Metadata of the chapter that will be visualized online

Chapter Title	Physical Networks' Approach in Train and Tram Systems' Investigation		
Copyright Year	2016 Springer International Publishing Switzerland		
Copyright Holder			
Corresponding Author	Family Name	Simic	
	Particle		
	Given Name	Milan	
	Suffix		
	Division	School of Aerospace, Mechanical and Manufacturing Engineering (SAMME)	
	Organization	RMIT University	
	Address	Bundoora East Campus, Plenty Road, Bundoora, Melbourne, VIC, 3083, Australia	
	Email	milan.simic@rmit.edu.au	
Abstract	systems that perform tranonlinearities, there are railroad characteristics? we have historical or I there are state-of-the-are extremely high ground and safety are the prima design. Global physical in this investigation. Pleanergy are studied, more this modeling application.	Large vehicles on rail networks are complex, nonlinear, engineering systems that perform translator motion. Apart from system components' nonlinearities, there are environmental influences as well, through railroad characteristics' changes on the long routes. On the one side, we have historical or legacy systems, still in place, and on the other, there are state-of-the-art train compositions that are capable of achieving extremely high ground speeds of transportation. In both cases reliability and safety are the primary objectives in system maintenance and system design. Global physical networks approach is presented here, and applied in this investigation. Physical quantities like speed, force, power, and energy are studied, monitored, and presented. The main contribution of this modeling application is in its capability to obtain various data from any part of the system which could be used for the improvement of	
Keywords (separated by "-")	Physical network - Network elements - Train - Tram - Composition - Rail network - Traffic safety - System reliability		

Chapter 4 Physical Networks' Approach in Train and Tram Systems' Investigation

Milan Simic

2

19

Abstract Large vehicles on rail networks are complex, nonlinear, engineering systems that perform translator motion. Apart from system components' nonlinearities, 6 there are environmental influences as well, through railroad characteristics' changes 7 on the long routes. On the one side, we have historical or legacy systems, still 8 in place, and on the other, there are state-of-the-art train compositions that are 9 capable of achieving extremely high ground speeds of transportation. In both cases 10 reliability and safety are the primary objectives in system maintenance and system 11 design. Global physical networks approach is presented here, and applied in this 12 investigation. Physical quantities like speed, force, power, and energy are studied, 13 monitored, and presented. The main contribution of this modeling application is in 14 its capability to obtain various data from any part of the system which could be used 15 for the improvement of overall system safety and reliability.

Keywords Physical network • Network elements • Train • Tram • Composition 17 • Rail network • Traffic safety • System reliability 18

4.1 Introduction

We could easily say that the train is among the longest, mobile, mechanical 20 engineering systems that humans can build, nowadays. Train compositions, that 21 can stretch few kilometers, usually have distributed power units, i.e., locomotive 22 engines positioned in front of, between wagons, and behind them. Such long and 23 heavy transportation systems express nonlinearities of different types. That also 24 depends heavily on the environment conditions. For example, friction between the 25 rails and the wheels is changing drastically when the weather changes from the 26 very dry and sunny conditions to heavy rain, or snow and ice on the rails. Those 27 conditions are extremely important for the acceleration and braking, having in 28 mind that we perform motion control of the overall mass of few 10⁷ kg. There are 29

AQ2 M. Simic (⋈)

School of Aerospace, Mechanical and Manufacturing Engineering (SAMME), RMIT University, Bundoora East Campus, Plenty Road, Bundoora, Melbourne, VIC 3083, Australia e-mail: milan.simic@rmit.edu.au

AQ1

[©] Springer International Publishing Switzerland 2016 R.N. Jazar, L. Dai (eds.), *Nonlinear Approaches in Engineering Applications*, DOI 10.1007/978-3-319-27055-5_4

42

68

various mathematical models and simulations used in the systems' study and design 30 (Durica 2015; A mathematical model for a train run). In various large and complex, 31 nonlinear, engineering systems investigation, physical networks approach is one of 32 the valuable tools adapted and already presented (Simic 2015). Application area 33 is now extended and results are presented here. Velocities, forces, displacements, power, and energy have been monitored.

Initially, a physical networks' model of a single wagon is created taking in 36 consideration the mass of the vehicle together with the stiffness and friction 37 components of the interfacing elements between wagons and with the rails. Starting 38 from that basic model, the whole train composition model, as a large network, is set 39 up and simulations performed. Any physical quantity can easily be monitored and 40 displayed. This gives valuable information on the subsystems and system design.

Physical Networks Approach in Modeling 4.2

Physical network is a geometrical structure of interconnected ideal network ele- 43 ments, with two connection points. Network elements represent mathematical 44 relationships between two dependent system variables in the physical system. 45 Engineering systems are built using various sets of elements, specific for the system 46 type. Basic definitions, principles, and rules for solving equations represented by a 47 network are independent of physical system which that network is representing.

Energy through the system is transferred and transformed using two types of 49 system variables. Flow, f, type system variables are representing physical quantities 50 that are traveling *through* the systems elements, and their connections. *Potential*, p, 51 type variables are expressing the state established across the system elements and 52 between any two network points, i.e., nodes. Potential of a point in the network is a 53 relative quantity and depends on the reference point chosen. For example, speed is 54 relative, as we know, and depends on the reference.

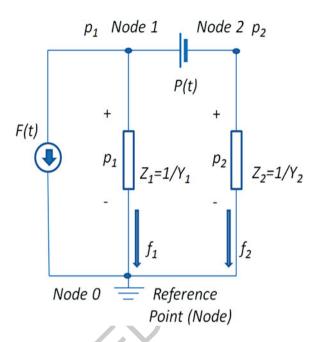
A simple physical network example is shown in Fig. 4.1. Looking from the 56 energy point of view, there are passive and active network elements in each network. 57 Generic name for any passive element is impedance, Z, or admittance, Y, where 58 Z = I/Y. Active elements, or energy suppliers to the system, are ideal flow and 59 potential sources, as well as initial conditions expressed as initial values of the flow 60 through, and potential across network elements.

Ideal flow source, shown as F(t) in Fig. 4.1, has infinite internal resistance, called 62 impedance, Z_{in} , Z_{in} -> ∞ while ideal potential source, P(t), has zero value of the 63 internal impedance, $Z_{in} = 0$. Flows through branches are shown, and labeled as f_1 64 and f_2 , while the node potentials are marked as p_1 and p_2 . In any physical network, 65 product of instant values of two network variables, flow f(t) and potential p(t), is 66 giving the value of the instant power p(t), that particular network element dissipates 67 or stores, as given by Eq. (4.1).

$$p(t) = f(t) * p(t) \tag{4.1}$$

4 Physical Networks' Approach in Train and Tram Systems' Investigation

Fig. 4.1 Generic physical network diagram: Ideal flow source is labeled as F(t), while ideal potential source is labeled as P(t)



The unity of the nature is expressed in the extraordinary analogies of the 69 differential equations used to represent various physical phenomena. The same 70 type of equations, ordinary differential equations (ODE), is used for the study of 71 mechanical systems with translation, mechanical systems with rotation, hydrody-72 namics, and for the electrical circuits. The theory of turbulence in liquids and the 73 theory of friction in gases show great similarities with the electromagnetic theory. 74 Network elements represent mathematical relationships between two dependent 75 system variables in a physical system. There are three types of relationships: 76 proportionality, differentiation, and integration. For example, in an electrical circuit 77 those basic elements are resistor, capacitor, and the coil. Often, real systems are 78 extremely complex, but they can be simplified, or they may have linear subsystems 79 as their integral parts.

Examples of physical variables in an electric circuit are *electrical current*, as a 81 *through variable*, and *electrical potential*, as an *across variable*. Current, i, through 82 electrical conductors, or a network element, is directly related to the *mechanical* 83 flow of electrons, i.e., charge, dq, over time dt, as per Eq. (4.2). 84

$$i = \frac{dq}{dt} \tag{4.2}$$

The charge of a single electron is $e = -1.602 \times 10^{-19}$ coulomb. Following that, the 85 current of *IA* corresponds to the flow of 6.241509×10^{18} electrons per second. 86

Electrical potential, V_C , for example, is related to the number of accumulated 87 electrons, on capacitor C, plates, as given by Eq. (4.3), 88

$$V_C = \frac{1}{C} \int_0^T i dt = \frac{1}{C} \int_0^T \frac{dq}{dt} dt = \frac{Q(T)}{C}; \quad \text{if } Q(0) = 0$$
 (4.3)

where Q(T) refers to the accumulated charge over the period T and initial charge 89 on the capacitor plates, for t=0, was 0 *coulomb*. Potential difference between two 90 nodes is called voltage. The universal reference point, in electric circuits, is ground 91 potential of 0 V.

We have *force* and *velocity* as network variables in a mechanical system with translation, or *torque* and *angular speed* in a mechanical system with rotation. In a hydraulic system we have *flow* and *pressure*.

ODE with constant coefficients, A_i , i = 0 - n, are used for modeling various 96 physical systems. An ODE, shown by Eq. (4.4), is a relation between two variables: 97 independent variable t and dependent y = y(t), and the derivatives of y as follows 98 $\frac{dy}{dt}$, $\frac{d^2y}{dt^2}$, ..., $\frac{d^ny}{dt^n}$. 99

$$A_n \frac{d^n y}{dt^n} + A_{n-1} \frac{d^{n-1} y}{dt^{n-1}} + \dots + A_1 \frac{dy}{dt} + A_0 y = f(t)$$
 (4.4)

On the right-hand side, we can have any function of time, f(t). The special case when f(t) = 0 is known as homogenous equation. Equation (4.4) is called ordinary because only one independent variable exists, which is usually time. It is linear because only the first exponent of dependent variable, or its derivatives, is present in the expression. Examples of network components in a generic physical network, then in an electrical circuit, mechanical system with translation and mechanical system with rotation, are given in Table 4.1. Equations for the stored energy and power losses are also presented.

In a generic physical system, integration, proportion, and differentiation of 108 network variables are associated with elements labeled as A, B, and C. The general 109 name for all of them is impedance, Z, or admittance Y, as already shown in Fig. 4.1. 110 In an electrical circuit we have inductivity, L, conductivity G, i.e., resistivity, 111 R = 1/G, and capacity C. Finally for the translation we have k for stiffness, B for 112 friction, and M for mass of the object. Translator network variables are force, F, 113 and velocity V. There are also other physical systems like thermal and fluids where 114 analogies could easily be established, as given in (de Silva 2005 and Sanford 1965). 115

4.3 Mechanical System with Translation: Basic Model

Let us consider a mechanical system with translation. Two approaches in modeling of a basic network, which includes all three passive network elements and a power source, are presented here. Passive network elements are mass, *m*, expressing 119

4 Physical Networks' Approach in Train and Tram Systems' Investigation

DescriptionPrototypeElectricalTranslationThrough variable $Flow - f$ $Current - i$ $Force - F$ Across variable $Potential - p$ $Voltage - u$ $Velocity - v$ ElementGenericInductivity LStiffness k Element $f = A \int pdt$ $\frac{L^2}{L}$ Stiffness k Accumulated $\frac{L^2}{L^4}$ $\frac{L^2}{L}$ $\frac{L^2}{L}$ Accumulated $\frac{L^2}{L^4}$ $\frac{L^2}{L}$ $\frac{L^2}{L}$ BenentGeneric element B Conductivity $G/Resistivity$ R Damping constant B Power dissipation $fp = \frac{L^2}{R} = p^2B$ $iu = i^2R = \frac{u^2}{R}$ $F = Bv$ Power dissipation $fp = \frac{L^2}{R} = p^2B$ $iu = i^2R = \frac{u^2}{R}$ $F = Bv$ Accumulated $f = C\frac{dp}{dt}$ $f = C\frac{dp}{dt}$ $f = C\frac{dp}{dt}$ Accumulated $\frac{Cp^2}{2}$ $\frac{Cq^2}{2}$ $\frac{mu^2}{2}$		Table 4.1 Various physical network components	network components			
Through variable $Flow - f$ $Current - i$ $Force - F$ Across variable $Potential - p$ $Voltage - u$ $Velocity - v$ $Element$ $Generic Element A$ $i = \frac{1}{L} \int u dt$ $F = k \int v dt$ $F = k \int v dt$ Accumulated $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2}$		Description	Prototype	Electrical	Translation	Rotation
Across variable $Potential - p$ $Voltage - u$ $Velocity - v$ $Element$ $Generic$ Inductivity L $Element$ $f = A \int p dt$ $I = \frac{1}{L} \int u dt$ $I = \frac{1}{L}$	t3.1	Through variable	Flow - f	Current - i	Force - F	Torque, or Momentum - M
Element Generic Inductivity L Stiffness k integration $f = A \int p dt$ $f = A \int p dt$ $f = A \int p dt$ Accumulated $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ $\frac{L^2}{2A}$ energy Generic element B Conductivity G/Resistivity A Damping constant B proportion $A = A \cap A \cap A$ $A \cap \cap A$ A	t3.2	Across variable	Potential - p	Volage - u		Angular Velocity - w
Accumulated $\frac{f^2}{2A}$ Accumulated $\frac{f^2}{2A}$ Bower dissipation $f = Bp$ $f = Bp$ $f = Bp$ Element $f = Bp$ Power dissipation $f = \frac{f^2}{R} = p^2B$ $f = \frac{u^2}{R}$ Element $f = Bp$ Benefit $f = Bp$ For example $f = Bp$ For example $f = Bp$ Element $f = Bp$ For example $f = Bp$ Element $f = Bp$ For example $f = Bp$ Element $f = Bp$ Ele	t3.3	Element integration	Generic Element A		Stiffness k $E = k \int v_1 dt$	Rotational Stiffness <i>k</i>
Accumulated $\frac{L^2}{2A}$ $\frac{\mu^2}{2}$ $\frac{\mu^2}{2}$ $\frac{\mu^2}{2}$ energyGeneric element B Conductivity G /Resistivity R Damping constant B Element $f = Bp$ $i = Gu = \frac{1}{R}u$ $F = Bv$ Power dissipation $fp = \frac{L^2}{B} = p^2B$ $iu = i^2R = \frac{u^2}{R}$ $Fv = \frac{E^2}{B} = v^2B$ ElementGeneric element C Capacity C Mass m differentiation $f = C\frac{du}{dt}$ $F = m\frac{du}{dt}$ Accumulated $\frac{Cp^2}{2}$ $\frac{Ca^2}{2}$ $\frac{Ca^2}{2}$			$f = A \int p dt$			$M = k \int w dt$
Element Generic element B Conductivity G/Resistivity R Damping constant B $i = Gu = \frac{1}{R}u$ Damping constant B Figuration $fp = \frac{L^2}{R} = p^2B$ $iu = i^2R = \frac{u^2}{R}$ Fower dissipation $fp = \frac{L^2}{R} = p^2B$ $iu = i^2R = \frac{u^2}{R}$ Mass m Generic element C Capacity C	t3.4	Accumulated energy	$\frac{f^2}{2A}$	\frac{1}{2}	$\frac{F^2}{2k} = k\frac{x^2}{2}$ $x = \text{distance}$	$\frac{M^2}{2k}$
proportion $f = Bp$ $i = Gu = \frac{1}{R}u$ Damping constant B Power dissipation $fp = \frac{L^2}{B} = p^2B$ $iu = i^2R = \frac{\mu^2}{R}$ $Fv = \frac{F^2}{B} = v^2B$ ElementGeneric element C Capacity C Mass m differentiation $f = C\frac{dv}{dt}$ $f = C\frac{dw}{dt}$ $f = m\frac{dw}{dt}$ Accumulated $\frac{Cp^2}{2}$ $\frac{Car^2}{2}$ $\frac{mv^2}{2}$	t3.5	Element	Generic element B	Conductivity G/Resistivity R		Angular
Power dissipation $fp = \frac{L^2}{B} = p^2 B$ $iu = i^2 R = \frac{\mu^2}{R}$ $Fv = \frac{F^2}{B} = v^2 B$ ElementGeneric element C Capacity C Mass m differentiation $f = C\frac{dv}{dt}$ $F = m\frac{dv}{dt}$ Accumulated $\frac{Cp^2}{2}$ $\frac{Car^2}{2}$ $\frac{mv^2}{2}$		proportion	f = Bp	$i = Gu = \frac{1}{R}u$	Damping constant B F = Bv	damping D $M = Dw$
Element Generic element C Capacity C Mass m differentiation $f = C \frac{dp}{dt}$ $i = C \frac{du}{dt}$ $F = m \frac{dv}{dt}$ Accumulated $\frac{Cp^2}{2}$ $\frac{Ca^2}{2}$ $\frac{mv^2}{2}$	t3.6	Power dissipation	$fp = \frac{f^2}{B} = p^2 B$		$Fv = \frac{F^2}{B} = v^2 B$	$Mw = \frac{M^2}{D} = w^2 D$
Accumulated $\frac{Cp^2}{2}$ $\frac{Cd^2}{2}$ $\frac{mv^2}{2}$ energy	t3.7	Element differentiation	Generic element C $f = C \frac{dp}{dt}$			Moment of Inertia $F = M \frac{dw}{dw}$
	t3.8	Accumulated energy	$\frac{Cp^2}{2}$	$\frac{Gu^2}{2}$	2	$\frac{Mw^2}{2}$

128

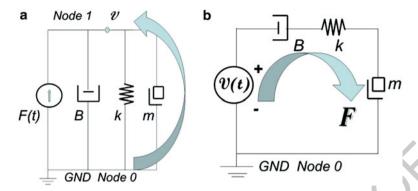


Fig. 4.2 (a) Basic mechanical network model with ideal force power source F(t). (b) Basic mechanical network model with ideal velocity power source V(t)

inertia, spring element with its stiffness, k, and damping element, B. Active 120 elements, presented here, are an ideal force source, F(t), as shown in the first layout, 121 Fig. 4.2a, and an ideal velocity source, V(t), as shown in the second layout, Fig. 4.2b. 122 Basic translational motion mechanical network with ideal force source F(t) can 123 be expressed with Eq. (4.5), i.e., Eq. (4.6) as follows:

$$Bv + m\frac{dv}{dt} + k \int v dt = F \tag{4.5}$$

or in an operator form

$$\left(B + m\frac{d}{dt} + k\int dt\right)v = F \tag{4.6}$$

On the other side, basic translational motion mechanical network with ideal 126 velocity source V(t) can be expressed with Eq. (4.7), i.e., Eq. (4.8) as follows: 127

$$\frac{F}{B} + \frac{1}{k}\frac{dF}{dt} + \frac{1}{m}\int Fdt = v \tag{4.7}$$

or in an operator form

$$\left(\frac{1}{B} + \frac{1}{k}\frac{d}{dt} + \frac{1}{m}\int dt\right)F = v \tag{4.8}$$

In Fig. 4.2a the same velocity, v, is measured across all network elements as 129 it is an *across variable*. Since there are no initial condition shown, the sum of 130 forces through passive elements equals the force supplied by ideal force source 131 F(t). Analogue story is for the network shown in Fig. 4.2b, where the same force 132

is measured through all network elements. In this case the sum of all velocities 133 measured across all passive elements equals to the velocity supplied by the ideal 134 velocity source V(t).

4.4 Modeling a Single Wagon

We will now consider a single wagon model. Vehicle has four pairs of wheels 137 that support the body by springs and dry friction dampers. A wagon is shown in 138 Figs. 4.3a and 4.4, while connection interface can be seen from Fig. 4.3b. Initial 139 model design would include basic sub-networks as already shown in Fig. 4.2a, just 140 without force power source component. We have eight sub-models, each with all 141 three basic network elements. Since the velocity is same, in the node 1, we can 142 use equivalent representation. Following that, in the next step of modeling we will 143 represent the system with just two support points which very much correspond to 144 the mechanical design. The system is nonlinear and multidimensional, but motion 145 and vibrations along other axes might be subject of another investigation, since we 146 now just consider the motion along the line connecting two points on the railroad. 147 We will neglect gravitational stiffness since we will consider just one dimensional 148 problem of translation along x axis.





Fig. 4.3 (a) A single wagon as an example for basic tram/train elements modeling; (b) Connection interface that will be modeled as a spring

this figure will be printed in b/w

this figure will be printed in b/w

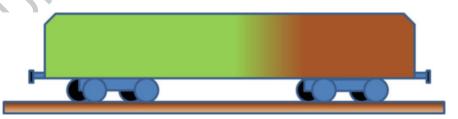


Fig. 4.4 A standard wagon with four sets of wheels

136

149

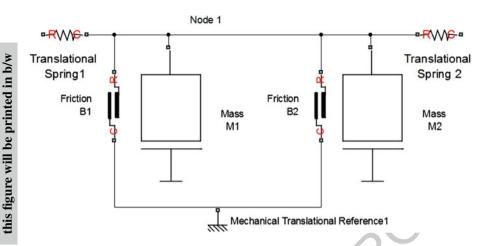


Fig. 4.5 A Simulink model of a single wagon with 2 support points and connection interface

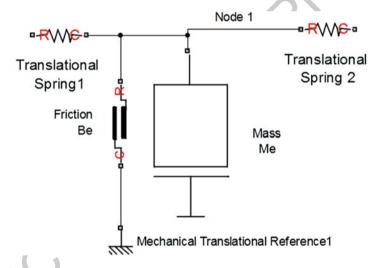


Fig. 4.6 Final Simulink model of a single wagon with connection interface

Two support points model designed in Simulink is shown in Fig. 4.5. Connection 150 interface is presented by translational springs. Further simplification of the model is 151 shown in Fig. 4.6. Once again, since the velocity in the node 1 is applied *across* all 152 network elements we can represent the network from Fig. 4.5 with the equivalent 153 one given in Fig. 4.6. Total equivalent mass Me is the sum of M1 and M2, while 154 the Be is the sum of B1 and B2. Comparing translational mechanical system to 155 an electrical system, we can see that the mass of an object shows analogy with 156 the *capacity* while the *friction* is similar to the *conductivity*, i.e., reciprocal to the 157 resistivity, G = 1/R.

4.5 System of Two Wagons

Let us now consider the process of joining two wagons. One of them is in stationary state while the other one is approaching with the speed of $v_0 = 2$ m/s. Using the equivalent wagon model presented in Fig. 4.6 we have designed system's model of two wagons as shown in Fig. 4.7. The presented model is ready to run, but we should be able to monitor changes in the network variables. In our case, basic physical variables of interest are speed and force. Position, power, and energy could be monitored as well, based on the set of Eqs. (4.9), (4.10), and (4.11).

Position =
$$\int_{0}^{T} v(t)dt$$
 (4.9)

159

Power =
$$p(t) = F(t) * v(t)$$
 (4.10)

Energy =
$$E = \int_{0}^{T} p(t)dt = \int_{0}^{T} F(t) * v(t)$$
 (4.11)

In order to monitor physical quantities as mentioned above we need to introduce sensors and display devices. While measuring velocity as an *across variable* we have to place the sensor *across* network element. Our Ideal Translational Motion Sensor, as defined in Simulink environment, has to be placed across measurement node and the Mechanical Translational Reference, which is equivalent to mechanical 1711

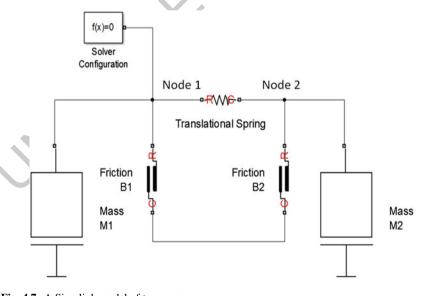


Fig. 4.7 A Simulink model of two wagons

this figure will be printed in b/w

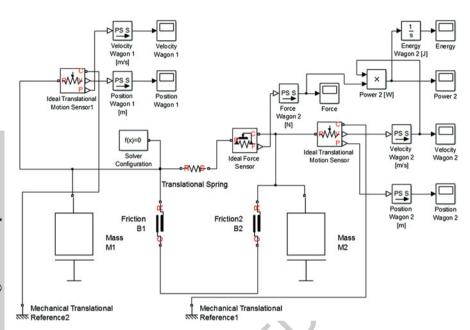


Fig. 4.8 Final Simulink model of two wagons with sensors and monitors

motion ground, i.e., $V_{\rm GND} = 0$ m/s. Opposite to that, measurement of a through 172 variable, such as force in our case, requires placement of the sensor in the network. 173 According to this a new simulation model is designed and presented in Fig. 4.8. 174 Simulation results for the wagon one velocity, wagon two velocity, path traveled, 175 i.e., position and force at the wagon two, are presented in Fig. 4.9.

We can see that the speed of the first wagon is going down from the initial value 177 of $v_0 = 2$ m/s to 0.64 m/s, oscillating and then stabilizing at the value of 1 m/s as 178 expected.

Similarly, after the impact, the speed of the second wagon is increasing from 180 0 m/s to 1.36 m/s, oscillating and then stabilizing at 1 m/s. The force is maximum 181 just after the contact and then oscillating and going down to zero. The power 182 diagram is shown in Fig. 4.10. Variables are expressed in SI systems units [W]. 183 SI units are used in the whole paper. Finally energy carried by wagon 2 is shown in 184 Fig. 4.11.

Since the friction elements are involved, we have inelastic collision of two 186 masses, where one of them was stationary. Assumption was made that the masses 187 are the same. Inelastic collisions do not conserve kinetic energy, but the conservation 188 of moment is in place. After the collision two masses are joined together and travel 189 in the same direction. In Eq. (4.12) speed is shown as a vector quantity. We can see 190 that in the particular case of inelastic collision, as simulated by our model, expected

4 Physical Networks' Approach in Train and Tram Systems' Investigation

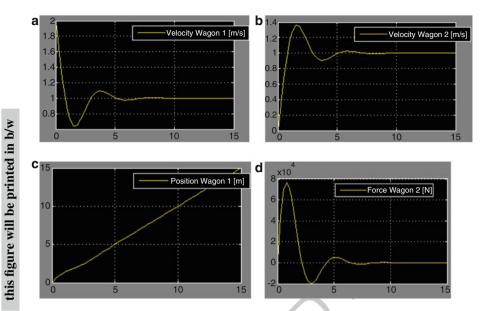
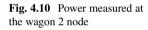
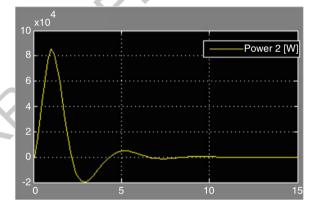


Fig. 4.9 (a) Wagon 1 velocity. (b) Wagon 2 velocity. (c) Path traveled. (d) Force at wagon 2 node





this figure will be printed in b/w

> final velocity should be half of the initial velocity. That can easily be verified by 191 looking at Fig. 4.9a, b.

$$M1 = M2 = m,$$

$$m\mathbf{v}_0 = m\mathbf{v}_f + m\mathbf{v}_f = 2m\mathbf{v}_f$$

$$\mathbf{v}_f = \frac{1}{2}\mathbf{v}_0 \tag{4.12}$$

Fig. 4.11 Kinetic energy carried by the wagon 2

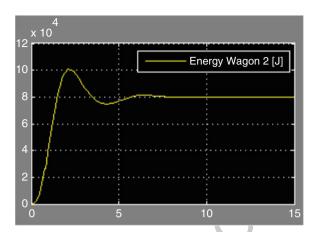


Fig. 4.12 Energy dissipation in friction element



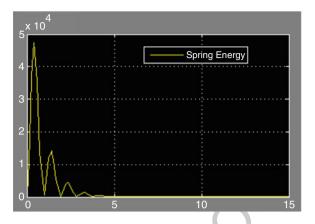
In Eq. (4.12) v_0 is an initial velocity of the wagon 1, as already given, while v_f is 193 the final value of the joint system velocity. We assumed that wagons have the same 194 mass. Energy losses through one of the equivalent friction elements are calculated 195 using expression $E = v^2 B$, as given in Table 4.1. Graph representing simulation 196 results is given in Fig. 4.12.

The spring interfacing element is accumulating and releasing energy as per 198 equation $E = k\frac{x^2}{2}$. Spring energy graph is given in Fig. 4.13.

Figure 4.14 shows distribution of kinetic and spring energy measured at the node 200 2, as labeled in Fig. 4.7.

Figure 4.15 presents final model of the systems with all sensors, calculations, and 202 monitors shown. 203 4 Physical Networks' Approach in Train and Tram Systems' Investigation

Fig. 4.13 Spring energy



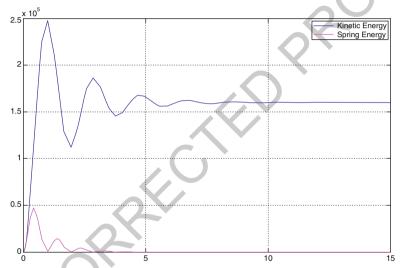


Fig. 4.14 Kinetic and spring energy distribution measured at the node 2

Train Composition Model

We are now going to simulate whole train composition as shown in Fig. 4.16. The 205 only difference now, comparing to previous modeling, is the way how we supply 206 the energy to the system. Locomotive is simulated as a velocity source as shown in 207 Fig. 4.17. The next Fig. 4.18 shows velocity pattern generated by the locomotive.

As with the previous model, we could add sensors, calculators, and monitors to 209 trace changes in the physical quantities, in the various parts of this complex system. 210

System model is shown in Fig. 4.19. It can be loaded with more sensors and 211 calculators for monitoring purposes.

204

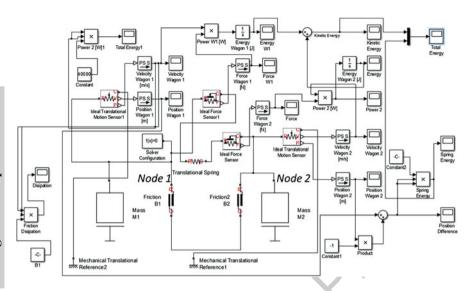


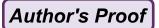
Fig. 4.15 Two wagon model with sensors, calculators, and monitors attached



Fig. 4.16 An ordinary train composition subject to simulation

As examples, forces and velocities in few network nodes are presented in 213 Figs. 4.20 and 4.21.

Other physical quantities can easily be monitored, as already shown in the 215 investigation of the less comprehensive system model, with two wagons and initial 216 conditions present.



4 Physical Networks' Approach in Train and Tram Systems' Investigation

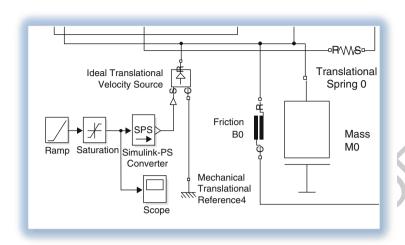


Fig. 4.17 Velocity driving source

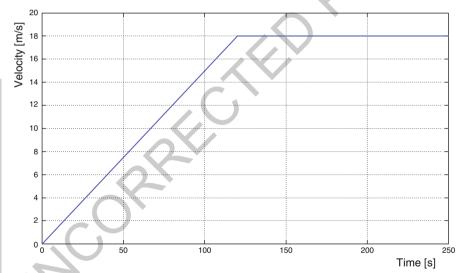


Fig. 4.18 Velocity pattern

4.7 Conclusion 218

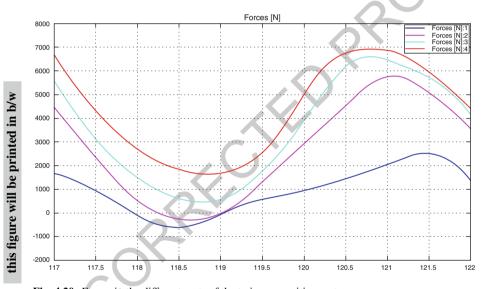
Based on ODE, which are a common way to express various physical systems, 219 physical networks approach is a comprehensive and global tool to model and 220 simulate all sorts of engineering systems. We can perform modeling of mechanical, 221

electrical, or hydro systems easily. Using this approach we simply manage issues

this figure will be printed in b/w

this figure will be printed in b/w

Fig. 4.19 Basic Simulink model of a train composition as shown in Fig. 4.16



Forces in the different parts of the train composition system

with energy conversions, from one to another system. In each system two basic 222 types of physical quantities exist, while energy conversions are conducted using 223 various sensors and actuators.

As good examples of mechanical systems that conduct translation motion, train 225 and tram systems were modeled using this approach. Train composition is an 226 extremely nonlinear and multidimensional system. Modeling and simulation is 227 presented in just one dimension, as per translation motion vector directions. It is 228 shown how key quantities and performances of the system can be monitored. Motion 229 in other directions, then vibrations and other phenomena, can also be investigated 230 with more comprehensive modeling and simulations. That will be subject to the 231 future physical network applications and presentations.

224

References

AQ3

AQ4

4 Physical Networks' Approach in Train and Tram Systems' Investigation

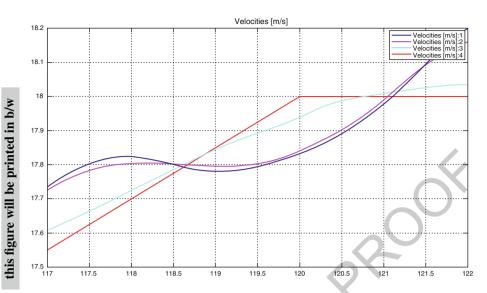
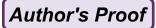


Fig. 4.21 Velocities of the different parts of the train composition system

234
235
236
237
238
239
240
241



AUTHOR QUERIES

- AQ1. Abstracts are provided twice in this book for every chapter (i.e., "abstracts in chapter file" and "abstracts in main file- front maters and abstracts.pdf" in FM elements). Please check.
- AQ2. Please check whether the affiliation is ok as typeset.
- AQ3. Please check the inserted publisher location for reference "de Silva 2005".
- AQ4. Please provide the location details for reference "Simic 2015 and Sanford 1965".

