

SINUSOIDAL STEADY-STATE RESPONSE OF DIGITAL FILTERS

D

D.1 SINUSOIDAL STEADY-STATE RESPONSE

Analysis of the sinusoidal steady-state response of the digital filters will lead to the development of the magnitude and phase responses of digital filters. Let us look at the following digital filter with a digital transfer function $H(z)$ and a complex sinusoidal input

$$x(n) = Ve^{j(\Omega n + \phi_x)}, \quad (\text{D.1})$$

where $\Omega = \omega T$ is the normalized digital frequency, while T is the sampling period and $y(n)$ denotes the digital output, as shown in Fig. D.1.

The z -transform output from the digital filter is then given by

$$Y(z) = H(z)X(z). \quad (\text{D.2})$$

Since $X(z) = \frac{Ve^{j\phi_x}z}{z - e^{j\Omega}}$, we have

$$Y(z) = \frac{Ve^{j\phi_x}z}{z - e^{j\Omega}} H(z). \quad (\text{D.3})$$

Based on the partial fraction expansion, $Y(z)/z$ can be expanded as the following form:

$$\frac{Y(z)}{z} = \frac{Ve^{j\phi_x}}{z - e^{j\Omega}} H(z) = \frac{R}{z - e^{j\Omega}} + \text{sum of the rest of partial fractions.} \quad (\text{D.4})$$

Multiplying the factor $(z - e^{j\Omega})$ on both sides of Eq. (D.4) yields

$$Ve^{j\phi_x} H(z) = R + (z - e^{j\Omega})(\text{sum of the rest of partial fractions}). \quad (\text{D.5})$$

Substituting $z = e^{j\Omega}$, we get the residue as

$$R = Ve^{j\phi_x} H(e^{j\Omega}).$$

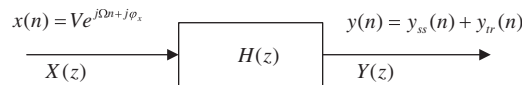


FIG. D.1

Steady-state response of the digital filter.

Then substituting $R = Ve^{j\phi_s}H(e^{j\Omega})$ back into Eq. (D.4) results in

$$\frac{Y(z)}{z} = \frac{Ve^{j\phi_s}H(e^{j\Omega})}{z - e^{j\Omega}} + \text{sum of the rest of partial fractions}, \quad (\text{D.6})$$

and multiplying z on both sides of Eq. (D.6) leads to

$$Y(z) = \frac{Ve^{j\phi_s}H(e^{j\Omega})z}{z - e^{j\Omega}} + z \times \text{sum of the rest of partial fractions}. \quad (\text{D.7})$$

Taking the inverse z -transform leads to two parts of the solution:

$$y(n) = Ve^{j\phi_s}H(e^{j\Omega})e^{j\Omega n} + Z^{-1}(z \times \text{sum of the rest of partial fractions}). \quad (\text{D.8})$$

From Eq. (D.8), we have the steady-state response

$$y_{ss}(n) = Ve^{j\phi_s}H(e^{j\Omega})e^{j\Omega n} \quad (\text{D.9})$$

and the transient response

$$y_{tr}(n) = Z^{-1}(z \times \text{sum of the rest of partial fractions}). \quad (\text{D.10})$$

Note that since the digital filter is a stable system, and the locations of its poles must be inside the unit circle on the z -plane, the transient response will be settled to zero eventually. To develop filter magnitude and phase responses, we write the digital steady-state response as

$$y_{ss}(n) = V|H(e^{j\Omega})|e^{j\Omega n + j\phi_s + \angle H(e^{j\Omega})}. \quad (\text{D.11})$$

Comparing Eq. (D.11) and Eq. (D.1), it follows that

$$\begin{aligned} \text{Magnitude response} &= \frac{\text{Amplitude of the steady state output}}{\text{Amplitude of the sinusoidal input}} \\ &= \frac{V|H(e^{j\Omega})|}{V} = |H(e^{j\Omega})| \end{aligned} \quad (\text{D.12})$$

$$\text{Phase response} = \frac{e^{j\phi_s + j\angle H(e^{j\Omega})}}{e^{j\phi_s}} = e^{j\angle H(e^{j\Omega})} = \angle H(e^{j\Omega}). \quad (\text{D.13})$$

Thus we conclude that

$$\text{Frequency response} = H(e^{j\Omega}) = H(z)|_{z=e^{j\Omega}}. \quad (\text{D.14})$$

Since $H(e^{j\Omega}) = |H(e^{j\Omega})| \angle H(e^{j\Omega})$

$$\text{Magnitude response} = |H(e^{j\Omega})| \quad (\text{D.15})$$

$$\text{Phase response} = \angle H(e^{j\Omega}). \quad (\text{D.16})$$

D.2 PROPERTIES OF THE SINUSOIDAL STEADY-STATE RESPONSE

From Euler's identity and trigonometric identity, we know that

$$\begin{aligned} e^{j(\Omega + k2\pi)} &= \cos(\Omega + k2\pi) + j\sin(\Omega + k2\pi) \\ &= \cos\Omega + j\sin\Omega = e^{j\Omega}, \end{aligned} \quad (\text{D.17})$$

where k is an integer taking values of $k=0, \pm 1, \pm 2, \dots$. Then:

$$\text{Frequency response: } H(e^{j\Omega}) = H(e^{j(\Omega + k2\pi)}) \quad (\text{D.18})$$

$$\text{Magnitude frequency response: } |H(e^{j\Omega})| = |H(e^{j(\Omega + k2\pi)})| \quad (\text{D.19})$$

$$\text{Phase response: } \angle H(e^{j\Omega}) = \angle H(e^{j(\Omega + k2\pi)}). \quad (\text{D.20})$$

Clearly, the frequency response is periodical, with a period of 2π . Next, let us develop the symmetric properties. Since the transfer function is written as

$$H(z) = \frac{Y(z)}{X(z)} = \frac{b_0 + b_1 z^{-1} + \dots + b_M z^{-M}}{1 + a_1 z^{-1} + \dots + a_N z^{-N}}, \quad (\text{D.21})$$

Substituting $z = e^{j\Omega}$ into Eq. (D.21) yields

$$H(e^{j\Omega}) = \frac{b_0 + b_1 e^{-j\Omega} + \dots + b_M e^{-jM\Omega}}{1 + a_1 e^{-j\Omega} + \dots + a_N e^{-jN\Omega}}. \quad (\text{D.22})$$

Using Euler's identity, $e^{-j\Omega} = \cos \Omega - j \sin \Omega$, we have

$$H(e^{j\Omega}) = \frac{(b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega) - j(b_1 \sin \Omega + \dots + b_M \sin M\Omega)}{(1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega) - j(a_1 \sin \Omega + \dots + a_N \sin N\Omega)}. \quad (\text{D.23})$$

Similarly,

$$H(e^{-j\Omega}) = \frac{(b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega) + j(b_1 \sin \Omega + \dots + b_M \sin M\Omega)}{(1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega) + j(a_1 \sin \Omega + \dots + a_N \sin N\Omega)}. \quad (\text{D.24})$$

Then the magnitude response and phase response can be expressed as

$$|H(e^{j\Omega})| = \frac{\sqrt{(b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega)^2 + (b_1 \sin \Omega + \dots + b_M \sin M\Omega)^2}}{\sqrt{(1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega)^2 + (a_1 \sin \Omega + \dots + a_N \sin N\Omega)^2}} \quad (\text{D.25})$$

$$\begin{aligned} \angle H(e^{j\Omega}) &= \tan^{-1} \left(\frac{-(b_1 \sin \Omega + \dots + b_M \sin M\Omega)}{b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega} \right) \\ &\quad - \tan^{-1} \left(\frac{-(a_1 \sin \Omega + \dots + a_N \sin N\Omega)}{1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega} \right) \end{aligned} \quad (\text{D.26})$$

Based in Eq. (D.24), we also have the magnitude and phase response for $H(e^{-j\Omega})$ as

$$|H(e^{-j\Omega})| = \frac{\sqrt{(b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega)^2 + (b_1 \sin \Omega + \dots + b_M \sin M\Omega)^2}}{\sqrt{(1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega)^2 + (a_1 \sin \Omega + \dots + a_N \sin N\Omega)^2}} \quad (\text{D.27})$$

$$\begin{aligned} \angle H(e^{-j\Omega}) &= \tan^{-1} \left(\frac{b_1 \sin \Omega + \dots + b_M \sin M\Omega}{b_0 + b_1 \cos \Omega + \dots + b_M \cos M\Omega} \right) \\ &\quad - \tan^{-1} \left(\frac{a_1 \sin \Omega + \dots + a_N \sin N\Omega}{1 + a_1 \cos \Omega + \dots + a_N \cos N\Omega} \right). \end{aligned} \quad (\text{D.28})$$

Comparing (D.25) with (D.27) and (D.26) with (D.28), respectively, we conclude the symmetric properties as

$$|H(e^{-j\Omega})| = |H(e^{j\Omega})| \quad (\text{D.29})$$

$$\angle H(e^{-j\Omega}) = -\angle H(e^{j\Omega}) \quad (\text{D.30})$$