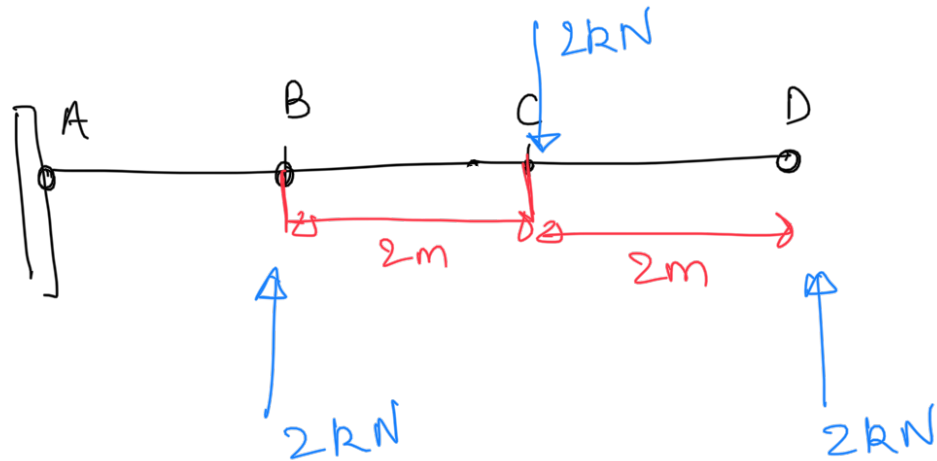
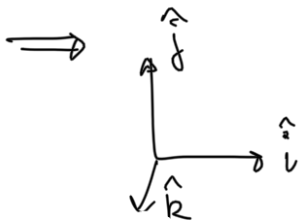


Q. 2.1.11

Equivalent force couple at B & D ?

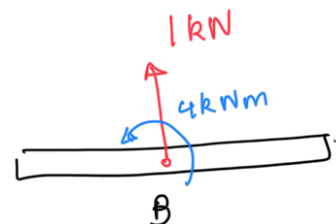


Since nothing is mentioned about whether the body is in equilibrium or not, ignoring the reaction forces & considering entire figure as F_{B1}

$$a) \therefore \sum \text{Forces at B} = +1\text{ kN} + 2\text{ kN} - 2\text{ kN} = 1\text{ kN } \hat{j}$$

$$\therefore \sum \text{Moment at B} = -(2\text{ kN} \times 2\text{ m}) \hat{k} + (2\text{ kN} \times 4\text{ m}) \hat{k} \\ = 4\text{ kNm } \hat{k}$$

\therefore Equivalent Force-couple system

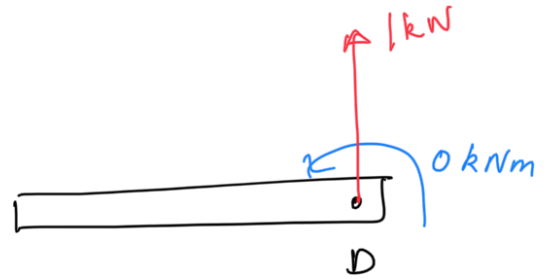


$$b) \therefore \sum \text{Forces at D} = +1\text{ kN} + 2\text{ kN} - 2\text{ kN} = 1\text{ kN}$$

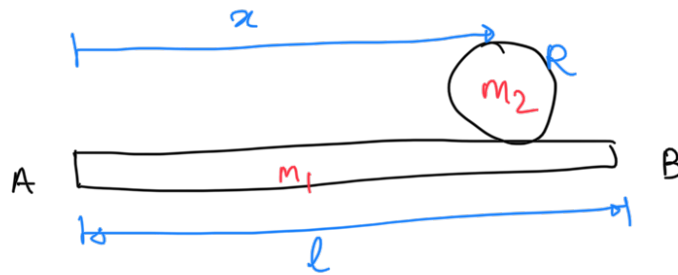
$$\therefore \sum \text{Moment at D} = (1\text{ kN} \times -4\text{ m}) \hat{k} + (-2\text{ kN} \times -2\text{ m}) \hat{k}$$

$$= 0 \text{ kNm}$$

\therefore Equivalent force-couple system



Q. 2.2.4



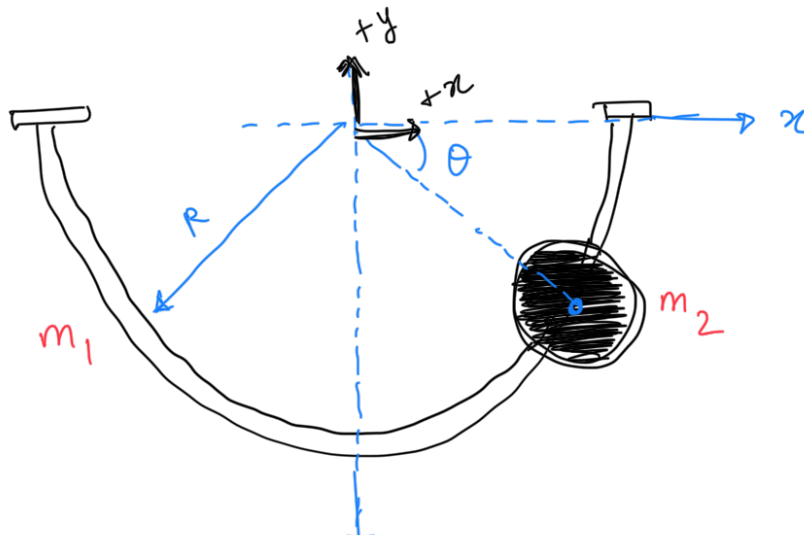
$$\& M = \frac{m_1}{m_2}$$

$$\therefore r_{com}^{m_1} = \frac{l}{2} \quad \& \quad r_{com}^{m_2} = x \quad [\text{assuming } x \text{ is measured from A to centre of cylinder}]$$

$$\therefore r_{com}^{total} = \frac{m_1 r_{com}^{m_1} + m_2 r_{com}^{m_2}}{m_1 + m_2}$$

$$r_{com}^{total} = \frac{m_1 (l/2) + m_2 (x)}{m_1 + m_2} = \frac{M l/2 + x}{1 + M}$$

Q. 2.2.9

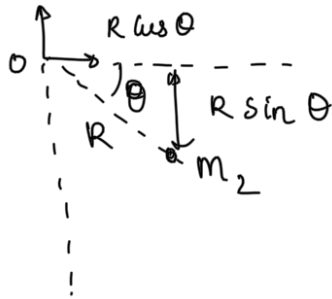


$$R = 1 \text{ m}$$

$$m_1 = 0.1 \text{ kg}$$

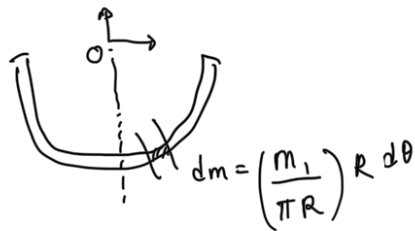
$$m_2 = 0.25 \text{ kg}$$

$$\therefore r_{com} = ? @ \theta = 30^\circ$$



$$\therefore (r_{com})_{m_2} = \begin{bmatrix} x_{m_2} \\ y_{m_2} \end{bmatrix} = \begin{bmatrix} R \cos \theta \\ -R \sin \theta \end{bmatrix}$$

\therefore for m_1



$$\therefore (r_{com})_{m_1} = \begin{bmatrix} x_{m_2} \\ y_{m_2} \end{bmatrix} = \begin{bmatrix} 0 \\ \frac{\int_0^\pi R \sin \theta dm}{m_1} \end{bmatrix}$$

due to symmetry

$$= \begin{bmatrix} 0 \\ - \frac{\int_0^\pi R \sin \theta \left(\frac{m_1}{\pi R} \right) R d\theta}{m_1} \end{bmatrix} = \begin{bmatrix} 0 \\ -\frac{2R}{\pi} \end{bmatrix}$$

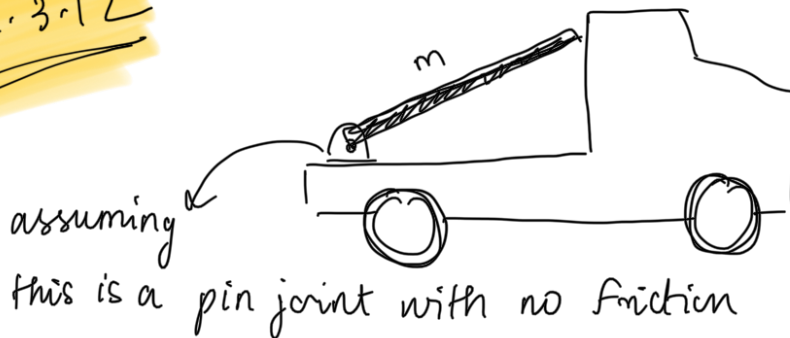
$$\therefore r_{total} = \frac{m_1 (r_{com})_{m_1} + m_2 (r_{com})_{m_2}}{m_1 + m_2} = \begin{bmatrix} \frac{m_2 R \cos \theta + 0}{m_1 + m_2} \\ \frac{-m_2 R \sin \theta + m_1 \left(-\frac{2R}{\pi} \right)}{m_1 + m_2} \end{bmatrix}$$

$$\therefore r_{total} = \begin{bmatrix} R m_2 \cos \theta / (m_1 + m_2) \\ - \frac{R (\pi m_2 \sin \theta + 2 m_1)}{\pi (m_1 + m_2)} \end{bmatrix}$$

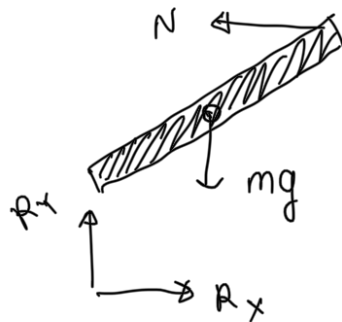
$$\therefore h_{\text{total}} @ \theta = 30^\circ = \left[\begin{array}{c} 1 \times 0.25 \cos 30^\circ / 0.1 + 0.25 \\ - 1 \times \left(\frac{\pi \cdot 0.25 \cdot \sin 30^\circ + 2 \times 0.1}{\pi (0.1 + 0.25)} \right) \end{array} \right]$$

$$= \left[\begin{array}{c} 0.61 \text{ m} \\ - 0.53 \text{ m} \end{array} \right]$$

Q. 2.3.12



\therefore FBD is



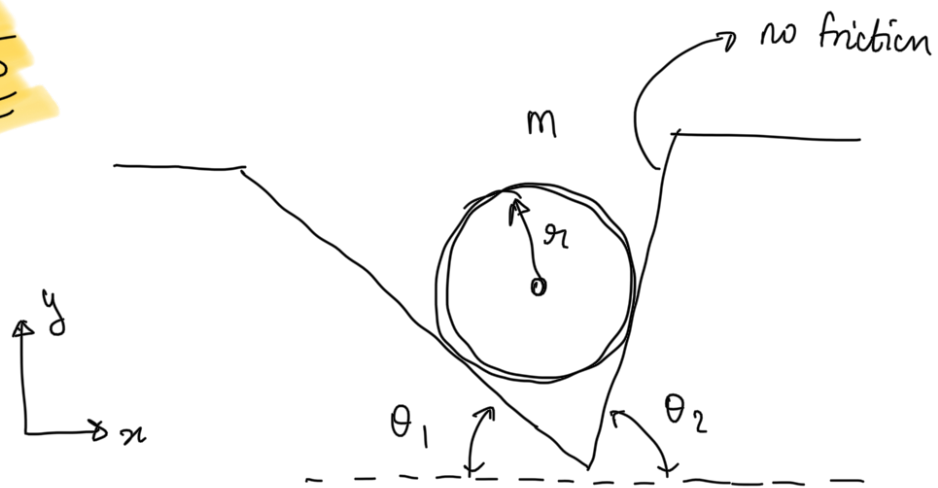
N : normal rxn from the flatbed truck

mg : weight due to gravity

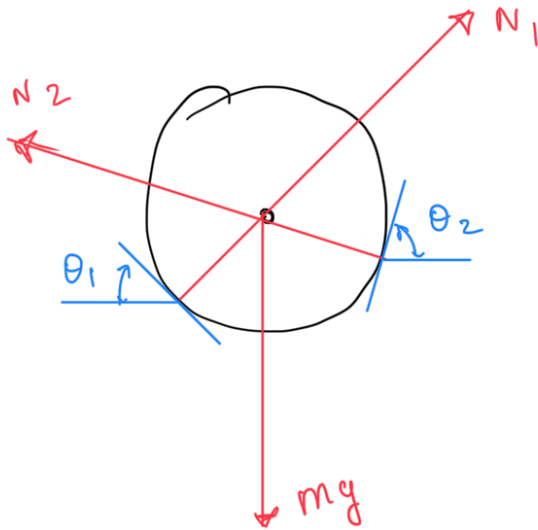
R_y : vertical rxn due to the joint

R_x : Horizontal rxn due to the joint

Q. 2.3.15



a]



b]



$$\therefore \sum F_y = 0 \quad (\text{since at rest})$$

$$\therefore -mg + N_1 \cos \theta_1 + N_2 \cos \theta_2 = 0 \quad \text{--- (1)}$$

$$\text{Similarly } \sum F_x = 0; \quad N_1 \sin \theta_1 - N_2 \sin \theta_2 = 0 \quad \text{--- (2)}$$

\therefore using (1) & (2);

$$mg = \left(\frac{N_2 \sin \theta_2}{\sin \theta_1} \right) \cos \theta_1 + N_2 \cos \theta_1$$

$$\therefore N_2 = mg \sin \theta_1$$

$$\frac{\sin \theta_2 \cos \theta_1 + \cos \theta_2 \sin \theta_1}{\sin(\theta_1 + \theta_2)} = \frac{mg \sin \theta_1}{\sin(\theta_1 + \theta_2)}$$

$$\therefore N_1 = \frac{mg \sin \theta_2}{\sin(\theta_1 + \theta_2)}$$

$$\begin{aligned} \therefore \vec{N}_1 &= N_1 \sin \theta_1 \hat{i} + N_1 \cos \theta_1 \hat{j} \\ &= \frac{mg \sin \theta_1 \sin \theta_2}{\sin(\theta_1 + \theta_2)} \hat{i} + \frac{mg \cos \theta_1 \sin \theta_2}{\sin(\theta_1 + \theta_2)} \hat{j} \end{aligned}$$

$$\begin{aligned} \vec{N}_2 &= -N_2 \sin \theta_2 \hat{i} + N_2 \cos \theta_2 \hat{j} \\ &= -\frac{mg \sin \theta_1 \sin \theta_2}{\sin(\theta_1 + \theta_2)} \hat{i} + \frac{mg \sin \theta_1 \cos \theta_2}{\sin(\theta_1 + \theta_2)} \hat{j} \end{aligned}$$

c) $\vec{N}_1 + \vec{N}_2 + m\vec{g} = 0$ (one can easily verify using results from b))

d) Net moment = $M_{\text{com}} = 0$ since there is point contact at the surface & all normals to a circle pass through its centre, so moment due to normal is zero. Similarly, weight due to gravity is through centre so moment = 0

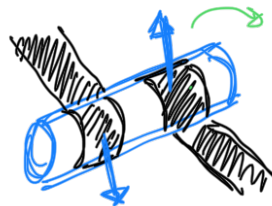
Q. 2-3-16

Assuming the muscles apply only torques



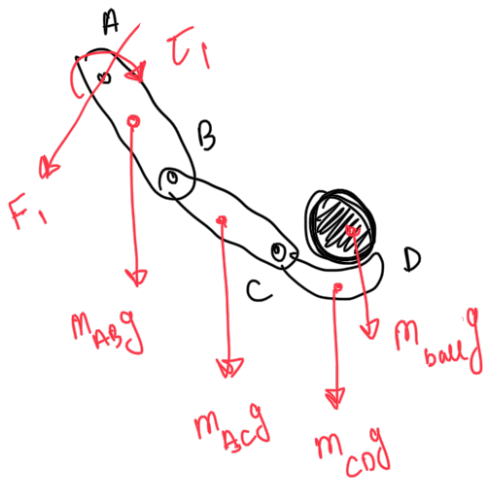
muscles that generate torque

also assuming the pin joint only apply reaction forces



reaction on pin joint

a] arm + ball

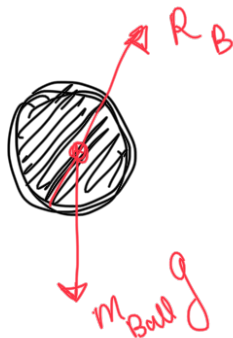


T_1 : Torque applied by the muscles of shoulder on link A

F_1 : rxn force due to pin joint between link AB & shoulder

$m_{AB}g$, $m_{BC}g$, $m_{CD}g$ & $m_{ball}g$ are force due to gravity

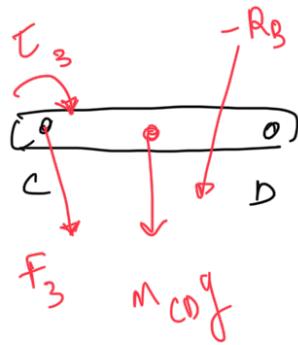
b] Ball



R : reaction on the ball due to link CD

$m_{ball}g$: weight

c] Hand



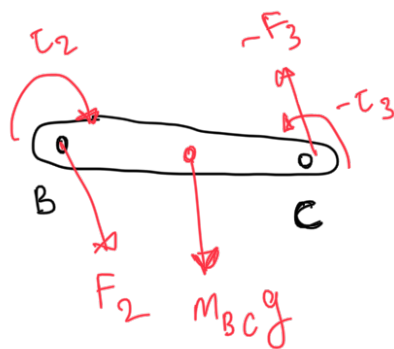
F_3 : rxn force due to pin joint on link CD

τ_3 : torque applied on CD due to muscles of link BC

$m_{CD}g$: force due to gravity

$-R_B$: rxn force due to ball on

d) Fore arm

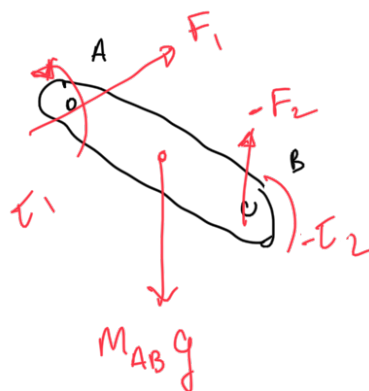


F_2 : rxn force on BC due to pin joint b/w BC & AB

τ_2 : torque applied on BC due to muscles of link AB

$m_{BC}g$: force due to gravity

e) Upper arm



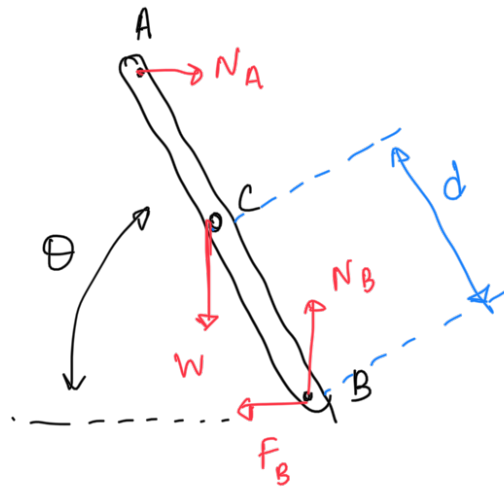
F_1 : rxn force on AB due to pin joint

τ_1 : torque applied on AB due to muscles of shoulder

$m_{AB}g$: force due to gravity

Q. 2.4.4

a]



N_A : normal reaction @ A

W : weight of the ladder

N_B : normal reaction @ B

F_B : Friction force @ B

b] If the ladder is about to slip then; $F_B = \mu N_B$

$$\therefore \sum F_y = 0 \quad \& \quad \sum F_x = 0$$

$$\therefore W = N_B \quad \& \quad \therefore N_A = F_B$$

$$\& \quad \sum M_B = 0$$

$$\therefore (W \cos \theta) - (2d \sin \theta N_A) = 0$$

$$N_A = \frac{W}{2 \tan \theta}$$

$$\therefore F_B = \frac{W}{2 \tan \theta}$$

$$\therefore N_B = \frac{W}{2 \mu \tan \theta}$$

\therefore Total force

$$= \begin{bmatrix} -W/2 \tan \theta \\ W/2 \mu \tan \theta \end{bmatrix}$$

\therefore The direction of total force at B is given by

$$\hat{U} = \frac{-\frac{W}{2 \tan \theta} \hat{i} + \frac{W}{2 \mu \tan \theta} \hat{j}}{\sqrt{\frac{W^2}{2^2 \tan^2 \theta} + \frac{W^2}{2^2 \mu^2 \tan^2 \theta}}} = \frac{-1 \hat{i} + 1/\mu \hat{j}}{\sqrt{1 + 1/\mu^2}}$$

$$= \frac{-\mu \hat{i} + 1 \hat{j}}{\sqrt{\mu^2 + 1}}$$

$$\sqrt{\mu^2 + 1}$$

Now relative positions of A & B will alter θ , but there is no θ present in the final direction vector \hat{u} .

\therefore No effect on \hat{u} !