Understanding the autoregressive filter used for second-stage control

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In his 2023 SPIE paper, Ben uses this filter to separate out the signals going into the SHWFS and FAST:

$$\begin{split} c_{H\{n\}} &= \alpha c_{H\{n-1\}} + \alpha (c_n - c_{n-1}) \\ c_{L\{n\}} &= \alpha c_{L\{n-1\}} + (1-\alpha) c_{n-1} \end{split}$$

where $\alpha = e^{-f_{\text{cutoff}}/f_{\text{loop}}}$. I'd like to convince myself that these do actually define high- and low-pass filters respectively, so I'll calculate their frequency responses.

Since Ben ran these filters in separate terminals, the $c_{H\{n\}}$ s and $c_{L\{n\}}$ s can't technically see each other, but they do interact since both wavefront sensors read off the coefficients c_n , which get set by the commands from both wavefront sensors. For our purposes here I'll assume $c_n = c_{H\{n\}} + c_{L\{n\}}$; I think this is accurate up to the assumption that both wavefront sensors agree on the overall reconstruction.

Using this, we can rewrite the filter to eliminate c_n :

$$\begin{split} c_{H\{n\}} &= \alpha c_{H\{n-1\}} + \alpha \Big(c_{H\{n\}} + c_{L\{n\}} - c_{H\{n-1\}} - c_{L\{n-1\}} \Big) \\ c_{L\{n\}} &= \alpha c_{L\{n-1\}} + (1-\alpha) \Big(c_{H\{n-1\}} + c_{L\{n-1\}} \Big) \end{split}$$

or

$$\begin{split} c_{H\{n\}} &= \frac{\alpha}{1-\alpha} \Big(c_{L\{n\}} - c_{L\{n-1\}} \Big) \\ c_{L\{n\}} &= c_{L\{n-1\}} + (1-\alpha) c_{H\{n-1\}} \end{split}$$

which we can rewrite further so that it's just in terms of a state vector. Let $\vec{c}_n = \left[c_{H\{n\}} \ c_{L\{n\}}\right]^T$, then:

$$\vec{c}_n = \begin{bmatrix} 1 & 0 \\ 1 - \alpha & 1 \end{bmatrix} \vec{c}_{n-1} + \vec{x}_n$$

where I've added in driving noise \vec{x}_n .

Let's compute a frequency response by allowing $\vec{x}_n = \left[e^{i\omega_H n} \ e^{i\omega_L n}\right]^T$ and setting $\vec{c}_n = F(\omega_H, \omega_L) \vec{x}_n$ where F is a 2x2 matrix (generally we'd use H for this but that's overloaded.)

$$\begin{split} F(\omega_H,\omega_L) \begin{bmatrix} e^{i\omega_H n} \\ e^{i\omega_L n} \end{bmatrix} &= \begin{bmatrix} 1 & 0 \\ 1-\alpha & 1 \end{bmatrix} F(\omega_H,\omega_L) \begin{bmatrix} e^{i\omega_H(n-1)} \\ e^{i\omega_L(n-1)} \end{bmatrix} + \begin{bmatrix} e^{i\omega_H n} \\ e^{i\omega_L n} \end{bmatrix} \\ F(\omega_H,\omega_L) &= \begin{bmatrix} 1 & 0 \\ 1-\alpha & 1 \end{bmatrix} F(\omega_H,\omega_L) \begin{bmatrix} e^{-i\omega_H} & 0 \\ 0 & e^{-i\omega_L} \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \\ F(\omega_H,\omega_L) &= \begin{bmatrix} e^{-i\omega_H} & 0 \\ (1-\alpha)e^{-i\omega_H} + e^{-i\omega_L} & e^{-i\omega_L} \end{bmatrix} F(\omega_H,\omega_L) + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \\ F(\omega_H,\omega_L) &= \mathrm{inv} \left(\begin{bmatrix} 1-e^{-i\omega_H} & 0 \\ (\alpha-1)e^{-i\omega_H} - e^{-i\omega_L} & 1-e^{-i\omega_L} \end{bmatrix} \right) \end{split}$$

which gives us the final result,

$$F(\omega_H,\omega_L) = \frac{1}{e^{-i\omega_L} + e^{-i\omega_H} - e^{-i(\omega_L + \omega_H)}} \begin{bmatrix} 1 - e^{-i\omega_L} & 0 \\ (1-\alpha)e^{-i\omega_H} + e^{-i\omega_L} & 1 - e^{-i\omega_H} \end{bmatrix}$$

Let's try some substitutions!

- $F(0,0) = \begin{bmatrix} 0 & 0 \\ 2-\alpha & 0 \end{bmatrix}$; a DC offset gets sent from the high-frequency component to the low-frequency component, and then gets removed.
- $F(\omega,0)=\begin{bmatrix}0&0\\(1-\alpha)e^{-i\omega}+1&1-e^{-i\omega}\end{bmatrix}$; a pure high frequency survives only in the low-frequency component? I don't think this is what I want the filter to do.
- $F(0,\omega)=\begin{bmatrix}1-e^{-i\omega}&0\\1-\alpha+e^{-i\omega}&0\end{bmatrix}$; a pure low frequency gets completely ignored? I'm not sure I'm reading these right.

I think what I'd hope this shows me is the filter can take in a signal with a frequency above $f_{\rm cutoff}$ and keep it only in the first component, and one with a frequency below $f_{\rm cutoff}$ and keep it only in the second component. But I don't think that's what this is saying. I might not be interpreting it the right way.