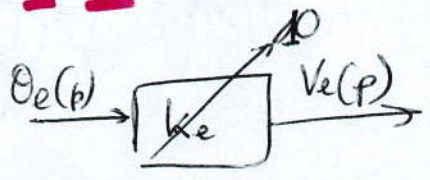
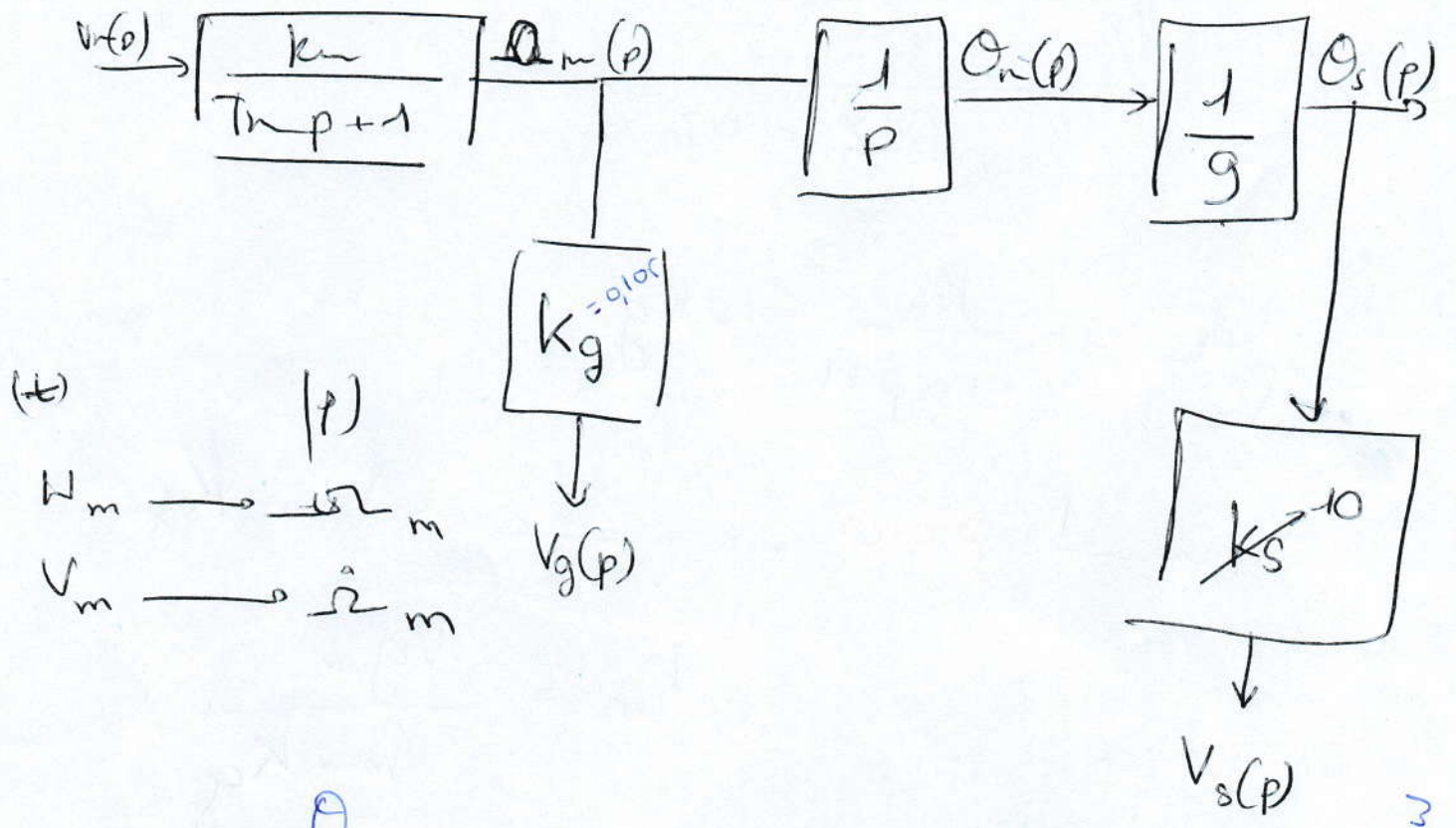


~~TD 12 - 13 - 14 - 15 - 16 - 17 - 18 - 19 - 20 - 21 - 22 - 23 - 24 - 25 - 26 - 27 - 28 - 29 - 30 - 31 - 32 - 33 - 34 - 35 - 36 - 37 - 38 - 39 - 40 - 41 - 42 - 43 - 44 - 45 - 46 - 47 - 48 - 49 - 50 - 51 - 52 - 53 - 54 - 55 - 56 - 57 - 58 - 59 - 60 - 61 - 62 - 63 - 64 - 65 - 66 - 67 - 68 - 69 - 70 - 71 - 72 - 73 - 74 - 75 - 76 - 77 - 78 - 79 - 80 - 81 - 82 - 83 - 84 - 85 - 86 - 87 - 88 - 89 - 90 - 91 - 92 - 93 - 94 - 95 - 96 - 97 - 98 - 99 - 100~~

III - 1 schema bloc



$$p \quad \frac{1}{p}$$



$$\frac{\theta_s}{\theta_m} = \frac{1}{g} \Rightarrow \theta_s = \frac{\theta_m}{g}$$

$$V_m(p) \cdot (K_m) = \omega_m(p) = T_m (\dot{\omega}_m(t) + \omega_n(t))$$

$$T_m \ddot{\theta}_m(t) + \dot{\theta}_m(t) = K_m V_m(t) \quad \dot{\theta}_m(t)$$

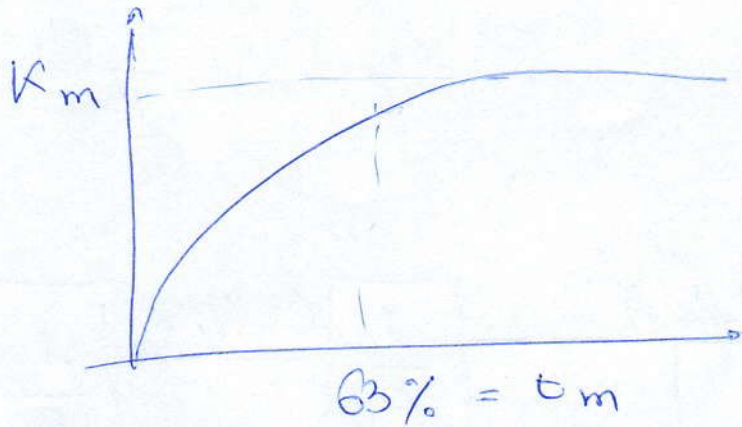
$$T_m p + 1 = k_m p$$

$$T_m \omega_m(t) + \omega_m(t) = k_m v_m(t)$$

1

$$\frac{\omega_m(t) (T_m + 1)}{v_m(t)} = k_m \quad \frac{T_m \omega_m(t)}{v_m(t)} = \frac{k_m}{T_m + 1}$$

Rep indicielle 1^{re} Ordre.



$$K_m = \frac{K_g \cdot K_m}{V_g}$$

$$\frac{V_g}{V_m} = \frac{K_m}{T_m p + 1} \cdot K_g$$

Quand $p=0 \Rightarrow \frac{V_g}{V_m} = K_m \cdot K_g$

$$K_m = \frac{V_g \cdot K_g}{V_m \cdot K_g}$$

III-2

$$\frac{\theta_s(p)}{\theta_e(p)} = \left(V_m(p) \cdot \frac{K_m}{T_m p + 1} \right) \left(\frac{1}{p} \cdot \frac{1}{g} \right)$$

$$\theta_e = K_e \cdot V_e(p)$$

$$\theta_s = \frac{1}{g} \cdot \theta_m(t) = V_s / K_s$$

Donc

$$\theta_s(p) = \frac{1}{g} \cdot \frac{1}{p} \cdot \left(\frac{K_m}{T_m p + 1} \cdot V_m \right)$$

$$\theta_e(p) K_e$$

$$K_1 (V_e - \underbrace{V_s(t)})$$

$$\theta_s \cdot K_s$$

2

$$\theta_s(p) = \frac{1}{g_p} \cdot \left(\frac{K_m}{T_m p + 1} \left(K_1 (\theta_e(p) K_e - \theta_s K_s) \right) \right)$$

$$\theta_s(p) \left(1 + \frac{1}{g_p (T_m p + 1)} \right) = \frac{1}{g_p} \cdot \left(\frac{K_m \cdot K_1 \cdot K_e}{T_m p + 1} \right) \cdot \theta_e(p)$$

$$\frac{\theta_s(p)}{\theta_e(p)} = \frac{K_m \cdot K_1 \cdot K_e}{g_p (T_m p + 1)} \cdot \frac{1}{1 + \frac{K_m K_s K_1}{g_p (T_m p + 1)}}$$

$$= \frac{K_m \cdot K_1 \cdot K_e}{T_m g_p^2 + g_p} \cdot \frac{g_p}{g T_m p^2 + g_p + K_m K_s K_1}$$

$V_m =$
 $V_g = 2,36V$

Input
SVCC
 $f = 0,242$

$T_m = 336 \text{ ms}$
 63%
 $= 0,336 \text{ s}$

TF = $\frac{K_m \cdot K_1 \cdot K_e}{g T_m p^2 + g_p + K_m K_s K_1}$

$V_m = 4$

$V_g = 2,36$

$R_g = 0,105$

$K_m = 5,619$

$T_m = 0,336$

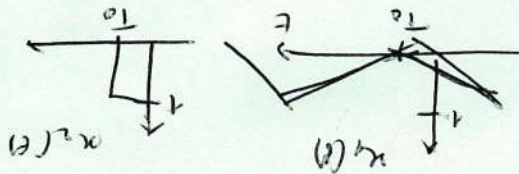
experiment
element

3

III.3.6

Tracer diag Bode
 $\begin{cases} \text{bode}(T) \\ \text{margin}(T) \end{cases}$

$$\mathcal{L}(z) \cdot h(z) \propto \int$$



$$= (z)^2$$

$$(z)^{\frac{1}{m}} \frac{1}{r} = (z)^{\frac{1}{m}}$$

$$(\frac{1}{m} - 1) \frac{1}{r} = (z)^{\frac{1}{m}}$$

$$g T_m p^2 + g p + k_m k_s k_1$$

p^2	$g T_m$	$k_m k_s k_1$
p^1	g	0
p^0	$k_m k_s k_1$	0

$$\frac{1}{a_{n-1}} = \frac{1}{g}$$

$$b_n = -\frac{1}{g} \det \begin{bmatrix} g T_m & k_m k_s k_1 \\ g & 0 \end{bmatrix} = \frac{1}{g} (g T_m \times 0 - g k_m k_s k_1)$$

$$\frac{b_n}{g} = \frac{g T_m \times 0 - g k_m k_s k_1}{g} = -k_m k_s k_1$$

III.3.5

système stable

Critère de Routh ✓
 car n'a ni signe
 et n'a ni zéro
 (1^{er} colonne)

p^2	$g T_m$	$k_m k_s k_1$
p^1	g	0
p^0	$k_m k_s k_1$	0

$= 10 > 0$
 $5,619 > 0$

$$b_{n-1} = a_n \times 0 - 0 \times 0 = 0$$

$$c_n = k_m k_s k_1 \times 0 - 0 \times 0 = 0$$

Exercice 3

⑧

Metlab

$$① M^4 - 4M^2 + 4I = 0$$

$$K_1 = 1$$

$$T_{n63\%} = 0,36 \Rightarrow A = 0,78$$

$$D = 0,31$$

$$T_r = 0,32$$

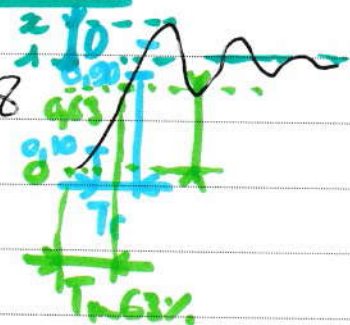
$$h_1 = 2,7$$

$$T_{n63\%} = 0,186$$

$$D = 0,51$$

$$T_r = 0,114$$

$$D = 1 - \alpha$$



⑫

$$h = 2,7$$

$$6,76$$

$$h = 1$$

$$3,76$$

$$\omega_R = \text{~~6,76~~ rad/s} \quad \omega_R = \text{~~3,76~~ rad/s}$$

pulsation de ^{coupure} ~~asymptote~~

$$h = 2,7$$

$$\omega_c = 10,7 \text{ rad/s}$$

$$h = 1$$

$$\omega_c = 6,13 \text{ rad/s}$$

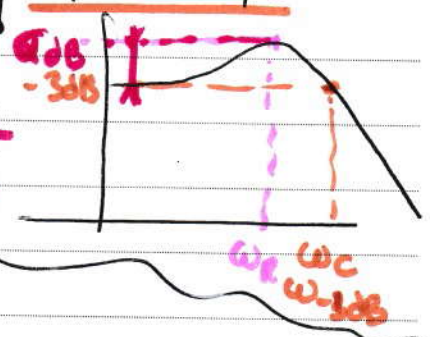
coef de surtension

$$h = 2,7$$

$$Q_{dB} = G_{dB}(6,76) - G_{dB}(0) = 7,73$$

$$h = 1$$

$$Q_{dB} = G_{dB}(3,76) - G_{dB}(0) = 3,76$$



TP2

① (raison) \Rightarrow voir photo Tableau

② $M_f \Rightarrow$ rajoute un pôle et un zéro

$$h = \frac{1 + a \tau p}{1 + \tau p}$$

car on a augmenté trop h

(bien que cela rajoute l'erreur de vitesse)
la réponse sera trop rapide et le système physique
n'aura pas le temps de réagir à sa commande



③ $k =$

$a =$

$\tau =$

quest 5

$M_{\phi \text{ act}} = 23,7^\circ$

$M_{\phi \text{ désirée}} = 45^\circ$

$\alpha = 1,2$

$$\Delta \gamma_{\max} = \alpha (45 - 23,7)$$

$$= 25,56$$

$$a = \frac{1 + \sin(25,56)}{1 - \sin(25,56)} = 2,42$$

$\tau =$

$$W_{\max} = \frac{1}{\tau \cdot \sqrt{a}} \Rightarrow \tau = \frac{1}{W_{\max} \cdot \sqrt{a}}$$

$W_{\max} = 6,82$

$\tau = 0,643$

$k = K_1 = 2,7$

$C = \frac{\tau}{R_2}$ avec $C = \frac{\tau}{R_2}$
 $R_1 = a - 1 = \frac{\tau}{C} - 1$
 $R_2 = \frac{\tau}{C}$

quest 6

⑥ $P_m = 41,7 \text{ deg}$

soit $1 + \frac{R_2}{R_1}$

⑦ Déduire de a et τ les valeurs des résistances R_1 R_2 et du condensateur C

$$\frac{1 + a\tau p}{1 + \tau p} \Leftrightarrow \frac{1 + (R_1 + R_2)Cp}{1 + R_1 Cp}$$

$\frac{R_1 C p + R_2 C}{R_1 C}$

soit $\begin{cases} a\tau = (R_1 + R_2)C \\ \tau = R_1 C \end{cases} \Rightarrow \begin{cases} a = \frac{R_1 + R_2}{R_1} \\ \tau = R_1 C \end{cases}$

$$\alpha \tau = (R_1 + R_2) C_B$$

$$\tau = R_1 C$$

1NF sur la vignette

$$\frac{6435}{10^{-6}} = 643500 \Omega \approx 64 k\Omega$$

$$\frac{R_1}{\alpha - 1} = \frac{643500}{242 - 1} = 453169 \Omega \approx 45 k\Omega$$