
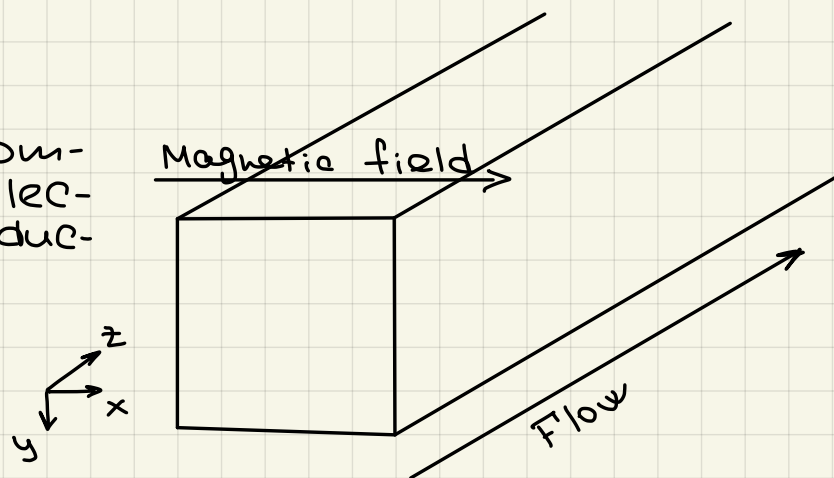


Magnetohydrodynamics (MHD)



viscous incompressible electrically conducting fluid



I. Derive the MHD eq-s for this flow

non-dim. $\left\{ \begin{array}{l} \bar{u} = u(x, y) \bar{e}_z \\ p = p(z), \quad p'(z) = \text{const} \\ \bar{b} = \underbrace{\bar{e}_x}_{\text{applied}} + \underbrace{b(x, y) \bar{e}_z}_{\text{induced magn. field}} \end{array} \right.$

$\left\{ \begin{array}{l} \bar{x}_{\text{dim}} \rightarrow L \bar{x} \\ \bar{u}_{\text{dim}} \rightarrow U \bar{u} \\ \bar{b}_{\text{dim}} \rightarrow B_0 \bar{b} \end{array} \right.$

$\bar{\nabla} \cdot \bar{u} = 0, \quad \sim \frac{U}{V} \quad \text{the Lorentz force}$

$\partial_t \bar{u} + \bar{u} \cdot \bar{\nabla} \bar{u} = -\bar{\nabla} p + \frac{1}{Re} \bar{\nabla}^2 \bar{u} + \int_{B_0}^{\frac{Ma^2}{Re}} \bar{j} \times \bar{b},$

$\partial_t \bar{b} + \bar{u} \cdot \bar{\nabla} \bar{b} = \bar{b} \cdot \bar{\nabla} \bar{u} + \frac{1}{Re_m} \bar{\nabla}^2 \bar{b},$

$\bar{\nabla} \cdot \bar{b} = 0$

1) $-\frac{\partial p}{\partial z} + \frac{1}{Re} \bar{\nabla}^2 u + \frac{Ma^2}{Re} (\bar{j} \times \bar{b})_z = 0,$

$(\bar{j} \times \bar{b})_z = \cancel{j_x b_y} - j_y b_x = -j_y$

$\bar{j} = \frac{1}{Re_m} \bar{\nabla} \times \bar{b} \quad \text{Ampère's eq-n}$

$j_y = -Re_m^{-1} \frac{\partial b}{\partial x}$

$\Rightarrow \bar{\nabla}^2 u + Ma^2 Re_m^{-1} \frac{\partial b}{\partial x} = p' Re = K$

$$2) \left(\frac{\partial}{\partial x} + b \frac{\partial}{\partial z} \right) u + Re_m^{-1} \nabla^2 b = Re_m^{-1} \nabla^2 b + \frac{\partial u}{\partial x} = 0$$

$$\begin{cases} \nabla^2 u + Ma^2 Re_m^{-1} \frac{\partial b}{\partial x} = \kappa, \\ Re_m^{-1} \nabla^2 b + \frac{\partial u}{\partial x} = 0. \end{cases}$$

$$b = Re_m^{-1} b^{old}$$

$$\begin{cases} \nabla^2 u + Ma^2 \frac{\partial b}{\partial x} = \kappa, \\ \nabla^2 b + \frac{\partial u}{\partial x} = 0. \end{cases} \quad \text{--- } \{u, b\}$$

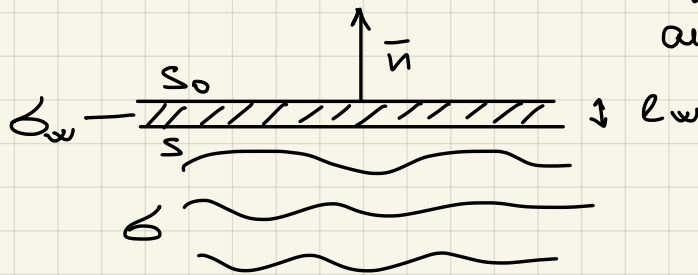
$$BC: u = 0, b?$$

electr. conductivity of each wall

$$\text{II. } \sigma_{w,1}, \sigma_{w,2}, \sigma_{w,3}, \sigma_{w,4} \rightarrow \text{given}$$

Assume

$\underbrace{l_w}_{\text{thickness of the wall}} \ll \underbrace{L}_{\text{width of the duct}}$



In the general case we solve Maxwell eq.-s in the fluid and in the wall and "connect" them
 \rightarrow here, due to $l_w \ll L$ assumption, we replace sol. in the wall with the BC.

Step 1. Use Maxwell's BC for the tangential component of \vec{E} at the interface to derive the BC for the electric current.

$$(\vec{E} - \vec{E}_w) \cdot \vec{\tau} = 0$$

contin. of E_t

$$\vec{j} = \sigma(\vec{E} + \vec{u} \times \vec{b})$$

$$\left(\frac{1}{\sigma} \vec{j} - \frac{1}{\sigma_w} \vec{j}_w \right) \cdot \vec{\tau} = 0,$$

$$\begin{aligned} (\vec{j} \cdot \vec{\tau}) \vec{\tau} &= -\vec{n} \times (\vec{n} \times \vec{j}) = \vec{n} \times (\vec{j} \times \vec{n}) \\ \Rightarrow \left(\frac{1}{\sigma} \vec{j} - \frac{1}{\sigma_w} \vec{j}_w \right) \times \vec{n} &= 0. \end{aligned}$$

Step 2. Use Ampère's law to derive the BC for the induced magnetic field.

$$\vec{\nabla} \times \vec{b} = \mu_0 \vec{j}$$

$$\begin{aligned} \vec{j} \times \vec{n} &= \frac{1}{\mu_0} (\vec{\nabla} \times \vec{b}) \times \vec{n} = \frac{1}{\mu_0} [\vec{\nabla} \times (b \vec{e}_z)] \times \vec{n} \\ &= \frac{1}{\mu_0} [b \cancel{\vec{\nabla} \times \vec{e}_z} + (\vec{\nabla} b) \times \vec{e}_z] \times \vec{n} \\ &= \frac{1}{\mu_0} \vec{e}_z \left[\underbrace{\vec{n} \cdot (\vec{\nabla} b)}_{\frac{\partial b}{\partial n}} \right] - \frac{1}{\mu_0} \cancel{(\vec{\nabla} b) (\vec{e}_z \cdot \vec{n})} \end{aligned}$$

$$\Rightarrow \frac{1}{\epsilon} \frac{\partial b}{\partial n} - \frac{1}{\epsilon_w} \frac{\partial b_w}{\partial n} = 0$$

Step 3. How can we utilize the assumption of a thin wall, $l_w \ll 1$, to express the BC for \vec{b} in terms of flow variables only?

$$b|_s = b|_{s_0} + l_w \frac{\partial b_w}{\partial n} + \frac{l_w^2}{2} \frac{\partial^2 b_w}{\partial n^2} + \dots$$

$$l_w \ll 1 \Rightarrow b|_s = \cancel{b|_{s_0}} + l_w \frac{\partial b_w}{\partial n}$$

insul. medium
outside the duct

$$\frac{1}{l_w} b = \frac{\partial b_w}{\partial n}$$

$$\Rightarrow \frac{1}{\epsilon} \frac{\partial b}{\partial n} - \frac{1}{l_w \epsilon_w} b = 0$$

thin-wall BC

Non-dim. : $\vec{b} \rightarrow B_0 \vec{b}$, $\vec{x} \rightarrow L \vec{x}$

$$\Rightarrow \frac{B_0}{L \epsilon} \frac{\partial b}{\partial n} - \frac{B_0}{l_w \epsilon_w} b = 0$$

$$\Rightarrow \frac{\partial b}{\partial n} - \frac{L \epsilon}{l_w \epsilon_w} b = 0$$

$\frac{1}{\epsilon}$ conductance ratio

Limit case: $\epsilon_w \rightarrow 0$ (perf. insul. materials)

$$\Rightarrow c=0 \Rightarrow b=0$$

$\epsilon_w \rightarrow \infty$ (perf. cond. materials)

$$\Rightarrow \frac{\partial b}{\partial n} = 0$$

The magnetic Reynolds number is a dimensionless parameter that estimates the relative contributions of advection and diffusion of a magnetic field in a conducting medium.

$$Re_m \sim \frac{\text{advection}}{\text{diffusion}} \sim \frac{|\nabla \times (\bar{u} \times \bar{B})|}{|\eta \nabla^2 \bar{B}|} \sim \frac{U B}{L} \cdot \frac{L^2}{\eta B} = \frac{UL}{\eta}$$

$$\frac{\partial \bar{B}}{\partial t} = \underbrace{\nabla \times (\bar{u} \times \bar{B})}_{\text{advection}} + \underbrace{\eta \nabla^2 \bar{B}}_{\text{diffusion}}$$

$$\Rightarrow Re_m = \frac{UL}{\eta}$$

For most industrial liquid metals Re_m is small:
 $\eta \sim 1 \text{ m}^2/\text{s}$, $L \sim 0.1 \text{ m}$, $U \sim 0.01 \text{ m/s}$

$$\Rightarrow Re_m \sim 10^{-3}$$

For many liquid metals we commonly apply a so-called quasi-static approximation:

$$Re_m \ll 1.$$

$$\frac{\partial \bar{u}}{\partial t} + (\bar{u} \cdot \nabla) \bar{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \bar{u} + \frac{1}{\rho} \bar{j} \times \bar{B},$$

$$\frac{\partial \bar{B}}{\partial t} = \nabla \times (\bar{u} \times \bar{B}) + \eta \nabla^2 \bar{B},$$

$$\nabla \cdot \bar{u} = 0,$$

$$\nabla \cdot \bar{B} = 0.$$

Consider the motion of an incompressible liquid metal in a stationary uniform magnetic field. What are the quasi-static MHD equations?

$$\vec{B} = \vec{B}_0 + \vec{b}$$

$$\frac{\partial \vec{B}}{\partial t} = \vec{\nabla} \times (\vec{u} \times \vec{B}) + \eta \nabla^2 \vec{B}$$

$$\Rightarrow \frac{\partial \vec{b}}{\partial t} = \underbrace{\vec{\nabla} \times (\vec{u} \times \vec{B}_0)} + \underbrace{\vec{\nabla} \times (\vec{u} \times \vec{b})} + \eta \nabla^2 \vec{b}$$

$$1. \quad \vec{\nabla} \times (\vec{A} \times \vec{C}) = \vec{A}(\vec{\nabla} \cdot \vec{C}) - \vec{C}(\vec{\nabla} \cdot \vec{A}) + (\vec{C} \cdot \vec{\nabla})\vec{A} - (\vec{A} \cdot \vec{\nabla})\vec{C}$$

$$\Rightarrow \underbrace{(\vec{B}_0 \cdot \vec{\nabla})\vec{u}}_{\frac{B_0 U}{L}} - \cancel{(\vec{u} \cdot \vec{\nabla})\vec{B}_0} + (\vec{b} \cdot \vec{\nabla})\vec{u} - (\vec{u} \cdot \vec{\nabla})\vec{b}$$

$$\frac{\eta |\nabla^2 \vec{b}|}{|(\vec{u} \cdot \vec{\nabla})\vec{b}|} \sim \frac{\eta |\nabla^2 \vec{b}|}{|(\vec{b} \cdot \vec{\nabla})\vec{u}|} \sim \frac{\eta |\vec{b}|}{L^2} \cdot \frac{L}{|\vec{b}|U} = \frac{1}{Re_m} \gg 1$$

$$\Rightarrow \frac{\partial \vec{b}}{\partial t} = (\vec{B}_0 \cdot \vec{\nabla})\vec{u} + \eta \nabla^2 \vec{b} \quad \left\{ \begin{array}{l} \text{diffusion eq-n} \\ \text{for } \vec{b} \text{ with ex. 4.} \\ \text{force} \end{array} \right.$$

$$\frac{\partial \vec{b}}{\partial t} = \eta \nabla^2 \vec{b} + \vec{f}(\vec{x}, t)$$

After some very small $t_f \rightarrow \eta \nabla^2 \vec{b} = -(\vec{B}_0 \cdot \vec{\nabla})\vec{u}$
as $\eta \gg 1$

$$\frac{\tau_{diff}}{\tau_u} \sim \frac{|\vec{b}|}{|\eta \nabla^2 \vec{b}|} \cdot \frac{U}{L} \sim \frac{L^2}{\eta} \cdot \frac{U}{L} = Re_m$$

Magn. f. adjusts to \vec{u} instant.

$$\eta \nabla^2 \vec{b} = -(\vec{B}_0 \cdot \vec{\nabla})\vec{u}$$

induct. eq-n under the quasi-static approx.

$$|\vec{b}| \sim \frac{B_0 U}{L} \cdot \frac{L^2}{\eta} = Re_m B_0$$

$$\Rightarrow |\vec{b}| \ll B_0$$

In the quasi-static approx. the induced magn. f. is negligible compared to the applied one

$$\frac{1}{\rho} \vec{j} \times \vec{B} = \frac{1}{\rho} \vec{j} \times \vec{B}_0 = \frac{c}{\rho} (\vec{E} + \vec{u} \times \vec{B}_0) \times \vec{B}_0 \rightarrow \text{Lor. f.}$$

Helmholtz's th. : $\vec{E} = -\vec{\nabla}\phi + \vec{\nabla} \times \vec{a}$

$\vec{\nabla} \times \dots = 0$ (irrot.) $\vec{\nabla} \cdot \dots = 0$ (solenoidal)

Use Faraday's law $\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$

$$\vec{\nabla} \times \vec{E} = \vec{\nabla} \times (\vec{\nabla} \times \vec{a}) \sim \frac{|\vec{B}|}{\tau} \sim \frac{Re_m B_0 U}{L}$$

$$\Rightarrow \vec{\nabla} \times \vec{a} \sim Re_m B_0 U$$

$$\vec{E} \approx -\vec{\nabla}\phi$$

Lor. force: $\frac{c}{\rho} (-\vec{\nabla}\phi + \vec{u} \times \vec{B}_0) \times \vec{B}_0$

\downarrow
 electrostatic potential

$$\left\{ \begin{array}{l} \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u} = \frac{1}{\rho} \vec{\nabla} p + \nu \vec{\nabla}^2 \vec{u} + \frac{c}{\rho} (-\vec{\nabla}\phi + \vec{u} \times \vec{B}_0) \times \vec{B}_0 \end{array} \right.$$

Diverg. of the Ohm's law:

$$\vec{\nabla} \cdot \vec{j} = 0 = c (-\vec{\nabla}^2 \phi + \vec{\nabla} \cdot (\vec{u} \times \vec{B}_0))$$

$$\Rightarrow \vec{\nabla}^2 \phi = B_0 \cdot (\vec{\nabla} \times \vec{u}) = \vec{B}_0 \cdot \vec{\omega},$$

$$\vec{\nabla} \cdot \vec{u} = 0$$

the quasi-static MHD eq-s in potential formulation