about 20 dB for  $N = 3$ .

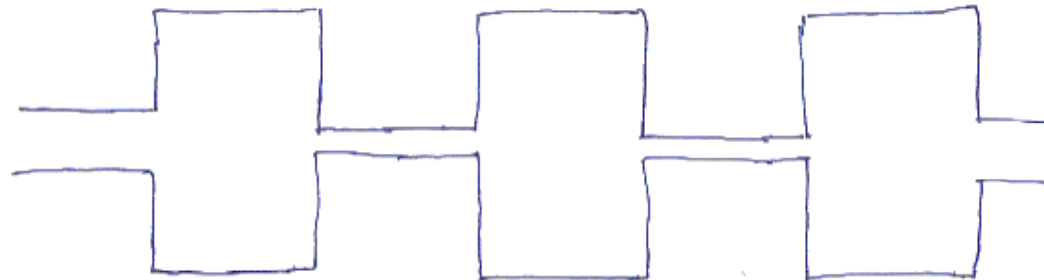
# Design of Stepped Impedance Low Pass Filters

So the series inductors of a low-pass prototype can be replaced with high-impedance line sections ( $Z_0 = Z_h$ ), and the shunt capacitors can be replaced with low-impedance line sections ( $Z_0 = Z_\ell$ ).

# Design of a Coupled Line BPF

## Stepped Impedance Low Pass Filters

- Alternating sections of very high and very low characteristic impedances.
- $H_i - z$  ,  $L_o - z$  filters
- Easy to design when compared to stubs
- Takes up less space
- Limited to applications where sharp cutoff is not required. (rejecting out – of – band mixer products)



## How to design

1. Choose the highest & lowest impedances that are practical.

Series inductor  $\rightarrow$  high impedance line

Shunt capacitor  $\rightarrow$  low impedance line

2. Solve for electrical lengths

$$\beta l = \frac{LR_0}{Z_h}$$

$$\beta l = \frac{CZ_L}{R_0}$$

L and C:  $g$  values from prototype

$$R_0 = \text{filter impedance} > 50\Omega$$

3. Solve for widths (material,  $\epsilon_r$ , thickness, Impedance)

4. Solve for  $l = \frac{2\pi}{\lambda_g} / \beta$

## EXAMPLE 8.6 STEPPED-IMPEDANCE FILTER DESIGN

Design a stepped-impedance low-pass filter having a maximally flat response and a cutoff frequency of 2.5 GHz. It is desired to have more than 20 dB insertion loss at 4 GHz. The filter impedance is  $50\ \Omega$ ; the highest practical line impedance is  $120\ \Omega$ , and the lowest is  $20\ \Omega$ . Consider the effect of losses when this filter is implemented with a microstrip substrate having  $d = 0.158\text{ cm}$ ,  $\epsilon_r = 4.2$ ,  $\tan \delta = 0.02$ , and copper conductors of 0.5 mil thickness.

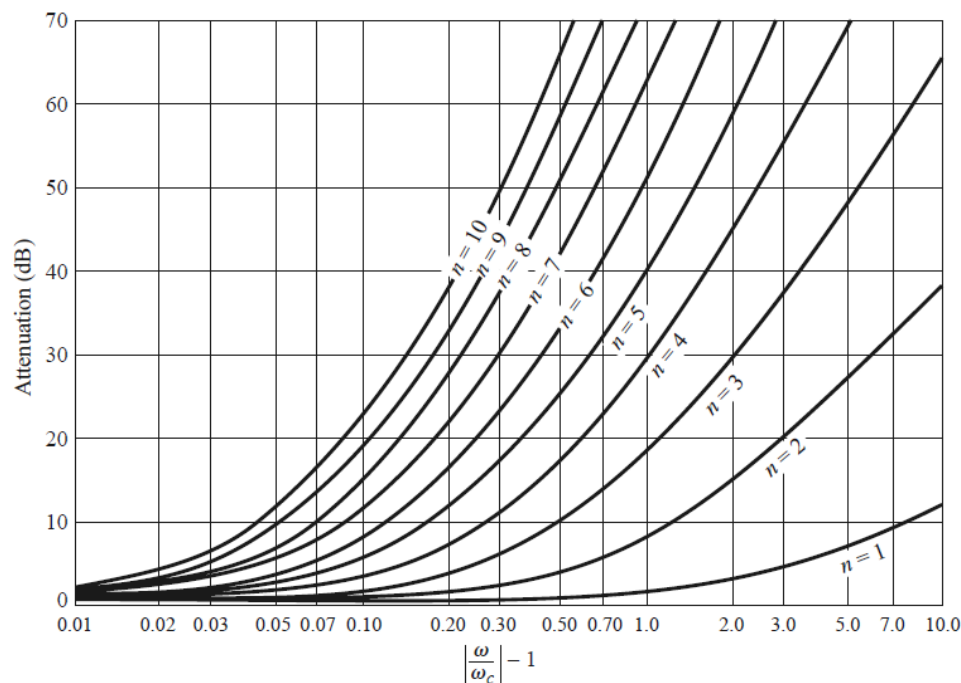


TABLE 8.3 Element Values for Maximally Flat Low-Pass Filter Prototypes ( $g_0 = 1$ ,  $\omega_c = 1$ ,  $N = 1$  to 10)

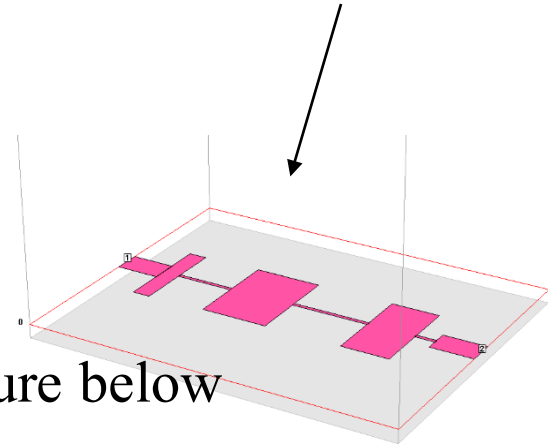
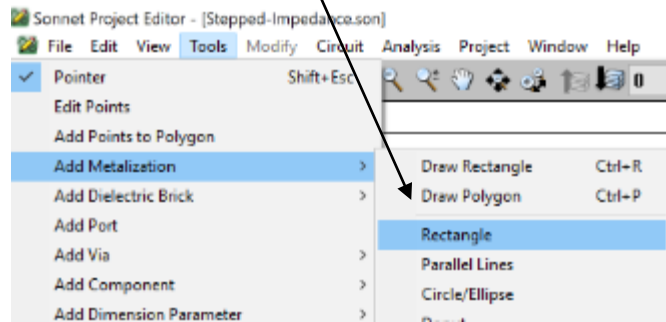
$N$	$g_1$	$g_2$	$g_3$	$g_4$	$g_5$	$g_6$	$g_7$	$g_8$	$g_9$	$g_{10}$	$g_{11}$
1	2.0000	1.0000									
2	1.4142	1.4142	1.0000								
3	1.0000	2.0000	1.0000	1.0000							
4	0.7654	1.8478	1.8478	0.7654	1.0000						
5	0.6180	1.6180	2.0000	1.6180	0.6180	1.0000					
6	0.5176	1.4142	1.9318	1.9318	1.4142	0.5176	1.0000				
7	0.4450	1.2470	1.8019	2.0000	1.8019	1.2470	0.4450	1.0000			
8	0.3902	1.1111	1.6629	1.9615	1.9615	1.6629	1.1111	0.3902	1.0000		
9	0.3473	1.0000	1.5321	1.8794	2.0000	1.8794	1.5321	1.0000	0.3473	1.0000	
10	0.3129	0.9080	1.4142	1.7820	1.9754	1.9754	1.7820	1.4142	0.9080	0.3129	1.0000

Source: Reprinted from G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, Dedham, Mass., 1980, with permission.

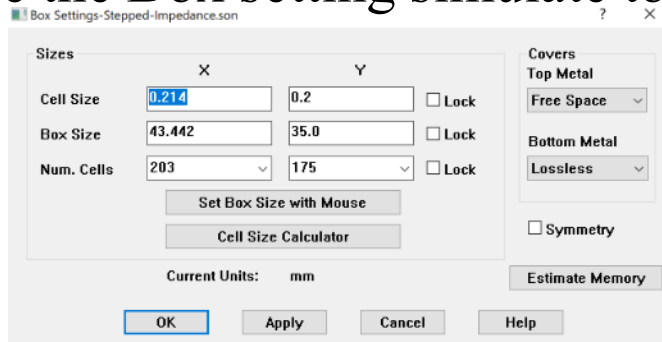
# Lab 6

❑ Using the filter design in Example 8.6, obtain the S11 and S21 using Sonnet.

➤ Use “Rectangle” function shown below to create the geometry



➤ Use the Box setting simulate to the figure below



➤ Run the simulation between 0.1 to 5.0 GHz





# Stepped-Impedance Low-Pass Filter (Due April 13<sup>th</sup> Midnight Online Submission)

☐ Name:

☐ Geometry

☐ Simulation Results (S11 and S21)

Discuss the simulation results

1.

2.

3.