

Energy-Aware Planning-Scheduling for Autonomous Aerial Robots

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Abstract—The letter presents a planning-scheduling approach for battery-powered autonomous aerial robots, which plans in-flight a coverage path and simultaneously schedules onboard computational tasks. It derives a novel variable coverage motion robust to airborne constraints and an empirically motivated differential periodic energy model. The model is enhanced with the time and energy contribution of the path and tasks, utilizing a previously proposed automatic modeling tool. Accounting for uncertainty, an initial “plan-schedule” is re-planned and re-scheduled in the function of the battery, exploiting all the available resources yet avoiding possible in-flight failure in case of unexpected battery drops, e.g., due to adverse atmospheric conditions.

Index Terms—Aerial Systems: Perception and Autonomy, Optimization and Optimal Control, Planning, Scheduling and Coordination, Planning under Uncertainty

I. INTRODUCTION

USE CASES involving aerial robots span broadly. They compromise diverse planning and scheduling strategies and often require high autonomy under strict energy budgets. A typical instance is an aerial robot visiting each point in a given space [1], running some onboard computational tasks, a problem in the literature under coverage path planning (CPP) [2], [3]. Here, the aerial robot might detect ground patterns and notify other ground-based actors with little human interaction (see Figure 1). Such use cases arise in, e.g., precision agriculture [4], where harvesting involves ground [5]–[10], damage prevention aerial robots [11], [12]. In these and many others, the robot frequently mounts microcontroller and heterogeneous computing hardware [13] (i.e., with CPUs and GPUs) running power-demanding computational tasks [14]–[17]. We refer to computational tasks that can be scheduled with an energy impact as computations. We are interested in the simultaneous energy optimization of motion plans and computations schedules in-flight and refer to it as energy-aware planning-scheduling. Generic mobile robotics studies that deal with planning-scheduling energy awareness are scarce [18]–[21] and focused on ground-based robots [13], [20]–[23]. Yet, aerial robots are particularly affected by various energy considerations. Indeed it would be generally required

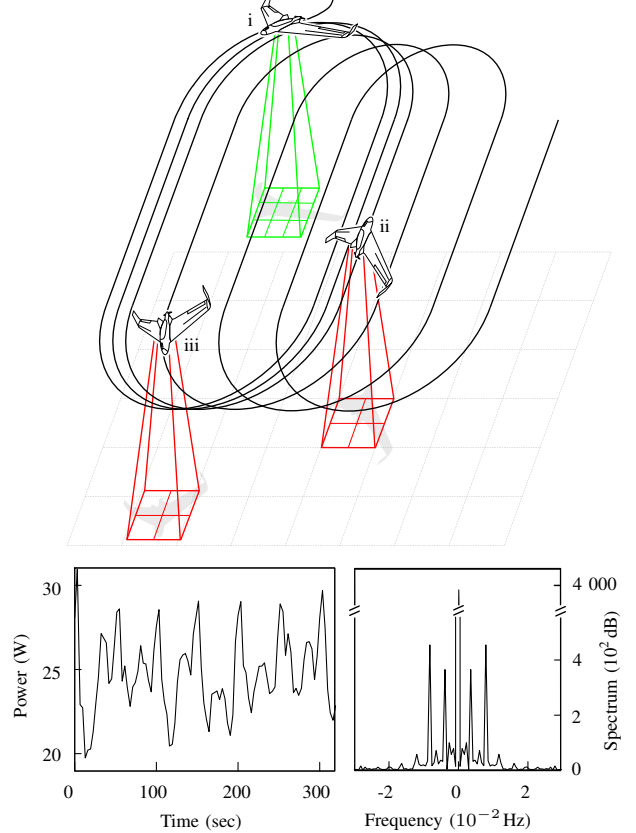


Fig. 1: Illustrative example of planning-scheduling. An initial plan (in **i**) is re-planned in-flight computations-wise (in **ii**) and motion-wise (in **iii**). Follow the collected energy data of a physical aerial robot flying the use case.

to land to recharge the battery [24]. Such a state of practice has prompted us to propose a planning-scheduling approach for autonomous aerial robots. It combines the past body of knowledge, addressing aerial robots’ peculiarities such as the atmospheric, battery, and turning radius constraints. Numerical simulations and experimental data of both static and dynamic plans-schedules show improved power savings and fault tolerance with the aerial robots remedying in-flight failures. Fig. 1 illustrates the intuition: an aerial robot flies full plan-schedule (i), that is optimized w.r.t. the battery (ii), and altered due to, e.g., unexpected battery defects (iii).

There are numerous planning algorithms applied to a variety of robots. An instance is an algorithm selecting an energy-optimized trajectory [25] by, e.g., maximizing the operational time [26]. Many apply to a small number of robots [27] and focus exclusively on planning the trajectory [28], despite evidence of the energy influence of consumptions [13], [18], [19], [21]. In view of the availability of powerful heterogeneous computing hardware [29], the use of computations is further expected to increase in the foreseeable future [30]–[32]. In this context, planning-scheduling energy awareness is

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a recent research direction. Early studies (2000–2010) varied hardware-dependent aspects, e.g., frequency, voltage, along with motion aspects, e.g., motor and travel velocities [13], [18], [22], [33] whereas the literature from the past decade derives energy-aware plans-schedules in broader terms. These include simultaneous considerations for planning-scheduling in perception [21], localization [20], navigation [23], [34], [35], and anytime planning [19]. We extend the relevant literature to the case of CPP with aerial robots.

Our focus is on fixed wings, i.e., airborne robots where wings provide lift, propellers forward thrust, and control surfaces maneuvering. Here, motion and computations energies are within an order of magnitude from each other [36]. Indeed there are other classes where planning-scheduling energy awareness leads to irrelevant savings, i.e., when the motion energy contribution far outreaches the computations and vice-versa. The occurrence frequently happens with rotary-wing aerial robots (e.g., quadrotors or quadcopters, hexacopters, etc.) and lighter-than-air aerial robots (e.g., blimps). It is a common theme with wider planning-scheduling literature, focusing on energy-efficient ground-based robots such as Pioneer 3DX [13], [23], [34], [35], ARC Q14 [20], [21], and Pack-Bot UGV [22].

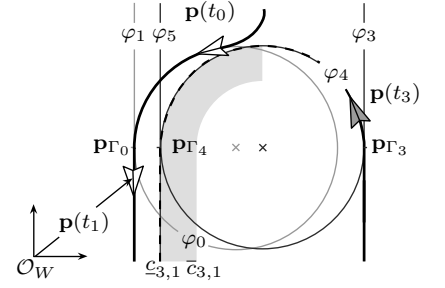
To guarantee energy awareness, our approach uses optimal control where both the paths and schedules variations are trajectories, varying between given bounds (e.g., physical constraints of the robot and computing hardware, the desired quality of the coverage, etc.). Numerous past planning-scheduling studies also employ optimization techniques [18], [20], [21], [33], whereas some others greedy [13], [19], [22] and reinforcement learning-based approaches [23], [34], [35]. Both the variations trajectories are derived for future time instants employing computations and motion energies and battery models. The energy model for the computations uses regression analysis from our earlier study on heterogeneous computing hardware energy modeling [37], [38], whereas the battery an equivalent circuit model (ECM) from the literature [39]–[41]. The motion wraps the past two in a cohesive model that uses differential and periodic modeling to predict future energy behavior of various plans-schedules. In Fig. 1, collected energy data (bottom left) and spectrum analysis (right) of a fixed-wing aerial robot flying CPP motivates the motion energy model: the evolution is periodic, an observation we exploit in Section III for the computations and motion energies and battery models.

The remaining sections of the letter are then organized as follows. Sec. II provides basic constructs, such as the concepts of the plan, stages, triggering and final points, and path functions, as well as the problem formulation. Sec. IV describes in detail the methodology of planning-scheduling. Sec. V presents the results and showcases the performances, and Sec. VI concludes and provides future perspectives. Appendices provide supplementary information.

II. PROBLEM FORMULATION

Before defining the problem of energy-aware planning-scheduling in Sec. II-B, Sec. II-A provides necessary preliminaries. For CPP and, e.g., pattern detections in precision

Fig. 2: Defs. II.1–4 on a slice of the plan Γ . $\mathbf{p}_{\Gamma_1}, \dots$ are triggering points in which proximity happens change of stages Γ_1, \dots . Each contains a path function φ_1, \dots and parameters to alter the path and schedule $c_{1,1}, \dots$.



agriculture, we assume that aerial robot travels a *plan* with information about the path and the schedule.

A. Preliminaries

Definition II.1 (Plan). Given a generic point $\mathbf{p}(t) \in \mathbb{R}^2$ w.r.t. a reference frame \mathcal{O}_W of the aerial robot flying at a given altitude $h \in \mathbb{R}_{>0}$, the *plan* is a finite state machine (FSM) Γ , where the state-transition function $s : \bigcup_i \Gamma_i \times \mathbb{R}^2 \rightarrow \bigcup_i \Gamma_i$ maps a stage and a point to the next stage

$$s(\Gamma_i, \mathbf{p}(t)) := \begin{cases} \Gamma_{i+j} & \exists j \in \mathbb{Z}, \text{ if } \|\mathbf{p}(t) - \mathbf{p}_{\Gamma_i}\| < \varepsilon_i \\ \Gamma_i & \text{otherwise} \end{cases}.$$

Here, Γ_i is a *stage*, and \mathbb{Z} denotes the set of integers. At each stage, the aerial robot travels a path and runs a schedule on the computing hardware. Both are to be altered in Sec. IV within given boundaries with *path*- and *computations*-specific *parameters*. ε_i is a stage-dependent value detailed after Definition II.4.

Definition II.2 (Stage). The i th stage Γ_i at time instant t of a plan Γ is

$$\Gamma_i := \{\varphi_i(\mathbf{p}(t), c_i^\rho), c_i^\sigma \mid \forall j \in [\rho]_{>0}, c_{i,j} \in \mathcal{C}_{i,j}, \forall k \in [\sigma]_{>0}, c_{i,\rho+k} \in \mathcal{S}_{i,k}\},$$

where c_i^ρ and c_i^σ are ρ *path* and σ *computations parameters*. $\mathcal{C}_{i,j} := [\underline{c}_{i,j}, \bar{c}_{i,j}] \subseteq \mathbb{R}$ is the j th path parameter $c_{i,j}$ constraint set, and $\mathcal{S}_{i,k} := [\underline{c}_{i,\rho+k}, \bar{c}_{i,\rho+k}] \subseteq \mathbb{Z}_{\geq 0}$ is the k th computation parameter constraint set.

The notation $[\cdot]$ denotes positive naturals up to \cdot , i.e., $\{0, 1, \dots, \cdot\}$. For a set \mathbb{X} , $\mathbb{X}_{\geq 0}$ then indicates it is positive, $\mathbb{X}_{>0}$ strictly positive.

The function φ_i is a *path function* specifying the path. These are stage-dependent mathematical functions the aerial robot tracks as it travels the coverage. The notation $[\underline{\cdot}, \bar{\cdot}]$ denotes the upper/lower bounds of a parameter \cdot , i.e.,

$$\underline{\cdot} \leq \cdot \leq \bar{\cdot}. \quad (1)$$

Definition II.3 (Path functions). $\varphi_i : \mathbb{R}^2 \times \mathbb{R}^\rho \rightarrow \mathbb{R}$, $\forall i \in \{1, 2, \dots\}$ are *path functions*, forming the path. They are a function of $\mathbf{p}(t)$ and path parameters $c_i^\rho(t)$ and are continuous and twice differentiable.

The change of stages happens in the proximity of given points termed *triggering points*, whereas the plan is complete at the occurrence of the *final point*.

Definition II.4 (Triggering and final points). The *triggering point* \mathbf{p}_{Γ_i} allows the transition between stages. The *final point* is the last triggering point \mathbf{p}_{Γ_i} relative to the last stage Γ_i .

The stage-dependent value $\varepsilon_i \in \mathbb{R}_{\geq 0}$ in Def. II.1 expresses the radius of an imaginary circle over \mathbf{p}_{Γ_i} .

Fig. 2 illustrates the concepts in Defs. II.1–4. $\varphi_0, \dots, \varphi_5$ are path functions. φ_0 and φ_4 are circles, while φ_1, φ_3 , and φ_5 are lines. They are relative to different stages Γ_1, \dots but Γ_0 , the starting stage, and are changed in the proximity of $\mathbf{p}_{\Gamma_0}, \dots$. It is possible to alter the paths $\varphi_1, \dots, \varphi_4$ with the parameters $c_{1,1}, \dots, c_{4,1}$; the gray area in the figure.

A convenient way of defining Γ is specifying a set of stages, a shift, and a final point. The set is termed *primitive stages* and iterated with the shift up to reaching the final point.

Definition II.5 (Primitive stages). Given the number of *primitive stages* $n \in \mathbb{Z}_{>0}$, a *shift* $\mathbf{d} \in \mathbb{R}^2$, and a final point \mathbf{p}_{Γ_f} , the stages $\Gamma_1, \Gamma_2, \dots, \Gamma_n$ are primitive if they form the remainder of the plan with \mathbf{d} up to \mathbf{p}_{Γ_f} .

In this case, the path functions have a constant distance e_j per each value in $[n]_{>0}$, i.e.,

$$\varphi_{(i-1)n+j}(\mathbf{p} + (i-1)\mathbf{d}, c_1^\rho) - \varphi_{in+j}(\mathbf{p} + i\mathbf{d}, c_1^\rho) = e_j, \quad (2)$$

holds $\forall i \in [l/n - 1]_{>0}, j \in [n]_{>0}$ assuming the total number of stages is known and is $l \in \mathbb{Z}_{>0}$. $e_j \in \mathbb{R}$ given a shift \mathbf{d} , initial point \mathbf{p} , and initial value of path parameters c_1^ρ .

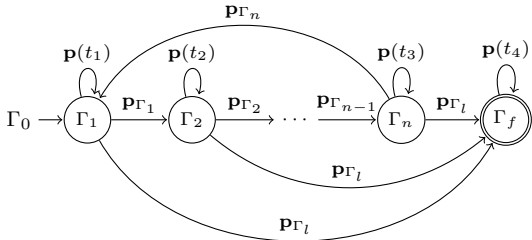


Fig. 3: Plan Γ with n primitive stages in Def II.5.

Fig. 3 illustrates the concepts in Def. II.5. A plan composed of n stages $\Gamma_1, \dots, \Gamma_n$ (containing primitive paths $\varphi_1, \dots, \varphi_n$) is reiterated with the shift \mathbf{d} . $t_1 < \dots < t_4$ are time instant $\in \mathbb{R}_{>0}$. Γ_f is the accepting stage, indicating the plan is completed, Γ_0 the initial stage where the aerial robot, e.g., awaits the starting command.

B. Energy-aware planning-scheduling problem

The problem of planning-scheduling is composed of two sub-problems. One is to form a static plan that visits each point in space, the other to re-plan and re-schedule the plan in-flight in an energy-aware way.

Problem II.1 (Coverage problem). Consider a finite set of vertices of a polygon $v := \{v_1, v_2, \dots\}$ where each vertex $v_i := (x_{v_i}, y_{v_i})$, $\forall i \in [|v|]_{>0}$ is a point w.r.t. \mathcal{O}_W . Let $\underline{r} \in \mathbb{R}_{\geq 0}$, the minimum turning radius, and $\mathbf{p}(t_0)$, the starting point at the time instant t_0 , be given. The *coverage problem* is the problem of finding a plan Γ that covers the polygon.

For a set \mathbb{X} , the notation $|\mathbb{X}|$ denotes the cardinality of \mathbb{X} .

Problem II.2 (Re-planning-scheduling problem). Consider an initial plan Γ in Def. II.1. The *re-planning-scheduling problem* is the problem of finding the optimal configuration of path and computations parameters $c_i(t)$, $\forall i \in \{1, 2, \dots\}$ under energy constraints and uncertainty at each time step t .

Here, c_i denotes a row vector with both the path and computations parameters in sequence, i.e., $c_i := [c_i^\rho \ c_i^\sigma]'$. The notation \cdot' denotes the transpose of \cdot .

III. ENERGY MODELS

The solution to Pb. II.2 requires accurate energy models, predicting the impact of changes to path and computations parameters on the battery at future time instants. To this end, Secs. III-A–C provide models for the motion and computations energies and battery.

A. Energy model for the motion

Let us return to the collected energy data and spectrum analysis in Fig. 1, illustrating the energy of a coverage plan Γ with four primitive path functions iterated with a shift. The data exhibit periodic behavior, an observation further backed by the power spectrum analysis. It indicates that to model the energy, three frequencies are adequate.

An intuitive way of modeling the energy data is thus a Fourier series of a given order $r \in \mathbb{Z}_{\geq 0}$ and period $T \in \mathbb{R}_{>0}$

$$h(t) = a_0/T + (2/T) \sum_{j=1}^r (a_j \cos \omega j t + b_j \sin \omega j t), \quad (3)$$

where $h : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}$ maps time to the instantaneous energy consumption, $\omega := 2\pi/T$ is the angular frequency, and $a, b \in \mathbb{R}$ the series coefficients.

The model in Equation (3) does not quantify the contribution of path and computations parameters c_i , where, e.g., different schedules result in different instantaneous energy. For this latter purpose, we use another model

$$\dot{\mathbf{q}}(t) = \mathbf{A}\mathbf{q}(t) + \mathbf{B}\mathbf{u}(t), \quad (4a)$$

$$y(t) = \mathbf{C}\mathbf{q}(t), \quad (4b)$$

where $y(t) \in \mathbb{R}$ is the instantaneous energy consumption. The state $\mathbf{q} \in \mathbb{R}^m$ with $m := 2r + 1$ contains energy coefficients

$$\mathbf{q}(t) = [\alpha_0(t) \ \alpha_1(t) \ \beta_1(t) \ \dots \ \alpha_r(t) \ \beta_r(t)]'. \quad (5)$$

The state transition matrix

$$\mathbf{A} = \begin{bmatrix} 0 & 0^{1 \times 2} & \dots & 0^{1 \times 2} \\ 0^{2 \times 1} & \mathbf{A}_1 & \dots & 0^{2 \times 2} \\ \vdots & \vdots & \ddots & \vdots \\ 0^{2 \times 1} & 0^{2 \times 2} & \dots & \mathbf{A}_r \end{bmatrix}, \quad \mathbf{A}_j := \begin{bmatrix} 0 & \omega j \\ -\omega j & 0 \end{bmatrix}, \quad (6)$$

where $\mathbf{A} \in \mathbb{R}^{m \times m}$ contains r sub-matrices \mathbf{A}_j and $0^{i \times j}$ is a zero matrix of i rows and j columns. In matrix \mathbf{A} , the top left entry is zero, the diagonal entries are $\mathbf{A}_1, \dots, \mathbf{A}_r$, the remaining entries are zeros.

The output matrix

$$\mathbf{C} = (1/T) \begin{bmatrix} 1 & \overbrace{1 \ 0 \ \dots \ 1 \ 0}^{2r} \end{bmatrix}, \quad (7)$$

where $\mathbf{C} \in \mathbb{R}^m$ (the first value in the first column is one, the pattern one–zero is then repeated $2r$ times).

Under favorable conditions, models in Eqs. (3–4) are equal.

Lemma III.1 (Signal, output equality). Given \mathbf{u} a zero vector, matrices \mathbf{A}, \mathbf{C} described by Eqs. (6–7), and the initial guess $\mathbf{q}(t_0) = \mathbf{q}_0$ at initial time instant t_0

$$\mathbf{q}_0 = [a_0 \ a_1/2 \ b_1/2 \ \dots \ a_r/2 \ b_r/2]'$$

h in Eq. (3) is equal to y in Eq. (4).

To define the nominal control and the output matrix, we exploit the effect of variation of path and computations parameters on the energy.

Lemma III.2 (Parameters, energy relation). Given $c_i(t)$ parameters at two following time instants $t \in \{t_j, t_{j+1}\} \subset \mathbb{R}_{\geq 0}$ s.t. $t_j < t_{j+1}$ for an arbitrary stage Γ_i , a change in parameters $c_i(t_j) \neq c_i(t_{j+1})$ results in different overall and instantaneous energies for path and computations parameters respectively.

Appendices A–B contain the proofs of Lemmas III.1–2.

Using the same notation from Lem. III.2, the nominal control in Eq. (4)

$$\mathbf{u}(t_{j+1}) := \hat{\mathbf{u}}(t_{j+1}) - \hat{\mathbf{u}}(t_j), \quad (8)$$

for all time instants. $\hat{\mathbf{u}}$ is then a scale transformation

$$\hat{\mathbf{u}}(t) := \text{diag}(\nu_i) c_i(t) + \tau_i, \quad (9)$$

where $\text{diag}(\cdot)$ is a diagonal matrix with items of a set \cdot on the diagonal and zeros elsewhere. $\nu_i := [\nu_{i,1} \ \cdots \ \nu_{i,n}]'$ and $\tau_i := [\tau_{i,1} \ \cdots \ \tau_{i,n}]'$ are scaling factors with $n := \rho + \sigma$ that transform parameters domain (see Def. II.2) to time and power domains.

Let us assume for ease of notation that the coverage time evolves linearly. Path parameters c_i^p can be transformed into a time measure with scaling factors

$$\nu_{i,j} = ((\bar{t} - \underline{t}) / (\bar{c}_{i,j} - \underline{c}_{i,j})) / \rho, \quad (10a)$$

$$\tau_{i,j} = (\underline{c}_{i,j}(\bar{t} - \underline{t}) / (\bar{c}_{i,j} - \underline{c}_{i,j}) + \underline{t}) / \rho, \quad (10b)$$

$\forall j \in [\rho]_{>0}$ where \bar{t}, \underline{t} are time measures needed to complete the coverage with configurations $\bar{c}_i^p, \underline{c}_i^p$.

Similarly to Eq. (10), computations parameters c_i^c can be transformed into an instantaneous energy measure with

$$\nu_{i,j} = (g(\bar{c}_{i,j}) - g(\underline{c}_{i,j})) / (\bar{c}_{i,j} - \underline{c}_{i,j}), \quad (11a)$$

$$\tau_{i,j} = \underline{c}_{i,j}(g(\bar{c}_{i,j}) - g(\underline{c}_{i,j})) / (\bar{c}_{i,j} - \underline{c}_{i,j}) + g(\underline{c}_{i,j}), \quad (11b)$$

$\forall j \in [\rho + 1, n]$. The function g is detailed in Sec. III-B and quantifies the power of the computing hardware.

The input matrix then includes the change in energy, i.e.,

$$B = \begin{bmatrix} 0^{1 \times \rho} & 1 & \cdots & 1 \\ 0^{1 \times \rho} & 0 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0^{1 \times \rho} & 0 & \cdots & 0 \end{bmatrix}, \quad (12)$$

where $B \in \mathbb{R}^{m \times n}$ contains zeros but in the first row where the first ρ columns are zeros and the remaining σ are ones.

B. Energy model for the computations

Models for heterogeneous computing hardware in the literature often rely on analytical expressions [42]–[45] or different techniques, including regressional analysis [37], [46], [47], aiding the selection of hardware- or software-specific parameters. This section summarizes an energy model from our early studies [37], [38] that relies on regressional analysis to quantify the computations energy of any configuration of computations c_i^c within the bounds (see Def. II.2).

The model compromises an automatic modeling and profiling tool [37] named `powprofiler` distributed [48] under

the open-source MIT license. It is segmented into two layers. In the *measurement layer*, the tool measures a discrete set of computations parameters and infers the energy of the remaining in the *predictive layer* via a piecewise linear regression.

Let us assume there is at least one measuring device, i.e., shunt or internal power resistor, multimeter, or amperemeter, quantifying the power drain of a specific component, e.g., CPU, GPU, memory, etc., or of the entire computing hardware.

Definition III.1 (Measurement layer). Given a measuring device, computations parameters, and initial and final time instants, the *measurement layer* is the function $\mathbf{g} : \mathbb{Z}_{>0} \times \mathbb{Z}^\sigma \times \mathcal{T} \rightarrow \mathbb{R}$ that returns an energy measure.

Here, the notation \mathcal{T} encloses all the time intervals from initial t_0 to final t_f , i.e., $\mathcal{T} := [t_0, t_f]$.

Definition III.2 (Predictive layer). Given a measuring device and computations parameters, the *predictive layer* is the function $g : \mathbb{Z}_{>0} \times \mathbb{Z}^\sigma \rightarrow \mathbb{R}$ that returns an energy measure.

The energy measures in Defs. III.1–2 can be either average or overall. Additionally, the tool supports the battery state of charge (SoC) detailed in Sec. III-C. The function g in Def. III.2 is contained in the computations scaling factors in Eq. (11), assuming the computations energy behaves linearly between c_i^c and \bar{c}_i^c , otherwise

$$g(c_i^c) = (\mathbf{g}(\lceil c_i^c \rceil, \mathcal{T}_1) - \mathbf{g}(\lfloor c_i^c \rfloor, \mathcal{T}_2)) / (c_i^c - \lfloor c_i^c \rfloor) + \mathbf{g}(\lfloor c_i^c \rfloor, \mathcal{T}_2), \quad (13)$$

where notation $\lceil c_i^c \rceil, \lfloor c_i^c \rfloor$ indicates two adjacent measurement layers, and $\mathcal{T}_1, \mathcal{T}_2$ are the corresponding two time intervals. The measuring device in both \mathbf{g} and g is implicit.

C. Battery model

The battery model predicts the battery SoC in the function of a given load at future time instants. There are multiple models in the literature [49] with varying complexity, accuracy, and ease of implementation ranging from accurate but costly physical models [50], [51], to abstract models [39]–[41], [52] that have compelling trade-offs in terms of the latter two.

We model a Li-ion battery of an aerial robot in-flight with an abstract “Rint” equivalent circuit model (ECM) in the literature [39]–[41].

Lemma III.3 (Battery SoC). Given the internal battery voltage $V \in \mathbb{R}$ measured in volts, resistance R_r in ohms, constant nominal capacity Q_c in amperes per hour, and a battery coefficient k_b , the *battery SoC* evolves

$$\dot{b}(y(t)) = -k_b \left(V - \sqrt{V^2 - 4R_r y(t)} \right) / (2R_r Q_c).$$

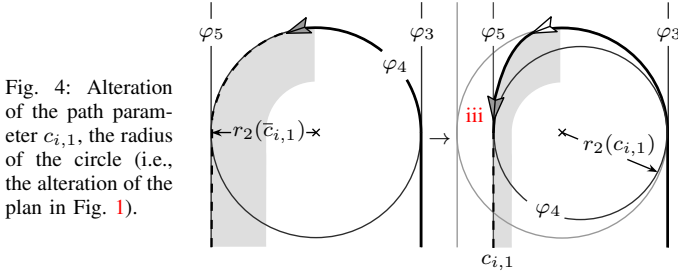
App. C contains the proof of Lem. III.3.

Eq. (4) states that the output y evolves in \mathbb{R} , conflicting with the findings in Lem. III.3.

Definition III.3 (Output constraint).

$$\mathcal{Y}(t) := \{y \mid y \in [0, b(y(t))Q_c V] \subseteq \mathbb{R}_{\geq 0}\},$$

is the *output constraint*, where $b(y(t))Q_c V$, the maximum instantaneous energy consumption measured in watts, is derived from Lem. III.3.



IV. PLANNING-SCHEDULING

The section solves Problems II.1–2. It provides a plan Γ and re-plans-schedules such plan energy-wise in Secs. IV-A–B.

A. Coverage

There are various approaches in the literature to solve CPP problems, such as Pb. II.1. Approaches that ensure the completeness of the cover are NP-hard [53] and use cellular decomposition, dividing the free-space into sub-regions to be easily covered [2], [3].

An intuitive way to solve the problem is with a back-and-forth motion, sweeping the space delimited by v we term \mathcal{Q}^v . Although abundant in both mobile ground-based [2], [54], [55] and aerial [56]–[59] robotics literature, the motion, called *boustrophedon motion* [2], is unsuitable for aerial robots broadly, especially for fixed-wing aerial robots. These robots have reduced maneuverability [60]–[63] and are generally unable to fly quick turns [64].

To address fixed wings and aerial robots generally, this section details a different motion with a wide turning radius. It is similar to another motion in the literature, the *Zamboni motion* [56], but additionally allows variable CPP at the very core of this work. The novel motion is termed *Zamboni-like motion* and is composed of four primitive paths (see Def. II.5): two lines φ_1, φ_2 and two circles φ_3, φ_4 (see Fig. 5).

Let us assume the vertices v_1, v_2, \dots are ordered from the top-left-most vertex in clockwise order, the aerial robot can overfly the edges formed by the vertices, and $v_x|_{v_y}$ indicates the edge formed by vertices v_x, v_y . Algorithm 1 details the procedure to generate the plan Γ that covers \mathcal{Q}^v per each discretized time step, i.e., $\mathcal{T} := \{t_0, t_0 + h, \dots, t_f\}$ for a given step $h \in \mathbb{R}_{>0}$. The algorithm assumes that the line parallel to $v_1|_{v_{|v|}}$ is always connected as it swipes \mathcal{Q}^v . Nonetheless, complex covering is possible by, e.g., dividing \mathcal{Q}^v into cells to be easily covered and subsequently covering each cell [2].

To implement the variable CPP, the radius r_2 of the second circle $\varphi_{|\Gamma|+4}$ on Line 13

$$r_2(c_{i,1}) := \sqrt{r^2 + c_{i,1}}, \quad (14)$$

and is expressed in the function of a path parameter $c_{i,1} \in (r^2 - r^2, 0]$ where $r \in \mathbb{R}_{>0}$ is a given ideal turning radius along with the minimum radius (see Pb. II.1). The center also changes

$$\varphi_{|\Gamma|+4} := (x - x_{\mathbf{p}_{|\Gamma|+3}} + r_2)^2 + (y - y_{\mathbf{p}_{|\Gamma|+3}})^2 - r_2^2, \quad (15)$$

where $(x_{\mathbf{p}}, y_{\mathbf{p}}) =: \mathbf{p}$ for any point \mathbf{p} . Fig. 4 illustrates the concept of $c_{i,1}$ altering the CPP. The radius of the first circle on Line 9 is then $r_1 := r + x_d/2$ (i.e., the radiuses of the two circles ensure that the primitive paths are shifted of \mathbf{d} in Def. II.5).

Algorithm 1 Zamboni-like motion for CPP

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1: for all  $i \in \mathcal{T}$  do
2:   if  $\mathbf{p}(i) = \mathbf{p}_{\Gamma_i}$  in Def. II.4 then return  $\Gamma$ 
3:   if  $\mathbf{p}(i) = \mathbf{p}_{\Gamma_j}$  then
4:      $j \leftarrow j + 1$ 
5:     if  $j \notin [n]_{>0}$  then
6:        $j \leftarrow 1$ 
7:        $\varphi_{|\Gamma|+1} \leftarrow$  line in Def. II.3 parallel to  $v_1|_{v_{|v|}}$  that inter-
         sects  $\mathbf{p}_{|\Gamma|}$ 
8:        $\mathbf{p}_{|\Gamma|+1} \leftarrow$  other intersection of  $\varphi_{|\Gamma|+1}$  and  $v$ 
9:        $\varphi_{|\Gamma|+2} \leftarrow$  circle whose left most point lays on  $\mathbf{p}_{|\Gamma|+1}$ 
10:       $\mathbf{p}_{|\Gamma|+2} \leftarrow$  other inter. of  $\varphi_{|\Gamma|+2}$  and  $v$ 
11:       $\varphi_{|\Gamma|+3} \leftarrow$  line par. to  $\varphi_{|\Gamma|+1}$  that inter.  $\mathbf{p}_{|\Gamma|+2}$ 
12:       $\mathbf{p}_{|\Gamma|+3} \leftarrow$  other inter. of  $\varphi_{|\Gamma|+3}$  and  $v$ 
13:       $\varphi_{|\Gamma|+4} \leftarrow$  circle in Eq. (15) whose right most point lays
        on  $\mathbf{p}_{|\Gamma|+3}$ 
14:       $\mathbf{p}_{|\Gamma|+4} \leftarrow$  other inter. of  $\varphi_{|\Gamma|+4}$  and  $v$ 
15:       $\Gamma \leftarrow \Gamma \cup \{\Gamma_{|\Gamma|+1}, \dots, \Gamma_{|\Gamma|+4}\}$  in Defs. II.1–2

```

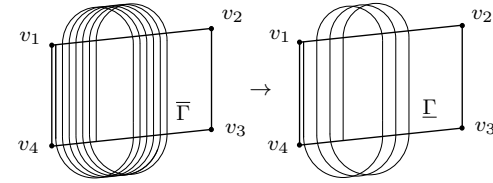


Fig. 5: Zamboni-like motion: (Γ) with four primitive paths (Lines 9–14 in Alg. 1) can be re-planned (Γ) with r_2 in Eq. (14).

Alg. 1 initializes j to minus one and builds the first four primitive functions $\varphi_1, \dots, \varphi_4$. The remaining Γ is built with the shift \mathbf{d} up to the given final point \mathbf{p}_{Γ_i} . The initial point is \mathbf{p}_{Γ_1} , placed s.t. the line φ_1 is at the same distance from an eventual previous line, e.g., $x_{\mathbf{p}_{\Gamma_1}} = x_{v_1} + x_d/2$ in Fig. 5.

B. Re-planning-scheduling

Past literature in planning-scheduling often relies on optimal control and optimization related approaches [18], [20], [21], [33]. We similarly derive an optimal control problem returning the trajectory of parameters $c_i(\mathcal{T})$ with $\mathcal{T} := [t_0, t_f]$ (see Def. III.1). Since the final time instant and the exact value of the state \mathbf{q} are not known, we use a technique in the literature named output model predictive control (MPC) that derives the configuration for a finite horizon on an estimated state $\hat{\mathbf{q}}$, i.e., $t_f := t_0 + N$ for a given $N \in \mathbb{R}_{>0}$.

An optimal control problem (OCP) that selects the highest configuration of c_i and respects the constraints, with $\mathbf{q}(t)$ and $c_i(t)$ the state and parameters trajectories

$$\max_{\mathbf{q}(t), c_i(t)} l_f(\mathbf{q}(t_f), t_f) + \int_{t_0}^{t_f} l(\mathbf{q}(t), c_i(t), t) dt, \quad (16a)$$

$$\text{s.t. } \dot{\mathbf{q}} = f(\mathbf{q}(t), c_i(t), t), \quad (16b)$$

$$c_{i,j}(t) \in \mathcal{C}_{i,j}, c_{i,\rho+k}(t) \in \mathcal{S}_{i,k} \forall j \in [\rho]_{>0}, k \in [\sigma]_{>0}, \quad (16c)$$

$$\mathbf{q}(t) \in \mathbb{R}^m, y(t) \in \mathcal{Y}(t), \quad (16d)$$

$$\mathbf{q}(t_0) = \hat{\mathbf{q}}_0 \text{ given (last estimated state), and} \quad (16e)$$

$$b(y(t_0)) = b_0 \text{ given,} \quad (16f)$$

where $l : \mathbb{R}^m \times \mathcal{C}_i \times \mathcal{S}_i \times \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}$ and $l_f : \mathbb{R}^m \times \mathbb{R}_{>0} \rightarrow \mathbb{R}$ given initial and final cost functions. Furthermore, Eq. (16b) is the differential periodic energy model in Eq. (4). Eq. (16c) are the parameters constraints sets in Def. II.2. Eq. (16d) is the state and output constraints in Def. III.3 that evolves

Algorithm 2 Coverage re-planning-scheduling

```

1: for all  $i \in \mathcal{T}$  do
16:  $\mathbf{q}(\mathcal{K} \setminus \{i + N\}), c_j(\mathcal{K}) \leftarrow \text{solve NLP } \arg \max_{\mathbf{q}(k), c_j(k)} l_f(\mathbf{q}(i + N), i + N) + \sum_{k \in \mathcal{K}} l_d(\mathbf{q}(k), c_j(k), k)$  in Eq. (16)
   on  $\mathcal{K} = \{i, i + h, \dots, i + N\}$ 
17:  $k \leftarrow i$ 
18: while  $b_d(y(k)) > 0$  do
19:   if  $k \in \mathcal{K}$  then
20:      $\mathbf{q}(k + h) \leftarrow \text{solve model in Eq. (4a)}$ 
21:      $b_d(y(k + h)) \leftarrow \text{solve model in Lem. III.3}$ 
22:      $k \leftarrow k + h$ 
23:    $t_b \leftarrow k - i$ 
24:    $t_s \leftarrow (\text{diag}(\nu_j^p) c_j^p(i) + \tau_j^p) \overbrace{[1 \ 1 \ \dots \ 1]}^p$ 
25:    $t_r \leftarrow (t_s / \bar{t})(\bar{t} - i)$ 
26:   if  $t_r < t_b$  then
27:      $c_j^p(i) \leftarrow \text{find } c_j^p \text{ with } t_c \in [0, t_b], \text{ otherwise take } \underline{c}_j^p$ 
28:    $\hat{\mathbf{q}}(i + h) \leftarrow \text{estimate } \mathbf{q} \text{ in Eq. (4a) with energy sensor } \Upsilon(i)$ 
29:    $\hat{y}(i + h) \leftarrow \text{derive } y \text{ from Eq. (4b) with est. state } \hat{\mathbf{q}}(i + h)$ 

```

the battery model in Lem. III.3. Eq. (16e) is the state guess estimated via state estimation (the very first estimate is given). Eq. (16f) is the initial battery SoC from, e.g., flight controller.

Line 16 in Alg. 2 contains a transformed version of the OCP in Eq. (16) into a nonlinear program (NLP) that can be easily solved with available NLP solvers [65]. Its solution leads to both trajectories of parameters and states for future N instants. Here, the sets \mathcal{K}, \mathcal{T} have possibly different steps h (not to be confused with the altitude), tuning the precision. The functions l_d, b_d are the discretized versions of Eq. (16a) and Lem. III.3, with, e.g., Runge-Kutta methods, Euler method, etc. [66].

Lines 17–23 estimate the time needed to completely drain the battery, exploiting the SoC already predicted previously on Line 16. The coverage is then replanned accordingly on Lines 24–27 using Lem. III.2 and scaling factors from Eq. (10). Lines 28–29 estimate the energy model's state with current energy sensor reading Υ , with, e.g., Kalman filter [67].

Alg. 2 implements Eq. (16) for the purpose of energy-aware re-planning-scheduling of Γ from Alg. 1, i.e., Lines 16–29 continue after Line 15 in Alg. 1.

V. RESULTS

Fig. 1 details the data of a physical flight in standard atmospheric conditions. Fig. 6 extends the flight with NVIDIA (R) Jetson Nano (TM) heterogeneous computing hardware aided by a flight simulation implemented in MATLAB (R). Upper-case roman numerals I, II indicate the plans are static (i.e., solely Alg. 1), lower-case i, ii exploit planning-scheduling in the letter. The computing hardware carries a camera as a peripheral and is evaluated independently of the aerial robot with the `powprofiler` (see Sec. III-B). The scheduler varies a computation parameter $c_{i,2}$ relative to the ground patterns detection rate from two to ten frames-per-second (FPS). The detection uses PedNet, a Convolutional Neural Network (CNN) [68], implemented through Robot Operating System (ROS) middleware [69] as well as the scheduler itself. The planner varies the path parameter $c_{i,1}$ in Eq. (14) between zero and -1000 (i.e., the planner-scheduler is the

concrete implementation of Algs. 1–2). The set of parameters is unaltered through the flight, i.e., $c_i := [c_{i,1} \ c_{i,2}]', \forall i$.

Fig. 6a illustrates the same plan Γ under different conditions. Flights I–i have a constant wind speed of five meters per second, a wind direction of zero degrees, and initial parameters $c_{i,1}, c_{i,2}$ values of zero and ten (i.e., full r_2 and detection). Flights II–ii (see added gray background for clarity) the same but a wind direction of 90 degrees and the initial parameters values of -1000 and two (i.e., minimum r_2 and detection).

Fig. 6b illustrates first the power ($\Upsilon(i)$ on Line 28 in Alg. 2), and then the energy model ($y(i)$ on Line 20). Flight i simulates a battery (green line, the battery behavior $b_0(i)$) drop at approximately one minute and a half and four minutes and a half. Planner-scheduler optimizes the path in the proximity of the drops to ensure that the flight is completed, whereas it maximizes the parameter $c_{i,2}$ when the battery is discharging, respecting the output constraint (Def. III.3). Flight ii simulates the opposite scenario. The lowest configuration of parameters and no battery defects. The path parameter increases as soon as the algorithm estimated enough data (two periods T) and the computation parameter decreases mapping the battery discharge rate. For both cases, scaling factors are derived empirically, the horizon N is set to six seconds similarly to relevant literature [70]–[73], order r is three (see Fig. 1) and the costs l_d, l_f are merely squared controls. The figure further details the energy model's estimate (see detail view for I–II) on an initial slice of the model ($\hat{y}(i)$), power ($\Upsilon(i)$), and period (T). The bottom detail of I illustrates the evolutions of the state \mathbf{q} in time, concluding that approximately two periods are sufficient to obtain a consistent state estimate.

Output MPC on Line 16 relies on a software framework for nonlinear optimization called CasADi [74]–[76], and the popular NLP solver IPOPT [77].

VI. CONCLUSIONS AND FUTURE DIRECTIONS

The letter provides a planning-scheduling approach for autonomous aerial robots powered by a limited power source, extending relevant past literature. It proposes a novel coverage motion for variable CPP robust to aerial robots constraints such as the turning radius of fixed wings. Energy modeling in the letter exploits collected empirical data of the fixed-wing aerial robot flying static CPP and further incorporates the energy of the computing hardware via the `powprofiler` tool. The approach comprises two algorithms: one derives a static coverage plan, whereas the other re-plans-schedules the plan on a finite horizon via MPC. It evolves the state of the energy model while optimizing battery usage and remedying possible defects. The plan compromise multiple stages, where at each the aerial robot flies a path and does some computations, allowing further extensibility in terms of constructs and approaches.

Indeed, we are currently extending the results to a standard flight controller. The guidance on the coverage, coverage with variable altitude, and distributed planning-scheduling merits alike further investigation, as well as the study of the implications of planning-scheduling on other energy-critical mobile robots. Here, our preliminary study led to possible savings [78], in line with relevant literature [20], [21].

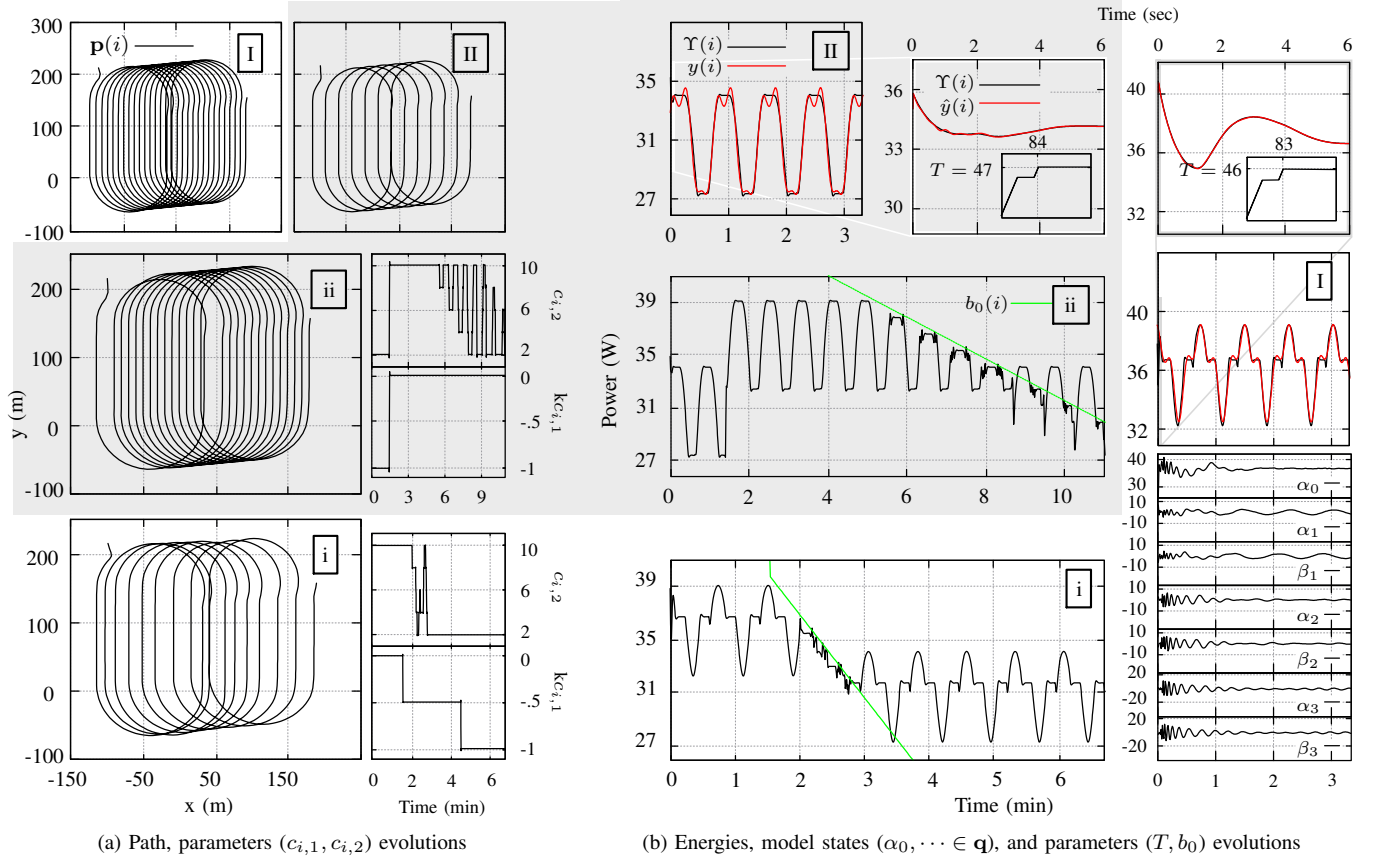


Fig. 6: CPP with novel Zamboni-like motion (I,II) and Planning-scheduling of CPP and ground patterns detections with PedNet CNN (i,ii) in terms of the path, energies, and plans-schedules under different conditions (I-i,II-ii), i.e., wind speed and direction, battery behavior, and parameters initial values.

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APPENDIX A: PROOF OF LEM. III.1

The proof justifies the items of A , C , and \mathbf{q}_0 in Lem. (III.1), s.t. the coefficients of the series a_0, \dots, b_r equal the coefficients α_0, \dots, β_r of the state \mathbf{q} .

Firstly, it is convenient to re-write Eq. (3) in complex form, with, e.g., $e^{it} = \cos t + i \sin t$. Given $t = \omega j t$, $\cos \omega j t = (e^{i\omega j t} + e^{-i\omega j t})/2$ and $\sin \omega j t = (e^{i\omega j t} - e^{-i\omega j t})/(2i)$ by substitution of $\sin \omega j t$ and $\cos \omega j t$ respectively [79]. Then

$$h(t) = a_0/T + (1/T) \sum_{j=1}^r e^{i\omega j t} (a_j - ib_j) + (1/T) \sum_{j=1}^r e^{-i\omega j t} (a_j + ib_j), \quad (17)$$

where i is this time the imaginary unit.

Secondly, the solution at t of Eq. (4) can be expressed $\mathbf{q} = e^{At} \mathbf{q}_0$ [80]. Here, a method to solve the matrix exponential e^{At} is the eigenvectors matrix decomposition method [81] by exploiting the similarity transformation $A = VDV^{-1}$. The power series definition of e^{At} implies $e^{At} = Ve^{Dt}V^{-1}$ [81].

Within this expression, we consider the non-singular matrix V , whose columns are eigenvectors of A , $V := [v_0 \ v_1^0 \ v_1^1 \ \dots \ v_r^0 \ v_r^1]$, and the diagonal matrix of eigenvalues, $D = \text{diag}(\lambda_0, \lambda_1^0, \lambda_1^1, \dots, \lambda_r^0, \lambda_r^1)$. V is built s.t. λ_0 is the eigenvalue associated with the first item of A . λ_j^0, λ_j^1 are the two eigenvalues associated with the block A_j . $Av_j = \lambda_j v_j, \forall j \in [m]_{>0}$, and so $AV = VD$.

The linear combination of the initial guess in Lem. III.2 and the generic solution of Eq. (4)

$$F\mathbf{q}(0) = \gamma_0 v_0 + \sum_{k=0}^1 \sum_{j=1}^r \gamma_j v_j^k, \quad (18a)$$

$$F\mathbf{q}(t) = \gamma_0 e^{\lambda_0 t} v_0 + \sum_{k=0}^1 \sum_{j=1}^r \gamma_j e^{\lambda_j^k t} v_j^k, \quad (18b)$$

where $F := [1 \ \dots \ 1]$ is simply a properly sized vector of ones.

The second expression in Eq. (18) is the linear combination of all the coefficients of the state at time t . By dividing the expression with the period

$$F\mathbf{q}(t)/T = \gamma_0 e^{\lambda_0 t} v_0/T + (1/T) \sum_{j=1}^r \gamma_j e^{\lambda_j^0 t} v_j^0 + (1/T) \sum_{j=1}^r \gamma_j e^{\lambda_j^1 t} v_j^1. \quad (19)$$

Finally, we prove that the eigenvalues $\lambda_0, \lambda_1^0, \lambda_1^1, \dots$ and eigenvectors in v_0, v_1^0, v_1^1, \dots are such that Eq. (19) is equivalent to Eq. (17).

The matrix A is a block diagonal matrix, s.t. its determinant is the multiplication of the determinants of its blocks $\det(A) = \det(0) \times \det(A_1) \times \dots \times \det(A_r)$.

The first terms of the Eq. (17) and (19) match. The eigenvalue from $\det(0) = 0$ is $\lambda_0 = 0$. The corresponding eigenvector can be chosen arbitrarily $(0 - \lambda_0)v_0 = [0 \ \dots \ 0] \ \forall v_0$, e.g., $v_0 = [1 \ 0 \ \dots \ 0]$. We find the value γ_0 of the vector γ so that the terms are equal, e.g., $\gamma_0 = [a_0 \ 0 \ \dots \ 0]$.

All the terms in the sum of both the Eq. (17) and (19) match. For the first block A_1 , the eigenvalues are found by $\det(A_1 - \lambda I) = 0$. The polynomial $\lambda^2 + \omega^2$, gives two complex roots, the two eigenvalues $\lambda_1^0 = i\omega$ and $\lambda_1^1 = -i\omega$. The eigenvector associated with the eigenvalue λ_1^0 is $v_1^0 = [0 \ -i \ 1 \ 0 \ \dots \ 0]^T$. The eigenvector associated with the eigenvalue λ_1^1 is $v_1^1 = [0 \ i \ 1 \ 0 \ \dots \ 0]^T$. Again, we find the values γ_1 of the vector γ such that the equivalences

$$\begin{cases} e^{i\omega t} (a_1 - ib_1) &= \gamma_1 e^{i\omega t} v_1^0 \\ e^{-i\omega t} (a_1 + ib_1) &= \gamma_1 e^{i\omega t} v_1^1 \end{cases}, \quad (20)$$

hold, e.g., $\gamma_1 = [b_1 \quad a_1]$.

The proof for the remaining $r - 1$ blocks is equivalent.

The initial guess is constructed s.t. the sum of the coefficients is the same in both Eq. (19) and (17). In the output matrix, the frequency $1/T$ accounts for the period. At time instant zero, the coefficients b_j are not present, and the coefficients a_j are doubled for each $j = [r]_{>0}$ (thus we multiply by one-half the corresponding coefficients in \mathbf{q}_0). To match the outputs $h(t) = y(t)$, or equivalently $F\mathbf{q}(t)/T = C\mathbf{q}(t)$, $C = (1/T) [1 \quad 1 \quad 0 \quad \cdots \quad 1 \quad 0]$. Eq. (19) and Eq. (17) are thus equal. Eq. (17) is merely the complex form of Eq. (3).

APPENDIX B: PROOF OF LEM. III.2

A change in computations parameters in Lem. III.2 results in different schedules on the computing hardware, which we assumed in Sec. I affects the instantaneous energy, i.e., computations are energy expensive computational tasks.

A change in the path parameters in Lem. III.2 alters the flight time, and consequently, the energy. The proof quantifies this time: consider the plan $\bar{\Gamma}$ in Fig. 5. It is composed of four primitive paths and the highest configuration of path parameter $c_{i,1}$. Let assume that the time to travel $\varphi_4(\bar{c}_{i,1})$ is $t_3 \in \mathbb{R}_{>0}$, φ_1, φ_3 , the two lines, is $2t_1 \in \mathbb{R}_{>0}$, and φ_2 is $t_2 \in \mathbb{R}_{>0}$. Further, assume that v is covered merely by the set of primitive paths in Fig. 5. The coverage time is $t_{\bar{\Gamma}} = 7(2t_1 + t_2 + t_3) + t_1$.

Conversely, assume the time needed to travel $\varphi_4(\underline{c}_{i,1})$ is $t_4 \in \mathbb{R}_{>0}$. Then $t_{\underline{\Gamma}} = 3(2t_1 + t_2 + t_4) + t_1$, and $t_{\bar{\Gamma}} > t_{\underline{\Gamma}}$ even under the unrealistic assumption $t_3 \cong t_4$.

APPENDIX C: PROOF OF LEM. III.3

The proof justifies the expression in Lem. III.3.

The battery SoC changes according to [82], [83], i.e.,

$$\dot{b}(y(t)) = -I(y(t))/Q_c, \quad (21)$$

where $I(y(t)) \in \mathbb{R}$ is the internal current measured in amperes, $y(t) \in \mathbb{R}_{\geq 0}$ the power drain, and $Q_c \in \mathbb{R}$ the battery constant nominal capacity in Lem. III.3. The ‘‘Rint’’ circuit models the battery as a perfect voltage source connected with a resistor $R_r \in \mathbb{R}$ in Lem. III.3, representing the battery resistance. The voltage on the extremes of ECM respects $V_e = V - R_r I$, where $V, V_e \in \mathbb{R}$ are the internal and external battery voltages measured in volts. The former can be retrieved from the battery data sheet [40] and depends on SoC [82].

If the voltage of the power drain is stable, Kirchhoff’s circuit laws lead to $V_s I_l = V_e I$, where I_l is the current required by the load measured in amperes. Combining $V_e, V_s I_l$ results in the quadratic expression $R_r I^2 - V I + V_s I_l = 0$. Solving the expression utilizing the negative solution (when I_l is zero, I should also be zero)

$$I(y) = (V - \sqrt{V^2 - 4R_r y(t)})/(2R_r), \quad (22)$$

as in Lem. III.3.