

MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
Physics Department

Physics 8.07: Electromagnetism II  
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## PROBLEM SET 4 SOLUTIONS

### PROBLEM 1: TRACELESS SYMMETRIC PART OF $\hat{n}_i \hat{n}_j \hat{n}_k \hat{n}_m \hat{n}_n$ (15 points)

The terms that can appear in the expansion of  $\{ \hat{n}_i \hat{n}_j \hat{n}_k \hat{n}_m \hat{n}_n \}_{\text{TS}}$  can be classified by the number of Kronecker  $\delta$ -functions that they contain. With 5 indices, there can be terms with no Kronecker  $\delta$ -functions, terms with one Kronecker  $\delta$ -function, and terms with two. Once the number of  $\delta$ -functions is specified, the symmetry in the indices dictates the form of the terms up to an unknown coefficient for each classification. So we can begin by writing

$$\begin{aligned} \{ \hat{n}_i \hat{n}_j \hat{n}_k \hat{n}_m \hat{n}_n \}_{\text{TS}} = & \hat{n}_i \hat{n}_j \hat{n}_k \hat{n}_m \hat{n}_n + c_1 (\hat{n}_i \hat{n}_j \hat{n}_k \delta_{mn} + 9 \text{ other permutations}) \\ & + c_2 (\hat{n}_i \delta_{jk} \delta_{mn} + 14 \text{ other permutations}) . \end{aligned} \quad (1.1)$$

There are 10 terms with one  $\delta$ -function, since a term can be identified by specifying the two indicies on the  $\delta$ -function. The first of these indices is one choice out of 5 possibilities, while the second is a choice out of 4 possibilities. This would give  $5 \cdot 4 = 20$  possible combinations, but the order of the two indices does not matter, so there are 10 possibilities. They can be listed in full:

$$\begin{aligned} \text{Terms with 1 } \delta\text{-function} = & \hat{n}_i \hat{n}_j \hat{n}_k \delta_{mn} + \hat{n}_j \hat{n}_k \hat{n}_m \delta_{in} + \hat{n}_i \hat{n}_k \hat{n}_m \delta_{jn} + \hat{n}_i \hat{n}_j \hat{n}_m \delta_{kn} \\ & + \hat{n}_j \hat{n}_k \hat{n}_n \delta_{im} + \hat{n}_i \hat{n}_k \hat{n}_n \delta_{jm} + \hat{n}_i \hat{n}_j \hat{n}_n \delta_{km} \\ & + \hat{n}_j \hat{n}_m \hat{n}_n \delta_{ik} + \hat{n}_i \hat{n}_m \hat{n}_n \delta_{jk} + \hat{n}_k \hat{n}_m \hat{n}_n \delta_{ij} . \end{aligned} \quad (1.2)$$

The terms with two  $\delta$ -functions can be identified by first specifying the index on  $\hat{n}$ , which is one choice out of 5 possibilities. For each choice of the index on  $\hat{n}$ , there are 3 ways of arranging the other indices. For example, suppose that the index on  $\hat{n}$  is  $i$ , so that the remaining indices are  $j, k, m$  and  $n$ . The  $\delta$ -functions can then pair  $j$  with either  $k, m$ , or  $n$ , and the term is completely specified once that choice is made. If we wish to write out all 15 terms, they are:

$$\begin{aligned} \text{Terms with 2 } \delta\text{-functions} = & \hat{n}_i \delta_{jk} \delta_{mn} + \hat{n}_i \delta_{jm} \delta_{kn} + \hat{n}_i \delta_{jn} \delta_{km} \\ & + \hat{n}_j \delta_{ik} \delta_{mn} + \hat{n}_j \delta_{im} \delta_{kn} + \hat{n}_j \delta_{in} \delta_{km} \\ & + \hat{n}_k \delta_{ij} \delta_{mn} + \hat{n}_k \delta_{im} \delta_{jn} + \hat{n}_k \delta_{in} \delta_{jm} \\ & + \hat{n}_m \delta_{ij} \delta_{kn} + \hat{n}_m \delta_{ik} \delta_{jn} + \hat{n}_m \delta_{in} \delta_{jk} \\ & + \hat{n}_n \delta_{ij} \delta_{km} + \hat{n}_n \delta_{ik} \delta_{jm} + \hat{n}_n \delta_{im} \delta_{jk} . \end{aligned} \quad (1.3)$$

Now we contract Eq. (1.1) on two indices. I will choose these indices as  $m$  and  $n$ , so I multiply the left- and right-hand sides by  $\delta_{mn}$ , insisting that the trace vanish. The first term on the right-hand side gives

$$\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \hat{\mathbf{n}}_m \hat{\mathbf{n}}_n \delta_{mn} = \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k, \quad (1.4)$$

since  $\hat{\mathbf{n}}_m \hat{\mathbf{n}}_n \delta_{mn} = \hat{\mathbf{n}} \cdot \hat{\mathbf{n}} = 1$ . The second term (proportional to  $c_1$ ) is more complicated. For the first term shown in Eq. (1.2),  $\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \delta_{km} \delta_{kn} = \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \delta_{kk} = 3\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k$ . For the 6 terms for which either  $m$  or  $n$  appears on the  $\delta$ -function, the result is  $\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k$  for each case. For the 3 terms for which both  $m$  and  $n$  appear on the  $\hat{\mathbf{n}}$ 's, the result is  $\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij}$ . So finally,

$$c_1(\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \delta_{mn} + 9 \text{ other permutations}) \delta_{mn} = c_1 \left[ 9\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k + (\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij}) \right]. \quad (1.5)$$

For the 15 terms proportional to  $c_2$ , 3 of them are proportional to  $\delta_{mn}$ . The result of multiplying these three terms by  $\delta_{mn}$  is then  $3(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij})$ . For 6 of the terms,  $m$  appears on one  $\delta$ -function and  $n$  appears on the other. The result for these 6 terms is then  $2(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij})$ . Finally, for 6 of the terms either  $m$  or  $n$  appears as the index of  $\hat{\mathbf{n}}$ , and the other appears as an index on one of the  $\delta$ -functions. These 6 terms also give the result  $2(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij})$ , so

$$c_2(\hat{\mathbf{n}}_i \delta_{jk} \delta_{mn} + 14 \text{ other permutations}) \delta_{mn} = 7(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij}). \quad (1.6)$$

Collecting the results of Eqs. (1.4), (1.5), and (1.6), we have

$$\begin{aligned} \{ \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \hat{\mathbf{n}}_m \hat{\mathbf{n}}_n \}_{\text{TS}} \delta_{mn} &= 0 \\ &= \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k + c_1 \left[ 9\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k + (\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij}) \right] \\ &\quad + 7c_2(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij}). \end{aligned} \quad (1.7)$$

To insure that the coefficient of  $\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k$  equals zero, we find

$$c_1 = -\frac{1}{9}. \quad (1.8)$$

To insure that the coefficient of  $(\hat{\mathbf{n}}_i \delta_{jk} + \hat{\mathbf{n}}_j \delta_{ik} + \hat{\mathbf{n}}_k \delta_{ij})$  is zero, we find

$$c_2 = -\frac{1}{7}c_1 = \frac{1}{63}. \quad (1.9)$$

So finally,

$$\begin{aligned} \{ \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \hat{\mathbf{n}}_m \hat{\mathbf{n}}_n \}_{\text{TS}} &= \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \hat{\mathbf{n}}_m \hat{\mathbf{n}}_n - \frac{1}{9}(\hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \delta_{mn} + 9 \text{ other permutations}) \\ &\quad + \frac{1}{63}(\hat{\mathbf{n}}_i \delta_{jk} \delta_{mn} + 14 \text{ other permutations}). \end{aligned}$$

(1.10)

As a check, we can rewrite Eq. (1.10) for  $\hat{\mathbf{n}} = \hat{\mathbf{z}}$ ,

$$\begin{aligned} \{ \hat{\mathbf{z}}_i \hat{\mathbf{z}}_j \hat{\mathbf{z}}_k \hat{\mathbf{z}}_m \hat{\mathbf{z}}_n \}_{\text{TS}} &= \hat{\mathbf{z}}_i \hat{\mathbf{z}}_j \hat{\mathbf{z}}_k \hat{\mathbf{z}}_m \hat{\mathbf{z}}_n - \frac{1}{9} (\hat{\mathbf{z}}_i \hat{\mathbf{z}}_j \hat{\mathbf{z}}_k \delta_{mn} + 9 \text{ other permutations}) \\ &+ \frac{1}{63} (\hat{\mathbf{z}}_i \delta_{jk} \delta_{mn} + 14 \text{ other permutations}) , \end{aligned} \quad (1.11)$$

as the coefficients do not depend on what unit vector is used in the construction. Then we can use Eq. (1.51) of Lecture Notes 1 to evaluate

$$\begin{aligned} P_5(\cos \theta) &= \frac{10!}{2^5 \cdot (5!)^2} \{ \hat{\mathbf{z}}_i \hat{\mathbf{z}}_j \hat{\mathbf{z}}_k \hat{\mathbf{z}}_m \hat{\mathbf{z}}_n \}_{\text{TS}} \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j \hat{\mathbf{n}}_k \hat{\mathbf{n}}_m \hat{\mathbf{n}}_n \\ &= \frac{63}{8} \left[ \cos^5 \theta - \frac{10}{9} \cos^3 \theta + \frac{15}{63} \cos \theta \right] \\ &= \frac{1}{8} [63 \cos^5 \theta - 70 \cos^3 \theta + 15 \cos \theta] , \end{aligned} \quad (1.12)$$

where the last line agrees with the standard expression for  $P_5(x)$ , as can be found, for example, in the Wikipedia. It can also be computed in Mathematica as LegendreP[5,x].

## PROBLEM 2: QUADRUPOLE AND OCTOPOLE TERMS OF THE MULTIPOLE EXPANSION (20 points)

- (a) [5 pts] The preamble said that this problem can be attacked in any one of three methods, so we give three different answers.

**Method (i)** (Using Griffiths' Eq. (3.95)): The starting equation is

$$V(\vec{\mathbf{r}}) = \frac{1}{4\pi\epsilon_0} \sum_{n=0}^{\infty} \frac{1}{r^{n+1}} \int (r')^n P_n(\cos \alpha) \rho(\vec{\mathbf{r}}') d^3x' , \quad (\text{Griffiths 3.95})$$

where I am using  $d^3x'$  where Griffiths uses  $d\tau'$ . Using the expression for  $P_2(x)$ , the quadrupole term becomes

$$\begin{aligned} V_{\text{quad}}(\vec{\mathbf{r}}) &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \int r'^2 P_2(\cos \theta') \rho(\vec{\mathbf{r}}') d^3x' \\ &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \int \frac{1}{2} (3r'^2 \cos^2 \theta' - r'^2) \rho(\vec{\mathbf{r}}') d^3x' . \end{aligned} \quad (2.1)$$

We are asked to show that we can rewrite the quadrupole term in terms of the quadrupole moment:

$$V_{\text{quad}}(\vec{\mathbf{r}}) = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \sum_{i,j=1}^3 \hat{\mathbf{r}}_i \hat{\mathbf{r}}_j Q_{ij} , \quad (2.2)$$

where

$$Q_{ij} = \frac{1}{2} \int [3r'_i r'_j - r'^2 \delta_{ij}] \rho(\vec{r}') d^3 x' . \quad (2.3)$$

If we write  $\cos \theta' = \hat{\mathbf{r}} \cdot \hat{\mathbf{r}}' = \hat{\mathbf{r}}_i \hat{\mathbf{r}}'_i$ , and then  $\cos^2 \theta' = \hat{\mathbf{r}}_i \hat{\mathbf{r}}_j \hat{\mathbf{r}}'_i \hat{\mathbf{r}}'_j$ , we see that

$$(3r'^2 \cos^2 \theta' - r'^2) = \hat{\mathbf{r}}_i \hat{\mathbf{r}}_j (3r'_i r'_j - r'^2 \delta_{ij}) , \quad (2.4)$$

and then Eq. (2.1) becomes

$$V_{\text{quad}}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \hat{\mathbf{r}}_i \hat{\mathbf{r}}_j \left[ \frac{1}{2} \int (3r'_i r'_j - r'^2 \delta_{ij}) \rho(\vec{r}') d^3 x' \right] , \quad (2.5)$$

which is the desired result.

**Method (ii)** (Using Griffiths' Eq. (2.29)): The starting equation in this case is

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho(\vec{r}')}{|\vec{r} - \vec{r}'|} d^3 x' , \quad (\text{Griffiths 2.29})$$

where I am using  $|\vec{r} - \vec{r}'|$  where Griffiths uses  $\mathfrak{A}$ . We now want to expand  $f(\vec{r}') \equiv 1/|\vec{r} - \vec{r}'|$  in a power series in  $r'_i$ , the components of  $\vec{r}'$ :

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int \rho(\vec{r}') \left[ f(\vec{0}) + \left. \frac{\partial f}{\partial r'_i} \right|_{\vec{r}'=\vec{0}} r'_i + \frac{1}{2} \left. \frac{\partial^2 f}{\partial r'_i \partial r'_j} \right|_{\vec{r}'=\vec{0}} r'_i r'_j + \dots \right] d^3 x' \quad (2.6)$$

The quadrupole term is the term quadratic in  $r'_i$ :

$$V_{\text{quad}}(\vec{r}) = \frac{1}{2} \frac{1}{4\pi\epsilon_0} \int \rho(\vec{r}') \left. \frac{\partial^2 f}{\partial r'_i \partial r'_j} \right|_{\vec{r}'=\vec{0}} r'_i r'_j d^3 x' . \quad (2.7)$$

To evaluate the partial derivatives of  $f$ , define  $w \equiv |\vec{r} - \vec{r}'|^2 = (r'_k - r_k)(r'_k - r_k)$ , so  $f(\vec{r}') = 1/w^{1/2}$ , and

$$\frac{\partial w}{\partial r'_i} = 2\delta_{ik}(r'_k - r_k) = 2(r'_i - r_i) . \quad (2.8)$$

Then

$$\frac{\partial f}{\partial r'_i} = -\frac{1}{2} \frac{1}{w^{3/2}} \frac{\partial w}{\partial r'_i} = -\frac{1}{w^{3/2}} (r'_i - r_i) , \quad (2.9)$$

and

$$\begin{aligned} \frac{\partial^2 f}{\partial r'_j \partial r'_i} &= -\frac{\frac{\partial}{\partial r'_j} (r'_i - r_i)}{w^{3/2}} + \frac{3}{2} \frac{1}{w^{5/2}} (r'_i - r_i) \frac{\partial w}{\partial r'_j} \\ &= \frac{1}{w^{5/2}} [3(r'_i - r_i)(r'_j - r_j) - w\delta_{ij}] . \end{aligned} \quad (2.10)$$

Then

$$\begin{aligned} \left. \frac{\partial^2 f}{\partial r'_j \partial r'_i} \right|_{\vec{r}'=0} r'_i r'_j &= \frac{1}{r^5} [3r_i r_j - r^2 \delta_{ij}] r'_i r'_j \\ &= \frac{1}{r^3} \hat{r}_i \hat{r}_j [3r'_i r'_j - r'^2 \delta_{ij}] , \end{aligned} \quad (2.11)$$

and finally, using Eq. (2.7), we find

$$V_{\text{quad}}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \hat{r}_i \hat{r}_j \left[ \frac{1}{2} \int [3r'_i r'_j - r'^2 \delta_{ij}] \rho(\vec{r}') d^3x' \right] . \quad (2.12)$$

**Method (iii)** (Using traceless symmetric tensors): The starting point in this case is Eqs. (2.26) and (2.27) of Lecture Notes 2:

$$V(\vec{r}) = \frac{1}{4\pi\epsilon_0} \sum_{\ell=0}^{\infty} \frac{1}{r^{\ell+1}} C_{i_1 \dots i_\ell}^{(\ell)} \hat{n}_{i_1} \dots \hat{n}_{i_\ell} , \quad (\text{Lecture Notes 2.26})$$

where

$$C_{i_1 \dots i_\ell}^{(\ell)} = \frac{(2\ell-1)!!}{\ell!} \int \rho(\vec{r}') \{ \vec{r}'_{i_1} \dots \vec{r}'_{i_\ell} \}_{\text{TS}} d^3x' . \quad (\text{Lecture Notes 2.27})$$

Identifying  $Q_{ij}$  with  $C_{ij}^{(2)}$ , we see that  $V(\vec{r})$  already has the desired form, so all we have to do is write out the quadrupole term,  $\ell = 2$ , explicitly:

$$\begin{aligned} Q_{ij} &= \frac{3}{2} \int \rho(\vec{r}') \{ r'_i r'_j \}_{\text{TS}} d^3x' \\ &= \boxed{ \frac{1}{2} \int \rho(\vec{r}') [3r'_i r'_j - r'^2 \delta_{ij}] d^3x' } . \end{aligned} \quad (2.13)$$

- (b) [5 pts] The square in Griffiths Fig. 3.30 has side  $a$  and lies in the  $xy$  plane, centered at the origin. From the definition of  $Q_{ij}$  given in the problem, or equivalently in

Eq. (2.3),

$$\begin{aligned}
 Q_{xx} = Q_{yy} &= \frac{1}{2} [3(a/2)^2 - (\sqrt{2}a/2)^2] (q - q + q - q) = \boxed{0} \\
 Q_{xz} = Q_{zx} = Q_{yz} = Q_{zy} &= \boxed{0} \quad \text{since } z = 0 \\
 Q_{zz} &= -\frac{1}{2} (\sqrt{2}a/2)^2 (q - q + q - q) = \boxed{0} \\
 Q_{xy} = Q_{yx} &= \frac{3}{2} \left[ \left(\frac{a}{2}\right) \left(\frac{a}{2}\right) q + \left(\frac{a}{2}\right) \left(\frac{-a}{2}\right) (-q) + \left(\frac{-a}{2}\right) \left(\frac{-a}{2}\right) q \right. \\
 &\quad \left. + \left(\frac{-a}{2}\right) \left(\frac{a}{2}\right) (-q) \right] = \boxed{\frac{3}{2} a^2 q} .
 \end{aligned} \tag{2.14}$$

(c) [5 pts] For a given charge distribution the quadrupole moment is defined as

$$Q_{ij} = \frac{1}{2} \int [3r_i r_j - r^2 \delta_{ij}] \rho(\vec{r}) d^3x . \tag{2.15}$$

When we move the reference frame by  $\vec{d}$ , the quadrupole moment in the new reference frame becomes:

$$\begin{aligned}
 Q'_{ij} &= \frac{1}{2} \int [3(r_i - d_i)(r_j - d_j) - |\vec{r} - \vec{d}|^2 \delta_{ij}] \rho(\vec{r}) d^3x \\
 &= \frac{1}{2} \int [3r_i r_j - r^2 \delta_{ij}] \rho d^3x - \frac{3}{2} d_i \int r_j \rho d^3x - \frac{3}{2} d_j \int r_i \rho d^3x + \frac{3}{2} d_i d_j \int \rho d^3x \\
 &\quad + \vec{d} \cdot \int \vec{r} \rho \delta_{ij} d^3x - \frac{1}{2} d^2 \delta_{ij} \int \rho d^3x \\
 &= Q_{ij} - \frac{3}{2} (d_i p_j + d_j p_i) + \frac{3}{2} d_i d_j Q + \delta_{ij} \vec{d} \cdot \vec{p} - \frac{1}{2} d^2 \delta_{ij} Q ,
 \end{aligned} \tag{2.16}$$

where  $Q = \int \rho d^3x$  and  $p_i = \int r_i \rho d^3x$ . So if  $\vec{p} = 0$  and  $Q = 0$  then  $Q'_{ij} = Q_{ij}$ .

Alternatively, using the notation of traceless symmetric tensors, we find

$$\begin{aligned}
 Q'_{ij} &= \frac{3}{2} \int \rho(\vec{r}) \{ (r_i - d_i)(r_j - d_j) \}_{\text{TS}} d^3x \\
 &= \frac{3}{2} \int \rho(\vec{r}) \{ r_i r_j - (r_i d_j + r_j d_i) + d_i d_j \}_{\text{TS}} d^3x' \\
 &= \frac{3}{2} [Q_{ij} - \{ p_i d_j + p_j d_i \}_{\text{TS}} + \{ d_i d_j \}_{\text{TS}} Q] ,
 \end{aligned} \tag{2.17}$$

so again we see that  $Q'_{ij} = Q_{ij}$  if  $p_i = Q = 0$ .

- (d) [5 pts] As in part (a), the preamble said that this problem can be attacked in any one of three methods:

**Method (i)** (Using Griffiths' Eq. (3.95)): Writing the  $n = 3$  term of Griffiths' Eq. (3.95),

$$\begin{aligned} V_{\text{oct}}(\vec{r}) &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^4} \int (r')^3 P_3(\cos \alpha) \rho(\vec{r}') d^3x' \\ &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^4} \int (r')^3 \left[ \frac{1}{2} (5 \cos^3 \alpha - 3 \cos \alpha) \right] \rho(\vec{r}') d^3x' . \end{aligned} \quad (2.18)$$

As in part (a), if we use  $\cos \alpha = \hat{r}_i \hat{r}'_i$ , the above equation can be rewritten as

$$\begin{aligned} V_{\text{oct}}(\vec{r}) &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^4} \hat{r}_i \hat{r}_j \hat{r}_k \int \left\{ \frac{1}{2} [5r'_i r'_j r'_k - r'^2 (\delta_{jk} r'_i + \delta_{ik} r'_j + \delta_{ij} r'_k)] \right\} \rho(\vec{r}') d^3x' \\ &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^4} \hat{r}_i \hat{r}_j \hat{r}_k Q_{ijk} , \end{aligned} \quad (2.19)$$

where

$$Q_{ijk} = \frac{1}{2} \int [5r'_i r'_j r'_k - r'^2 (\delta_{jk} r'_i + \delta_{ik} r'_j + \delta_{ij} r'_k)] \rho(\vec{r}') d^3x' . \quad (2.20)$$

**Method (ii)** (Using Griffiths' Eq. (2.29)): Continuing from part (a(ii)), the octopole term is the 3rd order term in the power expansion:

$$V_{\text{oct}}(\vec{r}) = \frac{1}{3!} \frac{1}{4\pi\epsilon_0} \int \rho(\vec{r}') \left. \frac{\partial^3 f}{\partial r'_i \partial r'_j \partial r'_k} \right|_{\vec{r}'=\vec{0}} r'_i r'_j r'_k d^3x' . \quad (2.21)$$

Starting from Eq. (2.10),

$$\begin{aligned} \frac{\partial^3 f}{\partial r'_i \partial r'_j \partial r'_k} &= \frac{\partial}{\partial r'_k} \left\{ \frac{1}{w^{5/2}} [3(r'_i - r_i)(r'_j - r_j) - w\delta_{ij}] \right\} \\ &= -\frac{5}{2} \frac{1}{w^{7/2}} [3(r'_i - r_i)(r'_j - r_j) - w\delta_{ij}] 2(r'_k - r_k) \\ &\quad + \frac{1}{w^{5/3}} [3\delta_{ik}(r'_j - r_j) + 3\delta_{jk}(r'_i - r_i) - 2\delta_{ij}(r'_k - r_k)] \\ &= -\frac{15}{w^{7/2}} (r'_i - r_i)(r'_j - r_j)(r'_k - r_k) \\ &\quad + \frac{3}{w^{5/3}} [\delta_{ik}(r'_j - r_j) + \delta_{jk}(r'_i - r_i) + \delta_{ij}(r'_k - r_k)] . \end{aligned} \quad (2.22)$$

Then

$$\left. \frac{\partial^3 f}{\partial r'_i \partial r'_j \partial r'_k} \right|_{\vec{r}'=\vec{0}} = \frac{3}{r^4} \left[ 5\hat{r}_i \hat{r}_j \hat{r}_k - (\delta_{jk} \hat{r}_i + \delta_{ik} \hat{r}_j + \delta_{ij} \hat{r}_k) \right], \quad (2.23)$$

and from Eq. (2.21) we have

$$V_{\text{oct}}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{1}{r^4} \hat{r}_i \hat{r}_j \hat{r}_k Q_{ijk}, \quad (2.24)$$

where

$$Q_{ijk} = \frac{1}{2} \int \rho(\vec{r}') \left[ 5r'_i r'_j r'_k - r'^2 (\delta_{jk} r'_i + \delta_{ik} r'_j + \delta_{ij} r'_k) \right] d^3 x'. \quad (2.25)$$

**Method (iii)** (Using traceless symmetric tensors): Identifying  $Q_{ijk}$  with  $C_{ijk}^{(3)}$ , we see that  $V(\vec{r})$  already has the desired form, so all we have to do is write out the octopole term,  $\ell = 3$ , of Lecture Notes 2 Eq. (2.27), quoted above in the solution to part (a).

$$\begin{aligned} Q_{ijk} &= \frac{5}{2} \int \rho(\vec{r}') \{ r'_i r'_j r'_k \}_{\text{TS}} d^3 x' \\ &= \frac{1}{2} \int \rho(\vec{r}') \left[ 5r'_i r'_j r'_k - r'^2 (\delta_{jk} r'_i + \delta_{ik} r'_j + \delta_{ij} r'_k) \right] d^3 x'. \end{aligned} \quad (2.26)$$

The expansion of  $\{ r'_i r'_j r'_k \}_{\text{TS}}$  in the above equation can be found directly from the definition, which says that it is equal to  $r'_i r'_j r'_k$ , combined with terms proportional to at least one Kronecker delta function to make it traceless. It is the same calculation that was done in Eq. (1.44) of Lecture Notes 1.

### PROBLEM 3: NORMALIZING THE TRACELESS SYMMETRIC TENSOR REPRESENTATION OF THE LEGENDRE POLYNOMIALS (15 points)

From Eqs. (3.2) and (3.5) of the problem set, we have

$$N(\ell) = \frac{1}{\{ \hat{z}_{i_1} \dots \hat{z}_{i_\ell} \}_{\text{TS}} \hat{z}_{i_1} \dots \hat{z}_{i_\ell}},$$

so our goal is to evaluate

$$\{ \hat{z}_{i_1} \dots \hat{z}_{i_\ell} \}_{\text{TS}} \hat{z}_{i_1} \dots \hat{z}_{i_\ell}.$$



But Eq. (3.6) of the problem set tells us that

$$\{\hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_\ell}\}_{\text{TS}} \hat{\mathbf{z}}_{i_\ell} = \frac{\ell}{2\ell-1} \{\hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_{\ell-1}}\}_{\text{TS}} ,$$

where I have replaced  $\hat{\mathbf{n}}$  by  $\hat{\mathbf{z}}$ , since the equation was derived for any unit vector  $\hat{\mathbf{n}}$ . Now we can proceed by iterating this relation:

$$\begin{aligned} \{\hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_\ell}\}_{\text{TS}} \hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_\ell} &= \frac{\ell}{2\ell-1} \{\hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_{\ell-1}}\}_{\text{TS}} \hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_{\ell-1}} \\ &= \left(\frac{\ell}{2\ell-1}\right) \left(\frac{\ell-1}{2\ell-3}\right) \{\hat{\mathbf{z}}_{i_1} \dots \hat{\mathbf{z}}_{i_{\ell-2}}\}_{\text{TS}} \\ &= \left(\frac{\ell}{2\ell-1}\right) \left(\frac{\ell-1}{2\ell-3}\right) \dots \left(\frac{1}{1}\right) \{1\}_{\text{TS}} \\ &= \frac{\ell!}{(2\ell-1)!!} . \end{aligned}$$

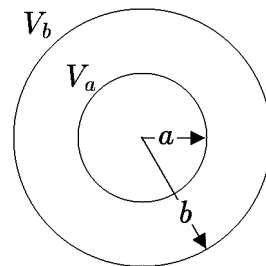
So

$$N(\ell) = \frac{(2\ell-1)!!}{\ell!} = \frac{(2\ell)!}{2^\ell (\ell!)^2} .$$

**PROBLEM 4: CONCENTRIC SPHERICAL SHELLS OF CHARGE** (25 points)

- (a) [5 pts] The situation is spherically symmetric, which means that only the  $\ell = 0$  solution of the multipole expansion is allowed. Thus,  $V(r)$  in any region has at most two terms, a constant and a term proportional to  $1/r$ . For the potential to vanish at infinity, the potential for  $r > b$  can have only a  $1/r$  term. Matching the boundary condition at  $r = b$  then gives

$$V(r) = \frac{bV_b}{r} \quad (\text{for } r \geq b) . \quad (4.1)$$



Similarly, the potential for  $r \leq a$  can only have the constant term, since the term proportional to  $1/r$  would diverge. The constant must then match the potential at  $r = a$ , so

$$V(r) = V_a \quad (\text{for } r \leq a) . \quad (4.2)$$

For  $a \leq r \leq b$ , both terms are allowed, but the potential must match  $V_a$  on the inside and  $V_b$  on the outside. Writing

$$V(r) = A + \frac{B}{r}$$

for this region, the two boundary conditions give

$$A + \frac{B}{a} = V_a , \quad A + \frac{B}{b} = V_b .$$

The problem is then solved by solving these two equations for  $A$  and  $B$ . For example, we can subtract the second equation from the first to find

$$B \left( \frac{1}{a} - \frac{1}{b} \right) = V_a - V_b ,$$

which implies that

$$B = \frac{ab}{b-a} (V_a - V_b) .$$

Then from the first equation,

$$A = V_a - \frac{B}{a} = V_a - \frac{b}{b-a} (V_a - V_b) = \frac{bV_b - aV_a}{b-a} .$$

Finally, then,

$$V(r) = \frac{1}{b-a} \left[ bV_b - aV_a + \frac{ab}{r} (V_a - V_b) \right] \quad (\text{for } a \leq r \leq b) . \quad (4.3)$$

- (b) [10 pts] In terms of the charge  $Q_a$  on the inner shell, the potential in the region  $a \leq r \leq b$  can be written as

$$V(r) = \frac{1}{4\pi\epsilon_0} \frac{Q_a}{r} + \text{const} ,$$

which can be compared with Eq. (4.3) found in part (a) to see that

$$Q_a = 4\pi\epsilon_0 \left( \frac{ab}{b-a} \right) (V_a - V_b) . \quad (4.4)$$

Similarly, the potential outside of both shells can be expressed in terms of the total charge on both shells as

$$V(r) = \frac{1}{4\pi\epsilon_0} \frac{Q_a + Q_b}{r} ,$$

where in this case we do not need to include a constant term, since we know that we have chosen  $V = 0$  at  $r = \infty$ . Comparing with Eq. (4.1), we see that

$$Q_a + Q_b = 4\pi\epsilon_0 b V_b .$$

Using Eq. (4.4), we find

$$\begin{aligned} Q_b &= 4\pi\epsilon_0 \left[ bV_b - \left( \frac{ab}{b-a} \right) (V_a - V_b) \right] \\ &= 4\pi\epsilon_0 \left[ \frac{b(b-a)V_b - ab(V_a - V_b)}{b-a} \right] \\ &= \boxed{4\pi\epsilon_0 \left( \frac{b}{b-a} \right) (bV_b - aV_a) .} \end{aligned} \tag{4.5}$$

The total electrostatic energy  $W$  is then given by

$$\boxed{W = \frac{1}{2}(Q_a V_a + Q_b V_b) .} \tag{4.6}$$

Substituting  $Q_a$  and  $Q_b$  from Eqs. (4.4) and (4.5), one finds

$$\boxed{W = \frac{2\pi\epsilon_0 b}{b-a} [aV_a^2 - bV_b^2 - 2aV_a V_b]} \tag{4.7a}$$

or, equivalently,

$$\boxed{W = \frac{2\pi\epsilon_0 b}{b-a} [a(V_a - V_b)^2 + (b-a)V_b^2]} . \tag{4.7b}$$

(c) [10 pts] The expression for  $V(r=b, \theta, \phi)$  can be rewritten as

$$V(r=b, \theta, \phi) = V_0 \hat{\mathbf{n}}_x \hat{\mathbf{n}}_y ,$$

or  $V_0 \hat{\mathbf{r}}_x \hat{\mathbf{r}}_y$ , depending on notation. This can be rewritten as

$$V(r=b, \theta, \phi) = C_{ij} \hat{\mathbf{n}}_i \hat{\mathbf{n}}_j ,$$

where

$$C_{ij} = \frac{1}{2} V_0 (\hat{\mathbf{x}}_i \hat{\mathbf{y}}_j + \hat{\mathbf{y}}_i \hat{\mathbf{x}}_j) .$$

One sees that  $\delta_{ij} C_{ij} = \hat{\mathbf{x}} \cdot \hat{\mathbf{y}} = 0$ , so  $C_{ij}$  is traceless and symmetric. Thus, the angular dependence is described entirely by the  $\ell = 2$  term of the general expansion (on the formula sheets),

$$V(\vec{\mathbf{r}}) = \sum_{\ell=0}^{\infty} \left( C_{i_1 i_2 \dots i_\ell}^{(\ell)} r^\ell + \frac{C_{i_1 i_2 \dots i_\ell}'^{(\ell)}}{r^{\ell+1}} \right) \hat{\mathbf{r}}_{i_1} \hat{\mathbf{r}}_{i_2} \dots \hat{\mathbf{r}}_{i_\ell} , \quad \text{where } \vec{\mathbf{r}} = r \hat{\mathbf{r}} .$$

For those who prefer standard spherical harmonics, one can see from the tables in the formula sheet that

$$V(r=b, \theta, \phi) = \frac{1}{2} V_0 \left( 4 \sqrt{\frac{2\pi}{15}} \right) \frac{Y_{2,2} - Y_{2,-2}}{2i} ,$$

so again it is pure  $\ell = 2$ . Thus, the allowed radial dependence, for solutions to Laplace's equation, is either  $r^2$  or  $1/r^3$ .

For  $r \leq a$ , we see that the boundary condition of  $V = 0$  at  $r = a$  is trivially matched by

$$\boxed{V(r) = 0 \quad (\text{for } r \leq a) .} \quad (4.8)$$

For  $r \geq b$ , a term proportional to  $r^2$  would not be allowed, since it blows up at infinity, so  $V$  must be proportional to  $1/r^3$ . It is then seen that the boundary condition at  $r = b$  is easily matched by writing

$$\boxed{V(r) = \left( \frac{b}{r} \right)^3 V_0 \sin^2 \theta \sin \phi \cos \phi \quad (\text{for } r \geq b) .} \quad (4.9)$$

Finally, the region  $a \leq r \leq b$  is the most complicated, since it can include both terms. We write

$$V(r) = V_0 \sin^2 \theta \sin \phi \cos \phi \left[ A r^2 + \frac{B}{r^3} \right] , \quad (4.10)$$

where the boundary conditions at  $r = a$  and  $r = b$  require that

$$Aa^2 + \frac{B}{a^3} = 0 , \quad Ab^2 + \frac{B}{b^3} = 1 . \quad (4.11)$$

Multiplying the first equation above by  $b^2$ , and the second equation above by  $a^2$ , and then subtracting the second equation from the first, one finds

$$B \left( \frac{b^2}{a^3} - \frac{a^2}{b^3} \right) = -a^2 ,$$

from which one finds

$$B = -\frac{a^5 b^3}{b^5 - a^5} .$$

Then, from the first of Eqs. (4.11),

$$A = -\frac{B}{a^5} = \frac{b^3}{b^5 - a^5} .$$

Substituting these values into Eq. (4.10), one finds

$$V(r) = \frac{V_0 \sin^2 \theta \sin \phi \cos \phi}{b^5 - a^5} \left[ b^3 r^2 - \frac{a^5 b^3}{r^3} \right] , \quad (4.12)$$

which could equivalently be written

$$V(r) = V_0 \sin^2 \theta \sin \phi \cos \phi \left( \frac{b^3}{b^5 - a^5} \right) \left( r^2 - \frac{a^5}{r^3} \right) . \quad (4.13)$$