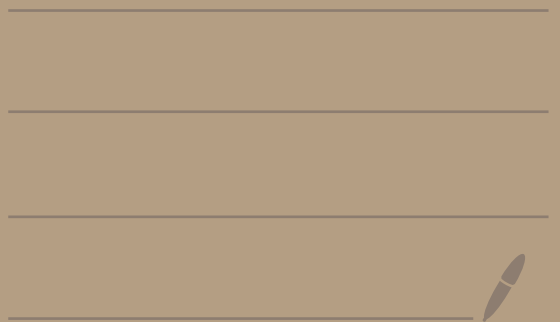


IV. Aerofoil Theory

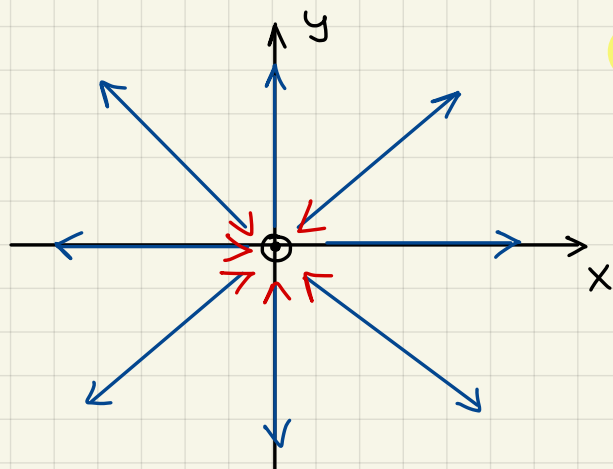


4.2 The velocity field

$$u_r = \frac{Q}{2\pi r}, \quad u_\theta = 0,$$

where Q is a constant, is called a **line source** flow if $Q > 0$ and a **line sink** if $Q < 0$. Show that it is irrotational and incompressible, save at $r = 0$, where it is not defined. Find the velocity potential and the stream function, and show that the complex potential is

$$w = \frac{Q}{2\pi} \log z.$$



Line source coincides with z -axis and emits fluid isotropically at the steady rate Q — the flow is directed away from $r=0$.

Line sink absorbs fluid at a rate Q .

$$\bar{\nabla} \times \bar{u} = 0 \quad \text{— irrot.}$$

$$\bar{\nabla} \cdot \bar{u} = u_r' + \frac{1}{r} u_r = -\frac{Q}{2\pi r^2} + \frac{Q}{2\pi r^2} = 0$$

incomp.

1) Veloc. potential ($\bar{\nabla} \times \bar{u}$)

$$\bar{u} = \bar{\nabla} \phi$$

$$u_r = \frac{\partial \phi}{\partial r}, \quad u_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = 0$$

$$\rightarrow \phi = f(r) = \frac{Q}{2\pi} \log r + C$$

2) Stream function ($\bar{\nabla} \cdot \bar{u}$)

$$u_x = \frac{\partial \psi}{\partial y}, \quad u_y = -\frac{\partial \psi}{\partial x}$$

$$\frac{D\psi}{Dt} = (\bar{u} \cdot \bar{\nabla}) \psi = \left(u_x \frac{\partial}{\partial x} + u_y \frac{\partial}{\partial y} \right) \psi = 0$$

$$u_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta}, \quad u_\theta = -\frac{\partial \psi}{\partial r} = 0$$

$$\psi = f(\theta) = \frac{Q}{2\pi} \theta$$

3) complex potential

$$u_x = \frac{\partial \psi}{\partial y} = \frac{\partial \phi}{\partial x}, \quad u_y = -\frac{\partial \psi}{\partial x} = \frac{\partial \phi}{\partial y},$$

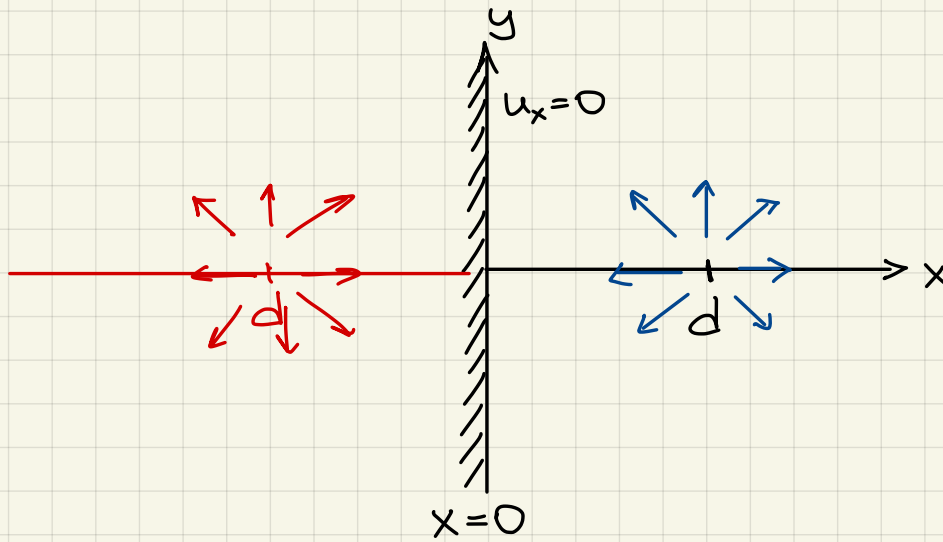
Cauchy-Riemann eq - s.

$$\underbrace{w(z) = \phi + i\psi}_{\text{complex potential}}$$

$$w(z) = \frac{Q}{2\pi} (\log r + i\theta) = \frac{Q}{2\pi} \log z.$$

$$z = re^{i\theta}, \quad \log z = \log r + i\theta$$

Fluid occupies the region $x > 0$, and there is a plane rigid boundary at $x = 0$. Find the complex potential for the flow due to a line source at $z = d > 0$, and show that the pressure at $x = 0$ decreases to a minimum at $|y| = d$ and thereafter increases with $|y|$.



$$\text{BC: } u_x = 0 \\ \Rightarrow \frac{\partial \Phi}{\partial x} = \frac{\partial \Psi}{\partial y} = 0$$

$$w(z) = w_1(z) + w_2(z)$$

$$w_1(z) = \frac{Q}{2\pi} \log(x_1 + iy) = \frac{Q}{2\pi} \log(x-d + iy) \\ = \frac{Q}{2\pi} \log(z-d)$$

$$w_2(z) = \frac{Q}{2\pi} \log(x_2 + iy) = \frac{Q}{2\pi} \log(z+d)$$

$$w(z) = \frac{Q}{2\pi} [\log(z-d) + \log(z+d)]$$

Analyze p at $x=0$.

$x=0$ is a streamline ($u_x=0$, $u_y \neq 0$)

Bern. streamline + h.: ideal fluid in a steady flow:

$$\frac{p}{\rho} + \frac{1}{2} \bar{u}^2 = \text{const} \quad \text{along a streamline}$$

$$w'(z) = \frac{\partial \Phi}{\partial x} + i \frac{\partial \Psi}{\partial x} = u - iv$$

$$w'(z) = \frac{Q}{2\pi} \left(\frac{1}{z-d} + \frac{1}{z+d} \right) \\ = \frac{Q}{2\pi} \left(\frac{1}{iy-d} + \frac{1}{iy+d} \right)$$

$$\begin{aligned}
&= \frac{Q}{2\pi} \left(\frac{1}{iy-d} \frac{iy+d}{iy+d} + \frac{1}{iy+d} \frac{iy-d}{iy-d} \right) \\
&= \frac{Q}{2\pi} \frac{-2iy}{y^2 + d^2} \\
\Rightarrow u &= 0 \text{ at } x=0, \quad v = + \frac{Q}{\pi} \frac{y}{y^2 + d^2}
\end{aligned}$$

$$p + \frac{\rho}{2} \frac{Q^2}{\pi^2} \frac{y^2}{(y^2 + d^2)^2} = \text{const}$$

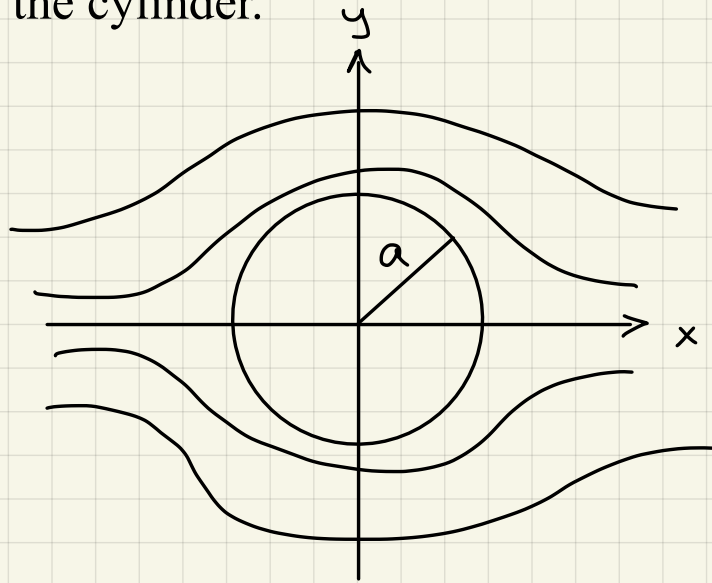
Find extrema of p :

$$\frac{dp}{dy} = - \frac{Q^2}{\pi^2} \frac{\rho}{2} \frac{d}{dy} \frac{y^2}{(y^2 + d^2)^2} = 0$$

4.3 An irrotational 2D flow has stream function

$$\psi = A(x - c)y,$$

where A and c are constants. A circular cylinder of radius a is introduced, its centre being at the origin. Find the complex potential, and hence the stream function, of the resulting flow. Use Blasius' theorem to calculate the force exerted on the cylinder.



$$\frac{\partial \phi}{\partial x} = \frac{\partial \psi}{\partial y}, \quad \frac{\partial \phi}{\partial y} = -\frac{\partial \psi}{\partial x}$$

$$\Rightarrow \phi = \int A(x - c) dy = \frac{A}{2} x^2 - Acx + f(y) + C_1$$

$$\phi = -\int Ay dy = -\frac{A}{2} y^2 + g(x) + C_2$$

$$\Rightarrow \phi(x, y) = \frac{A}{2} (x^2 - y^2) - Acx + \tilde{C}$$

In the abs. of a cyl:

$$w(z) = \phi + i\psi = \frac{A}{2} (x^2 - y^2) - Acx + iA(x - c)y$$

$$= \frac{A}{2} z^2 - Acz,$$

$$z^2 = x^2 + 2ixy - y^2$$

Milne-Thomson's circle theorem: suppose we have a flow with complex potential $w = f(z)$, where all the singularities of $f(z)$ lie in $|z| > a$. Then

$$w = f(z) + \overline{f(a^2/\bar{z})}$$

is the complex potential of a flow with (I) the same singularities as $f(z)$ in $|z| > a$ and (II) $|z| = a$ as a streamline.

$$w\left(\frac{a^2}{z}\right) = \frac{A}{2} \frac{a^4}{z^2} - Ac \frac{a^2}{z} = \frac{A}{2} \frac{a^4}{x^2 - 2ixy - y^2} - Ac \frac{a^2}{x - iy}$$

$$\frac{1}{(x - iy)^2} = \frac{1}{(x - iy)^2} \frac{(x + iy)(x + iy)}{(x + iy)(x + iy)} = \frac{z^2}{(x^2 + y^2)^2}$$

$$w\left(\frac{a^2}{z}\right) = \frac{A}{2} \frac{a^4 z^2}{(x^2 + y^2)^2} - Ac \frac{a^2 z}{x^2 + y^2}$$

$$w\left(\frac{a^2}{z}\right) = \frac{A}{2} \frac{a^4}{(x^2 + y^2)^2} (x^2 - 2ixy - y^2) - Ac \frac{a^2}{x^2 + y^2} (x - iy)$$

Complex pot. of a flow around the cyl.:

$$w(z) = \frac{A}{2} (x^2 + 2ixy - y^2) - Ac(x + iy) + \frac{A}{2} \frac{a^4}{(x^2 + y^2)^2} (x^2 - 2ixy - y^2) - Ac \frac{a^2}{x^2 + y^2} (x - iy)$$

$$\psi = \text{Im}(w)$$

$$\begin{aligned} \psi &= Axy - Acy - A \frac{a^4}{(x^2 + y^2)^2} xy + Ac \frac{a^2}{x^2 + y^2} y \\ &= Ay \left(x - \frac{a^4}{(x^2 + y^2)^2} x - c + c \frac{a^2}{x^2 + y^2} \right) \\ &= Ay \left(1 - \frac{a^4}{x^2 + y^2} \right) \left[x \left(1 + \frac{a^2}{x^2 + y^2} \right) - c \right] \end{aligned}$$

Blasius' theorem: let there be a steady flow with complex potential $w(z)$ about some fixed body which has as its boundary the closed contour C . If F_x and F_y are the components of the net force on the body, then

$$F_x - i F_y = \frac{1}{2} i \oint_C \left(\frac{dw}{dz} \right)^2 dz.$$

$$C \Rightarrow |z| = a^2$$

Use Residue theorem :

$$\oint_C f(z) dz = 2\pi i \sum_k \text{Res}(f, a_k)$$

4.4 Show that the problem of irrotational flow past a circular cylinder may be formulated in terms of the velocity potential as follows:

$$\frac{\partial^2 \Phi}{\partial r^2} + \frac{1}{r} \frac{\partial \Phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \Phi}{\partial \theta^2} = 0,$$

with

$$\Phi = Ur \cos \theta \text{ as } r \rightarrow \infty, \quad \frac{\partial \Phi}{\partial r} = 0 \text{ on } r=a,$$

and obtain the solution by using the method of separation of variables.

$$\nabla \cdot \bar{u} = \nabla^2 \Phi = 0$$

$$\text{At } r=a, \quad u_r = 0 \rightarrow \frac{\partial \Phi}{\partial r} = 0$$

$$\text{At } r \rightarrow \infty, \quad \bar{u} = \underbrace{(U, 0, 0)}_{\text{cartesian}} - \text{free-stream}$$

$$\bar{u} = U \bar{e}_x = U(\cos \theta \bar{e}_r - \sin \theta \bar{e}_\theta)$$

$$\Phi = \int u_r dr = Ur \cos \theta \quad \text{at } r \rightarrow \infty$$

$$\Phi(r, \theta) = f(r) g(\theta)$$

$$f'' g + \frac{1}{r} f' g + \frac{1}{r^2} f g'' = 0$$

$$r^2 \frac{f''}{f} + r \frac{f'}{f} = - \frac{g''}{g} = -K$$

$$\text{I. } g''(\theta) - K g(\theta) = 0$$

$$\text{Non-triv. if } K < 0, \quad K = -\lambda^2$$

$$g(\theta) = C_1 \cos \lambda \theta + C_2 \sin \lambda \theta$$

$$\text{At } r \rightarrow \infty, \quad \Phi = Ur \cos \theta \Rightarrow \begin{aligned} C_2 &= 0, \\ \lambda &= 1, \\ C_1 &= 1 \end{aligned}$$

$$\Rightarrow \Phi(r, \theta) = f(r) \cos \theta$$

$$\text{II. } f'' + \frac{1}{r} f' - \frac{1}{r^2} f = 0$$

$$\Leftrightarrow f'' + \left(\frac{f}{r} \right)' = 0$$

$$f' + \frac{f}{r} = C_3 \iff r f' + f = C_3 r$$

$$\iff (r f)' = r C_3$$

$$r f = \frac{C_3}{2} r^2 + C_4$$

$$f(r) = \frac{C_3}{2} r + C_4 \frac{1}{r}$$

$$\phi = \left(\frac{C_3}{2} r + C_4 \frac{1}{r} \right) \cos \theta$$

$$r \rightarrow \infty: \phi = \frac{C_3}{2} r \cos \theta = U r \cos \theta$$

$$\Rightarrow C_3 = 2U$$

$$r = a: \left(U - \frac{C_4}{a^2} \right) \cos \theta = 0$$

$$\rightarrow C_4 = U a^2$$

$$\phi = U \left(r + \frac{a^2}{r} \right) \cos \theta$$

$$\begin{cases} u_r = U \left(1 - \frac{a^2}{r^2} \right) \cos \theta \\ u_\theta = -U \left(1 + \frac{a^2}{r^2} \right) \sin \theta \end{cases}$$

When there is circulation round the cylinder, derive the equation

$$\frac{r}{a} = \frac{B}{2} + \left(\frac{B^2}{4} - 1 \right)^{\frac{1}{2}}, \quad \theta = \frac{3\pi}{2},$$

and confirm that the stagnation points vary in position with the parameter B .

$$\bar{u} = \bar{u}_0 + \bar{u}_v$$

$$\bar{u}_v = \frac{\Gamma}{2\pi r} \bar{e}_\theta, \quad \Gamma < 0.$$

$$\begin{cases} u_r = U \left(1 - \frac{a^2}{r^2} \right) \cos \theta \\ u_\theta = -U \left(1 + \frac{a^2}{r^2} \right) \sin \theta + \frac{\Gamma}{2\pi r} \end{cases}$$

Stagn. points at $r = a$:

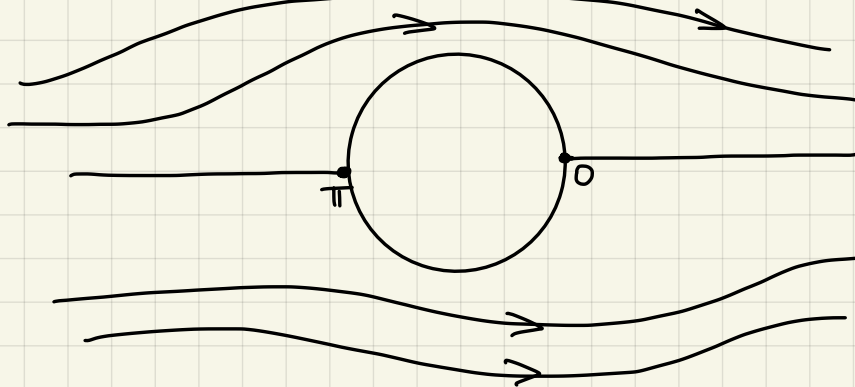
$$u_r = 0, \quad u_\theta = -2U \sin \theta + \frac{\Gamma}{2\pi a} = 0$$

$$\sin \theta = \frac{\Gamma}{4U\pi a} = -\frac{B}{2},$$

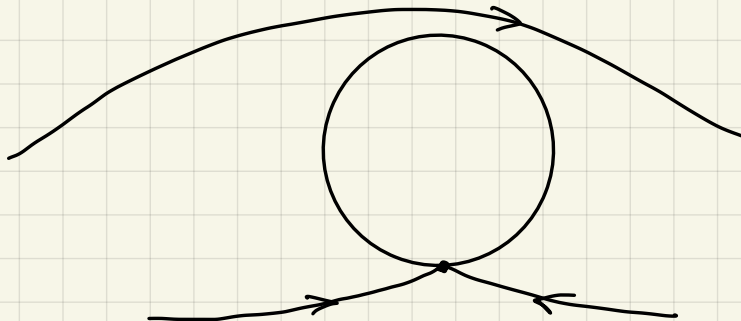
$$B = -\frac{\Gamma}{2U\pi a} > 0.$$

$$-1 \leq \sin \theta \leq 1 \Rightarrow 0 < B \leq 2$$

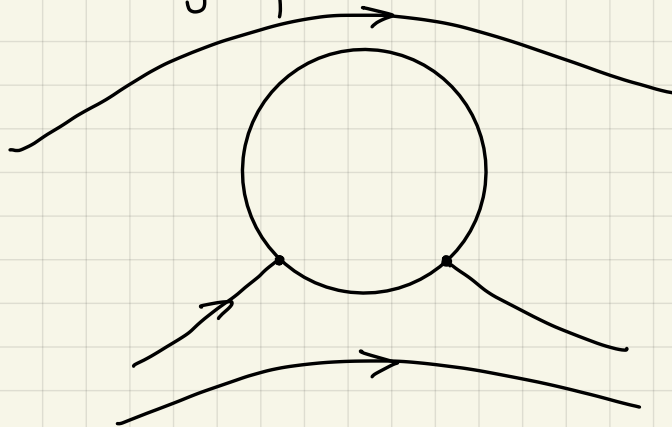
I. $B = 0 \rightarrow \sin \theta = 0 \rightarrow \theta_1 = 0, \theta_2 = \pi$



II. $B = 2 \rightarrow \sin \theta = -1 \Rightarrow \theta = -\pi/2$



III. $B < 2 \rightarrow 2$ stagn. points.



What about stagnation points at $r > a$? This implies

$$u_r = U \left(1 - \frac{a^2}{r^2} \right) \cos \theta = 0$$
$$\Rightarrow \cos \theta = 0 \rightarrow \theta = \pm \pi/2$$

If $\theta = \pi/2$,

$$u_\theta = -U \left(1 + \frac{a^2}{r^2} \right) + \frac{\Gamma}{2\pi r} = 0$$

this is our eq. for computing r .

Define $B = -\frac{\Gamma}{2\pi Ua}$,

$$1 + \frac{a^2}{r^2} = -\frac{Ba}{r}$$
$$\rightarrow r^2 + Bar + a^2 = 0.$$

If $\theta = -\pi/2$, our quadratic eq. is

$$r^2 - Bar + a^2 = 0$$

Solution: $\frac{r}{a} = \frac{B}{2} \pm \sqrt{\frac{B^2}{4} - 1}$.

We know that $r > a$

$$\rightarrow \frac{r}{a} = \frac{B}{2} + \sqrt{\frac{B^2}{4} - 1}$$

As r must be a real number,

$$\frac{B^2}{4} - 1 \geq 0$$

$$\rightarrow B^2 \geq 4.$$

By our choice, $B > 0 \Rightarrow B \geq 2$.

Moreover, as $r/a > 1$, $B > 2$.