

Experiment no: 2

Date: 3/10/16

Aim: 1. To find out the efficiency and regulation of a medium transmission line.

2. To find out the generalized constant of a medium transmission line.

THEORY:

Modeling of Medium Transmission Line:

The transmission line having its effective length more than 80 km but less than 160 km and the line voltage will be in between (21-100 KV), is generally referred to as a medium transmission line. Due to the line length being considerably high, in this case the shunt capacitance can be assumed to be lumped at the middle of the line or half of the shunt capacitance may be considered to be lumped each end of the line. The most commonly used methods for solution of medium transmission lines are: End condenser method, Nominal-T and Nominal- π respectively.

1. End Condenser Method:

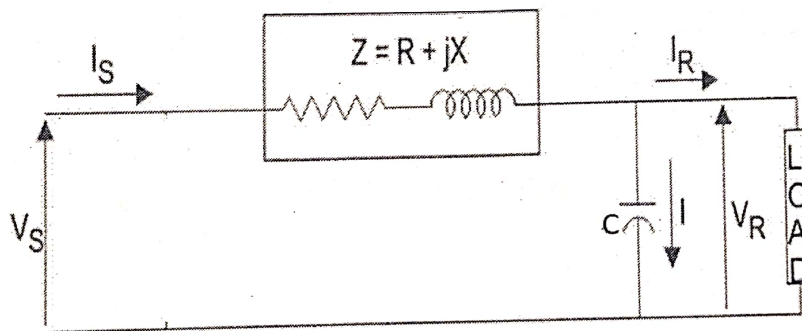


Fig: 1 End Condenser Method

In this method, the capacitance of the line is lumped or concentrated at the receiving or load end as shown in Fig 1. This method of localizing the line capacitance at the load end overestimates the effects of capacitance. In Fig 1. One phase of the 3-phase transmission line is shown as it is more convenient to work in phase instead of line-to-line values.

| | | |
|--------------|---|---|
| I_R | = | load current per phase |
| R | = | loop resistance i.e., resistance of both conductors |
| X_L | = | inductive reactance per phase |
| V_R | = | receiving end voltage |
| V_S | = | sending end voltage |
| $\cos\phi_r$ | = | receiving end power factor (lagging) |

By taking V_R as a reference from the phasor diagram,

We have, $V_R = V_R + j0$

Load Current $I_R = j I_R (\cos \phi_R - j \sin \phi_R)$

Capacitive current $I_C = j B_C V_R$

The sending end current (I_s) is the phasor sum of load current I_R and capacitive current I_C , i.e

$$I_s = I_R + I_C \quad (1)$$

$$W_r = V_R I_R \cos \phi_R$$

$$Z = (R + jX_L)$$

$$Y = j B_C \text{ neglecting conductance (G=0)}$$

$$I_C = V_R Y$$

$$V_S = V_R + I_s Z \quad (2)$$

$$W_S = V_S I_s \cos \phi_s$$

$$\text{Line losses} = I_s^2 R = W_S - W_R$$

$$\% \text{ voltage transmission efficiency} = \left(\frac{\text{Power delivered at receiving end}}{\text{Power sent from the sending end}} \right) * 100$$

$$\% \text{ Voltage regulation} = \left(\frac{(V_R (\text{no load}) - V_R (\text{load}))}{V_R (\text{no load})} \right) * 100$$

Eq 1 and 2 can be rewrite as

$$V_S = V_R + Z(I_R + I_C)$$

$$V_S = V_R + Z Y V_R + Z I_R$$

$$V_S = V_R(1 + ZY) + Z I_R$$

$$\text{And } I_s = Y V_R + I_R$$

Then the obtain constants are

$$A = 1 + YZ; \quad B = Z; \quad C = Y; \quad D = 1$$

2. Nominal T Representation of a Medium Transmission Line

In this method the whole capacitance is assumed to be connected at the middle point of the line and half the line resistance and reactance are lumped on its either side as shown in Fig 2.

From the Fig 2

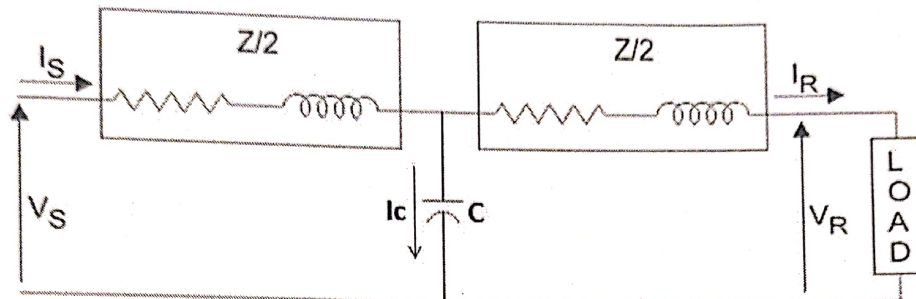


Fig 2. Normal T Method

$$Z = \left(\frac{R}{2} + j \frac{X}{2} \right)$$

$$V_C = V_R + I_R \left(\frac{Z}{2} \right)$$

$$I_S = I_R + I_C$$

$$I_S = I_R + Y V_C = I_R + Y (V_R + I_R \left(\frac{Z}{2} \right))$$

$$I_S = Y V_R + I_R \left(1 + \left(\frac{YZ}{2} \right) \right) \quad (1)$$

$$V_S = V_C + I_S \left(\frac{Z}{2} \right)$$

After substituting V_C and I_S in the above equation and solving

$$V_S = V_R (1 + YZ/2) + I_R Z (1 + YZ/2) \quad (2)$$

Compare 1 and 2

$$A = (1 + YZ/2); B = (1 + YZ/4); C = Y; D = (1 + YZ/2)$$

3 Nominal Π Representation of a Medium Transmission Line

In this method, the capacitance of each conductor is divided into two halves; one half being lumped at the sending end and the other half at the receiving end as shown in Fig 2. It is obvious that capacitance at the sending end has no effect on the line drop.

However, its charging current must be added to line current in order to obtain the total sending end current.

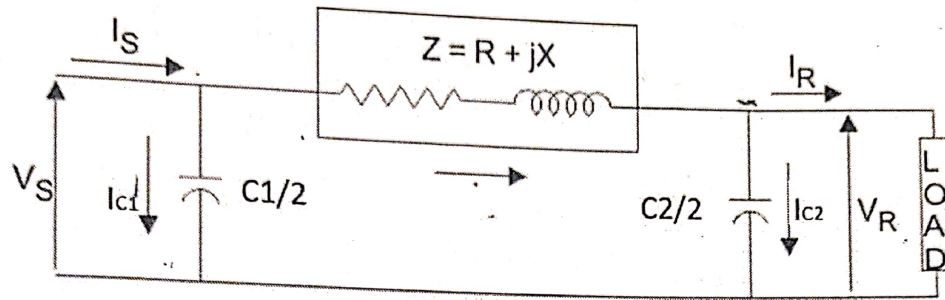


Fig 2. Normal Π Method

| | | |
|--------------|---|---|
| I_r | = | load current per phase |
| R | = | loop resistance i.e., resistance of both conductors |
| X_L | = | inductive reactance per phase |
| V_R | = | receiving end voltage |
| V_S | = | sending end voltage |
| $\cos\Phi_r$ | = | receiving end power factor (lagging) |

From the Fig:

$$Z = (R + jX)$$

$$\frac{Y}{2} = j \frac{B_C}{2}$$

$$I_{C2} = \left(\frac{Y}{2}\right) V_R$$

$$I = I_{C2} + I_R$$

$$I_S = I + I_{C1} \text{ \& } I_{C1} = \left(\frac{Y}{2}\right) V_S$$

$$I_S = \left(\frac{Y}{2}\right) V_R + I_R + \left(\frac{Y}{2}\right) V_S$$

$$V_S = V_R + IZ$$

$$V_S = V_R + Z \left(\left(\frac{Y}{2}\right) V_R + I_R \right) \quad (1)$$

And $I_S = I_R \left(1 + \left(\frac{YZ}{2}\right)\right) + V_R \left(1 + \left(\frac{YZ}{2}\right)Y\right)$ (2)

Compare 1 and 2 we get

$A = 1 + \left(\frac{YZ}{2}\right)$; $B = Z$; $C = Y \left(1 + \left(\frac{YZ}{2}\right)\right)$; $D = 1 + \left(\frac{YZ}{2}\right)Y$

PROCEDURE:

- 1) Connect 230V, 1phase, Ac supply at the input terminals of the panel through auto transformer.
- 2) Do not connect load bank at the output terminals of the panel.
- 3) Switch on the supply and note down the values of sending end and receiving end voltages.
- 4) Now, Connect Load bank at the output terminals of the panel.
- 5) Now using different Methods connect the short transmission kit and gradually increase the load by making the switches of the load bank ON and take different readings and tabulate then in table.
- 6) Compute $\cos\theta_r$, V_s , $W_s \cos\theta_s$ (from calculated value of W_s) efficiency and regulation.
- 7) Draw vector diagram to scale and confirm observed values.

OBSERVATION TABLE:

| Sr No | V_s | V_r |
|-------|-------|-------|
| 1 | 203 | 205 |
| 2 | 170 | 171.5 |
| | | |
| | | |

| Sr No | V_{c1} | V_{c2} | V_r | V_s | | I_r | I_s | W_r | $\cos\theta_r$ | W_s | | $\cos\theta_s$ | %n Efficiency | | % Regulation | |
|-------|----------|----------|-------|-------|-------|-------|-------|-------|----------------|-------|--------|----------------|---------------|-------|--------------|-------|
| | | | | Obs | Cal | | | | | Obs | Cal | | Obs | Cal | Obs | Cal |
| 1 | 187 | 187 | 171.5 | 201.5 | 189.0 | 0.55 | 0.56 | 70 | 0.7288 | 86 | 72.4 | 0.7919 | 87.5 | 96.22 | 17.5 | 10.25 |
| 2 | 191 | 191 | 171.5 | 201.5 | 193.7 | 0.48 | 0.48 | 65 | 0.7544 | 75 | 66.988 | 0.8451 | 86.67 | 97.03 | 12.25 | 7.91 |

| | | | | | | | | | | | | | | | | | |
|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |

Table 3: NOMINAL PI METHOD

$$V_{NL} = 206.1 \text{ V}$$

| Sr No | Vc1 | Vc2 | Vr | Vs | | Ir | Is | Wr | Cos θ_r | Ws | | Cos θ_s | %n Efficiency | | % Regulation | |
|-------|-----|-------|-------|-----|--------|------|------|----|----------------|-----|-------|----------------|---------------|-------|--------------|-------|
| | | | | Obs | Cal | | | | | Obs | Cal | | Obs | Cal | Obs | Cal |
| 1 | 203 | 172.5 | 172.5 | 203 | 190.26 | 0.56 | 0.56 | 90 | 0.7246 | 82 | 72.57 | 0.7952 | 85.36 | 96.26 | 17.68 | 10.29 |
| 2 | 203 | 171.8 | 171.8 | 203 | 194.35 | 0.49 | 0.48 | 65 | 0.7358 | 78 | 69.66 | 0.8293 | 83.33 | 96.82 | 12.9 | 8.31 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

TABLE 4: END CONDENSER METHOD:

$$V_{NL} = 204.1 \text{ V}$$

| Sr No | Vc1 | Vc2 | Vr | Vs | | Ir | Is | Wr | Cos θ_r | Ws | | Cos θ_s | %n Efficiency | | % Regulation | |
|-------|-----|-------|-------|-------|-------|------|------|----|----------------|-----|-------|----------------|---------------|-------|--------------|-------|
| | | | | Obs | Cal | | | | | Obs | Cal | | Obs | Cal | Obs | Cal |
| 1 | - | 170 | 170 | 201.5 | 189.6 | 0.56 | 0.56 | 90 | 0.7353 | 80 | 72.75 | 0.7352 | 87.5 | 96.21 | 18.53 | 10.37 |
| 2 | - | 171.5 | 171.5 | 201.5 | 188.7 | 0.56 | 0.54 | 90 | 0.8023 | 80 | 72.22 | 0.8150 | 87.5 | 96.94 | 15.47 | 8.13 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

Conclusion:

From this experiment we learned different model of medium transmission line and determined its efficiency and different performance parameters. We also studied the effect of load p.f. on different char. of medium transmission line.

Calculations:

Nominal T-method $Z = 10 + j40$, $C = 2 \times 10^{-6} \text{ F}$

$$\cos \phi_n = \frac{W_r}{V_r I_r} = \frac{70}{171.5 \times 0.56} = 0.7288$$

$$\phi_r = 43.2088^\circ$$

$$\rightarrow \vec{I}_r = 0.56 \angle -43.2088^\circ$$

$$\vec{V}_c = \vec{V}_R + (\vec{I}_r)(Z/2)$$
$$= 171.5 \angle 0^\circ + (0.56 \angle -43.2088^\circ)(5 + j20)$$

$$\vec{V}_c = 181.316 \angle 1.974^\circ$$

$$\vec{I}_c = j V_c (2\pi f C)$$
$$= j (181.316 \angle 1.974^\circ) (2 \times 3.14 \times 50 \times 2 \times 10^{-6})$$

$$\vec{I}_c = 0.114 \angle 91.974^\circ$$

$$\vec{I}_s = \vec{I}_c + \vec{I}_r$$

$$= 0.114 \angle 91.974^\circ + 0.56 \angle -43.2088^\circ$$

$$\vec{I}_s = 0.485 \angle -33.698^\circ$$

$$\vec{V}_s = \vec{V}_c + \vec{I}_s (Z/2)$$

$$\vec{V}_s = 189.07 \angle 3.937^\circ$$

$$W_s = W_r + I_r^2 R + I_s^2 R$$

$$(\text{cal}) = 70 + (0.56)^2 (5) + (0.485)^2 (5)$$

$$W_{s, \text{cal}} = 72.744 \text{ W}$$

$$\rightarrow \% \eta_{\text{obs}} = \frac{W_r}{W_{s, \text{obs}}} \times 100 = \frac{70}{80} \times 100 = 87.5\%$$

$$\rightarrow \% \eta_{\text{cal}} = \frac{W_r}{W_{s, \text{cal}}} \times 100 = \frac{70}{72.744} \times 100 = 96.228\%$$

$$\% V.R \text{ obs} = \frac{V_{\text{obs}} - V_r}{V_r} \times 100 = \frac{201.5 - 171.5}{171.5} \times 100 = 17.5\%$$

$$\% V.R \text{ cal} = \frac{V_{\text{scal}} - V_r}{V_r} \times 100 = \frac{189.07 - 171.5}{171.5} \times 100 = 10.28\%$$

② Nominal π -method

$$Z = 10 + j40, \quad C = 2 \mu F$$

$$\rightarrow \cos \phi_r = \frac{W_r}{V_r I_r} = \frac{70}{172.5 \times 0.56} = 0.7246$$

$$\phi_r = 43.56^\circ$$

$$\begin{aligned} \rightarrow \vec{I}_{C2} &= j V_r \left(\frac{\omega C}{2} \right) \\ &= j 172.5 \left(2\pi \times 90 \times \frac{2}{2} \times 10^{-6} \right) \\ &= 6.05419 \angle 90^\circ \end{aligned}$$

$$\vec{I}_R = 0.56 \angle -43.56$$

$$\vec{I} = \vec{I}_R + \vec{I}_{C2}$$

$$= 0.524 \angle -39.263$$

$$\vec{I}_S = \vec{I} + \vec{I}_{C1}$$

$$= 0.524 \angle -39.263 + j V_s \left(\frac{\omega C}{2} \right)$$

$$= 0.488 \angle -33.434$$

$$\vec{V}_S = \vec{V}_R + \vec{I} Z$$

$$= 172.5 + (0.524 \angle -39.263)(10 + j40)$$

$$= 190.26 \angle 3.89$$

$$\phi_s = 3.89 + 33.434$$

$$\phi_s = 37.324$$

$$\cos \phi_s = 0.7952$$

$$\begin{aligned}
 \rightarrow W_{scal} &= W_r + \text{losses} \\
 &= 70 + I^2 R \\
 &= 70 + (0.524)^2 (10) \\
 &= 72.745 \text{ W}
 \end{aligned}$$

$$\rightarrow \% \eta_{obj} = \frac{W_r}{W_{sobj}} = \frac{70}{82} \times 100 = 85.36\%$$

$$\rightarrow \% \eta_{cal} = \frac{W_r}{W_{scal}} = \frac{70}{72.745} \times 100 = 96.226\%$$

$$\rightarrow \% VR_{obs} = \frac{V_{sobj} - V_r}{V_r} \times 100 = \frac{203 - 172.5}{172.5} \times 100 = 17.68\%$$

$$\rightarrow \% VR_{cal} = \frac{V_{scal} - V_r}{V_r} \times 100 = \frac{190.26 - 172.5}{172.5} = 10.29\%$$

End Condenser Method:

$$\rightarrow \cos \phi_r = \frac{W_r}{V_r I_r} = \frac{70}{170 \times 0.56} = 0.7353$$

$$\phi_r = 42.6679^\circ$$

$$\rightarrow \vec{I}_r = 0.56 \angle -42.6679$$

$$\vec{I}_c = j V_r (2\pi f C)$$

$$= j 170 (2\pi \times 50 \times 1 \times 10^{-6})$$

$$= 0.0534 \angle 90^\circ$$

$$\vec{I}_s = \vec{I}_r + \vec{I}_c$$

$$= 0.525 \angle -38.38$$

$$\vec{V}_s = \vec{V}_r + \vec{V}_s \vec{Z}$$

$$= 170 + (0.525 \angle -38.38) (10 + j40)$$

$$= 187.628 \angle +4.037$$

$$\rightarrow \phi_s = 4.037 + 38.38$$

$$= 42.417$$

$$\cos \phi_s = 0.7382$$

$$W_{s \text{ cal}} = W_R + I_s^2 R$$

$$= 70 + (0.525)^2 (10)$$

$$= 72.756 \text{ W}$$

$$\rightarrow \% \eta_{\text{obs}} = \frac{70}{80} \times 100 = 87.5\%$$

$$\rightarrow \% \eta_{\text{cal}} = \frac{70}{72.756} \times 100 = 96.21\%$$

$$\rightarrow VR_{\text{obs}} = \frac{201.5 - 170}{170} \times 100 = 18.53\%$$

$$\rightarrow VR_{\text{cal}} = \frac{187.628 - 170}{170} \times 100 = 10.37\%$$