RMIT Classification: Trusted

Content

- Introduction
- Cartesian Space Schemes vs. Joint Space Schemes
- Cubic Polynomial
- Quintic Polynomial
- Linear Function with Parabolic Blends
- Matlab / Simulink Simulation



Quintic Polynomial -> smooth accelerations

- Using the cubic polynomial, we can only specify 4 constraints, because the cubic polynomial only has 4 parameters.
 - Start and end positions
 - Start and end velocities
- We had no control over the accelerations.
 - From the numerical example, we saw that the acceleration started and ended at 40 and -40 respectively.

0

If we want to be able to specify the start and end accelerations as well (i.e. now altogether 6 constraints), then we will need to use a polynomial with 6 parameters – The Quintic Polynomial.



The constraints are:

$$u(0) = a_0 + a_1 0 + a_2 0^2 + a_3 0^3 + a_4 0^4 + a_5 0^5 = a_0$$

$$u(t_f) = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3 + a_4 t_f^4 + a_5 t_f^5$$

$$\dot{u}(0) = a_1 + 2a_2 0 + 3a_3 0^2 + 4a_4 0^3 + 5a_5 0^4 = a_1$$

$$\dot{u}(t_f) = a_1 + 2a_2t_f + 3a_3t_f^2 + 4a_4t_f^3 + 5a_5t_f^4$$

$$\ddot{u}(0) = 2a_2 + 6a_30 + 12a_40^2 + 20a_50^3 = 2a_2$$

$$\ddot{u}(t_f) = 2a_2 + 6a_3t_f + 12a_4t_f^2 + 20a_5t_f^3$$

By differentiation of

$$u(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

By differentiation of

$$\dot{u}(t) = a_1 + 2a_2t + 3a_3t^2 + 4a_4t^3 + 5a_5t^4$$



Solving the simultaneous equations, the parameters are:

$$\Rightarrow a_0 = u_0 \qquad a_1 = \dot{u}_0 \qquad a_2 = \frac{\ddot{u}_0}{2} = 0$$

$$\Rightarrow a_3 = \frac{20u_f - 20u_0 - (8\dot{u}_f + 12\dot{u}_0)t_f - (3\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^3} = \frac{10}{4} \quad (U_f - U_0)$$

$$\Rightarrow a_4 = \frac{30u_0 - 30u_f + (14\dot{u}_f + 16\dot{u}_0)t_f + (3\ddot{u}_0 - 2\ddot{u}_f)t_f^2}{2t_0^4} = -\frac{15}{4} \quad (U_f - U_0)$$

Note!
$$a_{5} = \frac{12u_{f} - 12u_{0} - (6\dot{u}_{f} + 6\dot{u}_{0})t_{f} - (\ddot{u}_{0} - \ddot{u}_{f})t_{f}^{2}}{2t_{f}^{5}}$$



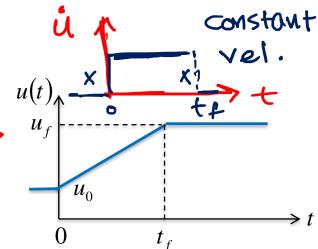
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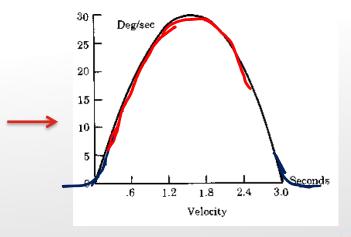
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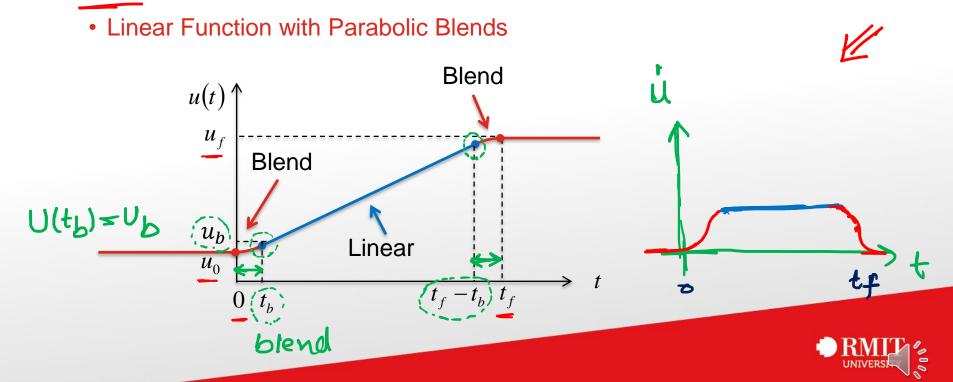
- The following summarizes the trajectories we have learnt so far:
 - Straight line:
 - Advantage: Constant velocity during motion.
 - Disadvantage: Discontinuous velocity at start and end points.
 - Polynomials:
 - Advantage: Smooth motion
 - Disadvantage: Velocity is not constant during motion.



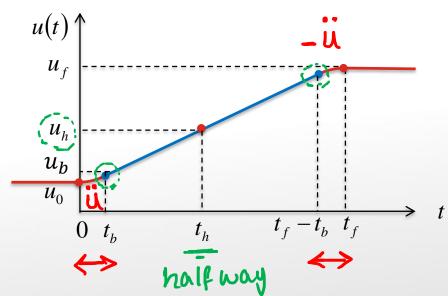




- Can we achieve:
- Constant velocity during motion, AND
- Smooth and continuous motion at the start and end points?
 - Yes! We combine the ideas from the straight line and from the polynomial curves:



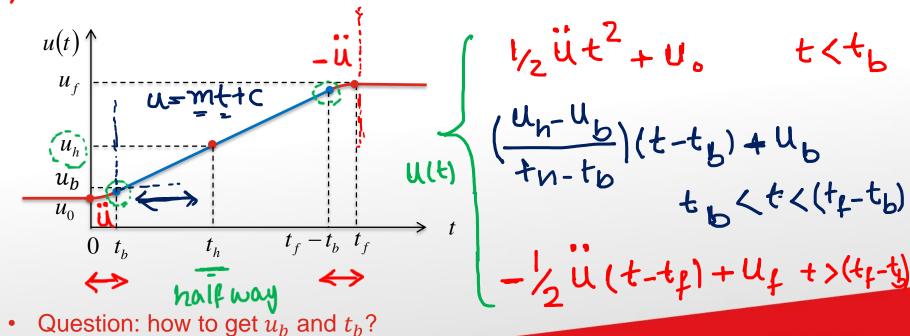
- Assumptions / requirements:
- Both the parabolic blends have the same time duration.
 - Therefore the same acceleration (apart from the sign) for both blends.
- \rightarrow The solution is symmetric about the halfway point in time (t_h) and position (u_h) .
- The velocity at the end of blend region same as that of linear region.



• Question: how to get u_b and t_b ?



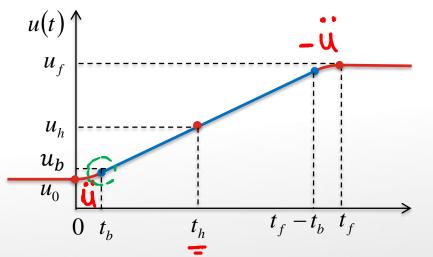
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- Assumptions / requirements:
 - Both the parabolic blends have the same time duration.
- 1

- Therefore the same acceleration (apart from the sign) for both blends.
- 2
- The solution is symmetric about the halfway point in time (t_h) and position (u_h).
- 3
- The velocity at the end of blend region same as that of linear region.



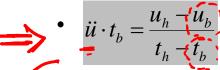
$$\frac{u_{h}-u_{b}}{u_{h}-t_{b}}$$

• Question: how to get u_b and t_b ?

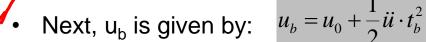




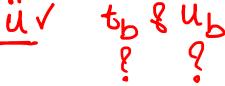
The last requirement translates to the following equations:



• $u \cdot t_b = \frac{u_h - u_b}{t_h - t_b}$ where u is the constant acceleration during blend region.



$$u_b = u_0 + \frac{1}{2}\ddot{u} \cdot t_b^2$$

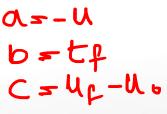


- At the desired end point, the position is u_f and the time is t_f .

Note that: $u_h = \frac{1}{2}(u_0 + u_f)$ and $t_h = \frac{1}{2}t_f$

$$t_h = \frac{1}{2}t_f$$

Combining all above equations and eliminating u_b, we have:





$$\ddot{u} \cdot t_b^2 - \ddot{u} \cdot t_f \cdot t_b + \left(u_f - u_0\right) = 0$$

$$\frac{tb}{2} = -b \pm \sqrt{b^2 - 400}$$

- Thus we can solve the above quadratic equation to get t_h .
- And then calculate u_b using $u_b = u_0 + \frac{1}{2}\ddot{u} \cdot t_b^2$

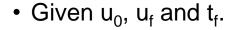
$$u_b = u_0 + \frac{1}{2}\ddot{u} \cdot t_b^2$$





- Summary:
- The steps in obtaining the linear function with parabolic blends are:







• Choose desired acceleration (ii.)



• Calculate
$$t_b$$
 based on: $\ddot{u} \cdot t_b^2 - \ddot{u} \cdot t_f \cdot t_b + (u_f - u_0) = 0$

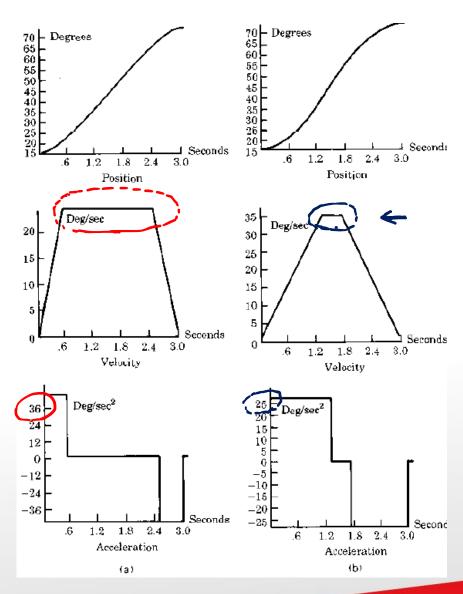
• i.e.
$$t_b = \frac{\ddot{u}t_f - 4\ddot{u}(u_f - u_0)}{2\ddot{u}}$$

Finally, calculate u_b based on:

$$t_b \longrightarrow u_b = u_0 + \frac{1}{2} \ddot{u} \cdot t_b^2$$

Choose "minus" only since t_b should be less than $\frac{1}{2}t_f$

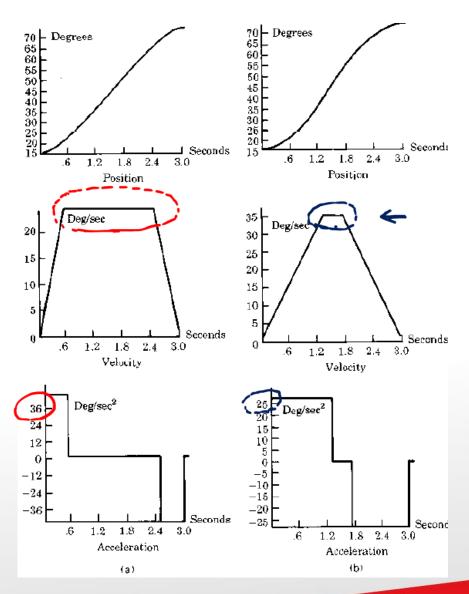




- Notes: Acceleration must be chosen to be high enough.
 Otherwise solution to t_b will not exist.
- E.g. if acceleration is small, the linear region shrinks.
- If acceleration is too small, there may be no more linear region.







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We will use Quintic Polynomial for the simulation:

$$u(t) = a_0 + a_1t + a_2t^2 + a_3t^3 + a_4t^4 + a_5t^5$$

The parameters are:

$$a_0 = u_0$$

$$a_1 = \dot{u}_0$$

$$a_2 = \frac{\ddot{u}_0}{2}$$

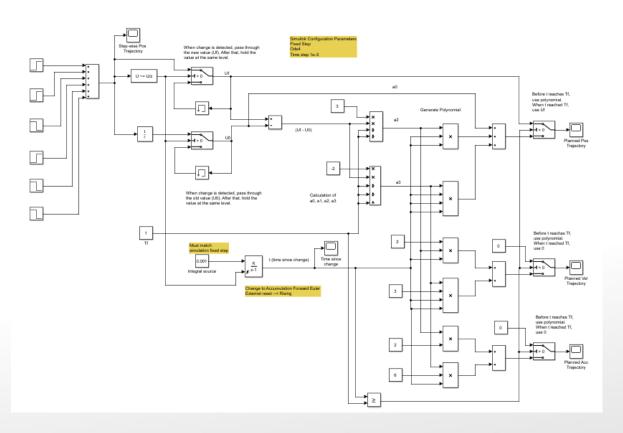
$$a_3 = \frac{20u_f - 20u_0 - (8\dot{u}_f + 12\dot{u}_0)t_f - (3\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^3}$$

$$a_4 = \frac{30u_0 - 30u_f + (14\dot{u}_f + 16\dot{u}_0)t_f + (3\ddot{u}_0 - 2\ddot{u}_f)t_f^2}{2t_f^4}$$

$$a_5 = \frac{12u_f - 12u_0 - (6\dot{u}_f + 6\dot{u}_0)t_f - (\ddot{u}_0 - \ddot{u}_f)t_f^2}{2t_f^5}$$



This can be done in the following way:



· Please see attached Matlab Simulink file in Canvas.



Thank you!

Have a good evening.

