

## 8 L10/L11: Introduction to Rigid Body Kinetics

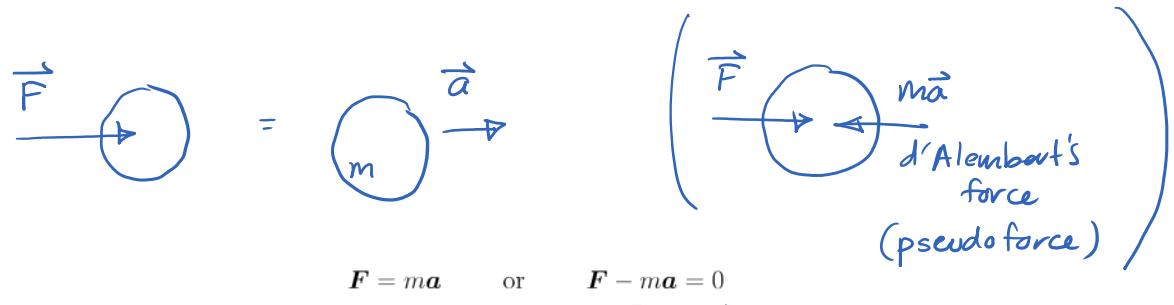
Readings

### 8.1 Objective

To apply Newton's Second Law to **planar** rigid bodies. This means that we need to account for the fact that the body being considered is NOT a point mass. We will use the concepts of Centre of Mass and Inertia, established in the previous lecture.

### 8.2 Review – Newton's Second Law

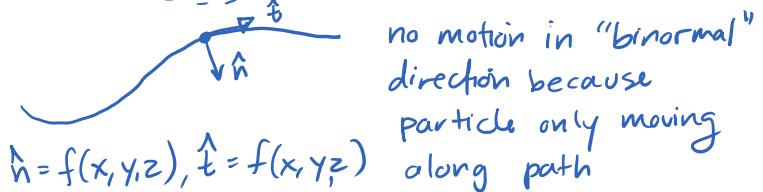
A particle acted on by an unbalanced force,  $\vec{F}$ , experiences an acceleration,  $\vec{a}$ , in the same direction as the force, and a magnitude that is directly proportional to the force.



$\vec{F}$  is a vector that represents the resultant of all forces acting on the body.

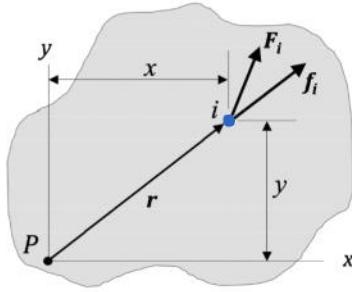
Thus, depending on the coordinate system selected, for a particle we would have the following set of equations:

Cartesian	Normal/Tangential	Polar/Cylindrical
$\sum F_x = ma_x$	$\sum F_n = ma_n$	$\sum F_r = ma_r$
$\sum F_y = ma_y$	$\sum F_t = ma_t$	$\sum F_\theta = ma_\theta$
$\sum F_z = ma_z$	$\sum F_b = 0$	$\sum F_z = ma_z$



### 8.3 Equations of Motion for a Planar Rigid Body

Consider what this means for a planar body – which is a collection of particles.



For each particle on the body we have:

$$\text{particle 1 : } \mathbf{F}_1 + \mathbf{f}_1 = m\mathbf{a}_1$$

$$\text{particle 2 : } \mathbf{F}_2 + \mathbf{f}_2 = m\mathbf{a}_2$$

⋮

$$\frac{\mathbf{F}_n + \mathbf{f}_n = m\mathbf{a}_n}{\sum_i \mathbf{F}_{\text{external}} + \sum_i \mathbf{f}_{\text{internal}} = \sum m_i \mathbf{a}_i}$$

Looking at each term:



$\sum_i \mathbf{f}_{\text{internal}}$  Rigid body assumption - otherwise the body will explode

$$\underline{\underline{= 0}}$$

$\sum m_i \mathbf{a}_i$  Centre of mass equation:

$$\underline{\underline{= m \bar{\mathbf{a}}_G}}$$

$$\mathbf{r}_G = \frac{\sum_i \mathbf{r}_i / m_i}{m}$$

$$\Rightarrow \underline{\underline{m \mathbf{r}_G = \sum_i \mathbf{r}_i / m_i}}$$

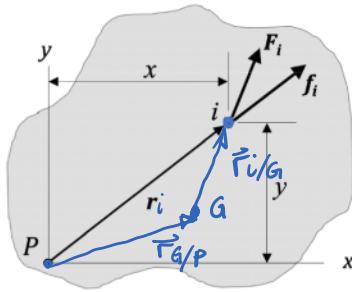
Differentiate twice:

$$\Rightarrow m \mathbf{a}_G = \sum_i \mathbf{a}_i / m_i$$

Putting this together we have Newton's second law as applied to a rigid body. The important thing to note is where the acceleration is measured – AT THE CENTRE OF MASS.

$$\boxed{\sum \underline{F_{ext}} = ma_G} @ COG \text{ only}$$

Now, let's look at the moment balance for this body. If we take moments about point P that is on the body:



$$\sum M_P = \sum (\underline{r_i} \times \underline{F_{ext}}) = \sum (\underline{r_i} \times m_i \underline{a_i})$$

Let us reference this equation in terms of G, the centre of mass of the body.

$$\underline{r_i} = \underline{r_{G/P}} + \underline{r_{i/G}} \Rightarrow \underline{r_{i/G}} = \underline{r_i} - \underline{r_G}$$

multi. by  $m_i$ , take sum

And we know from kinematics that at any point  $\underline{a_i}$ ,

$$\rightarrow \underline{a_i} = \underline{a_G} + \alpha \times \underline{r_{i/G}} - \omega^2 \underline{r_{i/G}}$$

$$\sum_i m_i \underline{r_{i/G}} = \sum_i m_i (\underline{r_i} - \underline{r_G}) = 0$$

If we plug these last two equations into the RHS of our moment equation and simplify using the fact that,

$$\begin{aligned} \underline{r_G} &= \underline{r_{G/P}} \\ P \text{ is the origin} \\ \underline{r_i} &= \underline{r_{i/P}} \end{aligned}$$

$$\sum_i m_i \underline{r_{i/G}} = \sum_i m_i (\underline{r_i} - \underline{r_G}) = \sum_i m_i \underline{r_i} - m \underline{r_G} = 0$$

*eqn' of centroid*

$$\underline{r_G} = \frac{\sum m_i \underline{r_i}}{m}$$

$$m \underline{r_G} = \sum m_i \underline{r_i}$$

$$\sum m_i \underline{r_i} - m \underline{r_G} = 0$$

we will get:

$$\begin{aligned} \sum M_P &= \sum_i m_i (\vec{r}_{G/P} + \vec{r}_{i/G}) \times (\vec{a}_G + \vec{\alpha} \times \vec{r}_{i/G} - \omega^2 \vec{r}_{i/G}) \\ &= \sum_i m_i [\vec{r}_{G/P} \times \vec{a}_G + \vec{r}_{G/P} \times (\vec{\alpha} \times \vec{r}_{i/G} - \omega^2 \vec{r}_{i/G}) + \vec{r}_{i/G} \times \vec{a}_G + \vec{r}_{i/G} \times (\vec{\alpha} \times \vec{r}_{i/G} - \omega^2 \vec{r}_{i/G})] \\ \boxed{\sum M_P = mr_{G/P} \times \vec{a}_G + \sum_i m_i r_{i/G}^2 \vec{\alpha}} \end{aligned}$$

$$\begin{aligned} \sum m_i \vec{r}_{i/G} &= 0 \\ \sum \vec{r}_{i/G} m_i \times \vec{\alpha}_G &= 0 \\ \vec{r}_{i/G} \times \vec{r}_{i/G} &= 0 \end{aligned}$$

The first part looks familiar – what we would expect if we simply multiplied our translational equation of motion by the torque arm around point  $P$ :  $\vec{r}_{G/P} \times m\vec{a}_G$

The second part of this equation is the effect of the rotation of the entire rigid body – this is the part that relates to rotational mass – INERTIA

$$I_G = \sum_i m_i r_{i/G}^2$$

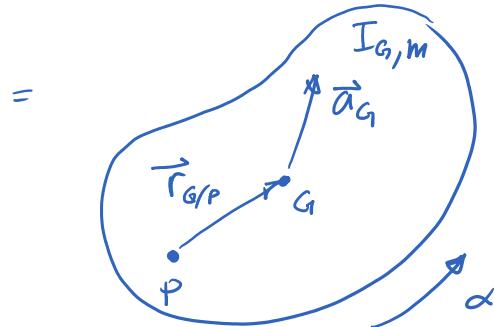
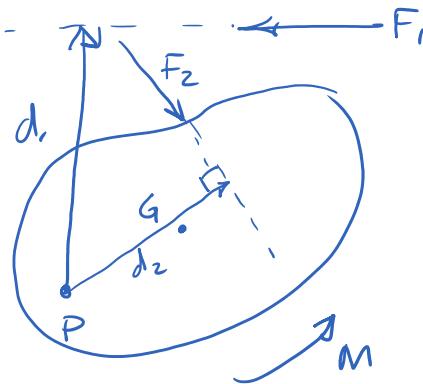
$$\vec{a}_G \underset{\text{any point on rigid body}}{\underset{\approx}{\sim}} I_G \vec{\alpha} @ COG.$$

So finally we have an equation for the effect of moments applied to a body, about a point  $P$ :

$$\boxed{\sum M_P = mr_{G/P} \times \vec{a}_G + I_G \vec{\alpha}}$$

$$\sum M_P = I_G \vec{\alpha}$$

any point on rigid body



$$\sum M_P: \underbrace{\vec{M}}_{F_1 d_1} + \underbrace{\vec{d}_1 \times \vec{F}_1}_{-F_2 d_2} + \underbrace{\vec{d}_2 \times \vec{F}_2}_{= m(\vec{r}_{G/P} \times \vec{a}_G) + I_G \vec{\alpha}}$$

### 8.4 Further Results

*so far...*

$$\begin{aligned} \sum \mathbf{F} &= m\mathbf{a}_G \\ * \sum M_P &= mr_{G/P} \times \underline{\mathbf{a}_G} + \underline{I_G \alpha} \end{aligned}$$

moment about P,  
but with terms  
wrt G

Applying our equation to measure the effect of Moments about at the Centre of Mass, G: ( $\mathbf{r}_{G/G} = 0$ )

*if P = G*

$$\boxed{\sum M_G = I_G \alpha}$$

For other points on the rigid body, we can also rewrite:

$$\mathbf{a}_G = \mathbf{a}_P - \omega^2 \mathbf{r}_{G/P} + \boldsymbol{\alpha} \times \mathbf{r}_{G/P}$$

If we substitute this into our equation for  $\sum M_P$ , we have:

$$\begin{aligned} \sum M_P &= mr_{G/P} \times (\mathbf{a}_P - \omega^2 \mathbf{r}_{G/P} + \boldsymbol{\alpha} \times \mathbf{r}_{G/P}) + I_G \alpha \\ &= mr_{G/P} \times \mathbf{a}_P - mr_{G/P}^2 (\mathbf{r}_{G/P} \times \mathbf{r}_{G/P}) + mr_{G/P} \times (\boldsymbol{\alpha} \times \mathbf{r}_{G/P}) + I_G \alpha \\ &= mr_{G/P} \times \mathbf{a}_P + mr_{G/P}^2 \boldsymbol{\alpha} + I_G \alpha \end{aligned}$$

\*  $\boxed{\sum M_P = mr_{G/P} \times \mathbf{a}_P + I_P \alpha}$

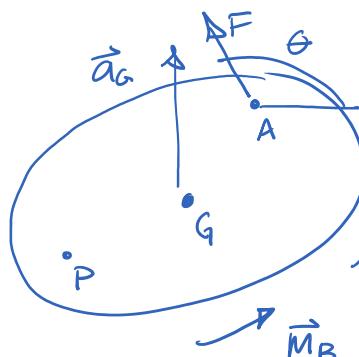
moment about P, expressed in terms of  $I_P$  and  $\boldsymbol{\alpha}_P$

$I_G + m r_{G/P}^2 = I_P$   
parallel axes

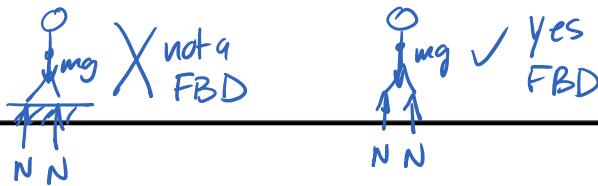
Finally, if point P is PINNED (fixed to ground but body is allowed to ROTATE around P):

$$\rightarrow \overline{\alpha}_P = 0 \quad (\text{pinned})$$

$$\boxed{\sum M_P = I_P \alpha} \quad \text{pinned @ P}$$



$$\begin{aligned} * \sum \mathbf{F} &= m\mathbf{a}_G \quad \text{always @ COG} \\ \sum F_x: F \cos \theta &= m a_{Gx} \\ \sum F_y: F \sin \theta &= m a_{Gy} \\ * \sum M_G: \vec{M}_B + \vec{r}_{A/G} \times \vec{F} &= I_G \vec{\alpha} \\ * \sum M_P: \vec{M}_B + \vec{r}_{A/P} \times \vec{F} &= I_P \vec{\alpha} + m \vec{r}_{G/P} \times \vec{\alpha}_G \\ \text{OR} &= I_P \vec{\alpha} + m \vec{r}_{G/P} \times \vec{\alpha}_P \end{aligned}$$



## 8.5 Method

FBD

1. Draw the free body diagram for each separate body thinking

2. Write Equations of Motion

- $\sum \mathbf{F} = m\mathbf{a}$  (for planar, two equations - in plane - such as  $\hat{i}, \hat{j}$ )

- $\sum M_G = I_G \alpha$  (for planar, one equation - out of the plane  $\hat{k}$  coordinate)  
(can use a different moment equation if appropriate - i.e. for pinned rotation)

$$\sum M_P = \boxed{\quad}$$

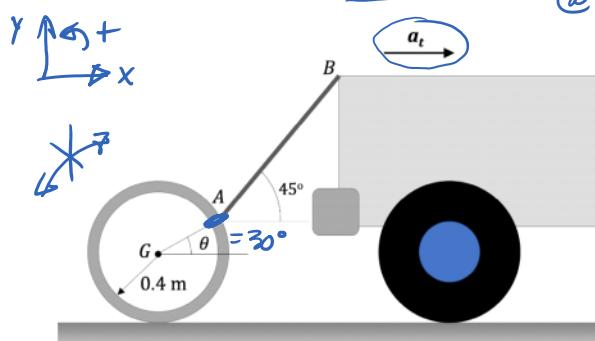
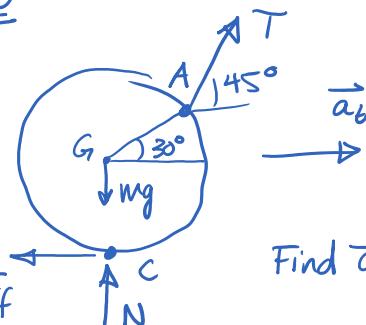
3. Apply KINEMATIC CONSTRAINTS thinking

4. Solve

## 8.5.1 Example 1

The pipe has a mass of  $800 \text{ kg}$  and is being towed behind a truck. If the angle  $\theta = 30^\circ$ , determine the acceleration of the truck and the tension in cable  $AB$ . The coefficient of kinetic friction between the pipe and the ground is  $\mu_k = 0.1$ .

@ steady state, dragging (not rolling)

FBDFind  $\vec{a}_t$  and  $\vec{T}$ EOM

$$\sum F_x: T \cos 45^\circ - F_f = m a_{Gx} \quad \text{CoG} \quad \textcircled{1}$$

$$\sum F_y: T \cos 45^\circ + N - mg = m a_{Gy} = 0 \quad \textcircled{2}$$

$$\sum M_G: \vec{r}_{A/G} \times \vec{T} - \vec{r}_{C/G} \times \vec{F}_f = I_G \ddot{\alpha} = 0$$

$$\vec{r}_{A/G} = 0.4 \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right)$$

$$\vec{r}_{C/G} = 0.4 (-\hat{j})$$

$$\vec{F}_f = F_f (-\hat{i})$$

$$\vec{T} = T \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right)$$

(Example continued)

$$\sum M_G: 0.4T\left(\frac{\sqrt{3}}{2}\hat{i} + \frac{1}{2}\hat{j}\right) \times \left(\frac{1}{12}\hat{i} + \frac{1}{12}\hat{j}\right) + (-0.4\hat{j}) \times (-F_f\hat{i}) = 0$$

$$\Rightarrow 0.4T\left(\frac{\sqrt{3}}{2\sqrt{2}}\hat{k} - \frac{1}{2\sqrt{2}}\hat{k}\right) - 0.4F_f\hat{k} = 0 \quad ③$$

$$F_f = \mu_k N$$

$$② \Rightarrow N = mg - \frac{T}{\sqrt{2}}$$

$$F_f = \mu \left( mg - \frac{T}{\sqrt{2}} \right)$$

$$②+③ \Rightarrow 0.4\left(\frac{\sqrt{3}}{2\sqrt{2}}\hat{i} - \frac{1}{2\sqrt{2}}\hat{j}\right) - 0.4\mu \underbrace{\left(mg - \frac{T}{\sqrt{2}}\right)}_{F_f} = 0$$

$$\Rightarrow T = 2382 \text{ N (mag.)}$$

$$\boxed{\vec{T} = 2382 \left(\frac{1}{12}\hat{i} + \frac{1}{12}\hat{j}\right) \text{ N}}$$

$$① \Rightarrow a_{Gx} = a_t = \frac{T}{\frac{m}{12}} - F_f$$

$$② \Rightarrow F_f = \mu \left( mg - \frac{T}{\sqrt{2}} \right) = 616 \text{ N}$$

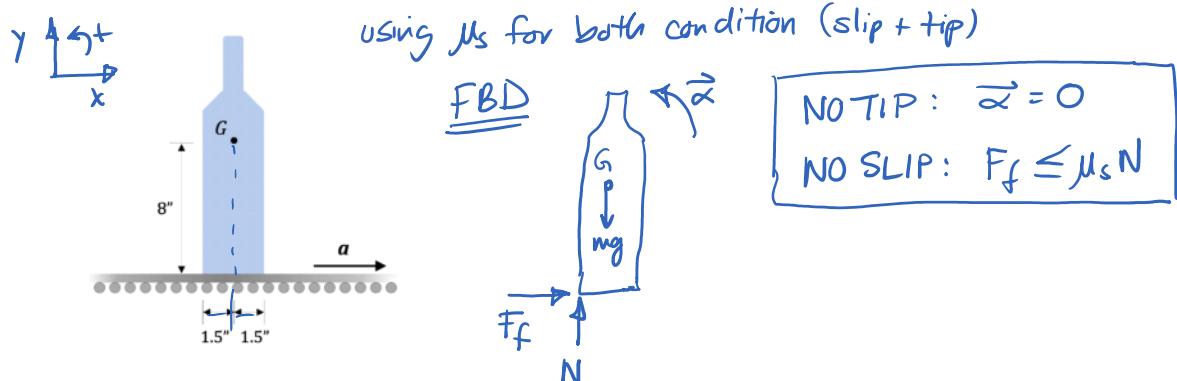
$$\boxed{\vec{F}_f = -616\hat{i} \text{ N}}$$

$$a_{Gx} = 1.33 \text{ m/s}^2$$

$$\boxed{\vec{a}_t = 1.33\hat{i} \text{ m/s}^2}$$

### 8.5.2 Example 2

The  $2 \text{ lb}$  bottle rests on a conveyor. If the coefficient of static friction is  $\mu_s = 0.2$  determine the largest acceleration the conveyor can have without causing the bottle to slip or tip.



$$\begin{aligned} \text{NOT TIP: } \vec{\alpha} &= 0 \\ \text{NO SLIP: } F_f &\leq \mu_s N \end{aligned}$$

EOM

$$\begin{aligned} \sum F_x: F_f &= m a_{Gx} \\ \sum F_y: N - mg &= m a_{Gy} = 0 \Rightarrow N = mg \\ \sum M_G: -8\uparrow \times F_f(1) + (-1.5\downarrow) \times N(\uparrow) &= I_G \vec{\alpha} = 0 \end{aligned}$$

SLIPPING:  $F_f \leq \mu_s mg$

$$F_f \leq \underline{0.2 mg}$$

will TIP  
before it SLIPS  
→ use lower  $F_f$   
to find  $\vec{\alpha}$

TIPPING:  $8F_f - 1.5N = 0$

$$\Rightarrow F_f = \frac{1.5}{8} N = \underline{0.19 mg} \quad \leftarrow \text{can't exceed}$$

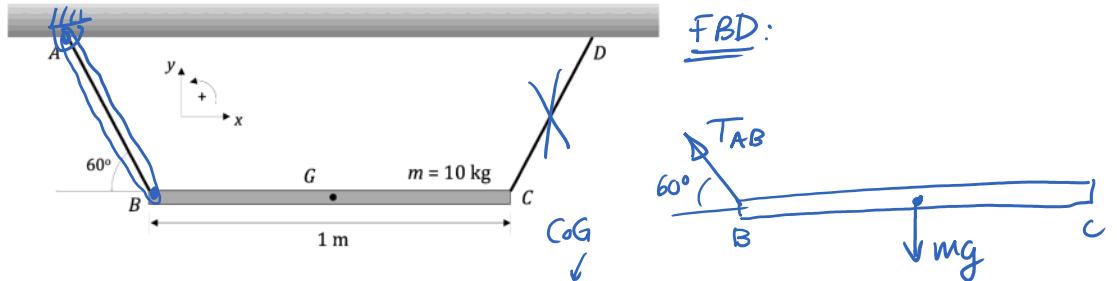
$$\sum F_x \Rightarrow F_f = m a_{Gx} \leq 0.19 mg$$

$$\Rightarrow a_{Gx} \leq 6.04 \text{ ft/s}^2$$

$$\boxed{\vec{a}_{max} = 6.04 \uparrow \text{ ft/s}^2}$$

## 8.5.3 Example 3

Bar  $CD$  is supported by two cables  $AB$  and  $CD$ . Cable  $CD$  suddenly breaks. Find the angular acceleration of the bar, and the tension in the cable  $AB$  immediately after  $CD$  breaks. The mass of the bar is  $10 \text{ kg}$  and is uniformly distributed over the length of  $1 \text{ m}$ .



$$\underline{\underline{\text{EOM:}}} \quad \sum F_x: -T_{AB} \cos 60^\circ = m \alpha_x$$

$$\sum F_y: T_{AB} \sin 60^\circ - mg = m \alpha_y$$

$$\sum M_G: \left(-\frac{1}{2}m\vec{u}\right) \times T_{AB} (-\cos 60^\circ \hat{i} + \sin 60^\circ \hat{j}) = I_G \vec{\alpha}$$

$$\Rightarrow -\frac{T_{AB}}{2} \sin 60^\circ \hat{k} = I_G \alpha \hat{k} \quad (\text{assume } \vec{\alpha} = \alpha \hat{k})$$

Unknowns:  $\alpha_{gx}, \alpha_{gy}, \alpha, T_{AB}$  [4]

eqns: 3

$\Rightarrow$  NEED ANOTHER EQN

KINEMATIC CONSTRAINT

Taut (tight) cable acts like a rigid body

$$\vec{\alpha}_B = \vec{\alpha}_A + \vec{\alpha}_{AB} \times \vec{\Gamma}_{B/A} - \omega_{AB} \vec{\Gamma}_{B/A} \quad (\text{starts from rest})$$

$$= \alpha_{AB} \hat{k} \times \vec{\Gamma}_{B/A} \left( \frac{1}{2} \hat{i} - \frac{\sqrt{3}}{2} \hat{j} \right)$$

$$= \alpha_{AB} \vec{\Gamma}_{B/A} \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right)$$

$$\alpha_B = |\vec{\alpha}_B| \quad \text{unit vector dir. of } \vec{\alpha}_B$$



$$\vec{\alpha}_{AB} = \alpha_{AB} \hat{k}$$

(Example continued)

ANOTHER EQN USING  $\vec{a}_B$

$$\vec{a}_G = \vec{a}_B + \vec{\alpha}_{BC} \times \vec{r}_{G/B} - g_{BC} \vec{r}_{G/B}$$

(starts from rect)

$$= a_B \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right) + \alpha_{BC} \hat{k} \times \left( \frac{1}{2} \hat{i} \right)$$

$$= a_B \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right) + \frac{\alpha_{BC}}{2} \hat{j} = a_{Gx} \hat{i} + a_{Gy} \hat{j}$$

Two eqns ( $\hat{i}, \hat{j}$ )  
add one unknown ( $a_B$ )

$$\Rightarrow \hat{i}: a_{Gx} = a_B \frac{\sqrt{3}}{2} \quad \textcircled{4}$$

$$\hat{j}: a_{Gy} = \frac{a_B}{2} + \frac{\alpha}{2} \quad \textcircled{5}$$

5 equations, 5 unknowns ( $a_{Gx}, a_{Gy}, \alpha, T_{AB}, a_B$ )

### SOLVE

$$+ \textcircled{4} \Rightarrow -T_{AB} \cdot \frac{1}{2} = m a_B \frac{\sqrt{3}}{2} \Rightarrow T_{AB} = -m a_B \frac{\sqrt{3}}{2}$$

$$+ \textcircled{5} \Rightarrow -mg + T_{AB} \frac{\sqrt{3}}{2} = m \left( \frac{a_B}{2} + \frac{\alpha}{2} \right)$$

$$\text{sub in } T_{AB} \Rightarrow -mg + (-m a_B \frac{\sqrt{3}}{2}) \frac{\sqrt{3}}{2} = m \left( \frac{a_B}{2} + \frac{\alpha}{2} \right)$$

$$-g - 2a_B = \frac{\alpha}{2} \quad \textcircled{6}$$

$$\textcircled{3} \Rightarrow -T_{AB} \frac{\sqrt{3}}{4} = I_G \alpha \quad I_G = \frac{1}{12} m l^2 = \frac{1}{12} m (1)^2 = \frac{m}{12}$$

$$\text{sub in } T_{AB} \Rightarrow -\left(-m a_B \frac{\sqrt{3}}{2}\right) \frac{\sqrt{3}}{4} = \frac{m}{12} \alpha \Rightarrow a_B = \frac{\alpha}{9}$$

$$\textcircled{6} \Rightarrow -g - 2\left(\frac{\alpha}{9}\right) = \frac{\alpha}{2} \Rightarrow \alpha = -\frac{18}{13}g = -\frac{180}{13} \text{ rad/s}^2 \Rightarrow \boxed{\alpha = -\frac{180}{13} \text{ rad/s}^2 \hat{k}}$$

$$a_B = \frac{\alpha}{9} = -\frac{180}{13} \frac{1}{9} = -\frac{20}{13} \text{ m/s}^2, \vec{a}_B = -\frac{20}{13} \left( \frac{\sqrt{3}}{2} \hat{i} + \frac{1}{2} \hat{j} \right) \text{ m/s}^2$$

$$\therefore T_{AB} = -m a_B \sqrt{3} = -10 \cdot \frac{20}{13} \left( \frac{-20}{13} \text{ m/s}^2 \right) \sqrt{3} = \frac{200 \sqrt{3}}{13} \text{ N}$$

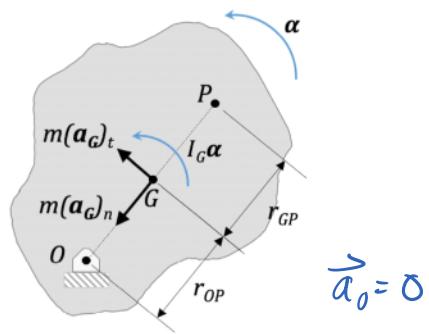
UBC  $\boxed{T_{AB} = \frac{200 \sqrt{3}}{13} \left( -\frac{1}{2} \hat{i} + \frac{\sqrt{3}}{2} \hat{j} \right) \text{ N}}$

## 8.6 Rotation About a Fixed Axis www.menti.com 102711

If a body is rotating about a fixed point (**pinned**) at O, then we can use this **kinematic constraint** to help solve the problem.

The equations of motion for any body are:

$$\begin{aligned}\sum \mathbf{F} &= m\mathbf{a}_G \\ \sum \mathbf{M}_G &= I_G \boldsymbol{\alpha}\end{aligned}$$



However, for this particular case we can use kinematics to write  $\mathbf{a}_G$  in terms of vectors parallel and perpendicular to the line between the pin and the centre of mass, OG:

$$\mathbf{a}_G = \underline{\boldsymbol{\alpha}} \times \mathbf{r}_{G/O} - \underline{\omega^2} \mathbf{r}_{G/O}$$

Thus:

$$\sum \mathbf{F} = m\underline{\boldsymbol{\alpha}} \times \mathbf{r}_{G/O} - m\underline{\omega^2} \mathbf{r}_{G/O}$$

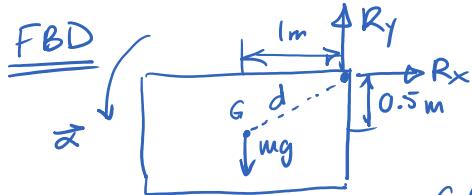
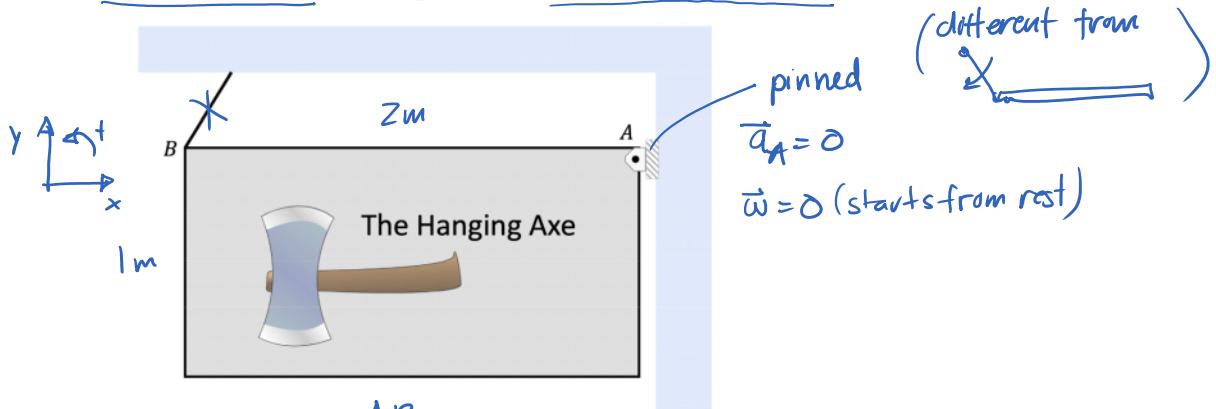
As well, we can use the equation for motion due to moments about a pinned point:

$$\sum \mathbf{M}_O = I_O \underline{\boldsymbol{\alpha}}$$

*parallel axes*

### 8.6.1 Example

The cable at point  $B$  supporting the  $2m \times 1m$  sign (mass  $10kg$ ) is suddenly broken. Find the angular acceleration of the sign and the reaction forces at point  $A$  just after the cable breaks.



$$\begin{aligned} I_A &= I_G + md^2 \\ &= \frac{1}{12}m(2^2 + 1^2) + m(1^2 + 0.5^2) \\ &= \frac{20}{12}m \end{aligned}$$

EOM

$$\begin{aligned} \sum F_x: R_x &= ma_{Gx} \quad ① \\ \sum F_y: R_y - mg &= ma_{Gy} \quad ② \\ \sum M_A: mg(1m) &= I_A \ddot{\alpha} \quad ③ \end{aligned} \quad \left. \begin{array}{l} \text{unknowns: } \ddot{\alpha}, a_{Gx}, a_{Gy}, R_x, R_y \text{ (5)} \\ 3 \text{ eqns} \end{array} \right\}$$

### KIN CONSTRAINTS

$$\begin{aligned} \ddot{\alpha}_A &= \ddot{\alpha}_A^0 + \ddot{\alpha} \times \vec{r}_{G/A} - \omega^2 \vec{r}_{G/A} \\ &= \ddot{\alpha} \hat{k} \times (-1\hat{i} - 0.5\hat{j}) \\ &= -\ddot{\alpha} \hat{j} + 0.5\ddot{\alpha} \hat{i} \quad \left. \begin{array}{l} 2 \text{ more eqns} \\ \text{eqns} \end{array} \right\} ④ \\ &= a_{Gy} \end{aligned}$$

SOLVE

$$\begin{aligned} ③ \Rightarrow \ddot{\alpha} &= \frac{mg}{I_A} = \frac{mg}{\frac{20}{12}m} = \frac{12}{20}g = \frac{3}{5}g \quad \boxed{\ddot{\alpha} = \frac{3}{5}g \text{ rad/s}^2 \hat{k}} \\ ①+④ \quad R_x &= m \left( 0.5 \left( \frac{3}{5}g \right) \right) = \frac{3}{10}mg \quad ②+④ \Rightarrow R_y = mg + m \left( \frac{-3}{5}g \right) = \frac{2}{5}mg \end{aligned}$$

$$\Rightarrow \vec{R} = \frac{3}{10}mg\hat{i} + \frac{2}{5}mg\hat{j} = 30N\hat{i} + 40N$$