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MECH 221 Dynamics Notes

6 L7: Absolute General Plane Motion

Reading

6.1 Objective

To relate rectilinear point motion with rotational motion on a rigid body.

6.2 Method

There are no "new equations". Use known geometric relationships. Try to relate angular rotation of a line fixed to the body, $\theta(t)$, $\dot{\theta}(t)$, $\ddot{\theta}(t)$, to the rectilinear (straight line) location of a point specified by a parameterized path, e.g.: $s = f(\theta)$.

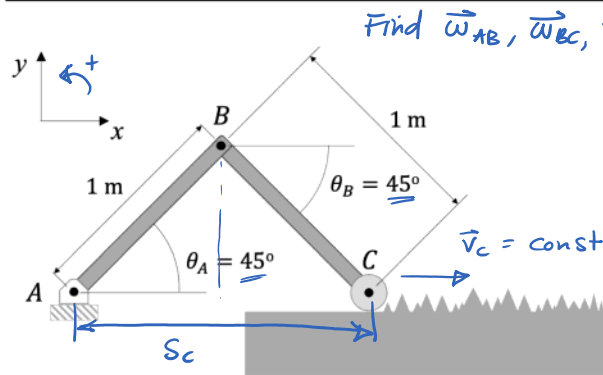
1. Draw it!
2. For a point P (translational point), define a position coordinate, s .
3. Draw a line through the body at reference angle θ .
4. Using geometry/trigonometry, find a parameterized relationship, $s = f(\theta)$.
5. Use time derivatives to relate:

$$v = f'(\theta)\dot{\theta} = f'(\theta)\omega$$

$$a = f''(\theta)\dot{\theta}^2 + f'(\theta)\alpha$$

6.2.1 Example

Consider the robotic grinder. Find the position, velocity and acceleration of the grinding wheel as a function of the angles θ_A and θ_B and their derivatives.



$$s_C = 2 (1 \text{ m}) \cos \theta_A$$

$$v_C = \dot{s}_C = 2 (-\sin \theta_A) \dot{\theta}_A \quad (1)$$

$$a_C = \dot{v}_C = -2 \cos \theta_A \ddot{\theta}_A^2 - 2 \sin \theta_A \ddot{\theta}_A \quad (2)$$

Isosceles triangle

$$AB = BC$$



$$\theta_A = -\theta_B$$



Set: $\theta_A = 45^\circ, v_C = 1 \text{ m/s}, a_C = 0$
(same as before)

differentiate:

$$\dot{\theta}_A = -\dot{\theta}_B$$

$$\ddot{\theta}_A = -\ddot{\theta}_B$$

$$(1) \quad \dot{\theta}_A = \frac{v_C}{(-2) \sin \theta_A} = \frac{1 \text{ m/s}}{(-2) \frac{1}{\sqrt{2}}} = -\frac{1}{\sqrt{2}} \text{ rad/s}$$

as before

$$\boxed{\vec{\omega}_{AB} = -\frac{1}{\sqrt{2}} \text{ rad/s} \hat{k}}$$

$$(2) \quad 0 = (-2) \cos \theta_A \dot{\theta}_A^2 + (-2) \sin \theta_A \ddot{\theta}_A$$

$$= -\frac{1}{\sqrt{2}} \left(-\frac{1}{\sqrt{2}}\right)^2 - \frac{1}{\sqrt{2}} \ddot{\theta}_A$$

$$\Rightarrow \ddot{\theta}_A = -\frac{1}{2} \text{ rad/s}^2$$

$$\boxed{\vec{\alpha}_{AB} = -\frac{1}{2} \text{ rad/s}^2 \hat{k}}$$

$$\dot{\theta}_A = -\dot{\theta}_B \Rightarrow \boxed{\vec{\omega}_{BC} = \frac{1}{\sqrt{2}} \text{ rad/s} \hat{k}}$$

$$\ddot{\theta}_A = -\ddot{\theta}_B \Rightarrow \boxed{\vec{\alpha}_{BC} = \frac{1}{2} \text{ rad/s}^2 \hat{k}}$$

6.3 Summary

Absolute general plane motion analysis can provide a quick, ad-hoc solution for 2-link problems with constrained motion. For more than 2 links, however, the math and geometry can get pretty ugly. Better to use relative frames.

Pros:

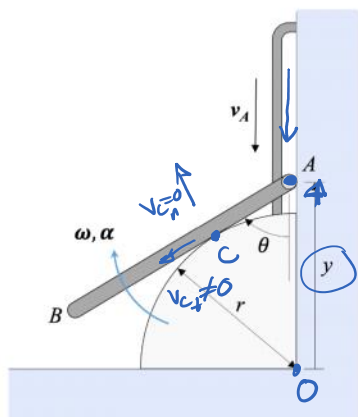
- Can yield a fast solution

Cons:

- Relationship may not be obvious
- If relationship is wrong, you've blown the whole problem (and it may be hard for the marker to give you part marks, unless they can understand what you have done)
- Method cannot easily be checked by vector analysis

6.3.1 Example

Point A at the end of a bar is moving downward in a slot with a constant velocity v_A . Find the angular velocity and angular acceleration of the bar as a function of the vertical position of A , y .



$$\vec{v}_A = \text{constant} \quad \text{Find } \omega \text{ \& } \alpha \text{ as function of } y$$

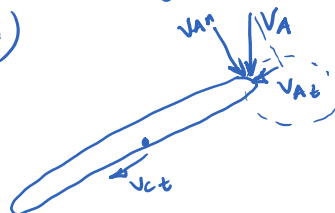
$$\vec{a}_A = 0$$

is C rolling w/o slipping? No

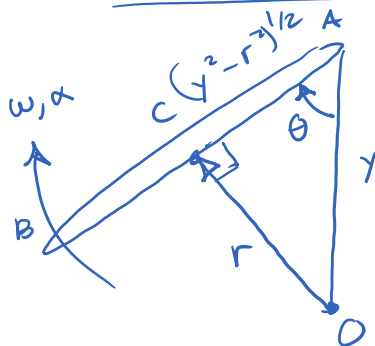
Has to slide because constrained by gravity and cam

v_C component along the bar (tangent to cam)

IF rolling w/o slipping
 $\vec{C} = IC$
 (not true)
 \vec{v}_A
 ϕ (not true)



(Example continued)

ABSOLUTE MOTION θ is in negative direction, but $\omega \propto$ arc also neg.

$$r = y \sin \theta \quad (r = y \sin(-\theta))$$

$$= -y \sin \theta \rightarrow \text{get same result}$$

$$\frac{d}{dt}: 0 = \dot{y} \sin \theta + y \cos \theta \dot{\theta}$$

$$\Rightarrow y \dot{\theta} \cos \theta = -\dot{y} \sin \theta$$

$$\dot{\theta} = \frac{-\dot{y} \sin \theta}{y \cos \theta}$$

$$\dot{y} = -v_A$$

$$\frac{\sin \theta}{\cos \theta} = \tan \theta$$

$$= \frac{r}{AC}$$

$$= \frac{r}{(y^2 - r^2)^{1/2}}$$

$$\dot{\theta} = \omega = \frac{v_A}{y} \cdot \frac{r}{(y^2 - r^2)^{1/2}}$$

$$[\vec{\omega} = -\omega \hat{k}] \text{ neg. dir}$$

$$\frac{d}{dt} (0 = \dot{y} \sin \theta + y \cos \theta \dot{\theta})$$

$$\Rightarrow 0 = \ddot{y} \sin \theta + \dot{y} \cos \theta \dot{\theta} + \dot{y} \cos \theta \dot{\theta} - y \sin \theta \dot{\theta}^2 + y \cos \theta \ddot{\theta}$$

$$0 = 2 \dot{y} \dot{\theta} \cos \theta - y \dot{\theta}^2 \sin \theta + y \cos \theta \ddot{\theta}$$

$$\cancel{y \ddot{\theta} \cos \theta} = \cancel{y \dot{\theta}^2 \sin \theta} - \frac{2 \dot{y} \dot{\theta} \cos \theta}{y}$$

$$\ddot{\theta} = \dot{\theta}^2 \tan \theta - \frac{2 \dot{y} \dot{\theta}}{y}$$

$$\text{recall: } \dot{y} = -v_A$$

$$\dot{\theta} = \frac{v_A}{y} \frac{r}{(y^2 - r^2)^{1/2}}$$

$$= \left(\frac{v_A}{y} \frac{r}{(y^2 - r^2)^{1/2}} \right)^2 \left(\frac{r}{(y^2 - r^2)^{1/2}} \right) - \frac{2(-v_A)}{y} \left(\frac{v_A}{y} \frac{r}{(y^2 - r^2)^{1/2}} \right)$$

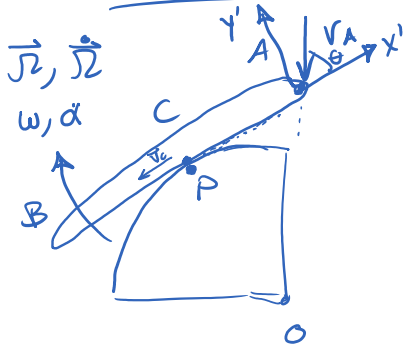
$$= \frac{v_A^2}{y^2} \left(\frac{r^3}{(y^2 - r^2)^{3/2}} + \frac{2r}{(y^2 - r^2)^{1/2}} \right) = \frac{v_A^2 r}{y^2} \left(\frac{r^2 + 2(y^2 - r^2)}{(y^2 - r^2)^{3/2}} \right)$$

$$\ddot{\theta} = \alpha = \frac{v_A^2 r}{y^2} \left(\frac{2y^2 - r^2}{(y^2 - r^2)^{3/2}} \right)$$

(Example continued)

ROTATING AXES REL. MOTION

C as a sticker on AB, same position as P (on cam)



$$\vec{v}_P = 0 = \vec{v}_A + \vec{\Omega} \times \vec{r}_{P/A} + (\vec{v}_{P/A})_{x'y'z'}$$

$$0 = -v_A \cos \theta \hat{i}' - v_A \sin \theta \hat{j}' + (-\Omega \hat{k}' \times (y^2 - r^2)^{1/2} (-\hat{i}')) + (v_{P/A})_{x'y'z'} \hat{i}'$$

$$= -v_A \cos \theta \hat{i}' - v_A \sin \theta \hat{j}' + \Omega (y^2 - r^2)^{1/2} \hat{j}' + (v_{P/A})_{x'y'z'} \hat{i}'$$

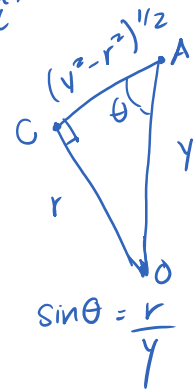
components:

$$\hat{i}': 0 = -v_A \cos \theta + (v_{P/A})_{x'y'z'}$$

$$(v_{P/A})_{x'y'z'} = v_A \cos \theta$$

$$\hat{j}': 0 = -v_A \sin \theta + \Omega (y^2 - r^2)^{1/2}$$

$$\dot{\theta} = \Omega = \frac{v_A \sin \theta}{(y^2 - r^2)^{1/2}} = \frac{v_A r}{y} \frac{1}{(y^2 - r^2)^{1/2}} \quad \sin \theta = \frac{r}{y}$$



$$\vec{a}_P = 0 = \vec{a}_A + \dot{\vec{\Omega}} \times \vec{r}_{P/A} - \Omega^2 \vec{r}_{P/A} + 2\vec{\Omega} \times (\vec{v}_{P/A})_{x'y'z'} + (\vec{a}_{P/A})_{x'y'z'}$$

$$\dot{\vec{\Omega}} = -\dot{\Omega} \hat{k}', \quad \vec{\Omega} = -\Omega \hat{k}', \quad \vec{r}_{P/A} = -(y^2 - r^2)^{1/2} \hat{i}'$$

$$(\vec{v}_{P/A})_{x'y'z'} = v_A \cos \theta \hat{i}'$$

$$(\vec{a}_{P/A})_{x'y'z'} = (a_{P/A})_t \hat{i}' - \underbrace{\Omega^2 r}_{\text{rolling up bar}} \hat{j}'$$

- Cross products

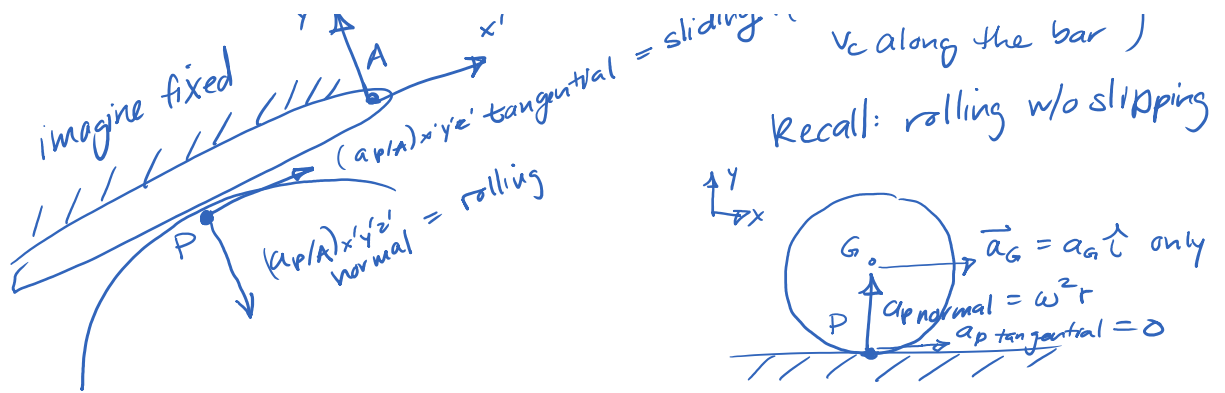
- Components

$$\Rightarrow \alpha = \dot{\Omega} = \frac{v_A^2 r}{y^2} \frac{(2y^2 - r^2)}{(y^2 - r^2)^{3/2}} \quad \left. \begin{array}{l} \text{same} \\ \text{(see complete} \\ \text{solution below)} \end{array} \right\}$$

Details on how we get $(\vec{a}_{P/A})_{x'y'z'}$:

Observing from the rotating frame: it appears that we are stationary, and the cam is sliding and rolling toward us

... fixed / / / / / longitudinal = sliding. (recall that we have v_c along the bar) ... like w/o slipping



Similarly, $|(a_{P/A})_{x'y'z'} \text{ normal}| = \Omega^2 r$
 and direction must be $-\hat{j}'$ since the cam cannot move through the bar and "rolling" will cause the cam point P to move away from the "fixed" bar.

$$\begin{aligned}\vec{a}_P &= \vec{a}_G + \vec{\alpha} \times \vec{r}_{P/G} - \omega^2 \vec{r}_{P/G} \\ \vec{r}_{P/G} &= -r \hat{j} \\ a_P \hat{j}' &= a_G \hat{i} + \alpha r \hat{i} + \omega^2 r \hat{j} \\ \underline{\underline{a_P = \omega^2 r (\uparrow)}}$$

Remainder of solution:

$$\begin{aligned}0 &= -\dot{\Omega} \hat{k} \times (-(y^2 - r^2)^{1/2}) \hat{i}' - \Omega^2 (-(y^2 - r^2)^{1/2}) \hat{i}' + 2(-\Omega \hat{k} \times v_A \cos \theta \hat{i}') \\ &\quad + (a_{P/A})_{x'y'z'} \hat{i}' - \Omega^2 r \hat{j}' \\ &= \dot{\Omega} (y^2 - r^2)^{1/2} \hat{j}' + \Omega^2 (y^2 - r^2)^{1/2} \hat{i}' - 2\Omega v_A \cos \theta \hat{j}' + (a_{P/A})_{x'y'z'} \hat{i}' - \Omega^2 r \hat{j}'\end{aligned}$$

Components:

$$\hat{j}': 0 = \dot{\Omega} (y^2 - r^2)^{1/2} - 2\Omega v_A \cos \theta - \Omega^2 r$$

$$\dot{\Omega} = \frac{2\Omega v_A \cos \theta + \Omega^2 r}{(y^2 - r^2)^{1/2}}$$

$$= \frac{2v_A \left(\frac{v_A r}{y^2}\right) + \frac{v_A^2 r^3}{y^2(y^2 - r^2)}}{(y^2 - r^2)^{1/2}}$$

$$= \frac{2v_A^2 r (y^2 - r^2) + \frac{v_A^2 r^3}{y^2}}{(y^2 - r^2)^{3/2}}$$

$$= \frac{v_A^2 r (2y^2 - 2r^2 + r^2)}{y^2 (y^2 - r^2)^{3/2}}$$

| 0 2 r 2 2 | same as

$$\text{recall: } \Omega = \frac{v_A r}{y} \frac{1}{(y^2 - r^2)^{1/2}}$$

$$\text{and } \cos \theta = \frac{(y^2 - r^2)^{1/2}}{y}$$

$$\begin{aligned}\Rightarrow \Omega \cos \theta &= \frac{v_A r}{y (y^2 - r^2)^{1/2}} \cdot \frac{(y^2 - r^2)^{1/2}}{y} \\ &= \frac{v_A r}{y^2}\end{aligned}$$

$$\dot{\Sigma} = \alpha = \frac{v_A^2 r}{y^2} \frac{(2y^2 - r^2)}{(y^2 - r^2)^{3/2}}$$

Same as before