

## ④ Filter design using pole/zero placement

→ ~~Based on what we've done, we can~~  
we can start designing filters!

→ methods in 5.4 are a bit crude but are used in practice

### BASIC concept

1) put pole near ~~things~~ <sup>we'd like to enhance</sup> zeros near <sup>we'd like to suppress</sup>

2) stable : all poles should be inside  $|z|=1$   
zeros can be anywhere

3) real : poles and zeros should occur in conjugate-symmetric pairs, or on the real axis.

4) decide if want FIR (no feedback) or IIR (feedback)

### Examples

single pole system:  $H_1(z) = \frac{1-a}{1-az^{-1}}$

see Fig 5.4.3 for  $a=0.9$

numerator  
 $1-a$  picked  
so at  $\omega=0, z=1$   
 $H_1(1) = 1$

single-pole, single zero:  $H_2(z) = \frac{1-a}{2} \frac{1+z^{-1}}{1-az^{-1}}$

see Fig 5.4.3 again

again,  
at  $\omega=0, z=1$   
 $H_2(1) \rightarrow \frac{(1-a)(2)}{2(1-a)} = 1$

(5)

### General formula :

- decide on form of function (# poles, # zeros) and write  $H(z)$  in terms of parameters
- impose a constraint on response for each free variable
- solve

Examples : 5.4.1, 5.4.2 — review for task (scan in pages)

### (5) Practical example: notch filter

→ system w/ very deep null at "problem frequency" i.e. 60 Hz, 50 Hz

→ simplest: ~~FFT~~ (FIR): null out frequency  $\omega_0$  by placing conjugate symmetric poles at  $\pm \omega_0$

→ problem: too wide. Solution: add a pole

show eqns on p. 339 (scanned)

### → MATLAB examples

→ show  $\angle H$ ,  $|H|$ , grating

show time to settle as notch deepens

show distortion on nearby signal

## Comb filter

from PPT  $y(n) = \frac{1}{M+1} \sum_{k=0}^M x(n-k)$

boord  $\left\{ \begin{aligned} H(z) &= \frac{1}{M+1} \sum_{k=0}^M z^{-k} \end{aligned} \right.$

use geometric series identity:

$$\sum_{i=0}^n x^i = \frac{1-x^{n+1}}{1-x}$$

~~plus 1~~

$z^{-1}$  looks like 'x' above

then get PPT result:  $H(z) = \frac{1}{M+1} \frac{[1 - z^{-(M+1)}]}{1 - z^{-1}}$

$$H(\omega) = H(z) \Big|_{e^{j\omega}}$$

$$= \frac{1}{M+1} \frac{[1 - e^{-j\omega(M+1)}]}{1 - e^{-j\omega}} = \frac{1}{M+1} \frac{e^{-j\omega(M+1)/2} [e^{+j\omega(M+1)/2} - e^{-j\omega(M+1)/2}]}{e^{-j\omega/2} [e^{j\omega/2} - e^{-j\omega/2}]}$$

~~put out~~  $e^{-j\omega(M+1)/2}$

$$= \frac{1}{M+1} e^{-j\omega(M+1)/2} \frac{\sin \omega (M+1)/2}{\sin \omega/2}$$

(1)

# Lecture: All-pass and minimum-phase systems

reading: P&M S.4.6 (AP) and S.5

## Warmup problem

We have a system  $H(z) = \frac{B(z)}{A(z)}$ . We'd like to find the inverse system  $H^{-1}(z) = \frac{A(z)}{B(z)}$ .

→ what is required for both  $H$  and  $H^{-1}$  to ~~be~~ be stable & causal?

→ why might we care about  $H^{-1}$ ?

P&M S.4.6

1) All pass systems

a) definition:  $|H_{AP}(w)| = 1$  (phase ~~will~~ shift)

b) simplest example: time delay

$$H(z) = z^{-k}$$

$$|H(w)| = 1, \quad \angle H(w) = wk$$

even tho simple, this is probably the most widely used AP... compensate for time delay of a linear phase filter

c) more interesting example: 1 zero, 1 pole

$$H(z) = \frac{z^{-1} - a}{1 - az^{-1}}$$

← zero at  $z^{-1} = a$ , or  $z = 1/a$

← pole at  $z^{-1} = 1/a$ ,  $z = a$

look at the magnitude:

$$\begin{aligned} |H(e^{jw})|^2 &= |H(e^{jw}) H^*(e^{jw})| = |H(e^{jw}) H(e^{-jw})| \\ &= |H(z) H(z^{-1})|_{z=e^{jw}} \end{aligned}$$

$$\text{here, } |H(w)|^2 = \left(\frac{z}{z}\right) \frac{z^{-1} - a}{1 - az^{-1}} \frac{z - a}{1 - az} = \left(\frac{1 - az}{z - a}\right) \left(\frac{z - a}{1 - az}\right) \Big|_{z=e^{jw}} = 1$$

↑  
multiph b

Ppt slides for speed?

(2)

This works b/c we have a reciprocal real pole + zero  
could also have reciprocal complex-conjugate P + Z

show figures 5.4.16, 5.4.17

d) general form - Eq 5.4.45

$$H_{\text{eq}}(z) = \prod_{k=1}^{N_z} \frac{z^{-1} - \alpha_k}{1 - \alpha_k^* z^{-1}} \prod_{k=1}^{N_p} \frac{(z^{-1} - \beta_k)(z^{-1} - \beta_k^*)}{(1 - \beta_k z^{-1})(1 - \beta_k^* z^{-1})}$$

e) why do we care?

- gives a way to compensate for undesired phase  
w/o changing magnitude → "phase equalizer"
- more uses ~~below~~ coming in lecture...

## 2) Minimum phase systems

a) Motivation - deconvolution

→ often, we have a measurement  $y$ ,  $y = h * x$   
we want to recover  $x$  ( $\omega$ ) or  $X(\omega)$

→  $x$  is a comm signal,  $h$  is receiver

→  $x$  is an image,  $h$  is optical system

→ thanks to F.T., this can be easy

$$Y(\omega) = H(\omega)X(\omega)$$

$$X(\omega) = \frac{Y(\omega)}{H(\omega)}$$

$$\text{or } X(z) = \frac{Y(z)}{H(z)}$$

→ but for this to work,  $H^{-1}$  must be stable + causal

(note: could do example 5.5.2 here;  
but what's wrong w/  $|z| > 1/2$  answer?)

think about  $|H(\omega)|^2$

$$|H(\omega)|^2 = H(\omega) H^*(\omega)$$

but if  $h$  is real,  ~~$H^*(e^{j\omega}) = H(e^{j\omega})$~~

$$= H(\omega) H(-\omega) \leftarrow \text{conj symmetry}$$

$$= H(z) H(z^{-1}) \Big|_{z=e^{j\omega}}$$

How to see last point?

$$H(z) = \sum_n h(n) z^{-n}$$

(det  $z$  transform)

$$\text{so } H(z^{-1}) = \sum_n h(n) z^n$$

$$H(z^{-1}) \Big|_{z=e^{j\omega}} = \sum_n h(n) e^{j\omega n}$$

$$= \sum_n h(n) \bar{e}^{(-\omega)n}$$

$$= H(-\omega) \quad \text{from DTFT}$$

If  $H(z)$  has ~~poles~~ zero  $z_k$  and poles  $p_k$   
 $H(z^{-1})$  has zero  $1/z_k$  and poles  $1/p_k$

pole - zero confusion

Q) Given  $|H(\omega)|^2$ , can we determine  $H(\omega)$ ?

say  $H(z)$  has zeros  $[z_1, z_2]$

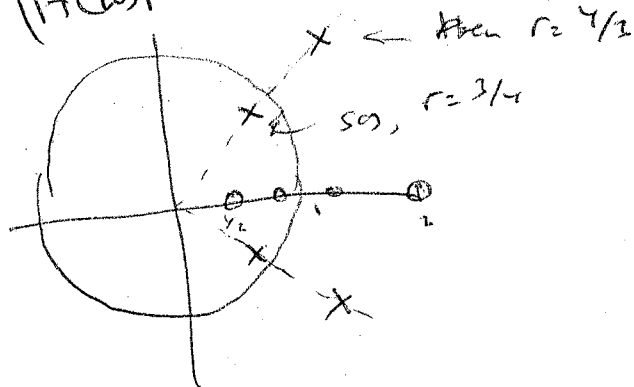
poles  $[p_1, p_2] \leftarrow$  complex conjugates

$$|H(\omega)|^2 = H(z)H(z^{-1})$$

$H(z^{-1})$  has zeros  $[\frac{1}{z_1}, \frac{1}{z_2}]$

poles  $[\frac{1}{p_1}, \frac{1}{p_2}]$

$|H(\omega)|^2$



Given poles/zeros of  $|H(\omega)|^2$

$[z_1, \frac{1}{z_1}, z_2, \frac{1}{z_2}]$

$[p_1, p_2, \frac{1}{p_1}, \frac{1}{p_2}]$

16 ~~unique~~ possible combinations!

even if we pick poles inside unit circle  
( $H$  stable) still 4 combinations possible

$(z_1, \frac{1}{z_1}), (z_1, z_2), (\frac{1}{z_1}, z_2), (\frac{1}{z_1}, \frac{1}{z_2})$

thus in general, we cannot distinguish  $H(\omega)$

there are special conditions where we can -  
minimum phase systems  
next lecture