











Week 10 – Trajectory Planning

Advanced Robotic Systems – MANU2453

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Lectures

Wk	Date	Lecture (NOTE: video recording)	Maths Difficulty	Hands-on Activity	Related Assessment
1	24/7	<ul style="list-style-type: none"> • Introduction to the Course • Spatial Descriptions & Transformations 			
2	31/7	<ul style="list-style-type: none"> • Spatial Descriptions & Transformations • Robot Cell Design 			Robot Cell Design Assignment
3	7/8	<ul style="list-style-type: none"> • Forward Kinematics • Inverse Kinematics 			
4	14/8	<ul style="list-style-type: none"> • ABB Robot Programming via Teaching Pendant • ABB RobotStudio Offline Programming 		ABB RobotStudio Offline Programming	Offline Programming Assignment
5	21/8	<ul style="list-style-type: none"> • Jacobians: Velocities and Static Forces 			
6	28/8	<ul style="list-style-type: none"> • Manipulator Dynamics 			
7	11/9	<ul style="list-style-type: none"> • Manipulator Dynamics 		MATLAB Simulink Simulation	
8	18/9	<ul style="list-style-type: none"> • Robotic Vision 		MATLAB Simulation	Robotic Vision Assignment
9	25/9	<ul style="list-style-type: none"> • Robotic Vision II 		MATLAB Simulation	
10	2/10	<ul style="list-style-type: none"> • Trajectory Generation 			
11	9/10	<ul style="list-style-type: none"> • Linear & Nonlinear Control 		MATLAB Simulink Simulation	
12	16/10	<ul style="list-style-type: none"> • Introduction to I4.0 • Revision 			Final Exam

Content

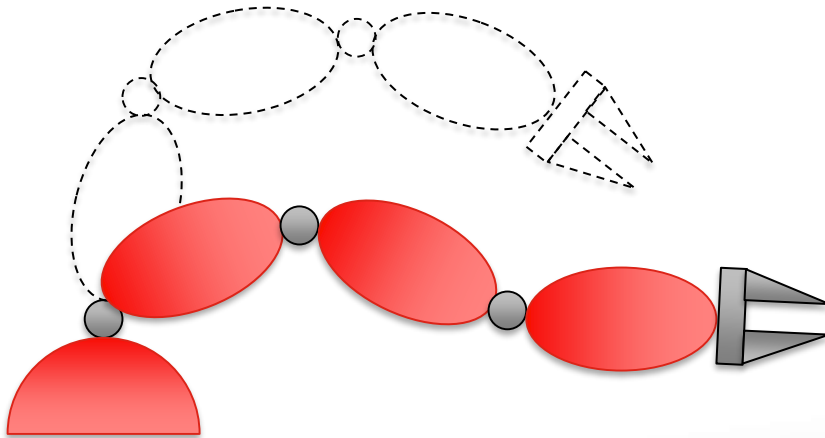
- Introduction
- Cartesian Space Schemes vs. Joint Space Schemes
- Cubic Polynomial
- Quintic Polynomial
- Linear Function with Parabolic Blends
- Matlab / Simulink Simulation

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Introduction

- In the past two weeks, you learnt how to find the target using vision. Today you will learn how to specify the **path from current position to the target**.
 - And next week, you will learn how to control the robot to follow this path.



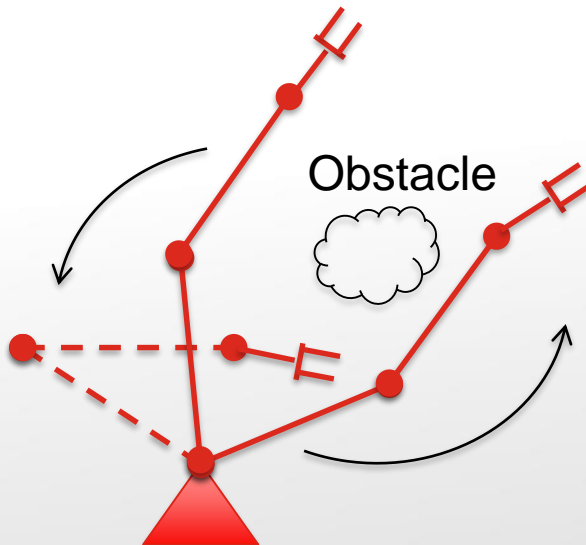
- Here, we use the term “**trajectory**” in place of path.
 - Trajectory means a **time history** of position, velocity and acceleration for each degree of freedom.
 - For e.g. we may specify: at time 0, robot is at $x=1, y=1$; at time 0.1, robot should go to $x=1.2, y=0.8$; at time 0.2, $x=1.3, y=0.7$ etc.

Introduction

- However, the above example of specifying point by point at different times is not convenient.
- Can we just specify the:
 - Desired **goal position and orientation** for the end-effector;
 - The **time** to reach goal position;
 - General **shape** of the path (straight line, polynomial etc.);
 - (Optional) Some intermediate points / “**via points**”
- and let the system figure out the trajectory?
- NOTE: The term “**points**” in this lecture should be interpreted as frames containing **both position and orientation**!

Introduction

- It is often desirable that the motion of the manipulator to be **smooth**.
 - **Continuous function**, with **continuous first derivative**.
 - It's even better if second derivative is continuous.
 - Reason: Rough and jerky motions causes vibrations due to resonance modes, as well as increases wear and tear.
- “Via points” are usually given for the purpose of collision avoidance.

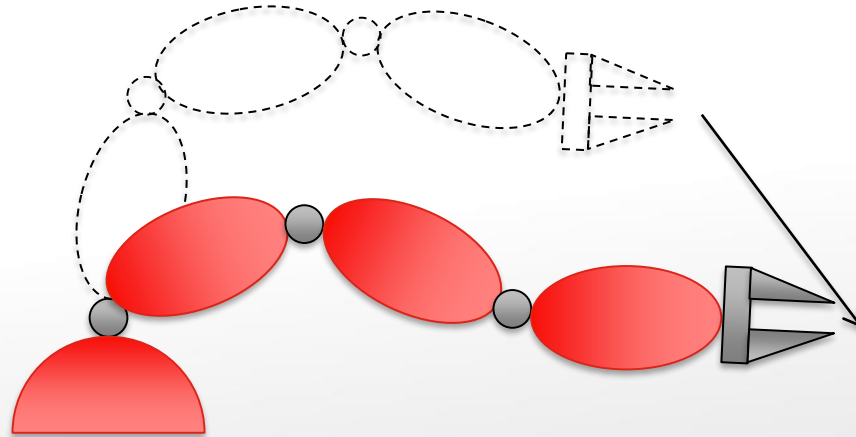


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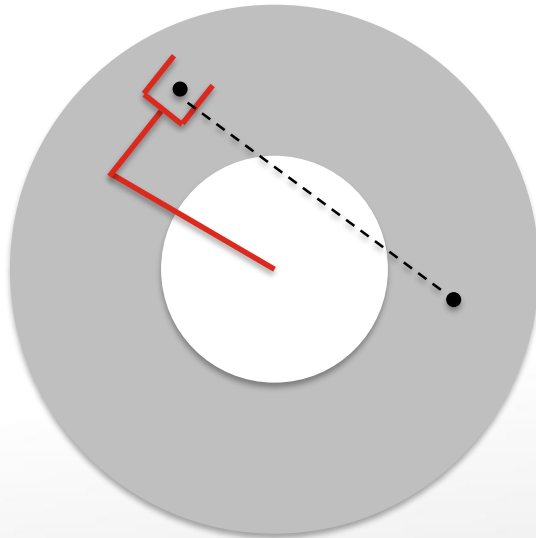
Cartesian Space Schemes

- Cartesian Space Schemes means specifying trajectory directly through **position and orientation of the end-effector**.
- The **advantage** of Cartesian Space Schemes is that we can enforce certain shape of the trajectory (for e.g. straight line), or enforce orientation of the end-effector (for e.g. maintain same orientation throughout).

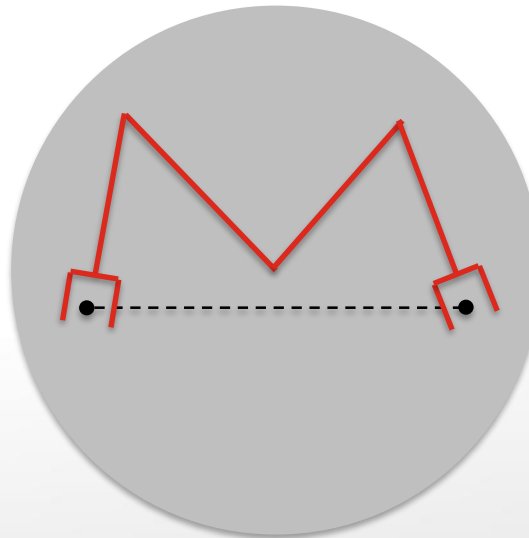


Cartesian Space Schemes

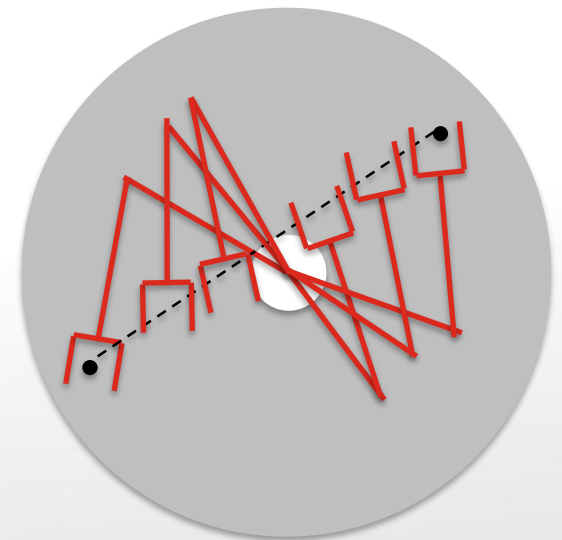
- However, Cartesian Space Schemes also have quite a few **disadvantages**:
 - **Computationally expensive**: After path is generated, **inverse kinematics** has to be solved at every time step (update rate) to calculate joint angles.
 - Prone to problems relating to **workspace and singularities**



Intermediate points
not reachable



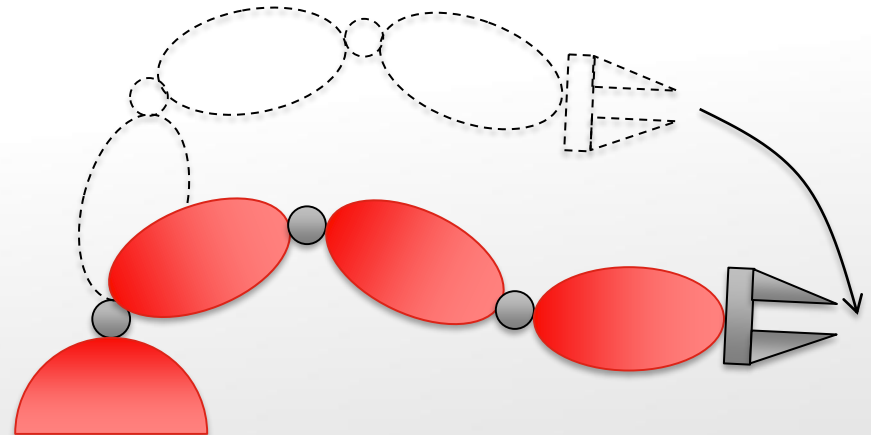
Start and end points
reachable but in
different configurations



High joint rates near
Singularities

Joint Space Schemes

- Joint Space Schemes means specifying trajectory directly through **the joint angles**.
 - **Advantages:**
 - Easy to compute.
 - No issue with singularities.
 - **Disadvantage:**
 - Path will not be linear.
 - This may be a problem if there are possible collisions.

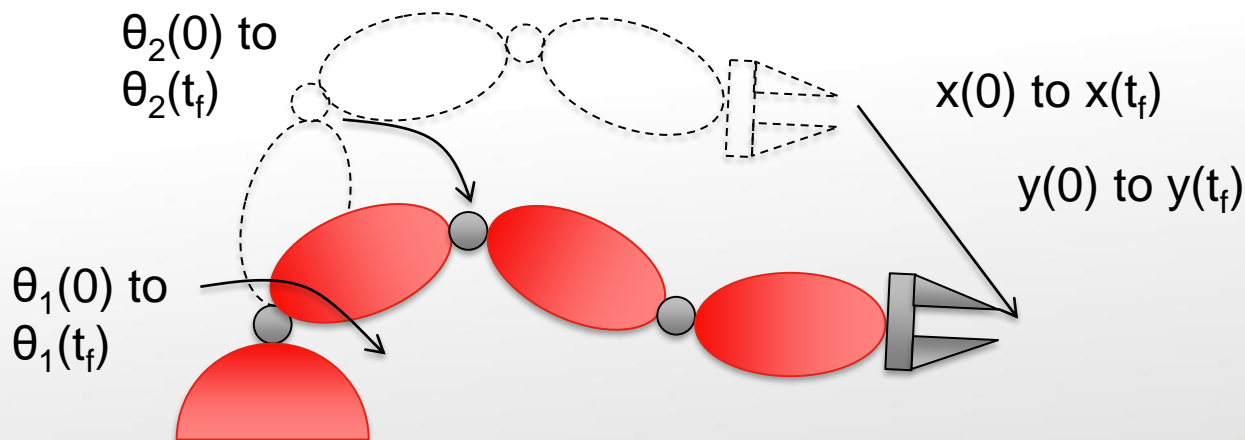


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General Solution

- In this section, we will use “ $u(t)$ ” to represent any of the variables, be it the Cartesian terms (x , y , z , angles) or the joint variables (θ).
- A reminder of our question:
 - Given the **start**, **end**, and possibly some **via points**;
 - And given the **time** to reach goal position;
 - Generate a **trajectory** $u(t)$ for the robot to follow.



Use “ $u(t)$ ” to represent any of the variables. Therefore: $u(0)$ to $u(t_f)$

Straight Line

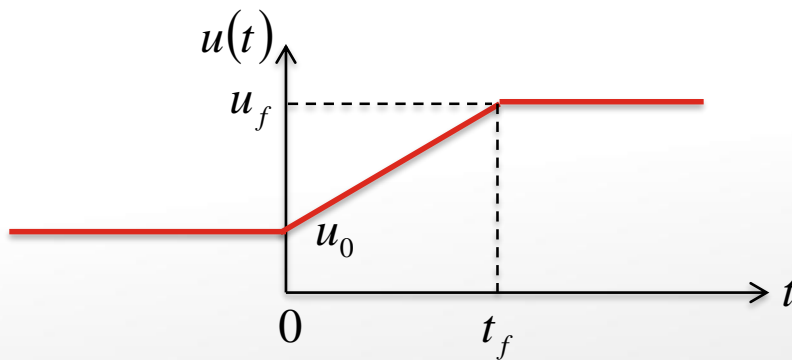
- We want to move from initial position to target position within time t_f .
- To do this, the general variable “ $u(t)$ ” will change from its initial value to the target value within time t_f .

Straight Line

- We want to move **from initial position** to **target position** within time t_f .
- To do this, the general variable “ $u(t)$ ” will change from its **initial value** to the **target value** within time t_f .

$$\begin{aligned}u(0) &= u_0 \\ u(t_f) &= u_f\end{aligned}$$

- The simplest path would be a straight line between the two values.



- Disadvantage: Discontinuous velocities at start and end points.

Cubic Polynomial

- To ensure that the velocities at the start and end points are zero, we can use a cubic polynomial:
- There are four parameters which can satisfy four constraints:

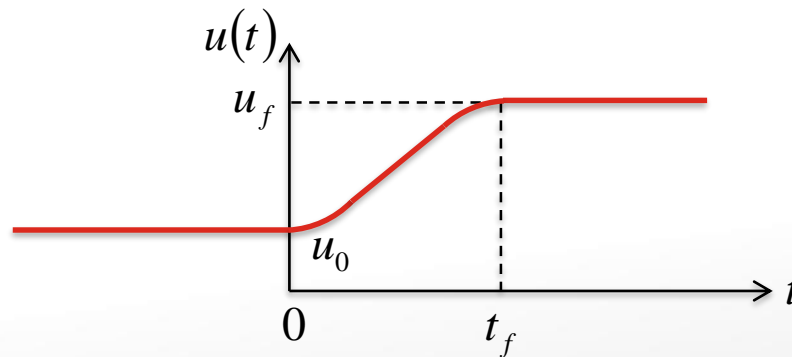
Cubic Polynomial

- To ensure that the velocities at the start and end points are zero, we can use a cubic polynomial:

$$u(t) = a_0 + a_1t + a_2t^2 + a_3t^3$$

- There are four parameters which can satisfy four constraints:

$$\begin{aligned} u(0) &= u_0 \\ u(t_f) &= u_f \\ \dot{u}(0) &= 0 \\ \dot{u}(t_f) &= 0 \end{aligned}$$



- The task is then to calculate the parameters a_0 , a_1 , a_2 and a_3 .

Cubic Polynomial

- This can be done by solving the following simultaneous equations:

$$u(0) = a_0 + a_1 \cdot 0 + a_2 \cdot 0^2 + a_3 \cdot 0^3 = u_0$$

$$\dot{u}(0) = a_1 + 2a_2 \cdot 0 + 3a_3 \cdot 0^2 = 0$$

$$u(t_f) = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3 = u_f$$

$$\dot{u}(t_f) = a_1 + 2a_2 t_f + 3a_3 t_f^2 = 0$$

- And the solution is:

$$a_0 = u_0$$

$$a_1 = 0$$

$$a_2 = \frac{3}{t_f^2} (u_f - u_0)$$

$$a_3 = -\frac{2}{t_f^3} (u_f - u_0)$$

Cubic Polynomial

- Example:

$$t_f = 3\text{sec}$$

$$u(0) = u_0 = 15\text{deg}$$

$$u(t_f) = u_f = 75\text{deg}$$

$$\dot{u}(0) = 0$$

$$\dot{u}(t_f) = 0$$

- The solution is:

$$a_0 = u_0 = 15$$

$$a_1 = 0$$

$$a_2 = \frac{3}{t_f^2}(u_f - u_0) = 20$$

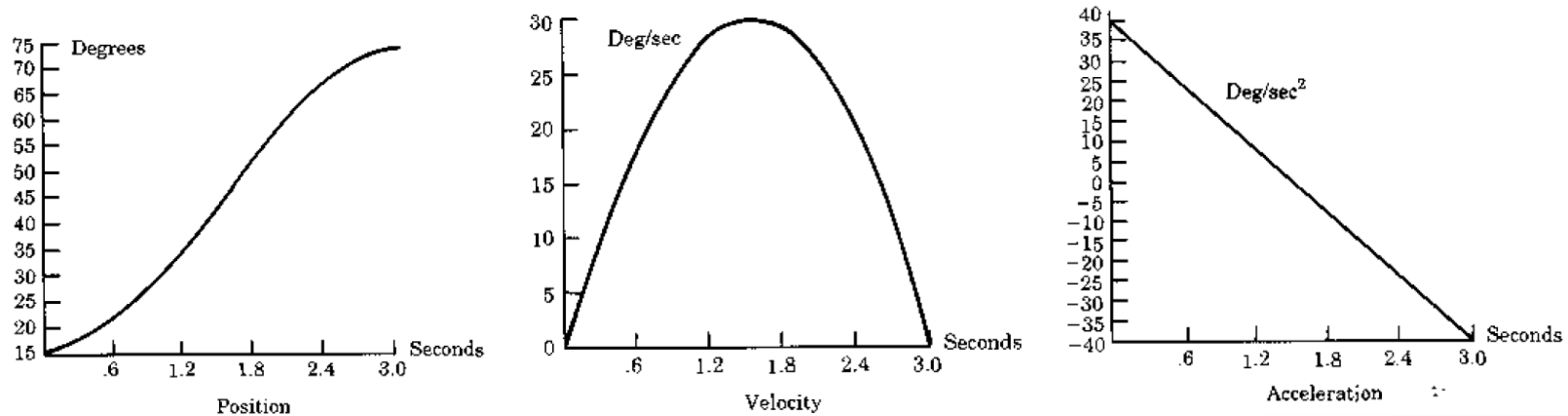
$$a_3 = -\frac{2}{t_f^3}(u_f - u_0) = -4.44$$

- Thus the trajectory is:

$$u(t) = 15 + 20t^2 - 4.44t^3$$

Cubic Polynomial

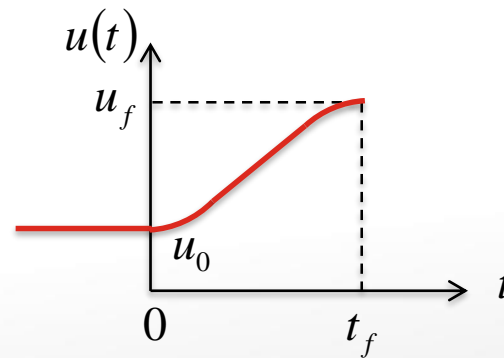
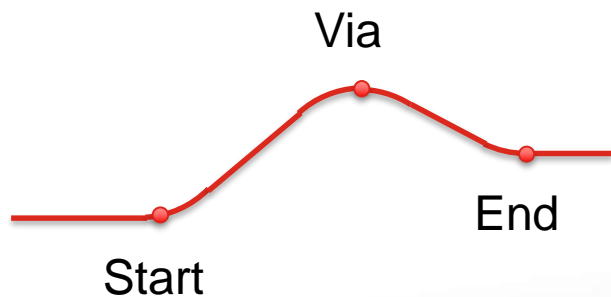
- The plots for position, velocity and acceleration are:



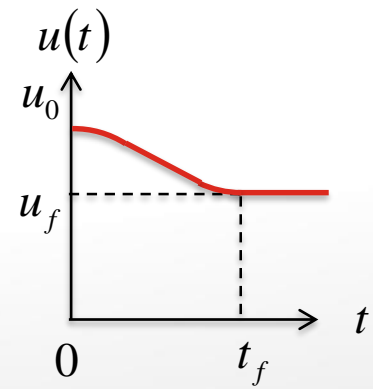
- Note that the **accelerations at start and end positions are not zero**.
 - This might create jerky motions.

Cubic Polynomial – Via Points

- We have looked at cubic polynomial connecting start and end point.
- What if we need the **path to pass through a via point**?
- Simple! Just split the path into **segments** (start to via point, via point to end) and derive cubic polynomial for each of them.



Segment 1



Segment 2

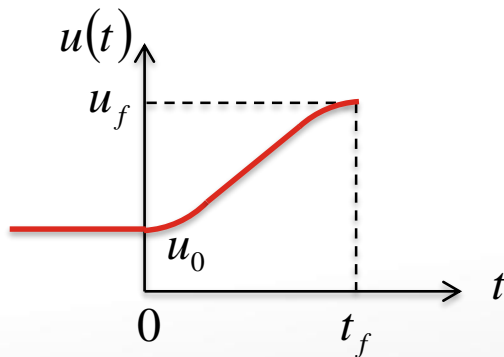
- However, the **velocity at via point** need not be zero:

Cubic Polynomial – Via Points

- For each segment, we will solve for a_0 , a_1 , a_2 and a_3 for the cubic polynomial

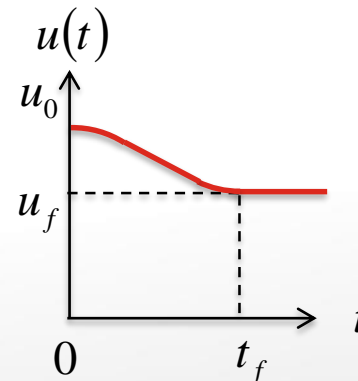
$$u(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

- Of course, the constraints will be different:



Segment 1

$$\begin{aligned} u(0) &= u_0 \\ u(t_f) &= u_{\text{via}} \\ \dot{u}(0) &= 0 \\ \dot{u}(t_f) &= \dot{u}_{\text{via}} \end{aligned}$$

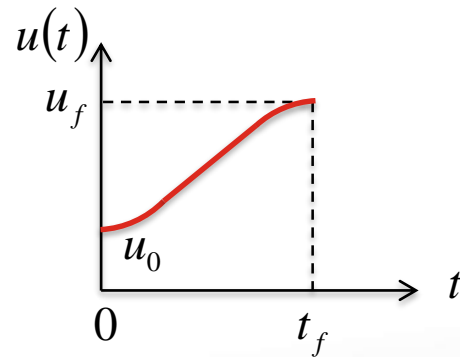


Segment 2

$$\begin{aligned} u(0) &= u_{\text{via}} \\ u(t_f) &= u_f \\ \dot{u}(0) &= \dot{u}_{\text{via}} \\ \dot{u}(t_f) &= 0 \end{aligned}$$

Cubic Polynomial – Via Points

- For an even more general case where we have **more than 1 via point**, we will do the same: Just split the path into many segments and solve the simultaneous solutions for each of the segments.
- The start and end velocities of the i^{th} segment need not be zero. Therefore:



Segment i

$$\begin{aligned}u(0) &= u_{\text{via}(i-1)} \\u(t_f) &= u_{\text{via}(i)} \\\dot{u}(0) &= \dot{u}_{\text{via}(i-1)} \\\dot{u}(t_f) &= \dot{u}_{\text{via}(i)}\end{aligned}$$

Cubic Polynomial

- The simultaneous equations to be solved are thus:

$$u(0) = a_0 + a_1 0 + a_2 0^2 + a_3 0^3 = u_{\text{via}(i-1)}$$

$$u(t_f) = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3 = u_{\text{via}(i)}$$

$$\dot{u}(0) = a_1 + 2a_2 0 + 3a_3 0^2 = \dot{u}_{\text{via}(i-1)}$$

$$\dot{u}(t_f) = a_1 + 2a_2 t_f + 3a_3 t_f^2 = \dot{u}_{\text{via}(i)}$$

By differentiation of

$$u(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

- And the solution is:

$$a_0 = u_{\text{via}(i-1)}$$

$$a_1 = \dot{u}_{\text{via}(i-1)}$$

$$a_2 = \frac{3}{t_f^2} (u_{\text{via}(i)} - u_{\text{via}(i-1)}) - \frac{2}{t_f} \dot{u}_{\text{via}(i-1)} - \frac{1}{t_f} \dot{u}_{\text{via}(i)}$$

$$a_3 = -\frac{2}{t_f^3} (u_{\text{via}(i)} - u_{\text{via}(i-1)}) + \frac{1}{t_f^2} (\dot{u}_{\text{via}(i)} - \dot{u}_{\text{via}(i-1)})$$

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Quintic Polynomial

- Using the cubic polynomial, we can only specify 4 constraints, because the cubic polynomial only has 4 parameters.
 - Start and end positions
 - Start and end velocities
- We had **no control over the accelerations**.
 - From the numerical example, we saw that the acceleration started and ended at 40 and -40 respectively.
- If we want to be able to **specify the start and end accelerations** as well (i.e. now altogether **6 constraints**), then we will need to use a **polynomial with 6 parameters** – The **Quintic Polynomial**.

$$u(t) = a_0 + a_1t + a_2t^2 + a_3t^3 + a_4t^4 + a_5t^5$$

Quintic Polynomial

- The constraints are:

$$u(0) = a_0 + a_1 0 + a_2 0^2 + a_3 0^3 + a_4 0^4 + a_5 0^5 = a_0$$

$$u(t_f) = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3 + a_4 t_f^4 + a_5 t_f^5$$

$$\dot{u}(0) = a_1 + 2a_2 0 + 3a_3 0^2 + 4a_4 0^3 + 5a_5 0^4 = a_1$$

$$\dot{u}(t_f) = a_1 + 2a_2 t_f + 3a_3 t_f^2 + 4a_4 t_f^3 + 5a_5 t_f^4$$

$$\ddot{u}(0) = 2a_2 + 6a_3 0 + 12a_4 0^2 + 20a_5 0^3 = 2a_2$$

$$\ddot{u}(t_f) = 2a_2 + 6a_3 t_f + 12a_4 t_f^2 + 20a_5 t_f^3$$

By differentiation of

$$u(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

By differentiation of

$$\dot{u}(t) = a_1 + 2a_2 t + 3a_3 t^2 + 4a_4 t^3 + 5a_5 t^4$$

Quintic Polynomial

- Solving the simultaneous equations, the parameters are:

$$a_0 = u_0$$

$$a_1 = \dot{u}_0$$

$$a_2 = \frac{\ddot{u}_0}{2}$$

$$a_3 = \frac{20u_f - 20u_0 - (8\dot{u}_f + 12\dot{u}_0)t_f - (3\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^3}$$

$$a_4 = \frac{30u_0 - 30u_f + (14\dot{u}_f + 16\dot{u}_0)t_f + (3\ddot{u}_0 - 2\ddot{u}_f)t_f^2}{2t_f^4}$$

$$a_5 = \frac{12u_f - 12u_0 - (6\dot{u}_f + 6\dot{u}_0)t_f - (\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^5}$$

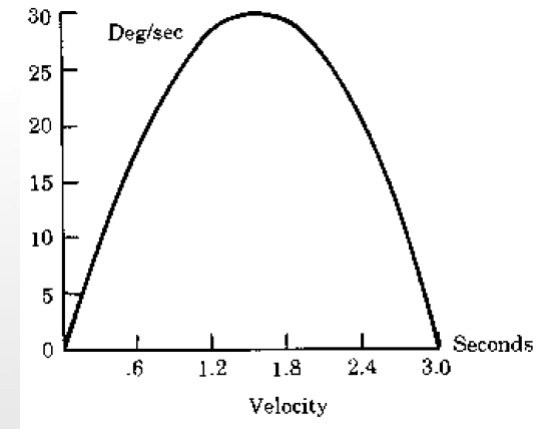
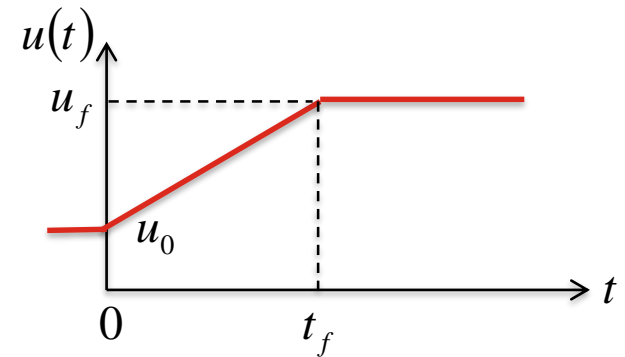
Note!

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- **Linear Function with Parabolic Blends**
- Matlab / Simulink Simulation

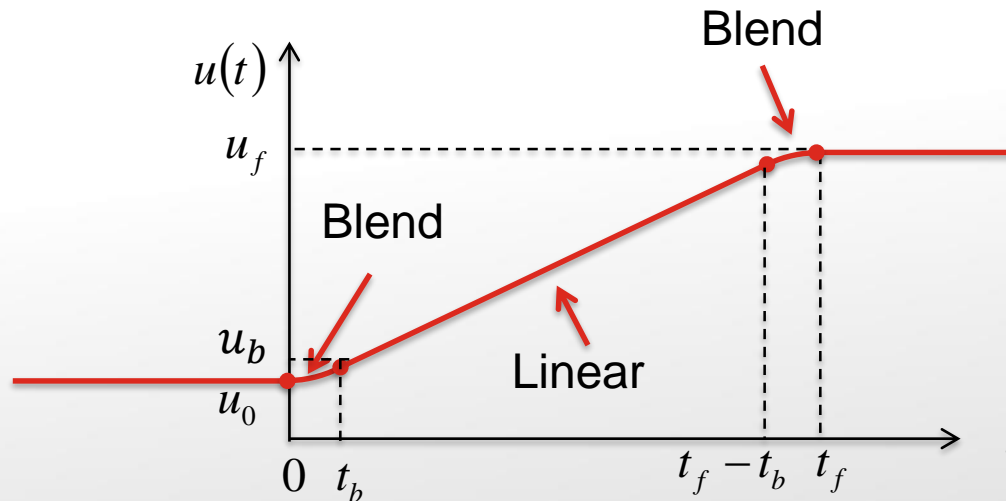
Linear Function w. Parabolic Blends

- The following summarizes the trajectories we have learnt so far:
 - Straight line:
 - Advantage: **Constant velocity** during motion.
 - Disadvantage: Discontinuous velocity at start and end points.
 - Polynomials:
 - Advantage: **Smooth motion**
 - Disadvantage: Velocity is not constant during motion.



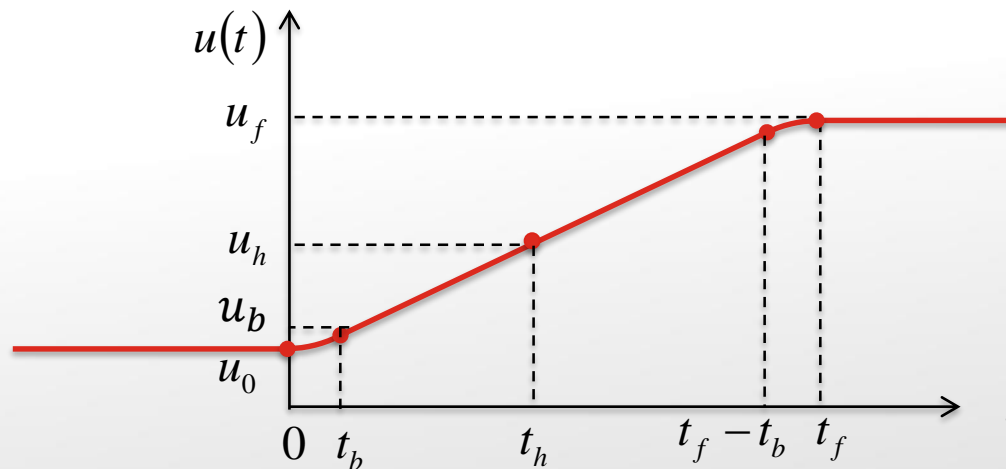
Linear Function w. Parabolic Blends

- Can we achieve:
 - Constant velocity during motion, **AND**
 - Smooth and continuous motion at the start and end points?
- Yes! We combine the ideas from the straight line and from the polynomial curves:
 - **Linear Function with Parabolic Blends**



Linear Function w. Parabolic Blends

- Assumptions / requirements:
 - Both the parabolic blends have the **same time duration**.
 - Therefore the same acceleration (apart from the sign) is used for both blends.
 - The solution is **symmetric** about the halfway point in time (t_h) and position (u_h).
 - The **velocity** at the end of blend region same as that of linear region.




- Question: how to get u_b and t_b ?

Linear Function w. Parabolic Blends

- The last requirement translates to the following equations:

- $$\ddot{u} \cdot t_b = \frac{u_h - u_b}{t_h - t_b}$$
 where \ddot{u} is the **constant acceleration** during blend region.

- Next, u_b is given by:
$$u_b = u_0 + \frac{1}{2} \ddot{u} \cdot t_b^2$$
- At the desired end point, the position is u_f and the time is t_f .
- Note that:
$$u_h = \frac{1}{2}(u_0 + u_f)$$
 and
$$t_h = \frac{1}{2}t_f$$
- Combining all above equations and eliminating u_b , we have:


$$\ddot{u} \cdot t_b^2 - \ddot{u} \cdot t_f \cdot t_b + (u_f - u_0) = 0$$

- Thus we can solve the above quadratic equation to get t_b .
- And then calculate u_b using
$$u_b = u_0 + \frac{1}{2} \ddot{u} \cdot t_b^2$$

Linear Function w. Parabolic Blends

- Summary:
- The **steps** in obtaining the linear function with parabolic blends are:

- Given u_0 , u_f and t_f .

- Choose desired acceleration \ddot{u} .

- Calculate t_b based on: $\ddot{u} \cdot t_b^2 - \ddot{u} \cdot t_f \cdot t_b + (u_f - u_0) = 0$

- i.e.

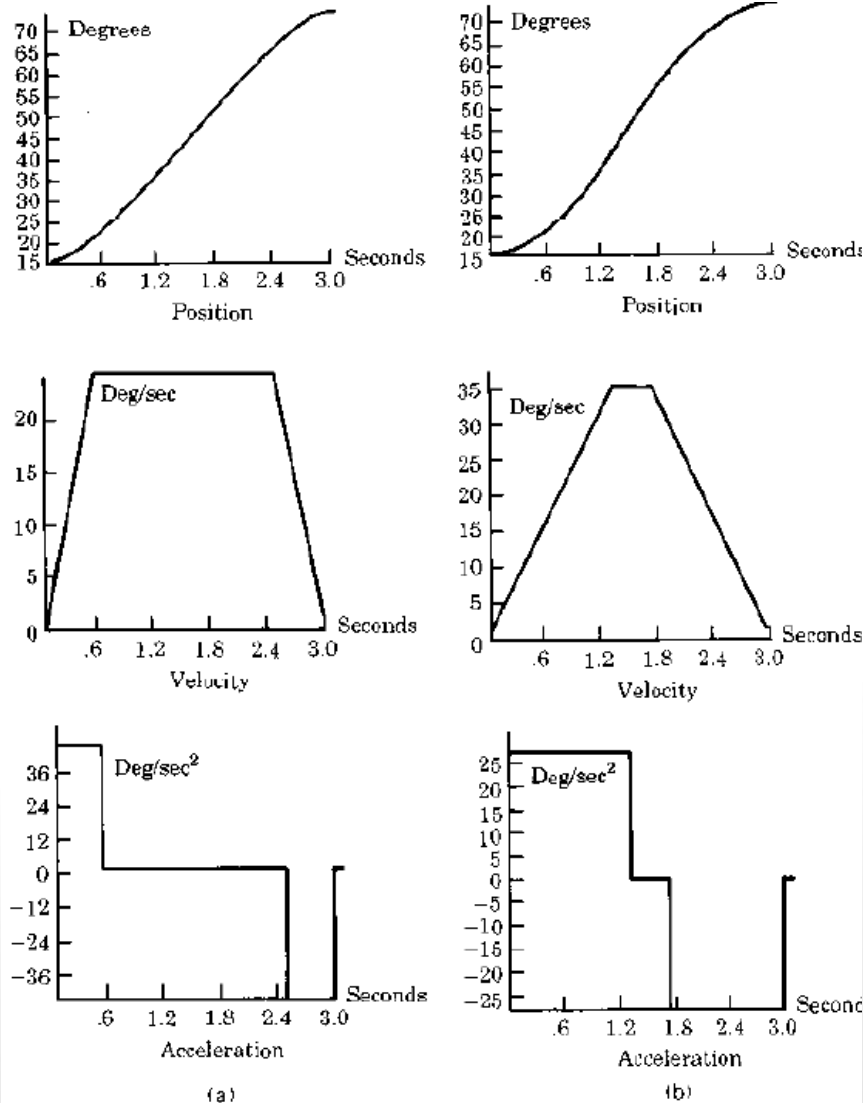
$$t_b = \frac{\ddot{u} t_f \pm \sqrt{\ddot{u}^2 t_f^2 - 4\ddot{u}(u_f - u_0)}}{2\ddot{u}}$$

Choose “minus” only
since t_b should be
less than $\frac{1}{2}t_f$

- Finally, calculate u_b based on:

$$u_b = u_0 + \frac{1}{2}\ddot{u} \cdot t_b^2$$

Linear Function w. Parabolic Blends



- Notes: **Acceleration must be chosen to be high enough.** Otherwise solution to t_b will not exist.
- E.g. if acceleration is small, the linear region shrinks.
- If acceleration is too small, there may be no more linear region.

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- **Matlab / Simulink Simulation**

Quintic Polynomial

- We will use Quintic Polynomial for the simulation:

$$u(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3 + a_4 t^4 + a_5 t^5$$

- The parameters are:

$$a_0 = u_0$$

$$a_1 = \dot{u}_0$$

$$a_2 = \frac{\ddot{u}_0}{2}$$

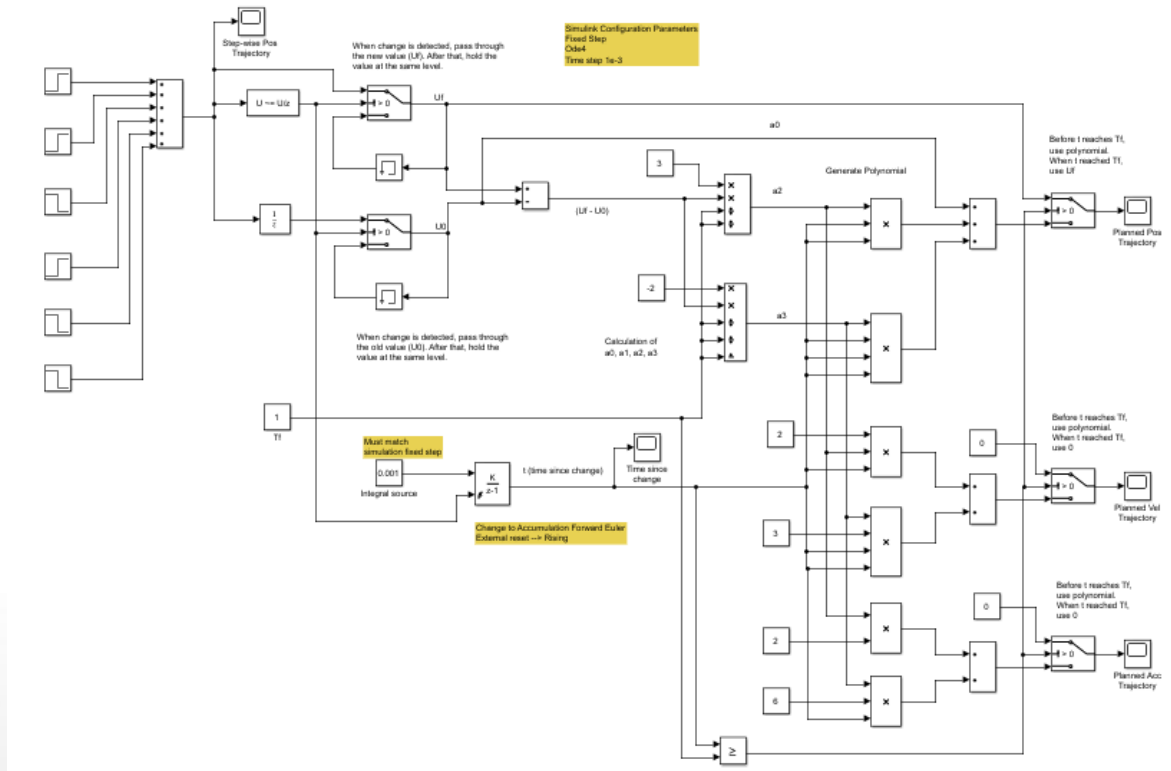
$$a_3 = \frac{20u_f - 20u_0 - (8\dot{u}_f + 12\dot{u}_0)t_f - (3\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^3}$$

$$a_4 = \frac{30u_0 - 30u_f + (14\dot{u}_f + 16\dot{u}_0)t_f + (3\ddot{u}_0 - 2\ddot{u}_f)t_f^2}{2t_f^4}$$

$$a_5 = \frac{12u_f - 12u_0 - (6\dot{u}_f + 6\dot{u}_0)t_f - (\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^5}$$

Quintic Polynomial

- This can be done in the following way:



- Please see attached Matlab Simulink file in Canvas.

Tutorial Assignments

- **Question 1:**

- A single-link robot with a rotary joint is motionless at $\theta = -5^\circ$. It is desired to move the joint in a smooth manner to $\theta = 80^\circ$ in 4 seconds.
- Find the coefficients of a cubic which accomplishes this motion and brings the arm to rest at the goal.
- Sketch the position, velocity and acceleration of the joint as a function of time.

Tutorial Assignments

- **Question 2:**

- A single-link robot with a rotary joint is motionless at $\theta = -5^\circ$. It is desired to move the joint in a smooth manner to $\theta = 80^\circ$ in 4 seconds and also stop smoothly.
- Find the corresponding parameters of a linear trajectory with parabolic blends.
- Sketch the position, velocity and acceleration of the joint as a function of time.

Tutorial Assignments

- **Question 3:**

- We wish to move a single joint from θ_0 to θ_f starting from rest, ending at rest, in time t_f .
- The values of θ_0 to θ_f are given, but we wish to compute t_f so that the velocity never exceeds a maximum value ($\dot{\theta}$ max), and the acceleration never exceeds a maximum value ($\ddot{\theta}$ max).
- Use a single cubic segment, and give an expression for t_f and for the cubic's coefficients.

Thank you!

Have a good evening.

