tr5frbj

12/08/24

Circuit Theory and Devices

↗ tut as well

Lab: LT Spice (2nd week onwards)

book: Engineering Circuit Analysis (9th Edition)

Relative grading

Labs	20%
Quiz (every 2 weeks (n−1))	20%
Mid sem	30%
End sem	30%

Scientific calc ⇐ {Mid sem, End sem}

Course: 9 modules   chapter 10 onwards

{continuation of BE}

* Lecture : 1

⇒ Linear Circuits

x (input) → [system] → y (output)

system is linear if

Kx → [sys] → Ky

where k is constant

"R" Resistor: linear element ✓
$V = iR$

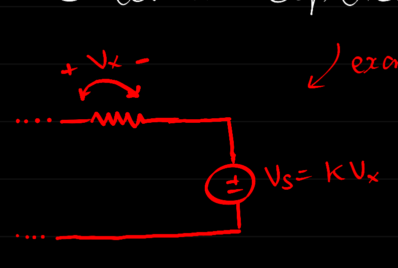
"L" Inductor: linear element ✓
$V = L\frac{di}{dt}$

"C" Capacitor: linear element ✓
$i = C\frac{dv}{dt}$

* Linear Electric Circuits:

consists of ⇒

1. R, L, C → linear elements
2. Independent voltage & current sources
3. linear dependent sources



example

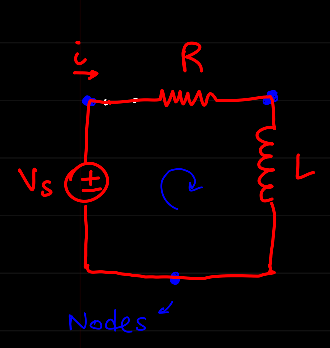
would not have been linear if $V_s = KV_x^2$

Note: diode and transistors are non-linear elements

* Response of a linear circuit

① full response = transient response + Steady State

transient response	Steady State
temporary	persists $t \to \infty$
due to sudden change	due to source
also called natural response	also called forced response
depends on linear elements R, L, C	depends on current/voltage source



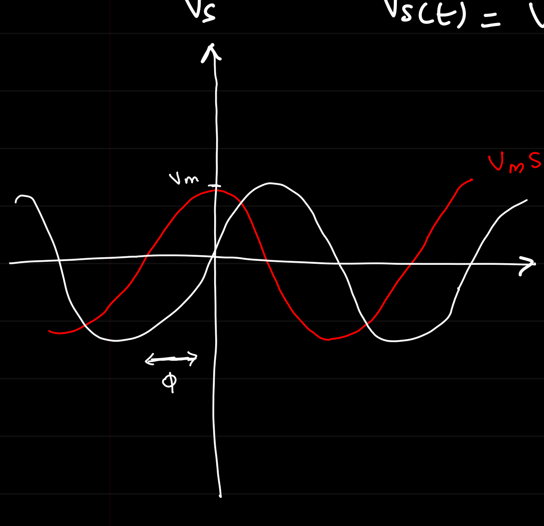
KVL : $-V_s + iR + L\frac{di}{dt} = 0$

$i_{final} = i_{transient} + i_{steady\ state}$

as $t \to \infty$, $i_{final} = i_{steady\ state}$

* Sinusoids & complex numbers

sinusoidally varying voltage source
$V_s(t) = V_m \cos(\omega t)$
$V_s(t) = V_m \sin(\omega t)$
$V_s(t) = V_m \sin(\omega t + \phi)$



② is leading ①
① is lagging ②
by angle ϕ

* TRIGO

$\sin(-\theta) = -\sin(\theta)$
$\cos(-\theta) = \cos(\theta)$
$\sin(A+B) = \sin A \cos B + \cos A \sin B$
$\cos(A+B) = \cos A \cos B - \sin A \sin B$

sin +ve	All +ve
tan +ve	cos +ve

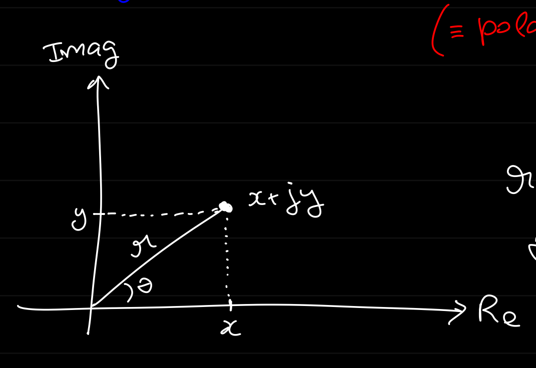
* Complex Numbers

Real : x
complex : $x + iy$ (rectangular form)
real part: x; imaginary part: y
$i = \sqrt{-1}$ a.k.a. j

⇒ Euler's identity : $\underbrace{e^{j\theta}}_{\text{exponential form}} = \underbrace{\cos\theta + j\sin\theta}_{\text{rectangular form}}$

Complex Number

- rectangular: $x + iy$
- exponential: $re^{j\theta}$ (≡ polar form : $r\angle\theta$)



$r = \sqrt{x^2 + y^2}$
$\theta = \tan^{-1}\left(\frac{y}{x}\right)$

$(r_1 e^{j\theta_1}) \times (r_2 e^{j\theta_2}) = (r_1 \cdot r_2)\, e^{j(\theta_1 + \theta_2)}$

AC	DC
• we can use transformers to vary voltage	• appliances need constant current
• transported easily over large distances	

AC → DC : using rectifiers

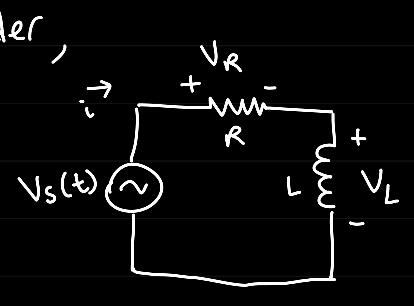
* MODULE : 1 {CH = 10}

10:30 am

⇒ Sinusoidal steady state analysis

assuming transient has died out long back

Consider,



$V_s(t) = V_m \cos(\omega t)$
find $i(t)$

$V_s(t) = iR + L\frac{di}{dt}$

⇒ $V_m \cos(\omega t) = iR + L\frac{di}{dt}$

both will take cos(wt) form

General form Solution : $i = I_1 \cos\omega t + I_2 \sin\omega t$

⇒ $V_m \cos(\omega t) = (I_1 \cos\omega t + I_2 \sin\omega t)R + L\frac{di}{dt}$

$\frac{di}{dt} = \frac{d}{dt}(I_1 \cos\omega t + I_2 \sin\omega t)$
⇒ $\omega(I_1(-\sin\omega t) + I_2 \cos\omega t)$
⇒ $\omega(I_2 \cos\omega t - I_1 \sin\omega t)$

$V_m \cos(\omega t) = (I_1 \cos\omega t + I_2 \sin\omega t)R + (I_2 \cos\omega t - I_1 \sin\omega t)L\omega$

⇒ $\cos\omega t \cdot (I_1 R + I_2 L) + \sin\omega t \cdot (I_2 R - I_1 L)$

⇒ $(I_1 R + I_2 L - V_m)\cos(\omega t) + (I_2 R - I_1 L)\sin(\omega t) = 0$

* at $t = 0$,
$(I_1 R + I_2 L - V_m)\cdot 1 + (I_2 R - I_1 L)\cdot 0 = 0$

$\boxed{I_1 R + I_2 L = V_m}$

* at $t = \frac{\pi}{2\omega}$, $(I_1 R + I_2 L - V_m)\cdot 0 + (I_2 R - I_1 L)\cdot 1 = 0$

$\boxed{I_1 = I_2 \cdot \frac{R}{L}}$

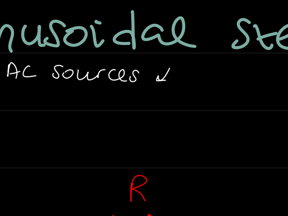
$I_1 R + I_2 L = V_m$ ⇒ $I_2 \frac{R^2}{L} + I_2 L = V_m$ ⇒ $I_2\left(\frac{R^2 + L}{L^2}\right) = V_m$ ⇒ $I_2 = \frac{V_m L^2}{R^2 + L}$

$I_1 = \frac{V_m L R}{R^2 + L}$

14/08/24 # Lecture : 2 9:30 AM

Wednesday → Quiz : Chp 1, 2, 3

* Sinusoidal steady state analysis
AC sources ↙ ↳ not considering any transient response



$V_s = V_m \cos(\omega t)$ ← angular freq

freq (hz) $= \frac{\omega}{2\pi}$

$$V_s(t) = i(t)R + L\frac{di(t)}{dt}$$

general sol^n: $i = I_1\cos(\omega t) + I_2\sin(\omega t)$

put i from gen sol^n in above eq^n

$$I_1 = \frac{RV_m}{R^2+\omega^2L^2}, \quad I_2 = \frac{\omega L V_m}{R^2+\omega^2L^2}$$

$$i(t) = \frac{RV_m}{R^2+\omega^2L^2}\cos(\omega t) + \frac{\omega L V_m}{R^2+\omega^2L^2}\sin(\omega t)$$

Note: use $\cos(A+B) = \cos A\cos B - \sin A \sin B$

⇒ So, $i(t) = A\cos(\omega t + \phi)$: general sol^n

becomes ⇒ $i(t) = A[\cos(\omega t)\cos(\phi) - \sin(\omega t)\sin(\phi)]$

$$\frac{RV_m}{R^2+\omega^2L^2}\cos(\omega t) + \frac{\omega L V_m}{R^2+\omega^2L^2}\sin(\omega t) = A\cos(\omega t)\cos(\phi) - A\sin(\omega t)\sin(\phi)$$

⇓

$$A\cos(\phi) = \frac{RV_m}{R^2+\omega^2L^2}, \quad A\sin(\phi) = \frac{-\omega L V_m}{R^2+\omega^2L^2}$$

$$A^2\cos^2(\phi) + A^2(\sin^2\phi) = A^2(1) = A^2 = \frac{R^2V_m^2 - \omega^2L^2V_m^2}{R^2+\omega^2L^2}$$

⇓

$$\frac{V_m^2(R^2-\omega^2L^2)}{R^2+\omega^2L^2}$$

$$A = \frac{V_m}{\sqrt{R^2+\omega^2L^2}}$$

$$\phi = -\tan^{-1}\left(\frac{\omega L}{R}\right)$$

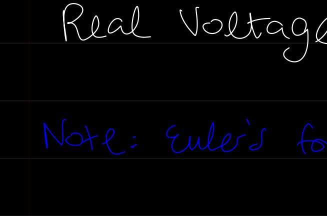
$$i(t) = \frac{V_m}{\sqrt{R^2+\omega^2L^2}}\cos\left(\omega t - \tan^{-1}\left(\frac{\omega L}{R}\right)\right)$$

⇒ Consider a complex source

$$V_m\cos(\omega t) + jV_m\sin(\omega t) = V_m e^{j\omega t}$$

Real Voltage source $= V_m\cos(\omega t) = Re\{V_m e^{j\omega t}\}$

Note: Euler's formula → $e^{j\theta} = \cos\theta + j\sin\theta$



$$V_m e^{j\omega t} = iR + L\frac{di}{dt}$$

dont integrate ✗
general sol^n ✓

Assume $i = I_m e^{j(\omega t + \phi)}$
put eq^n

$$V_m e^{j\omega t} = I_m e^{j\omega t + j\phi}R + L(j\omega)I_m e^{j\omega t + j\phi}$$

$$\Rightarrow I_m e^{j\omega t + j\phi} = \frac{V_m e^{j\omega t}}{R + j\omega L}$$

is this the real current? No
current cannot be complex

$$\text{Real } i(t) = Re\{I_m e^{j\omega t + j\phi}\} = Re\left\{\frac{V_m}{R+j\omega L}e^{j\omega t}\right\}$$

find the real part of this complex number by simplifying
{multiply by the conjugate ≡ factorize}

$$i(t) = \frac{V_m}{R+j\omega L}\left(\frac{R-j\omega L}{R-j\omega L}\right)e^{j\omega t} = \frac{V_m}{\sqrt{R^2+\omega^2L^2}}e^{-j\tan^{-1}\left(\frac{\omega L}{R}\right)}\cdot e^{j\omega t}$$

⇒ Note: rect form → polar form

$x + jy \rightleftarrows re^{j\theta}$

$x = r\cos\theta$, $y = r\sin\theta$

$r = \sqrt{x^2+y^2}$, $\theta = \tan^{-1}\left(\frac{y}{x}\right)$

$$\text{Real } i(t) = Re\left\{\frac{V_m}{\sqrt{R^2+\omega^2L^2}}\cdot e^{j\left(\omega t - \tan^{-1}\left(\frac{\omega L}{R}\right)\right)}\right\}$$

$$* \quad i(t) = \frac{V_m}{\sqrt{R^2+\omega^2L^2}}\cos\left(\omega t - \tan^{-1}\left(\frac{\omega L}{R}\right)\right)$$

Same answer as when we were not considering complex numbers

* PHASOR

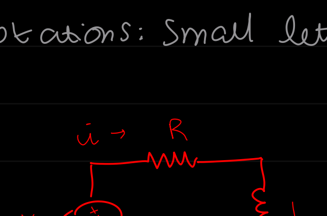
$$i(t) = I_m\cos(\omega t + \phi) = Re\{I_m e^{j\omega t + j\phi}\}$$

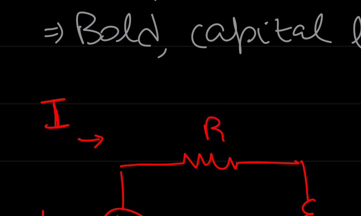
⇓ remove $e^{j\omega t}$, $Re\{\dots\}$

not changing with time
complex func ✗
complex number ✓

$$\underbrace{I_m e^{j\phi}}_{\text{phasor}} = I_m\angle\phi$$

time domain	phasor representation
$i(t) = I_m\cos(\omega t + \phi)$	$I_m\angle\phi$
$v(t) = V_m\cos(\omega t + \theta)$	$V_m\angle\theta$
⇒ real function of t	⇒ complex, constant
⇒ notations: small letters	⇒ Bold, capital letters





$i(t) = I_m\cos(\omega t + \phi)$ ✓
$i(t) = Re\{I_m e^{j\omega t + j\phi}\}$ ✓
$i(t) = I_m\angle\phi$ ✗ complex constant
$i(t) = I_m e^{j(\omega t + \phi)}$ ✗ complex
$i(t) = I_m\angle\omega t + \phi$ ✗ complex phasor notation
phasor notation

but we can write ⇒ phasor notation of $i(t) = I_m\angle\phi = I_m\angle(\omega t + \phi)$

Note: $\angle\phi = e^{j\phi}$ or $\angle\omega t + \phi = e^{j\omega t + j\phi}$

$$\underbrace{V_m e^{j\theta}}_{\mathbf{V}} = (R + j\omega L)\underbrace{I_m e^{j\phi}}_{\mathbf{I}}$$

$$\boxed{\mathbf{V} = (R + j\omega L)\mathbf{I}}$$
↳ phasor notation

* phasor representation of relationship between i and v for R, L, C

① RESISTOR
time domain

$v = iR$

consider complex voltage & current

$v = V_m e^{j(\omega t + \theta)}$
$i = I_m e^{j(\omega t + \phi)}$

$$V_m e^{j\omega t + j\theta} = R\cdot I_m e^{j\omega t + j\phi}$$

$$V_m \cancel{e^{j\omega t}}\cdot e^{j\theta} = R\cdot I_m \cancel{e^{j\omega t}}e^{j\phi}$$

$$V_m e^{j\theta} = R\cdot I_m e^{j\phi}$$

$$\underbrace{V_m\angle\theta}_{\mathbf{V}} = \underbrace{I_m\angle\phi}_{\mathbf{I}}\cdot R$$

$$\boxed{\mathbf{V} = \mathbf{I}R}$$

② INDUCTOR

$v = L\frac{di}{dt}$

$v \to V_m e^{j(\omega t + \theta)}$ $\quad$ $i \to I_m e^{j\omega t + j\phi}$

$$V_m e^{j\omega t}e^{j\theta} = L\, I_m e^{j\omega t}\cdot e^{j\phi}(j\omega)$$

$$\underbrace{V_m e^{j\theta}}_{\mathbf{V}} = j\omega L\cdot\underbrace{I_m e^{j\phi}}_{\mathbf{I}}$$

$$\boxed{\mathbf{V} = j\omega L\cdot\mathbf{I}}$$

③ CAPACITOR

$i = C\frac{dv}{dt}$

$i \to I_m e^{j(\omega t + \phi)}$
$v \to V_m e^{j(\omega t + \theta)}$

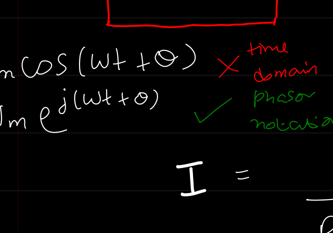
$$I_m\cancel{e^{j\omega t}}\cdot e^{j\phi} = C\cdot V_m\cancel{e^{j\omega t}}e^{j\theta}\cdot j\omega$$

$$\underbrace{I_m e^{j\phi}}_{\mathbf{I}} = C\cdot j\omega\cdot\underbrace{V_m e^{j\theta}}_{\mathbf{V}}$$

$$\mathbf{I} = j\omega C\cdot\mathbf{V}$$

$$\boxed{\mathbf{V} = \frac{1}{j\omega C}\cdot\mathbf{I}}$$

* PHASOR Representation using KVL



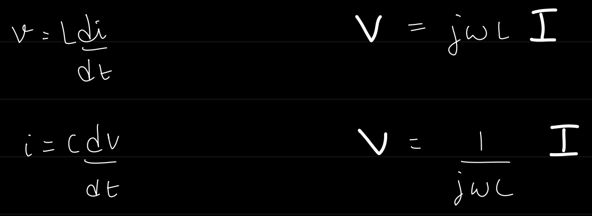
$V_s = V_m\cos(\omega t + \theta)$ ✗ time domain
$V_s = V_m e^{j(\omega t + \theta)}$ ✓ phasor notation

$$\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_L$$
$$= \mathbf{I}R + (j\omega L)\mathbf{I}$$
$$= \mathbf{I}(R + j\omega L)$$

$$\mathbf{I} = \frac{\mathbf{V}_s}{R + j\omega L} = \frac{V_m\angle\theta}{R + j\omega L}$$

Time domain	Phasor (= Frequency domain)
R: $v = iR$	$\mathbf{V} = \mathbf{I}R$
L: $v = L\frac{di}{dt}$	$\mathbf{V} = j\omega L\,\mathbf{I}$
C: $i = C\frac{dv}{dt}$	$\mathbf{V} = \frac{1}{j\omega C}\mathbf{I}$

⇒ Example



① Given: both AC sources, V_s & I_s operate at $\omega = 2$ rad/s

② Given: $I_c = 2\angle 28°$ A

Find (i) V_c
(ii) I_{R_2}
(iii) I_s

① $$V_c = \frac{I_c}{j\omega C} = \frac{1}{j(2)(1)}\cdot 2\angle 28°$$

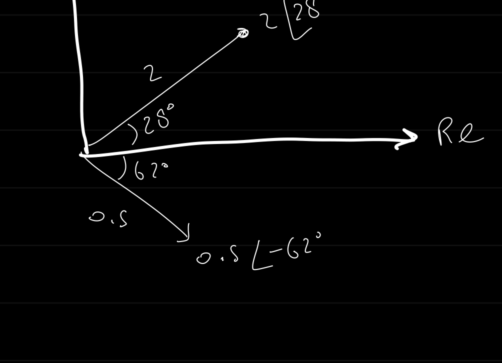
Note: $\frac{1}{j} = -j = -90°$

we add the angles directly which are being multiplied

$$V_c = (0.5\angle -90°)(2\angle 28°) = 1\angle -62°\text{ V}$$

② $$I_{R_2} = \frac{V_{R_2}}{R_2} = \frac{V_{R_2}}{2} = \frac{1\angle -62°}{2} = 0.5\angle -62°\text{ A}$$

③ $$I_s = 0.5\angle -62° + 2\angle 28°$$



$2.06\angle 14°$ A

* Lecture : 3

19/08/24 9:30Am

- Phasor : $i(t) = I_m \cos(\omega t+\phi) = Re\{I_m e^{j(\omega t+\phi)}\}$

Remove $e^{j\omega t}$ and $Re\{...\}$

$I_m e^{j\phi} = I_m \angle \phi$ } Phasor

exponential form — polar form

time domain ⇄ freq. domain

$V_R = IR \qquad V_L = j\omega L I \qquad V_c = \frac{1}{j\omega C} I$

* IMPEDANCE

$$Z = \frac{V}{I} = \frac{1}{R}$$

$Z_R = R$ — voltage and current in the same phase

$Z_L = j\omega L$ — voltage leads current by 90°

$Z_C = \frac{1}{j\omega C}$ — voltage lags current by 90°

$$Z = x + jy$$

resistance (x), reactance (y)

* Admittance

$$Y = \frac{1}{Z}$$

$$Y = x + jy$$

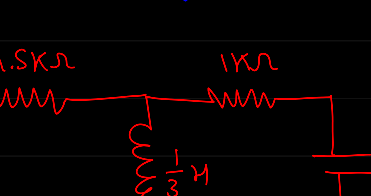
conductance (x), susceptance (y)

* Impedance combination

Series : $Z_{eq} = Z_1 + Z_2 + \dots Z_N$

Parallel : $Z_{eq} = \frac{1}{Z_1} + \frac{1}{Z_2} + \dots \frac{1}{Z_N}$

eg) Find impedance of series combination of an inductor L (L=5mH) and capacitor (C=100μF) $\omega = 10^4$ rad/s

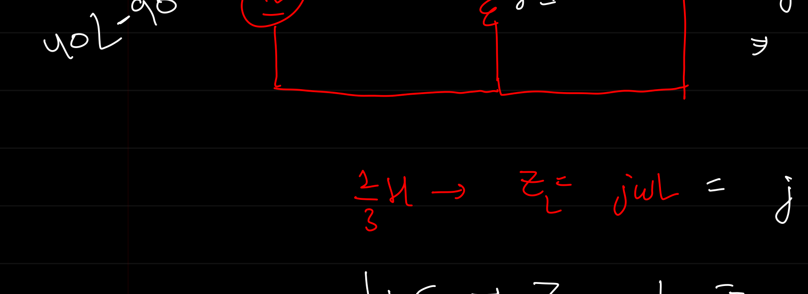


$\Rightarrow Z_{eq} = Z_L + Z_C = j\omega L + \frac{1}{j\omega C} = 10^4 \cdot j \cdot 5\times10^{-3} + \frac{10^{-4}\times10^{3}}{j\cdot 5\times 100 \times 10^{-6}}$

Note: $\frac{1}{j} = -j$ $\qquad \Rightarrow 50j - j = 49j$

Note: $e^{j\theta} = \cos\theta + j\sin\theta = e\angle\theta$ $\qquad \Rightarrow 0 + 49j = 49e^{j\cdot\frac{\pi}{2}}$

eg:

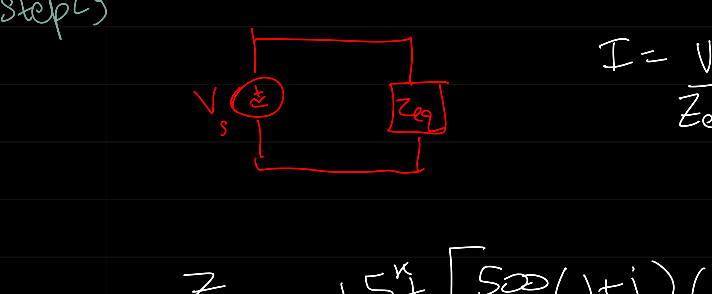


Find i(t)

$\frac{10^3(1-2j)(1+j)}{2}$

$500(1-2j)(1+j)$ ⇐ $\frac{10^3(1-2j)}{1-j}$

step1) Convert to freq. domain (write in terms of phasor and Z)



$1000 - 2000j \parallel 1000j$

$\left(\frac{1}{1000-2000j} + \frac{1}{1000j}\right)^{-1}$

$-j\cdot 2K\Omega$

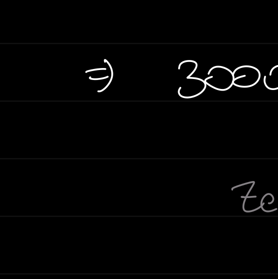
$\Rightarrow \frac{1-j}{\frac{10^3 - 2\cdot10^3 j}{1000j + 1000 - 2000j}}{(10^3 - 2\cdot 10^3 j)10^3 \cdot j}$

$\frac{1}{3}H \rightarrow Z_L = j\omega L = j\cdot 3000 \cdot \frac{1}{3} \Rightarrow j\cdot 1k$

$\frac{1}{6}\mu F \rightarrow Z_c = \frac{1}{j\omega C} = \frac{1}{j\cdot 3000 \times \frac{1}{6}\times 10^{-6}} \Rightarrow \frac{2\cdot 10^3}{j}$

$\Rightarrow -j\cdot 2K\Omega$

step2)



$$I = \frac{V_s}{Z_{eq}}$$

$Z_{eq} = 1.5^k + \left[500(1+j)(1-2j)\right]$

$\Rightarrow 1500 + 500\left[1 - 2j + j + 2\right)$

$\Rightarrow 500\left[3 + 3 - j\right] \Rightarrow 500[6 - j]$

$\Rightarrow 3000 - 500j$

$\frac{j(1-2j)(1+j)}{2} \Rightarrow \frac{(j+2)(1+j)}{2} \Rightarrow \frac{j+j^2+2+2j}{2}$ $K\Omega$

PPT) $\quad Z_{eq} = 1.5 + \frac{(jL)(1-j2)}{1-j}$ $\qquad \frac{3j+1}{2}$

$\Rightarrow \frac{4+3j}{2}$

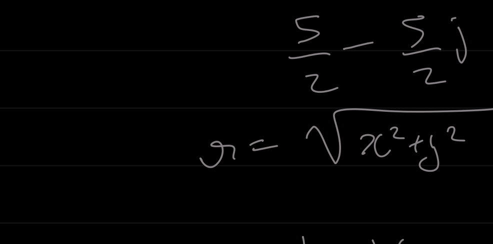
Note: complex number < $x+iy$, $r\angle\theta$

$r = \sqrt{x^2+y^2}$

$\theta = \tan^{-1}\left(\frac{y}{x}\right)$

$I_3 + I_2 = I_1$

eg)



find I_1, I_2, I_3

$Z_{eq} \overset{(1)}{=} \left(\frac{1}{5} + \frac{1}{5j}\right)^{-1} = \left(\frac{5j+5}{25j}\right)^{-1} = \frac{5j}{j+1}$

$Z_{eq} \Rightarrow^{(2)} -5j + \frac{5j}{j+1} \Rightarrow \frac{+5 - 5j + 5j}{j+1} = \frac{5}{j+1}$

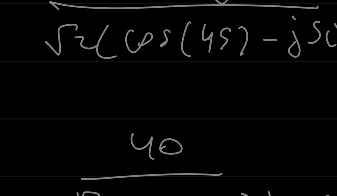
$\Rightarrow \frac{5(j-1)}{-2} \Rightarrow \frac{5-5j}{2}$

$\frac{5}{2} - \frac{5}{2}j$ $\qquad \frac{5\sqrt{2}}{2}$

$r = \sqrt{x^2+y^2} = \sqrt{\frac{25}{4} + \frac{25}{4}} = \frac{\sqrt{50}}{2}$

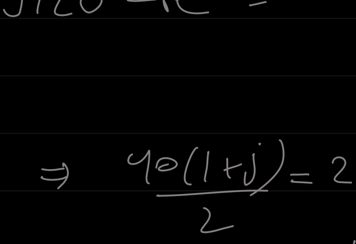
$\theta = \tan^{-1}(-1) \Rightarrow -45°$

Voltage division



$V_1 = V\cdot\frac{R_1}{R_1+R_2}$

Current division



$i_1 = i\cdot\frac{R_2}{R_1+R_2}$

$I_1 = \frac{V}{Z_{eq}} = \frac{\cancel{100}^{20}\angle 0°}{\frac{5\sqrt{2}}{2}\angle -45°} \Rightarrow \frac{40\angle 0°}{\sqrt{2}\angle -45°}$

$\frac{40(\cos 0 + j\sin 0)}{\sqrt{2}(\cos(45) - j\sin(45))}$ $\qquad r\angle\theta = re^{j\theta} =$

$\frac{40}{\sqrt{2}\left(\frac{1}{\sqrt{2}} - j\frac{1}{\sqrt{2}}\right)} \Rightarrow \frac{40}{1-j} \Rightarrow \frac{40(1+j)}{2} = 20(1+j)$

$20 + 20j$

$r = \sqrt{x^2+y^2} \Rightarrow \sqrt{400+400} \Rightarrow 20\sqrt{1+1} = 20\sqrt{2}$

$\theta = \tan^{-1}(1) = 45°$

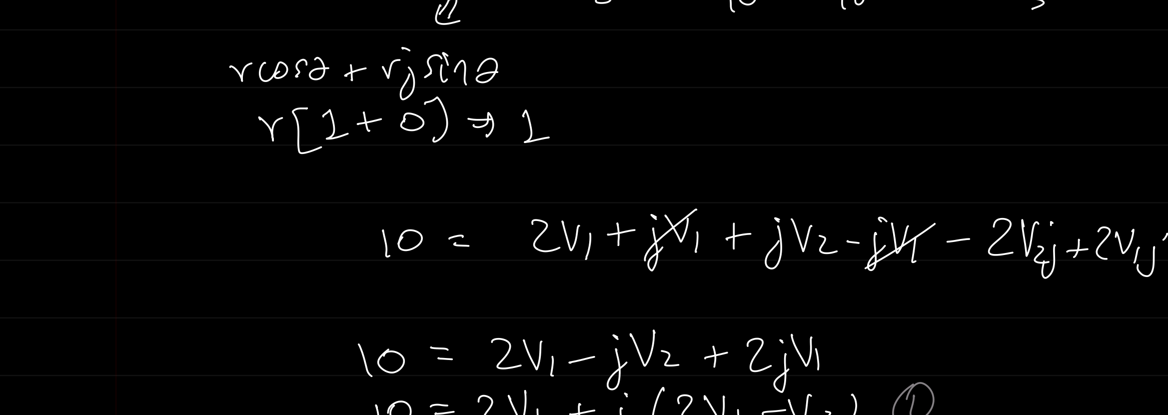
$I_1 = 20\sqrt{2}\angle 45°$

$I_2 = I_1 \times \frac{j5}{5+j5} \Rightarrow \cancel{20}^{10}\sqrt{2}\angle 45° \times \frac{j(1-j)}{2}$

$\Rightarrow 10\sqrt{2}\angle 45° \times (j+1)$

* NODAL ANALYSIS

Node ≡ Same voltage



at node 1:

$1\angle 0° = \frac{V_1}{5} + j\frac{V_1}{10} + \frac{(V_2-V_1)j}{10} - \frac{(V_2-V_1)j}{5}$

$r\cos\theta + rj\sin\theta$

$r[1 + 0) \Rightarrow 1$

$10 = 2V_1 + \cancel{jV_1} + jV_2 - \cancel{jV_1} - 2V_2 j + 2V_1 j$

$10 = 2V_1 - jV_2 + 2jV_1$

$10 = 2V_1 + j(2V_1 - V_2)$ ①

at node 2:

$\frac{V_2 - V_1}{j10} + \frac{V_2 - V_1}{-j5} + \frac{V_2}{j5} + \frac{V_2}{10} = 0.5\angle -90°$

$0.5\cos 90° - 0.5j\sin 90°$
$\Rightarrow -0.5j$

$V_2 - V_1 + 2V_1 - \cancel{2V_2} + \cancel{2V_2} + V_2 j = 5$

$3V_2 - V_1 + V_2 j = 5 \Rightarrow V_1 = 3V_2 - 5 + V_2 j$

Put value of V_1 in ①

$10 = 6V_2 - 10 + 2V_2 j + j(6V_2 - 10 + 2V_2 j - V_2)$

$10 = 6V_2 - 10 + 2V_2 j + 6V_2 j - 10j - 2V_2 - V_2 j$

$20 = 4V_2 + 7V_2 j - 10j$ $\qquad \frac{30-20j}{13}$

$20 + 10j = V_2(4 + 7j)$ $\qquad \frac{150-100j}{65}$

$V_2 = \frac{(20+10j)(4-7j)}{16+49} = \frac{80 - 140j + 40j + 70}{65}$

$V_2 = \frac{30}{13} - j\left(\frac{20}{13}\right)$ $\qquad r = \sqrt{\frac{900+400}{169}} = \frac{10}{\sqrt{13}}$

$\theta = \tan^{-1}\left(\frac{-2}{3}\right)$

$V_2 = \frac{10\sqrt{13}}{13}\angle -33.69°$

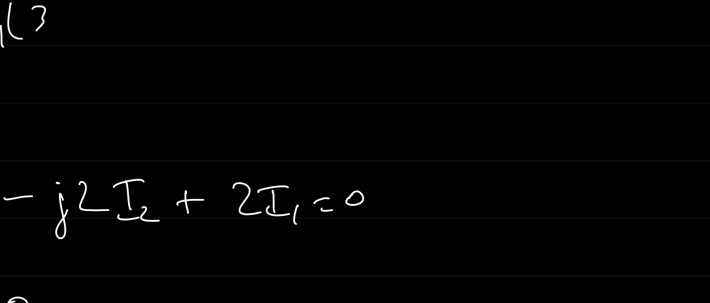
$= -\tan\left(\frac{2}{3}\right) =$
$= -33.69$

$V_1 = 3V_2 - 5 + jV_2$

$\Rightarrow V_2(3+j) - 5 = \frac{30}{13} - \frac{20j}{13}(3+j) - 5$

$\Rightarrow \frac{30 - 60j + 20 - 65}{13} = \frac{-60j - 15}{13} \Rightarrow V_1 = \frac{15\sqrt{17}}{13}\angle -104°$

* Mesh Analysis



2 meshes

$10\angle 0° = 3I_1 + j4(I_1 - I_2)$

$(I_2 - I_1)j4 - I_2(j2) + 2I_1 = 0$

$10\angle 0° = 10 = 3I_1 + j4(I_1 - I_2) = 3I_1 + j4I_1 - j4I_2$

$j4I_2 + 10 = I_1(3$

$j4I_2 - j4I_1 - j2I_2 + 2I_1 = 0$

$j4I_2 - j4(10 -$

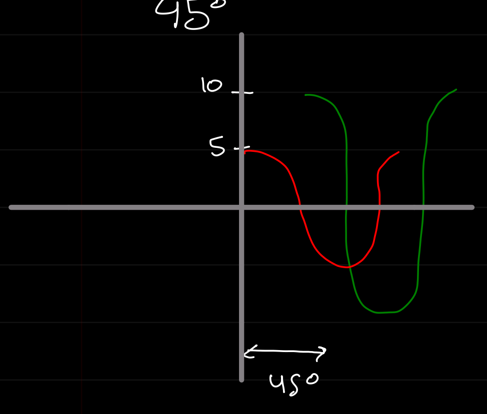
* CTD Tutorial : 1

19/08/24 1:00 - 3:00

Q1) Determine the angle by which v_1 leads i_2 if $V_1 = 10\cos(10t - 45^\circ)$ and i_1 is equal to

(1) $i_1 = 5\cos 10t$ (2) $i_1 = 5\cos(10t - 40^\circ)$

45° 5°



(2) $i_1 = 5\cos(10t - 80^\circ)$ (4) $i_1 = 5\cos(10t + 40^\circ)$

35° 85°

(5) $5\sin(10t - 19^\circ)$

$= 5\cos(10t - 19^\circ - 90^\circ)$

$= 5\cos(10t - 109^\circ)$

Ans: 64°

Q2) Determine which waveform in each of the following pairs is lagging

(1) $\cos 4t$ leads $\sin 4t$ by $\frac{\pi}{2}$ $\{90^\circ\}$

(2) $\cos(4t - 80^\circ)$ lags $\cos(4t)$ by 80°

(3) $\cos(4t + 80^\circ)$ leads $\cos(4t)$ by 80°

(4) $\sin(5t)$ lags $\cos(5t + 2^\circ)$ by 92°

(5) $\sin 5t + \cos 5t$

Q3) Perform the indicated operation {express in rectangular & polar form}

(a) $\frac{2 + j3}{1 + 8\angle 90^\circ} - 4$

$8\angle 90^\circ$

$\hookrightarrow r\cos\theta + j\sin\theta = 8 \cdot 0 + 8 \cdot j \cdot 1 = 8j$

$\Rightarrow \frac{2 + j3}{1 + 8j} - 4 \Rightarrow \frac{2 + j3 - 4 - j32}{1 + 8j} \times \frac{1 - 8j}{1 - 8j}$

$\Rightarrow \frac{(-2 + 29j)(1 - 8j)}{8} = -2 + 16j + 29j + (29 \times 8)$

$\Rightarrow 230 + 45j$

$\Rightarrow 46 + 9j$

$\frac{2 + j3}{1 + 8\angle 90^\circ} - 4$

$\Downarrow$

$8\angle 90^\circ = 8 \cdot \cos(90) + 8 \cdot j\sin(90) = 8j$

$\frac{2 + j3}{1 + j8} \times \frac{1 - 8j}{1 - 8j} - 4$

$\Rightarrow \frac{2 - 16j + j3 + 24}{65} - 4 \Rightarrow \frac{26 - 13j}{65} - 4$

$\Downarrow$

$\frac{-234 - 13j}{65} \Leftarrow \frac{26 - 13j - 260}{65}$

$x \quad y \quad \boxed{-\frac{18}{5} - \frac{1}{5} \cdot j}$ rectangular form

$\Downarrow$

$r = \sqrt{x^2 + y^2} = \sqrt{\frac{18^2}{25} + \frac{1}{25}}$

$\Rightarrow \sqrt{\frac{325}{25}} = \sqrt{13}$

$\theta = \tan^{-1}\left(\frac{y}{x}\right) = \tan^{-1}\left(\frac{1}{18}\right) = 3.179^\circ$

polar form $\boxed{\sqrt{13} \angle 3.179^\circ}$

(b) $\left(\frac{10\angle 25^\circ}{5\angle -10^\circ} + \frac{3\angle 15^\circ}{3 - 5j}\right) j2$

Q4) Transform into Phasor form

(a) $11 \sin 100t$

(b) $11 \cos 100t$

(c) $11\cos(100t - 90^\circ)$

(d) $3\cos 100t - 3\sin 100t$

Q5) Determine equivalent Admittance assuming $w = 1000$ rad/s

(a) 25Ω in series with $20mH$

$Z_L = jwL = j \times 1000 \times 20 \times 10^{-3}$

$= j \cdot 20$

Admittance $(Y) = \frac{1}{Z_{eq}}$

$Z_{eq} = 25 + j20 \nearrow Y = \frac{1}{25 + j20} \times \frac{25 - j20}{25 - j20}$

$\boxed{\frac{1}{41} - \frac{4}{205} \cdot j} \Leftarrow \frac{5 - j4}{205} \Leftarrow \frac{25 - j \cdot 20}{625 + 400} \Rightarrow \frac{25 - j \cdot 20}{1025}$

(b) 25Ω in parallel with $20mH$

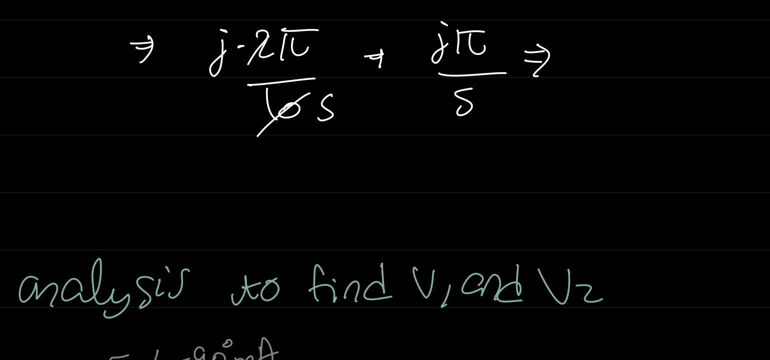
admittance $= \frac{1}{25} + \frac{1}{20j} = \frac{\overset{5}{\cancel{25}} + j\overset{4}{\cancel{20}}}{\underset{100}{\cancel{500}}j}$

$\frac{-j \cdot 5 - 4}{100} \Leftarrow \frac{-j(5 + j \cdot 4)}{100} \Leftarrow \frac{5 + j \cdot 4}{100j}$

$\hookrightarrow -\frac{1}{25} + \left(\frac{-j}{20}\right)$

Q6) Calculate the equivalent impedance as seen at the open terminals if the freq is ...

(a) 1Hz
(b) 1KHz
(c) 1MHz
(d) 1GHz



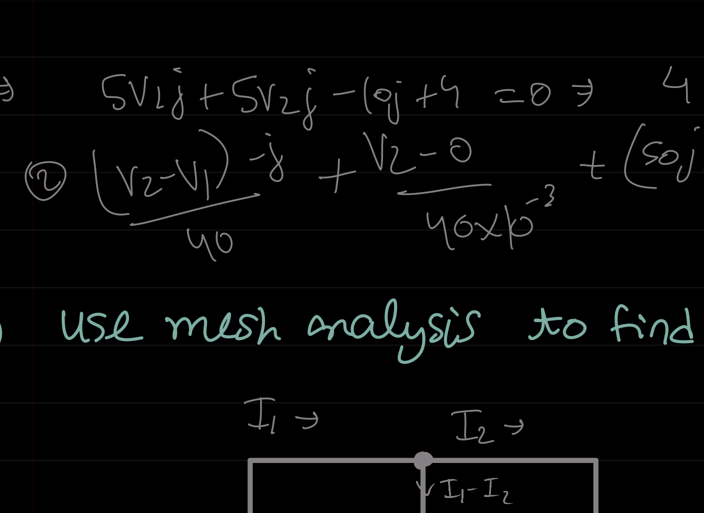
(a) $f = 1Hz$ $w = 2\pi f$ $= 2\pi$ radians/s

$Z_L = jwL = j \cdot 2\pi \cdot 100 \times 10^{-3}$

$\Rightarrow \frac{j \cdot 2\pi}{\cancel{10}5} \rightarrow \frac{j\pi}{5} \Rightarrow$

Q7) Use nodal analysis to find V_1 and V_2

$\frac{1}{-25 \times j \times 10^{-3}}$



$\boxed{V1}$

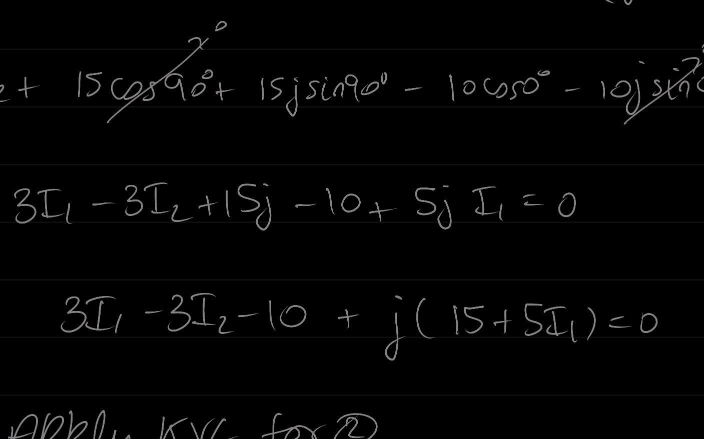
$\frac{V_1 \cdot j}{20} - \frac{(V_1 - V_2)j}{40} + (-50j \times 10^{-3}) + 20 \times 10^{-3} = 0$

$\Rightarrow \frac{5(V_1 j + V_2 j)}{10} - \frac{10j}{10} + \frac{4}{10} = 0$

$\Rightarrow 5V_1 j + 5V_2 j - 10j + 4 = 0 \Rightarrow 4 + j(5V_1 + 5V_2 - 10) = 0$

(2) $\frac{(V_2 - V_1) \cdot -j}{40} + \frac{V_2 - 0}{40 \times 10^{-3}} + (50j \times 10^{-3}) = 0$

Q8) Use mesh analysis to find I_1 and I_2



Apply KVL for (1):

$3(I_1 - I_2) + 15\angle 90^\circ - 10\angle 0^\circ + I_1(j5) = 0$

$3I_1 - 3I_2 + 15\cancel{\cos 90^\circ} + 15j\sin 90^\circ - 10\cos 0^\circ - 10j\cancel{\sin 0^\circ} + I_1 5 \cdot j = 0$

$3I_1 - 3I_2 + 15j - 10 + 5j I_1 = 0$

$3I_1 - 3I_2 - 10 + j(15 + 5I_1) = 0$

Apply KVL for (2)

$-4I_2 \cdot j + 20\angle 0^\circ - 15\angle 90^\circ + (I_2 - I_1)3 = 0$

$-4I_2 \cdot j + 20 - 15j + 3I_2 - 3I_1 = 0$

$3I_2 - 3I_1 + 20 + j(-15 - 4I_2) = 0$

$3I_1 = 3I_2 + 20 + j(-15 - 4I_2)$

Put (2) in (1)

$3I_1 - 3I_2 - 10 + j(15 + 5I_1) = 0$

$3\cancel{I_2} + 20 + j(-15 - 4I_2) - 3\cancel{I_2} - 10 + j(15 + 5I_1) = 0$

$10 + j(-15 - 4I_2) + j\left(15 + 5\left[\frac{3I_2 + 20 - 15j - 4I_2 \cdot j}{3}\right]\right) = 0$

$30 - 45j - 12I_2 j + j(45 + 15I_2 + 100 - 75j - 20I_2 j) = 0$

$30 - \cancel{45}j - 12I_2 j + \cancel{45}j + 15I_2 j + 100j + 75 + 20I_2 = 0$

$105 + 20I_2 + j(3I_2 + 100) = 0$

$105 + 20I_2 + j \cdot 3I_2 + j \cdot 100 = 0$

$I_2(20 + j \cdot 3) = -105 - j \cdot 100$

$I_2 = \frac{-105 - j \cdot 100}{20 + j \cdot 3} \times \frac{20 - j \cdot 3}{20 - j \cdot 3}$

$I_2 = \frac{-2100 + 315 \cdot j - 2000j - 300}{409}$

$I_2 = \frac{-2400 - 1685j}{409}$

Homework:1

19/08/24

* Section 10.1

Q1) (a) $5\sin(5t-9^\circ)$

$t=0 \Rightarrow 5\sin(-9^\circ) = -5\sin(9^\circ) = -0.782$

$t=0.01 \Rightarrow 5\sin(0.05-9^\circ) = -5\sin(8.95^\circ)$ X

$\Downarrow$ radians

$5\sin\left(\left[0.05\times\frac{180}{\pi}\right)-9^\circ\right) = 5\sin(2.86^\circ-9^\circ)$

$\Rightarrow -5\sin(6.14) = -0.534$

$t=0.1s \Rightarrow 5\sin(0.5-9^\circ) = 5\sin(28.64-9) = 5\sin(19.64)$

$\Rightarrow 1.6805$

(b) $4\cos 2t$

$t=0 \Rightarrow 4\cos(0) = 4$

$t=1 \Rightarrow 4\cos(2) = 3.997$

$t=1.5 \Rightarrow 4\cos(3) = 3.994$

(c) $3.2\cos(6t+15^\circ)$

$t=0 \Rightarrow 3.2\cos(15^\circ) = 3.09$

$t=0.01 \Rightarrow 3.2\cos(0.06+15^\circ) = 3.2\cos(3.43^\circ+15^\circ)$

$\Rightarrow 3.2\cos(18.43^\circ)$

$\Rightarrow 3.035$

$t=0.1 \Rightarrow 3.2\cos(0.6+15^\circ) = 3.2\cos(34.3^\circ+15^\circ)$

$= 3.2\cos(49.3)$

$= 2.086$

Q2) (a) $300\sin(628t) \rightarrow 300\cdot\cos(628t-90^\circ)$

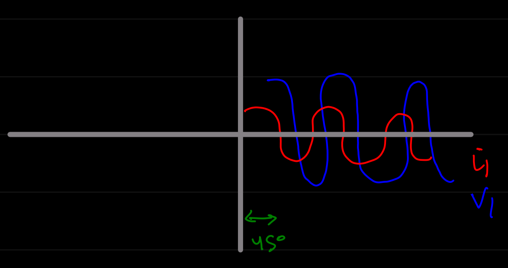
$4\sin(3\pi t+30^\circ) \rightarrow 4\cos(3\pi t-60^\circ)$

$14\sin(50t-5^\circ) - 10\cos 50t \rightarrow$

Q3) $v_1 = 10\cos(10t-45^\circ)$

(a) $i_1 = 5\cos 10t$

-45°

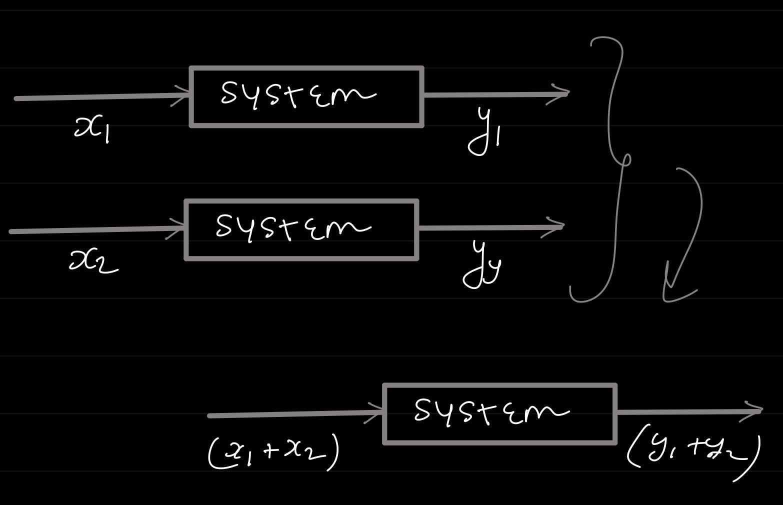


LECTURE : 4

9:30 – 11:00AM
21/08/24

* Superposition principle

active elements : provide energy eg: volt src/ curr src
passive element : consume/ store energy
eg: R/L/C

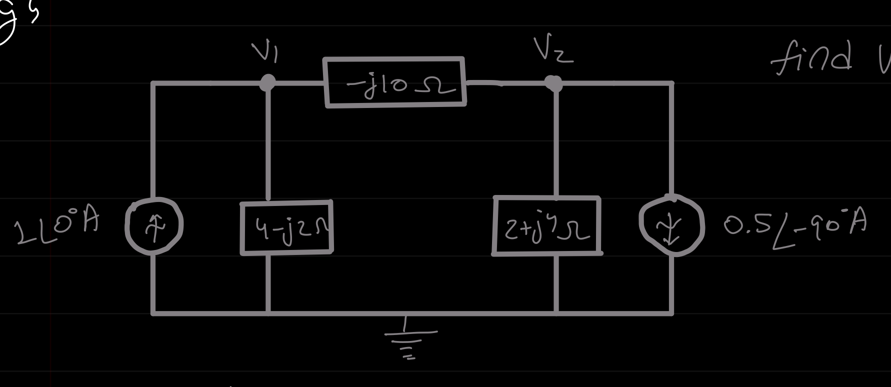


* Multiple independent sources

- consider separate independent sources "acting alone"
- add all responses

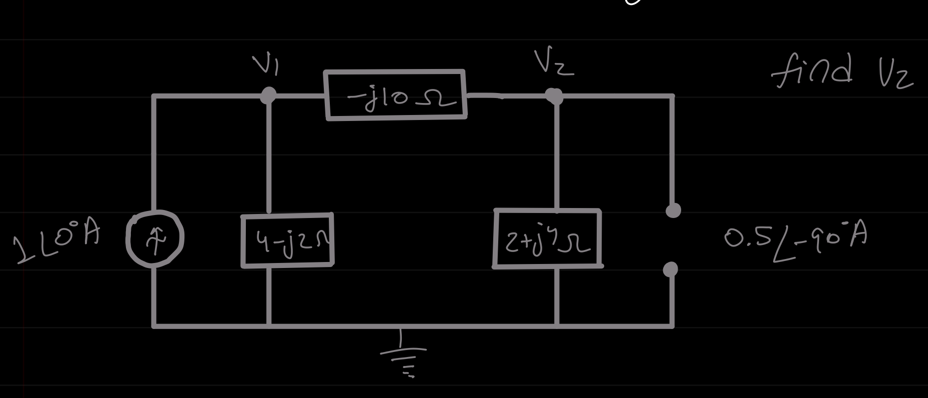
eg)

find V_2

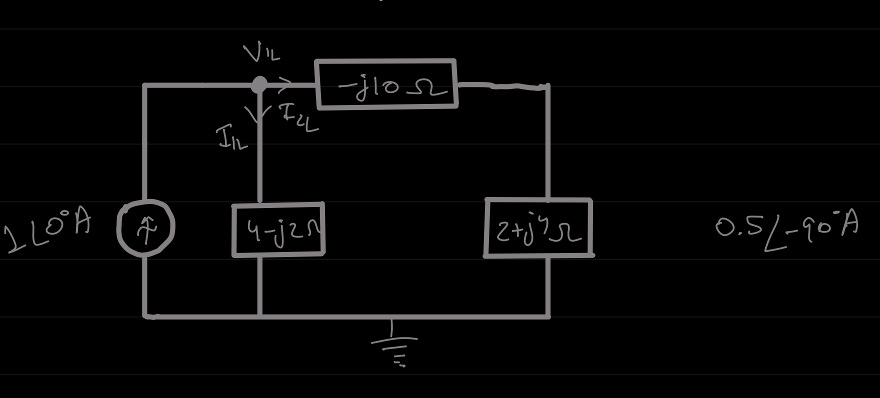


consider left side source
so we need to open the circuit at the right source

find V_2



$\Downarrow$



$V_{1L} = I_{1L}(4-j2)$

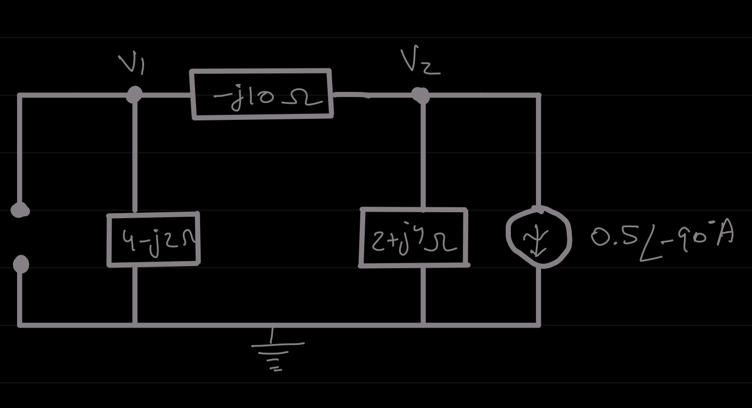
$$\Rightarrow \frac{-j10+2+j4}{(4-j2)+(-j10+2+j4)}(4-j2)$$

$$\Rightarrow \frac{(2-j6)(4-j2)}{6-j8} \Rightarrow \frac{8-j4-24j-12}{6-8j}$$

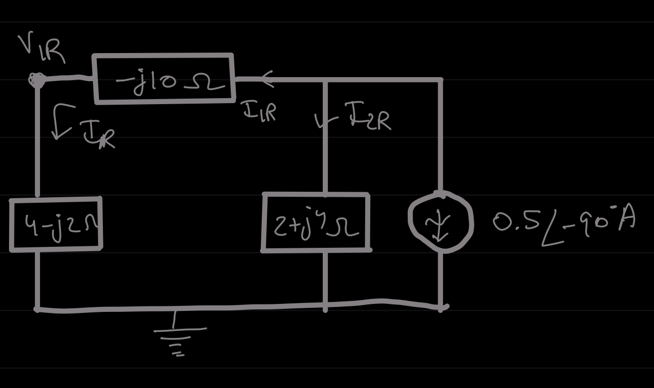
$$\Rightarrow \frac{-4-28j}{6-8j} = 2-j2\,V$$

$I_{1L} + I_{2L} = 1\angle 0^\circ = 1\cos 0^\circ + j1\sin 0^\circ = 1A$

consider right src



$\Downarrow$



$V_{1R} = I_{1R}(4-j2)$

$$I_{1R} = \frac{(-0.5\angle -90^\circ A)(2+j4)}{-j10+4-2j+2+j4}$$

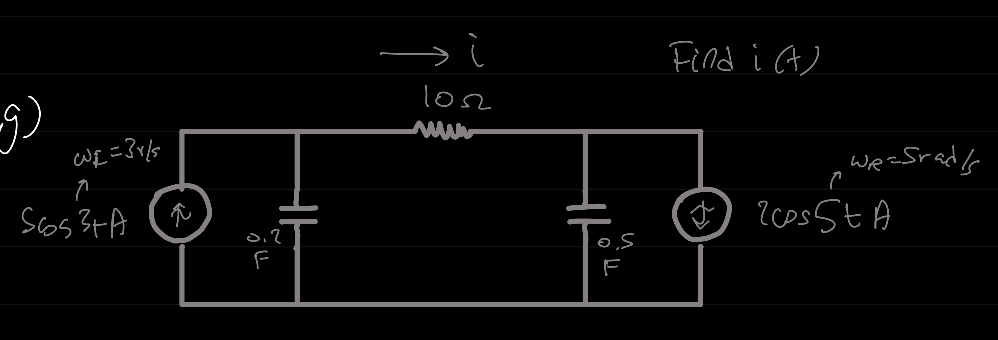
$$V_{1R} = \frac{(j\,0.5)(2+j4)(4-j2)}{6-j8}$$

$$\Rightarrow \frac{(j-2)(4-j2)}{6-j8} = \frac{j4+2-8+j4}{6-j8} = \frac{j8-6}{6-j8} = -1V$$

$V_1 = V_{1L} + V_{1R} = 2-j2-1 = \boxed{1-j2\,V}$

eg)

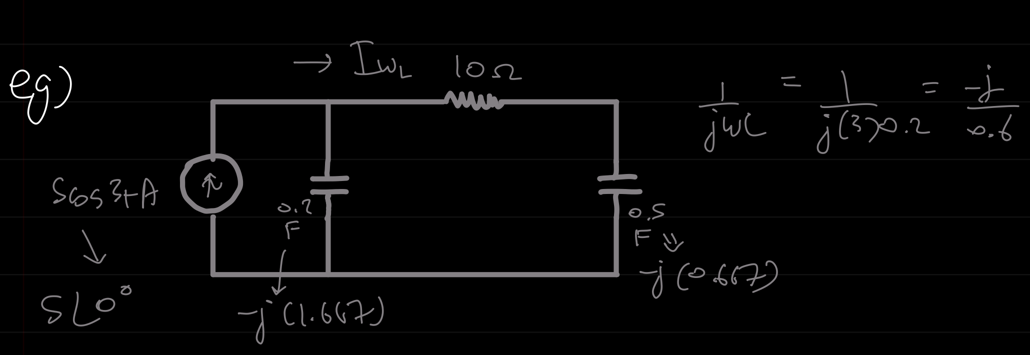
Find $i(t)$



Note: we have 2 sources operating at 2 different frequencies (ω)

① consider left src $\omega_L = 3\,rad/s$

eg)

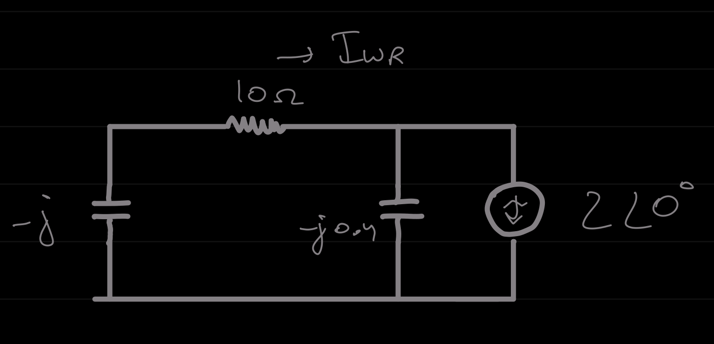


$$\frac{1}{j\omega C} = \frac{1}{j(3)0.2} = \frac{-j}{0.6}$$

$$I_{\omega_1} = 5\angle 0^\circ\left(\frac{-j(1.667)}{-j(1.667)+10-j(0.667)}\right)$$

$\Rightarrow 811.7\angle -76.86^\circ\,mA$

② consider right source $\omega_R = 5\,rad/s$



$$I_{\omega R} = 2\angle 0^\circ\left(\frac{-j\cdot 0.4}{-j0.4+10+-j}\right)$$

$$\Rightarrow \frac{-j(0.8)}{-j(1.4)+10} \Rightarrow \frac{-j(0.8)[10+j(1.4)]}{100+1.96}$$

$$\Downarrow$$

$$\frac{-j8+1.12}{101.96} \Rightarrow$$

$\Rightarrow 0.0792\angle -82.03^\circ\,A = 79.2\angle -82.03\,mA$

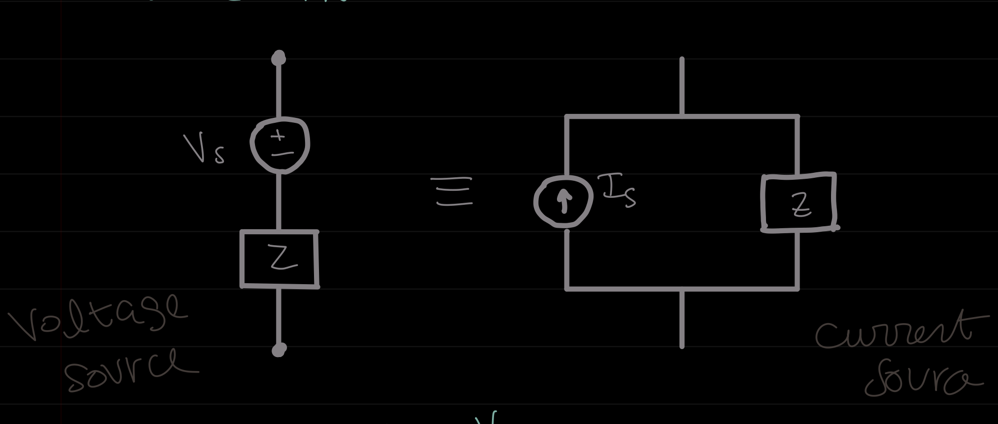
Applying superposition

$I = I_{\omega L} + I_{\omega R}$ ✗

Phasors can only be added when they correspond to same frequency

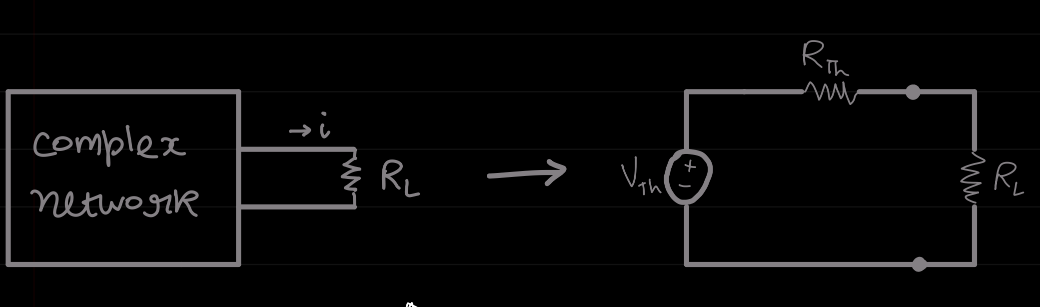
$i(t) = [811.7\cos(3t-76.86^\circ) + 79.25\cos(5t-82.03)]\,mA$

* SOURCE TRANSFORMATION

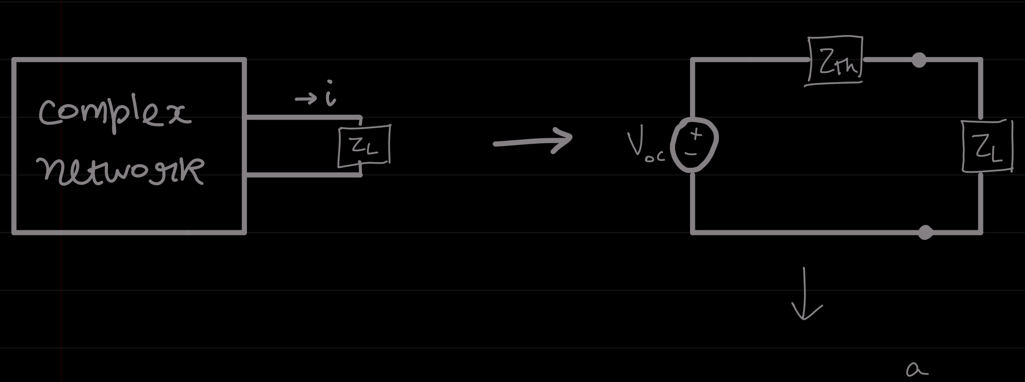


$I_s = \dfrac{V_s}{Z}$

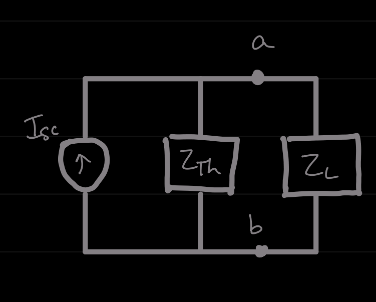
* THEVENIN & NORTON EQUIVALENT CKTS



Normally

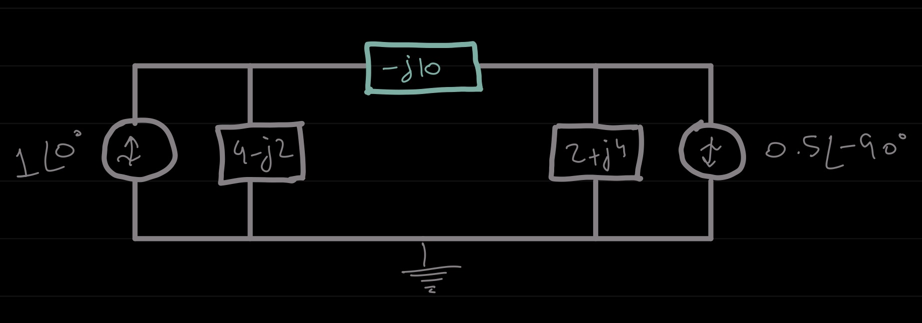


$V_{oc} = I_{sc} \cdot Z_{TH}$

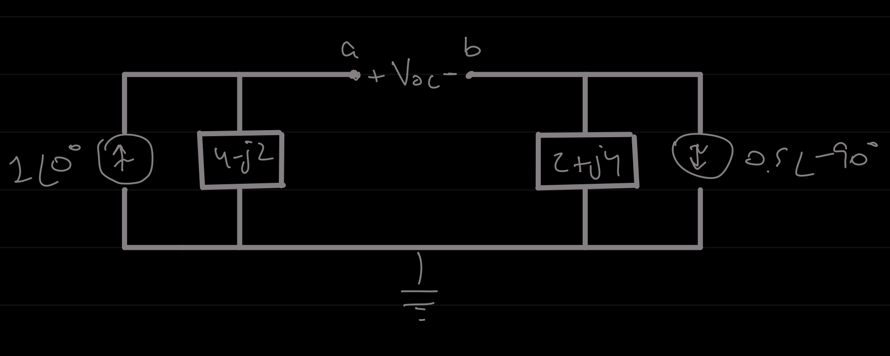


	by open circuiting V_{oc}	by short circuiting I_{sc}	Z_{TH} ratio of V_{oc} & I_{sc}
① Independent sources	✓	✓	✓
② Independent + dependent sources	✓	✓	✓
③ Dependent sources only	we need to consider test sources eg: 1A / 1V and then find $V_{oc} \Rightarrow I_{sc} \Rightarrow Z_{TH} = \frac{V_{oc}}{I_{sc}}$		

eg) find Thevenin equivalent seen by $-j10\,\Omega$



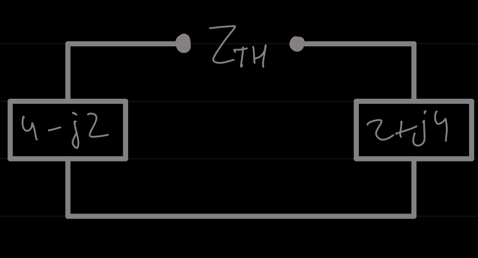
- : complex network
- : R_L



$V_{oc} = V_a - V_b = 1\angle 0^\circ(4-j2) - 0.5\angle -90^\circ(2+j4)$
$= 4-j2+2-j1 = 6-j3\,V$

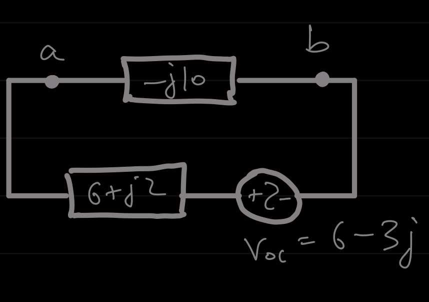
Find Z_{Th}

all volt src → short circuit
all curr src → open circuit



$Z_{TH} = 4-j2+2+j4 = 6+j2\,\Omega$

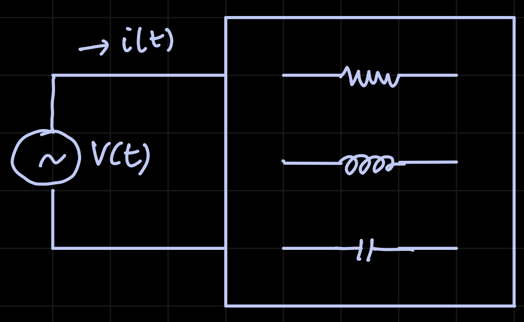
Equivalent circuit



$$I_{ab} = \frac{V_{oc}}{6+j2-j10} = \frac{V_{oc}}{6-j8}$$

* Lecture : 5 28/08/24

⇒ AC Power Analysis {Module : 3}



$\cos(A)\cos(B) = \frac{1}{2}[\cos(A+B) + \cos(A-B)]$

instantaneous power : $p(t) = v(t) \cdot i(t)$

$$v(t) = V_m \cdot \cos(\omega t + \theta)$$
$$i(t) = I_m \cdot \cos(\omega t + \phi)$$

$$p(t) = V_m \cdot \cos(\omega t + \theta) \cdot I_m \cdot \cos(\omega t + \phi)$$

$$p(t) = \underbrace{\frac{V_m I_m}{2} \cos(\theta - \phi)}_{\substack{\text{constant} \\ \text{(DC term)}}} + \underbrace{\frac{V_m I_m}{2} \cos(2\omega t + \theta + \phi)}_{\substack{\text{twice frequency} \\ \text{(harmonic)}}}$$

- Average Power

$$P_{avg} = \frac{1}{T}\int_0^T p(t)\,dt$$

$$= \frac{1}{T}\int_0^T \frac{V_m I_m}{2} \cos(\theta - \phi)\,dt + \underbrace{\frac{1}{T}\int_0^T \frac{V_m I_m}{2} \cos(2\omega t + \theta + \phi)}_{0}$$

$$\boxed{P_{avg} = \frac{V_m I_m}{2} \cdot \cos(\theta - \phi)}$$

$$P_{avg} = \frac{1}{2} Re\{\mathbf{V}\mathbf{I}^*\}$$

real number ✓
phasor ✗

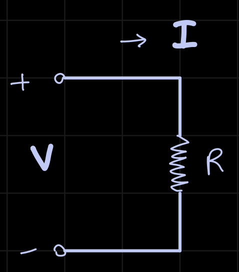
$\mathbf{I} = I_m e^{j\phi}$
$\mathbf{I}^* = I_m e^{-j\phi}$
(conjugate)

* Avg. Power absorbed

- by a purely resistive element

$$P_{avg} = \frac{V_m I_m}{2} \cdot \cos(\theta - \phi)$$

here, phase diff = 0°

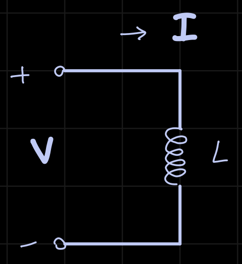


$$P_{avg} = \frac{V_m \cdot I_m}{2} = \frac{I_m^2 R}{2} = \frac{V_m^2}{2R}$$

- by a purely inductive element

$$P_{avg} = \frac{V_m I_m}{2} \cdot \cos(\theta - \phi)$$

here, phase diff = 90°

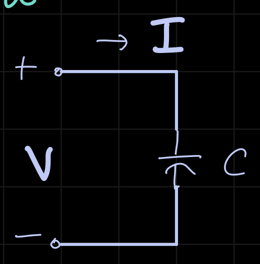


So,

$P_{avg} = 0$ for inductor

- by a purely capacitive element

$$P_{avg} = \frac{V_m \cdot I_m}{2} \cdot \cos(90°)$$



$P_{avg} = 0$ for capacitor

* Lecture : 6

$v(t) = V_m \cos(\omega t + \theta)$ ← Revision

↓

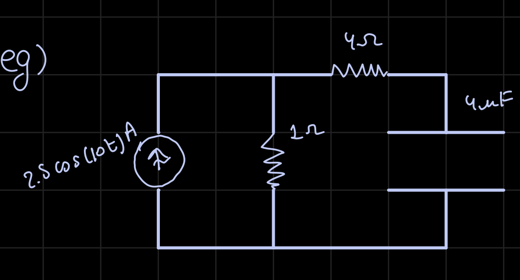
$v(t) = Re\{V_m e^{j\omega t} e^{j\theta}\}$

↓ $-e^{j\omega t}$

$V_m e^{j\theta} = V_m \angle \theta$

exponential   polar

• eg)

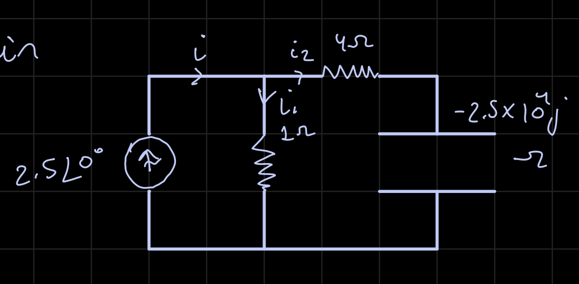


① find power delivered to each element at $t = 0, 10, 20ms$

② Find P_{avg} to each element

Ans) convert to freq. domain

$V_{1\Omega} = V_{4\Omega} + V_c$



① $P_{inst} = \frac{V_m I_m}{2}\cos(\theta - \phi) + \frac{V_m I_m}{2}\cos(2\omega t + \phi + \theta)$

$I_1 = -2.5 \times \left(\frac{4 - j2.5\times10^4}{1+4-j\,2.5\times10^4}\right) \simeq \underline{\underline{-2.5A}}$

imaginary part is way larger than real part

$\Rightarrow \frac{-10 + j625\times10^{\cancel{00}}}{5 - j\,25\times10^3} \Rightarrow \frac{-2+j125}{1-j50}$

$\Rightarrow \frac{-2+j\cdot125}{1-j50} \times \frac{1+j50}{1+j50} \Rightarrow$

$I_{1\Omega}(t) = 2.5\cos(10t)$

$V_{1\Omega} = (I_{1\Omega})(1\Omega) \Rightarrow V_{1\Omega}(t) = 2.5\cos(10t)$

$\cos^2(\theta) = \frac{1+\cos(2\theta)}{4}$

$p_{1\Omega}(t) = 2.5\cos(10t) \cdot 2.5\cos(10t)$ W

$p_{1\Omega}(t=0) = 6.25W$

$p_{1\Omega}(t=10ms) = 6.1877W$

$p_{1\Omega}(t=20ms) = 6.033W$

$(P_{avg})_{1\Omega} = 3.125W$

⇒ P delivered to 4Ω

$P_{4\Omega}(t) = V_{4\Omega}(t) \times I_{4\Omega}(t)$

$I_{4\Omega} = I_s \times \frac{1}{5 - j2.5\times10^4} = 10^{-4}\angle 90°A$

$V_{4\Omega} = 4 \times I_{4\Omega} = 4\times10^{-4}\angle 90°\ V$

convert to time domain

$p_{4\Omega}(t) = 2\times10^{-8} + 2\times10^{-8}\cos(20t)W$

$t=0: \ 4\times10^{-8}$ W

$t = 10ms = 3.96\times10^{-8}$ W

$t = 20ms = 3.87\times10^{-8}$ W

$P_{avg\,4\Omega} = 2\times10^{-8}$ W

⇒ P delivered to capacitor

$p_c(t) = V_c(t) \cdot I_c(t)$

$(p_{avg})_C = 0$ since phase diff = 90°

$I_c = I_2 = 10^{-4}\angle 90°A \Rightarrow I_c(t) = 10^{-4}\cos(10t + 90°)$

$V_c = (-j\,2.5\times10^{-4}) \times 10^{-4}\angle 90$

$-j\cdot 25\times10^3 \times (+j10^{-4})$

$\underline{\underline{2.5\ V}}$

$p_c(t) = 1.25\times10^{-4}\cos(20t + 90°)$ W

$t=0 \Rightarrow p = 0W$

$t = 10ms \Rightarrow p = 2.48\times10^{-5}$ W

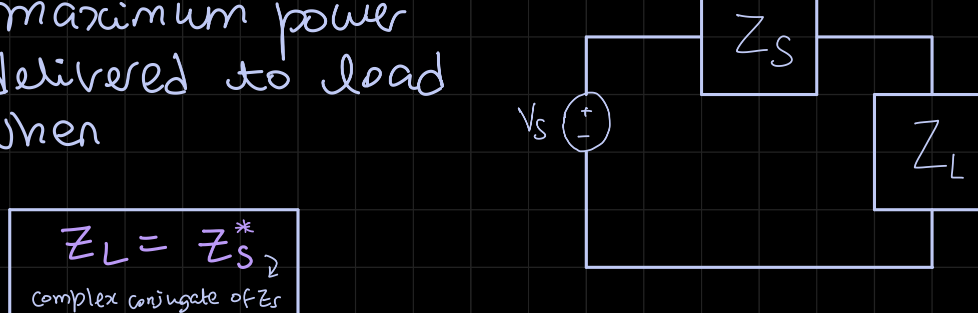
Note: we cannot multiply I_c and V_c in phasor form and then convert to time domain for getting P_c (power) because power does not has a phasor part. It is a real value.

* Correct or not ?

depends on t ✗ ① $p_{1\Omega}(t) + p_{4\Omega}(t) + p_c(t) = \text{constant}1$

✓ ② $P_{avg\,1\Omega} + P_{avg\,4\Omega} + P_{avg\,c} = \text{constant}2 \equiv P_{avg}$ source

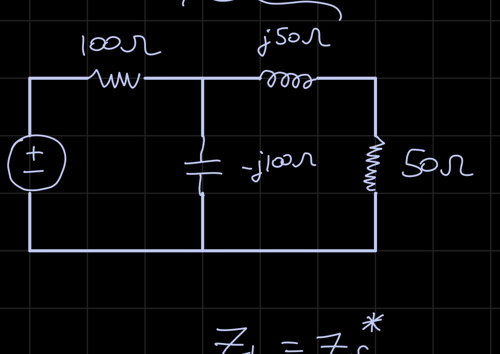
active sign convention   passive sign convention



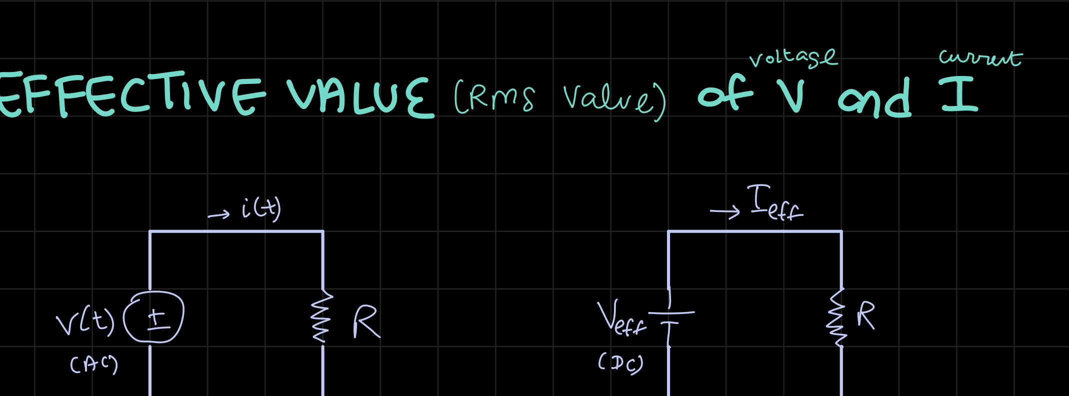
* Maximum Power Transfer Theorem

maximum power delivered to load when

$\boxed{Z_L = Z_S^*}$
complex conjugate of Z_s

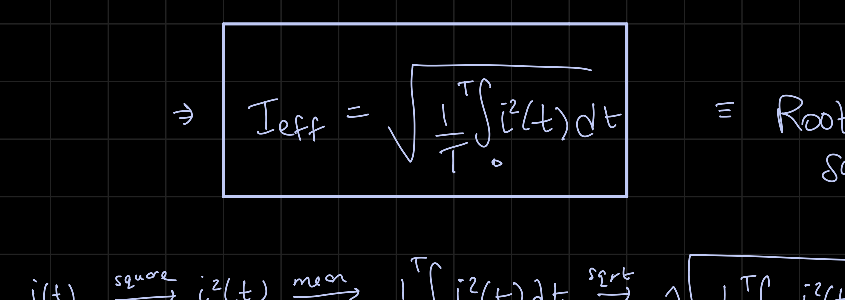


⇒ Impedance matching



$Z_L = Z_s^*$

* EFFECTIVE VALUE (Rms Value) of V and I
voltage   current



if $P_{avg_1} = P_{avg_2}$

$\Rightarrow \frac{1}{T}\int_0^T i^2(t) R\, dt = I_{eff}^2 R$

$\Rightarrow \boxed{I_{eff} = \sqrt{\frac{1}{T}\int_0^T i^2(t)\,dt}} \equiv$ Root mean square

$i(t) \xrightarrow{square} i^2(t) \xrightarrow{mean} \frac{1}{T}\int_0^T i^2(t)\,dt \xrightarrow{sqrt} \sqrt{\frac{1}{T}\int_0^T i^2(t)\,dt}$

• Sinusoidally varying voltage

$i(t) = I_m\cos(\omega t + \phi)$

$\cos^2 x = \frac{2\cos x + 1}{2}$

$I_{eff} = \sqrt{\frac{1}{T}\int_0^T I_m^2 \cos^2(\omega t + \phi)\,dt}$

$\boxed{I_{eff} = \frac{I_m}{\sqrt{2}}}$ current rms value   unit: A_{rms}

$\boxed{V_{eff} = \frac{V_m}{\sqrt{2}}}$ voltage rms value   unit: V_{rms}

not a phasor
it is real number
≡ magnitude of current / voltage

eg: $I = 10\angle 90°A \Rightarrow I = 5\sqrt{2}\angle 90°A$ rms

OR $V = 100\sqrt{2}\angle -60°\ V \Rightarrow V = 100\angle -60°\ V_{rms}$

* Apparent Power

$P_{apparent} = I_{eff} V_{eff}$ unit: VA, not W
volt ampere

* Power factor

$PF = \frac{\text{avg power}}{\text{apparent power}} = \frac{(V_m \cdot I_m)/2\ \cos(\theta - \phi)}{V_{eff}\cdot I_{eff}}$

$PF = \cos(\underbrace{\theta - \phi}_{\text{power factor angle}})$

* Lecture : 7

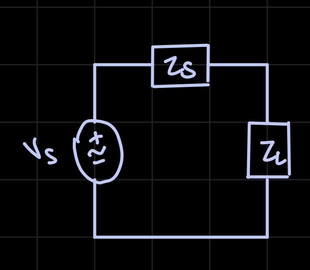
- Instantaneous Power : $p(t) = v(t)\, i(t)$
- Average Power : $P_{avg} = \frac{V_m I_m}{2} \cos(\theta - \phi) = \frac{1}{2} Re\{\mathbf{V}\mathbf{I}^*\}$
- $P_{avg.\,sources} = \Sigma P_{avg.\,elements}$

*** Note :** $\overset{\text{impedence}}{Z} = \underset{\text{resistive}}{R} + j\overset{\text{reactive}}{X}$

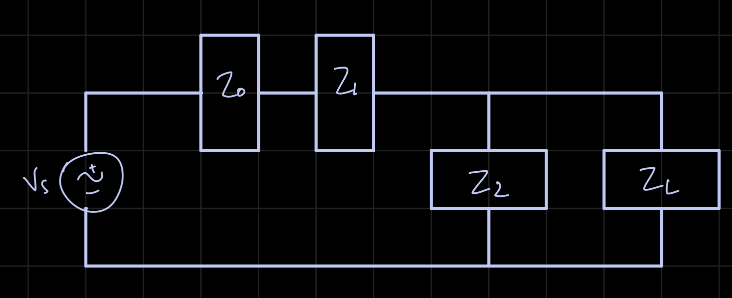
$P_{avg})_{resistive} : P \neq 0$

$P_{avg})_{reactive} : P = 0$

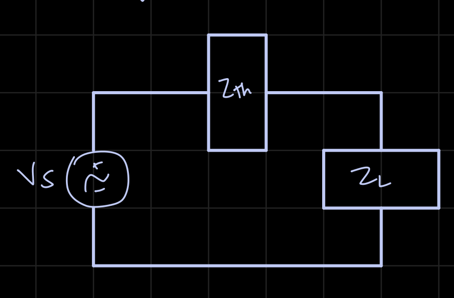
* Max Power Transfer :



Circuit has max. power when $Z_S = Z_L^*$ (complex conjugate)



⇓ apply thevenin's theorem



$Z_L = Z_{Th}^*$

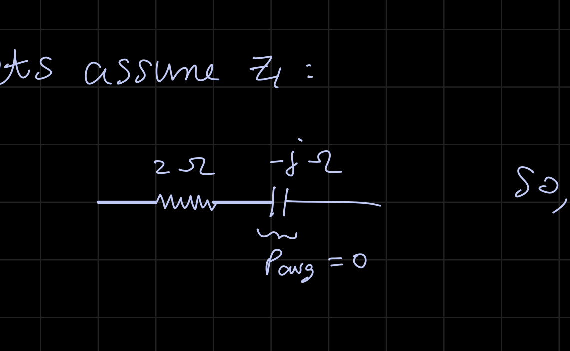
* Power Factor

$$PF = \cos(\underset{\text{angle of voltage phasor}}{\theta} - \underset{\text{angle of current phasor}}{\phi}) = \frac{P_{average}}{P_{apparent}}$$

for purely resistive load : PF = 1 {Max} $\theta - \phi = \pm 90°$
for purely reactive load : PF = 0 {min}

Note → PF = 0.5 leading → capacitive $(\theta - \phi) < 0°$
PF = 0.5 lagging → inductive $(\theta - \phi) > 0°$

eg)

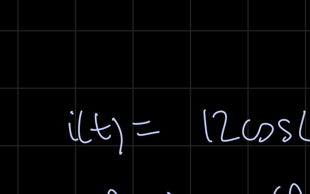


find
① Average power delivered to each load
② $P_{avg.\,source} = ?$
③ $P_{apparent.\,src} = ?$
④ PF of combined load = ?

Ans) $P_{avg\,Z_1} = \frac{1}{2} V_m I_m \cos(\theta - \phi) = \frac{1}{2} Re\{\mathbf{V}\mathbf{I}^*\}$

voltage across Z_1, not the src

lets assume Z_1 :



So, $P_{avg\,Z_1}$ = Power delivered to 2Ω resistor

$= I_{eff}^2 R$

find **I** by KVL :

$$-60\angle 0° + \mathbf{I}(2 - j1 + 1 + 5) = 0$$

$$\mathbf{I} = \frac{60\angle 0°}{3 + j4} = \underset{I_{rms}}{12\angle -53.13°} \text{ Arms}$$

$i(t) = 12\cos(\omega t - 53°)$ A rms

$\underset{I_{eff}}{(\text{Arms})} \rightarrow \underset{I_m}{(\text{A})}$: $I_{eff} = \frac{I_m}{\sqrt{2}} \Rightarrow I_m = I_{eff}\sqrt{2}$

$I_{eff} = 12$ Arms $\Rightarrow I_m = 12\sqrt{2}$ A

$i(t) = 12\sqrt{2} \cos(\omega t - 53°)$ A

$P_{avg\,(Z_1)} = (12)^2 \times 2 = 288$ W

note: $P_{avg} = \frac{1}{2} V_m I_m \cos(\theta - \phi) = V_{eff} I_{eff} \cos(\theta - \phi)$

Z_2 : I_{eff} same : series circuit

$I_{eff} = 12$

and $P_{avg})_{Z_2} = I_{eff}^2 R = (144)(1) = 144$ W

② $P_{avg})_{src} = V_{eff} I_{eff} \cos(\theta - \phi)$

$V_{src} = 60\angle 0°$ Vrms $\Rightarrow V_{eff} = 60$ Vrms

$I_{src} = 12\angle -53.13°$ Vrms $\Rightarrow I_{eff} = 12$ Arms

$\theta = 0°, \phi = -53.13°$

$P_{avg})_{src} = [60 \times 12] \cos(53.13°) = 432$W

we can observe that $288 + 144 = 432$
and hence,

$P_{avg.\,sources} = \Sigma P_{avg.\,elements}$ holds

③ $P_{apparent} = V_{eff} \cdot I_{eff} = (60)(12) = 720$ W

④ PF of combined loads = PF of source

$PF = \cos(\theta - \phi) = \cos(\underset{\theta - \phi > 0,\ \text{lagging}}{0 + 53.13°}) = 0.6$ lagging

***** $P_{avg} = \frac{1}{2} Re\{\mathbf{V}\mathbf{I}^*\}$ $\qquad \mathbf{V} = V_m\angle\theta$, $\mathbf{I} = I_m\angle\phi$

$V_{eff} = V_{eff}\angle\theta$
$I_{eff} = I_{eff}\angle\phi$

$P_{avg} = Re\{V_{eff} I_{eff}\}$

* Complex Power

$$S = V_{eff} I_{eff}^* \quad \text{Volt Ampere \{VA\}}$$

this is a complex number not a phasor of power

$$S = (V_{eff}\angle\theta)(I_{eff}\angle\phi) = V_{eff} \cdot I_{eff}\, e^{j(\theta - \phi)}$$

$$\Rightarrow S = \underbrace{V_{eff} I_{eff} \cos(\theta - \phi)}_{\substack{\text{average power} \\ P \\ \text{(watt) W}}} + j\underbrace{V_{eff} I_{eff} \sin(\theta - \phi)}_{\substack{\text{reactive power} \\ Q \\ \text{(volt ampere reactance) VAR}}}$$

(volt ampere) VA

$$\boxed{S = P + jQ}$$

$|S| = V_{eff} I_{eff} = P_{apparent}$ (volt amp)

note: $Z = R + jX$

Purely resistive load : $Z = R$, $X = 0$

$$S = \underset{V_{eff} I_{eff} \cos(0)}{P} + j\overset{V_{eff} I_{eff} \sin(\theta - \phi) = 0}{Q}$$

$P \neq 0$
$Q = 0$

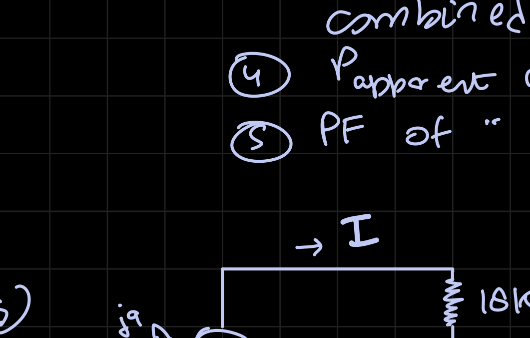
Purely reactive load

$$S = \underset{V_{eff} I_{eff} \cos(90°)}{P} + j\overset{V_{eff} I_{eff} \sin(\overset{90°}{\theta - \phi})}{Q}$$

$P = 0$, $Q \neq 0$

Q signifies energy flow rate into or out of reactive component of load

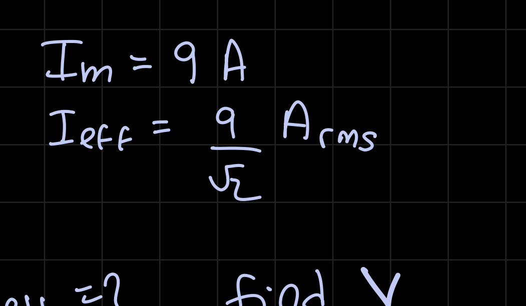
eg)



assume $C = 1\mu F$, $\omega = 45$ rad/s

find:
① complex Power provided by src
② Time average power absorbed by combined load
③ Reactive Power absorbed by combined load
④ $P_{apparent}$ absorbed " "
⑤ PF of " " "

Ans)



$9e^{j9} \equiv 9\cos(9°) + j9\sin(9°)$

$\frac{1}{j\omega C} = \frac{1}{j \times 45 \times 1 \times 10^{-6}} = -j\frac{10^6}{45}$

① $S_{source} = \overbrace{V_{eff} \times I_{eff}}^{\text{source}}$

$I_m = 9$ A
$I_{eff} = \frac{9}{\sqrt{2}}$ Arms

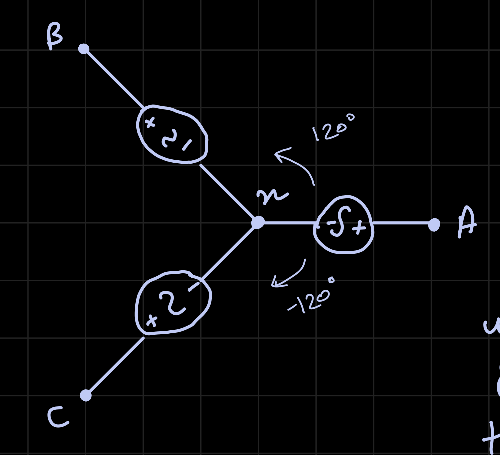
$V_{eff} = ?$, find V

$$V = I(Z_{eq}) = 9\angle 9° \left(18 \times 10^3 - j\frac{10^6}{45}\right)$$

* Lecture : 8

- Polyphase Circuits (Chp 12)

⇒ Three Phase Source



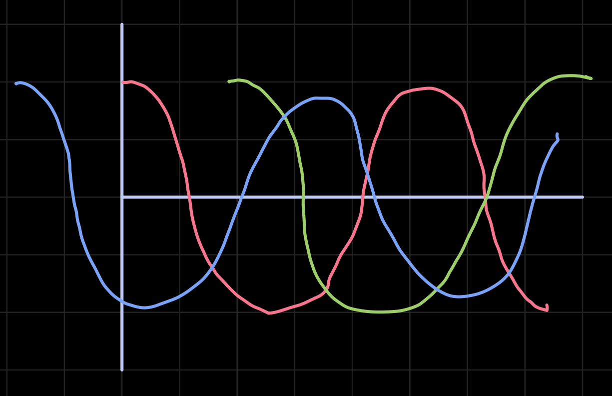
$V_{an} = 100\angle 0° \, V$
$V_{bn} = 100\angle 120° \, V$
$V_{cn} = 100\angle -120° \, V$

if $|V_{an}| = |V_{bn}| = |V_{cn}|$
& $V_{an} + V_{bn} + V_{cn} = 0$
then it is a

Balanced Source

total instantaneous power = constant

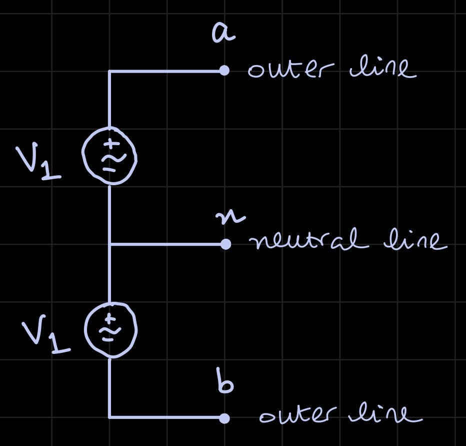
freq. domain	time domain
$100\angle 0°$	$100\cos(\omega t)$
$100\angle 120°$	$100\cos(\omega t + 120°)$
$100\angle -120°$	$100\cos(\omega t - 120°)$



total $p(t) \rightarrow$ constant

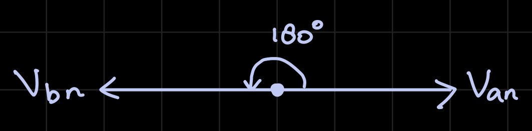
* Single Phase Three-wire Source

≡ Two phase source



$V_1 = V_m \angle 0°$

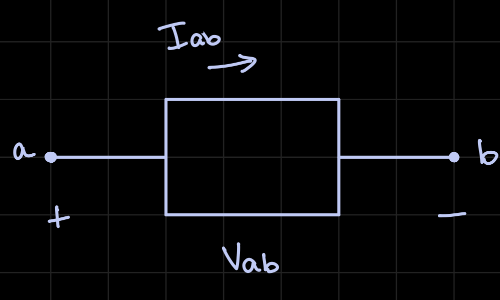
$V_{an} = V_1 = V_m \angle 0°$
$V_{bn} = -V_1 = V_m \angle 0° - 180°$



double script notation

$V_{ab} = V_{an} - V_{bn} = V_{an} + V_{nb}$
$V_{bn} = -V_{nb}$

$V_{an} = V_A$ wrt V_n

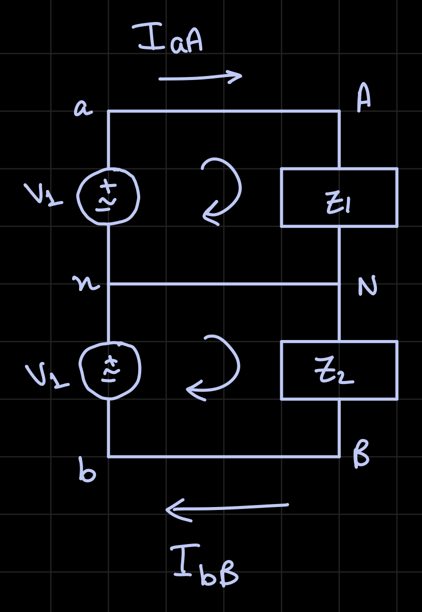


I_{ab}: current flowing from a to b

- Balanced single phase three wire source

Conditions:

$|V_{an}| = |V_{bn}|$
$V_{an} + V_{bn} = 0$
$\Big\} \Rightarrow$ Balanced Src



$I_{aA} = \frac{V_1}{Z_1}$

$I_{bB} = \frac{V_1}{Z_2}$

$I_{nN} = -I_{aA} + I_{bB}$

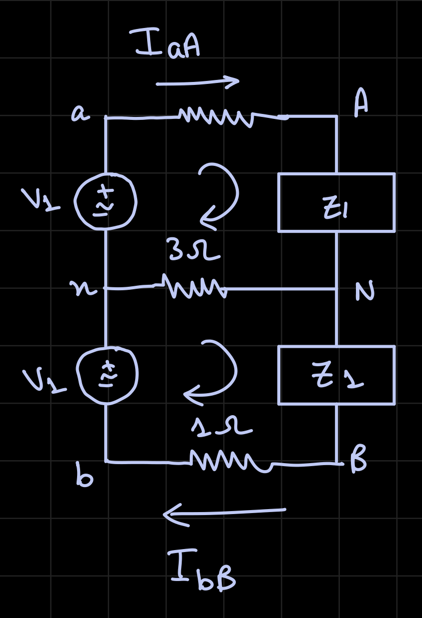
$\Rightarrow \frac{V_1}{Z_2} - \frac{V_1}{Z_1}$

Assume $Z_1 = Z_2$

$I_{nN} = \frac{V_1}{Z_1} - \frac{V_2}{Z_1} = 0$

when both srcs and loads are equal

Balanced Load : current in neutral line is equal to zero.



all terms are phasors

even with resistance
$I_{nN} = 0 = I_{bB} - I_{aA}$
due to
① Balanced Load
≡ Symmetry

* Lecture : 9

09/09/24

time domain	freq. domain
$V_p\cos(\omega t+\theta^\circ)$	$V_p\angle\theta^\circ$
$V_p\cos(\omega t+\theta^\circ-180^\circ)$	$V_p\angle\theta-180^\circ$

we cannot directly say,

$$P_{avg} = VI \quad \times$$

but $$P_{avg} = \frac{1}{2}Re\{VI^*\} \quad ✓$$

② a) $$I_{AB} = \frac{115\angle\theta^\circ + 115\angle\theta^\circ}{2(10+j2)} = \frac{230\angle\theta^\circ}{2(10+j2)}$$

$$= 11.27\angle(\theta^\circ - 11.3^\circ)A$$

$$\phi = \theta - 11.3^\circ$$

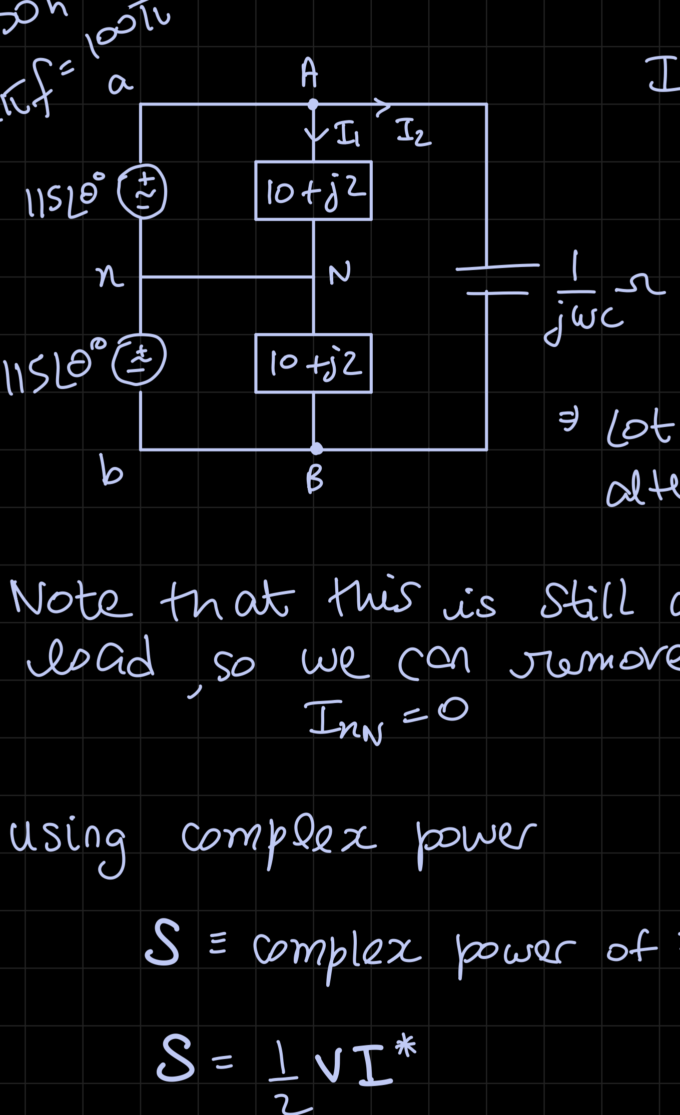
$$PF = \cos(\theta - \theta + 11.3^\circ) = 0.98 \text{ lagging}$$

because PF angle is +ve

b) $PF = 1 \Rightarrow \cos(\theta-\phi) = 1 \Rightarrow \theta - \phi = 0$

$\Rightarrow \theta = \phi$

$f = 50h$
$\omega = 2\pi f = 100\pi$



$$I_{aA} = I_1 + I_2$$

$$\Rightarrow \frac{115\angle\theta^\circ}{10+j2} + \frac{230\angle\theta^\circ}{\left(\frac{1}{j\omega C}\right)}$$

$\Rightarrow$ lot of calculation
alternative method $\Rightarrow$

Note that this is still a balanced load, so we can remove nN since $I_{nN} = 0$

using complex power

$S \equiv$ complex power of total load

$$S = \frac{1}{2}VI^*$$

$$PF = \frac{Re\{S\}}{|S|} = 1 \Rightarrow Re\{S\} = |S|$$

so, $Im\{S\} = 0$ here

$$S = \frac{1}{2}V_{an}I_{AN}^* + \frac{1}{2}V_{nb}I_{NB}^* + \frac{1}{2}V_{ab}I_{AB}^*$$

$$\Rightarrow \frac{1}{2}V_{an}\left(\frac{V_{an}}{Z_p}\right)^* + \frac{1}{2}V_{nb}\left(\frac{V_{nb}}{Z_p}\right)^* + \frac{1}{2}V_{ab}\left(\frac{V_{ab}}{Z_c}\right)^*$$

$$\Rightarrow \frac{1}{2}\frac{|V_{an}|^2}{|Z_p|^2}\times Z_p + \frac{1}{2}\frac{|V_{nb}|^2}{|Z_p|^2}\times Z_p + \frac{1}{2}\frac{|V_{ab}|^2}{|Z_c|^2}\times Z_c$$

$Re\{115\angle 0^\circ\}$

$$\Rightarrow \frac{|V_{an}|^2}{|Z_p|^2}\times Z_p + \frac{1}{2}\frac{|V_{ab}|^2}{|Z_c|^2}\times Z_c$$

$\sqrt{10^2+2^2}$

$Re\{\frac{1}{j\omega C}\} = \frac{1}{j\omega C}\times\frac{-1}{j\omega C}$

$$\Rightarrow \frac{115^2}{104}(10+j2) + \frac{1}{2}\left(\frac{230^2}{\left(\frac{1}{\omega C}\right)^2}\right)\left(\frac{-j}{\omega C}\right)$$

$\frac{-1}{-1(\omega C)^2}$

$$\Rightarrow 115^2\left(\frac{\cancel{10}+j2}{104} - 2j\omega C\right)$$

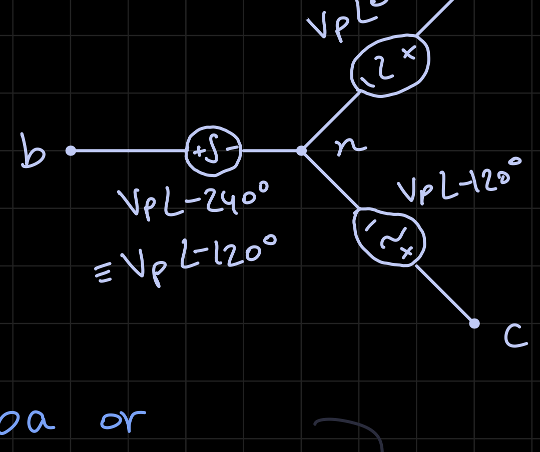
$$\Rightarrow 2\times115^2\left(\frac{j}{104} - j\omega C\right)$$

$$\Rightarrow 2\times115^2\left(\frac{1}{104} - \omega C\right) = 0$$

$$\frac{1}{104} - 100\pi C = 0$$

$$C = \frac{1}{10400\pi} = 30.60\,\mu F \quad ✓$$

* Three Phase Sources

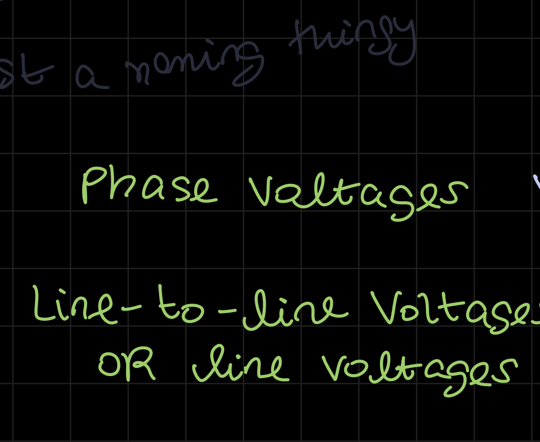


$V_{an} = V_p\angle 0^\circ$
$V_{bn} = V_p\angle -120^\circ$
$V_{cn} = V_p\angle 120^\circ)$

$|V_{an}| = |V_{bn}| = |V_{cn}| = V_p$
$V_{an} + V_{bn} + V_{cn} = 0$

balanced source

abc or
positive sequence



cba or
negative sequence

just a naming thingy

Phase voltages $\quad V_{an}, V_{bn}, V_{cn}$

Line-to-line Voltages OR line voltages $\quad V_{ab}, V_{bc}, V_{ac}$

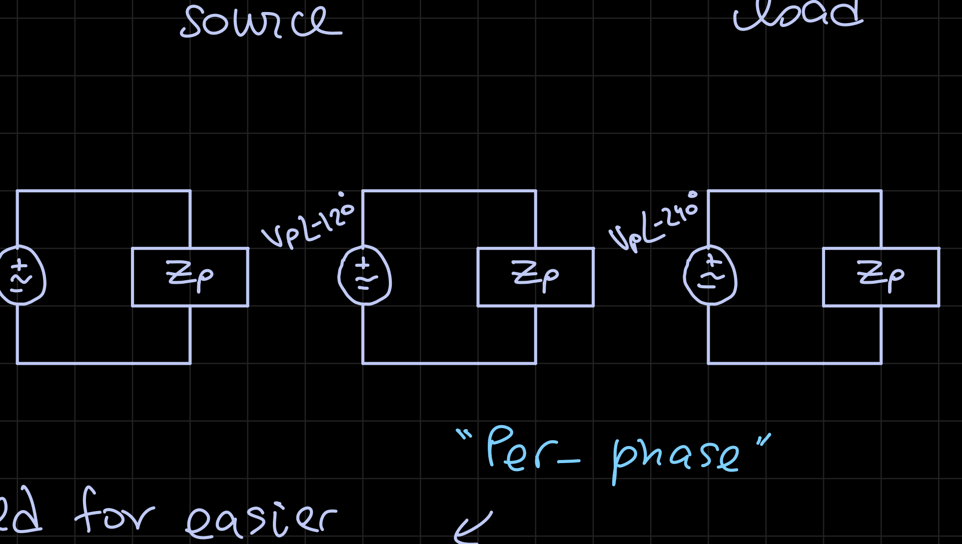
$$V_{ab} = V_{an} - V_{bn} = V_{an} + V_{nb}$$

$$V_{ab} = \sqrt{3}V_p\angle 30^\circ$$

$$V_{bc} = \sqrt{3}V_p\angle -90^\circ$$

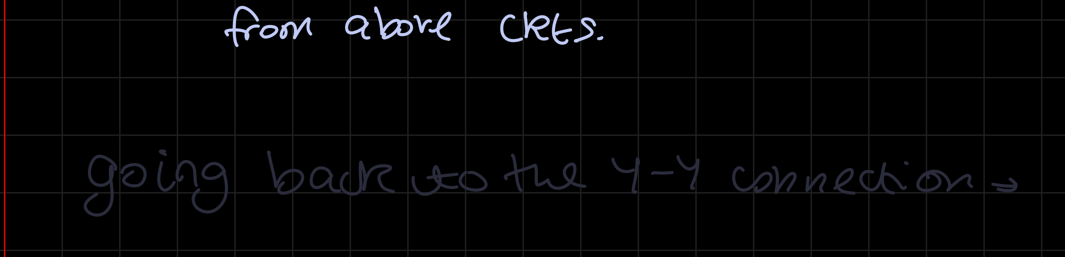
$$V_{ca} = \sqrt{3}V_p\angle -210^\circ$$

* Y-Y connection



balanced source

balanced load



"Per-phase"

used for easier analysis

eg. to find total power by ckt, just add the three individual power obtained from above ckts.

going back to the Y-Y connection $\Rightarrow$

$$I_{aA} = \frac{V_{an}}{Z_p}$$

$$I_{bB} = \frac{V_{bn}}{Z_p} = \frac{V_{an}\angle -120^\circ}{Z_p} = I_{aA}\angle -120^\circ$$

$$I_{cC} = \frac{V_{cn}}{Z_p} = \frac{V_{an}\angle +120^\circ}{Z_p} = I_{aA}\angle +120^\circ$$

$$I_{nN} = I_{aA} + I_{bB} + I_{cC} = 0$$

eg} consider three phase balanced Y-Y connected system

$$V_{an} = 200\angle 0^\circ\ V_{rms}$$
$$Z_p = 100\angle 60^\circ\ \Omega$$

find phase and line voltage & current and total avg power delivered to load

Ans}

$V_{an} = 200\angle 0^\circ\ V_{Rms}$
$V_{bn} = 200\angle -120^\circ\ V_{Rms}$
$V_{cn} = 200\angle +120^\circ\ V_{Rms}$

line voltage :

$$V_{ab} = \sqrt{3}V_p\angle 30^\circ = 200\sqrt{3}\angle 30^\circ\ V_{Rms}$$

$$V_{bc} = 200\sqrt{3}\angle -90^\circ\ V_{Rms}$$

$$V_{ca} = 200\sqrt{3}\angle -210^\circ = 200\sqrt{3}\angle 150^\circ\ V_{rms}$$

line currents:

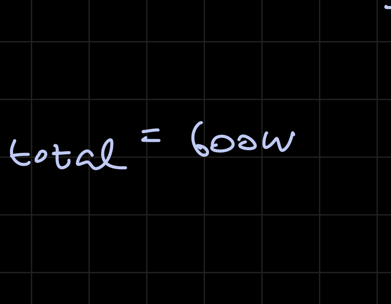
$$I_{aA} = \frac{V_{an}}{Z_p} = \frac{200\angle 0^\circ}{100\angle 60^\circ} = 2\angle -60^\circ A_{rms}$$

$$I_{bB} = 2\angle -180^\circ A_{rms}$$

$$I_{cC} = 2\angle -300^\circ A_{rms} = 2\angle 60^\circ A_{rms}$$

total avg. power: $P_{avg} = \frac{1}{2}Re\{VI^*\}$

in phase A :



$$P_{avg})_A = \frac{1}{2}Re\{VI^*\}$$

$$= Re\{V_{eff}I_{eff}\}$$

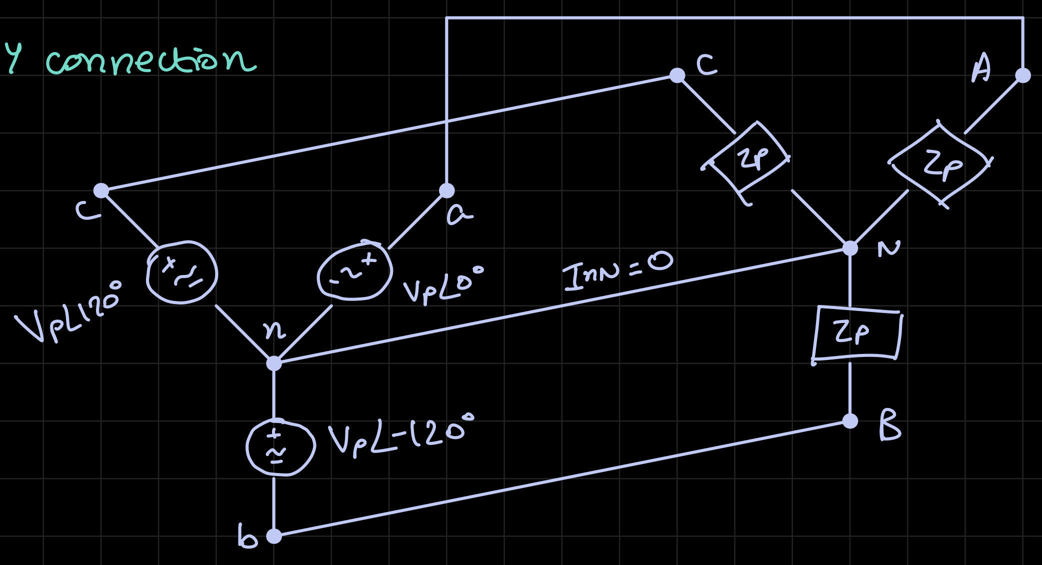
$$= Re\{200\angle 0^\circ \times 2\angle -60^\circ\}$$

$$\Rightarrow Re\{400\angle -60^\circ\} \Rightarrow 400\cos(-60) = 200W$$

$P_{avg})_B = 200W$
$P_{avg})_C = 200W$
} $P_{avg})_{total} = 600W$

* lecture : 10 11/09/24

→ Y-Y connection



balanced load : all load are same

balanced src : all src magnitudes are equal

line : lines connecting load to src
aA cC
bB nN

Phase Voltages: $V_{AN} = V_{an}$, $V_{BN} = V_{bn}$, $V_{CN} = V_{cn}$

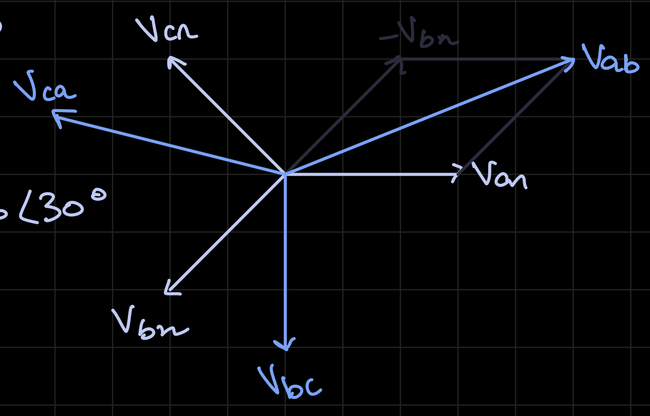
line voltages : V_{aA}, V_{bB}, V_{cC}

line currents : I_{aA}, I_{bB}, I_{cC}

phase currents : $I_{AN} = I_{aA}$, $I_{BN} = I_{bB}$, $I_{CN} = I_{cC}$

$V_{an} = V_p\angle 0^\circ$
$V_{bn} = V_p\angle -120^\circ$
$V_{cn} = V_p\angle -240^\circ$

$V_{ab} = V_{an} - V_{bn}$



$$\underbrace{\begin{aligned} V_{ab} &= V_{an} - V_{bn} = \sqrt{3}V_p\angle 30^\circ \\ V_{bc} &= \sqrt{3}V_p\angle -90^\circ \\ V_{ca} &= \sqrt{3}V_p\angle -210^\circ \end{aligned}}_{\text{line voltages}}$$

$V_{line} = \sqrt{3}V_{phase}$

line currents = phase currents

* Total Instantaneous Power

$$P_{total}(t) = p_A(t) + p_B(t) + p_C(t)$$

Classes & Attribs

interface (entity)

Bird
dmg (hits)

Pig
health (hits)

User
save stage
Score
level_status

level mng
max_score
no. of pigs
↳ blocks
↳ pigs
type (wood glass steel)

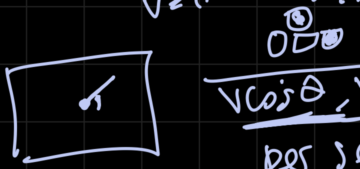
(entry point)
GAME
update score

Slingshot
angle
stretch

V=10

W/A

S,D



$V\cos\theta, V\sin\theta$

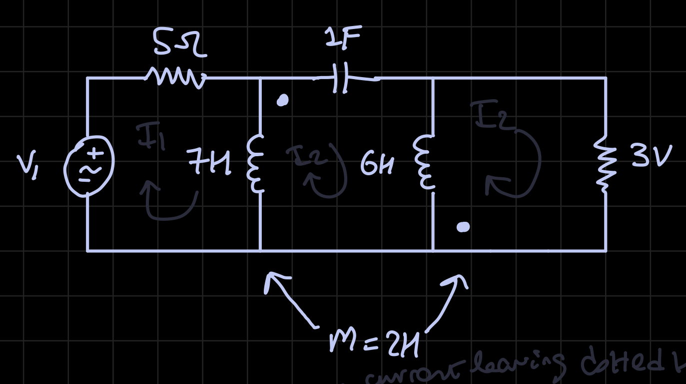
per second / rate

$-1 \to 0$

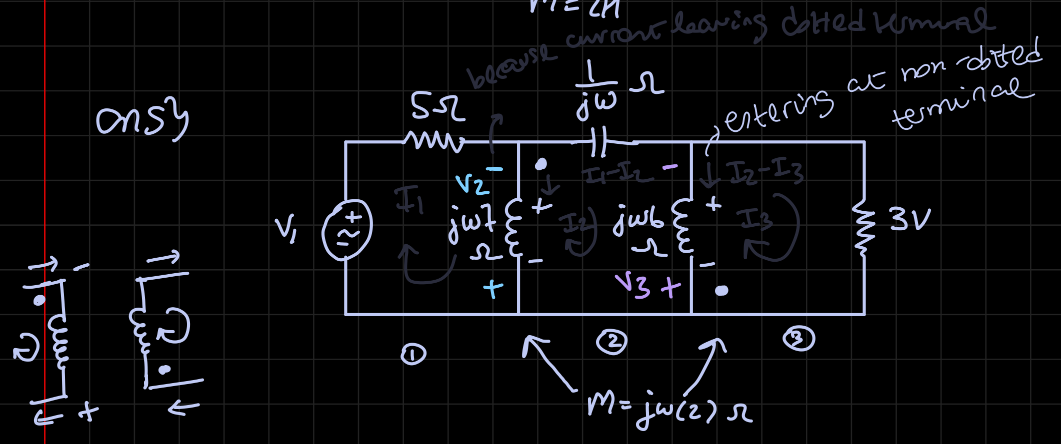
TODO : revise lecture 11 (missed due to SNS quiz)

* lecture 12:

eg 3



ans



① $-V_1 + 5I_1 - V_2 = 0$

$$V_2 = (j\omega 7)\,(I_1 - I_2)(-1)$$

because same sign of V_2 & V_3

$$V_2 = -j\omega 7(I_1 - I_2) + j2\omega\,(I_2 - I_3)$$

③ $3I_3 + V_3 = 0$

self + mutual inductance

same polarity

$$V_3 = -j6\omega(I_2 - I_3) + j2\omega(I_1 - I_2)$$

② $V_2 + \frac{1}{j\omega} I_2 - V_3 = 0$

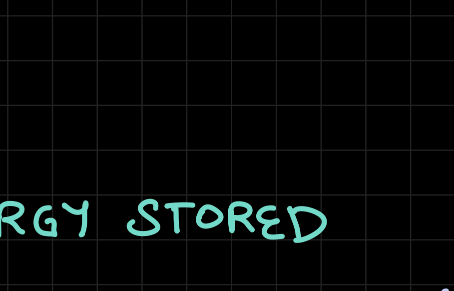
$$-j\omega 7(I_1 - I_2) + j2\omega(I_2 - I_3) + j6\omega(I_2 - I_3) - j2\omega(I_1 - I_2) + \frac{I_2}{j\omega} = 0$$

$$I_1(-j5\omega) + I_2(j17\omega) + I_3(-j8\omega) + \frac{I_2}{j\omega} = 0$$

$$I_1(-j5\omega) + I_2\left(j17\omega + \frac{1}{j\omega}\right) + I_3(-j8\omega) = 0$$

eg3

entering at dotted terminal



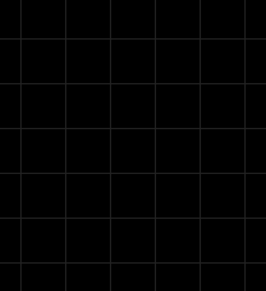
$-V_1 + 5I_1 + V_2 = 0$

$V_2 = (j\omega 7)(I_1 - I_2)$
$+ (j\omega 2)(I_2 - I_3)$

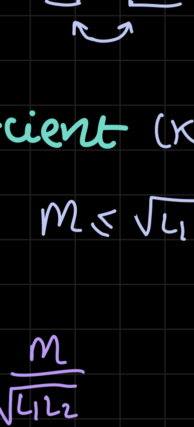
we donot need to care abt this sign if we use V_2, V_3 method.

* ENERGY STORED

$$w(t) = \frac{1}{2} L (i(t))^2$$ for only one inductor



$$w(t) = \frac{1}{2} L(i_1)^2 + \frac{1}{2} L(i_2)^2 \pm M i_1(t) i_2(t)$$



$\boxed{+ve}$ sign will occur iff both i_1 and i_2 are entering either dotted or undotted

$\boxed{-ve}$ sign iff both enter different (dotted / undotted)

• coupling coefficient (K)

$$M \leq \sqrt{L_1 L_2}$$

$$K = \frac{M}{\sqrt{L_1 L_2}} \Rightarrow 0 \leq K \leq 1$$

$\boxed{K \to 0}$ poor coupling or no coupling

$\boxed{K \to 1}$ strong coupling (very close to each other)

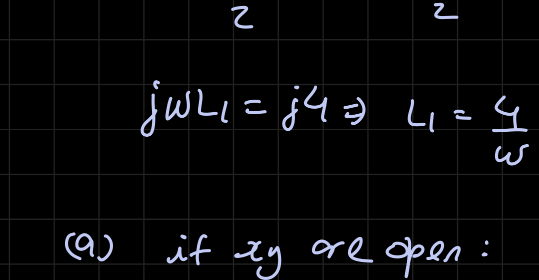
⇒ K depends on : distance btw coils ; size of coils ; ferrite core

$y \propto \frac{1}{x}$ $\quad$ $y \propto x$ $\quad$ $y \propto x$

uses : wireless power transfer (inductively coupled)
- electric vehicle charging
- magsafe charging

eg3 let $i_s = 2\cos(10t)$ A. find total energy stored in network at $t = 0$ if $k = 0.6$ and

(a) xy terminals are open circuited
(b) xy are short circuited



Ans $w(t) = \frac{1}{2} L_1 (i_1)^2 + \frac{1}{2} L_2 (i_2) \pm M i_1(t) i_2(t)$

$$j\omega L_1 = j4 \Rightarrow L_1 = \frac{4}{\omega} = 0.4\ H$$

(a) if xy are open : $i_2 = 0$

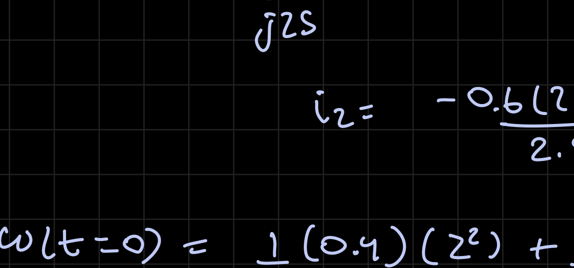
$$\text{so, } w(t) = \frac{1}{2} \times 0.4 \times (2\cos 10t)^2$$

$$w(t) = 0.8\cos^2(10t)$$

at $t = 0 \Rightarrow w(t) = 0.8\ J$

(b) $w(t) = \frac{1}{2} L_1 \cdot i_1^2 + \frac{1}{2} L_2 i_2^2 - M \cdot i_1 \cdot i_2$

$$i_1 = i_s = 2\angle 0°$$



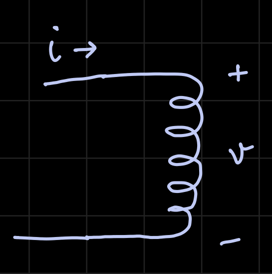
$i_2 = \frac{V_x}{j25}$ and $V_x = -j\omega M I_1$

$$i_2 = \frac{-0.6(2\angle 0°)}{2.5} = -0.48A$$

$$w(t=0) = \frac{1}{2}(0.4)(2^2) + \frac{1}{2}(\cdots$$

* Lecture : 11 {Revision} [absent] 24/9/24

• MODULE 5: Magnetically coupled circuits



$$v = L\frac{di}{dt}$$

current → magnetic flux

$i \propto \phi$ — ①

magnetic flux → induced voltage

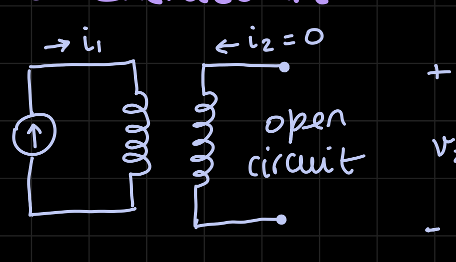
$v \propto \frac{d\phi}{dt}$ — ②

① and ② → $V = L\frac{di}{dt}$

for DC source : current is constant

hence $\frac{di}{dt} = 0$ and $\therefore v = 0$ (induced)

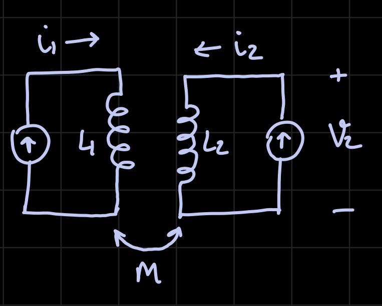
• Mutual Inductance



$v_2 \propto \frac{di_1}{dt}$

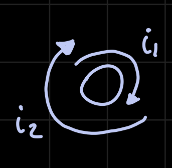
$V_2 = M\frac{di_1}{dt}$

L : self inductance — M : mutual inductance

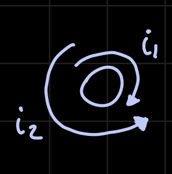


$$v_2 = \underbrace{L\frac{di_2}{dt}}_{\text{self inductance}} + \underbrace{M\frac{di_1}{dt}}_{\text{mutual inductance}}$$

* Additive / Substractive Property {two different coils}



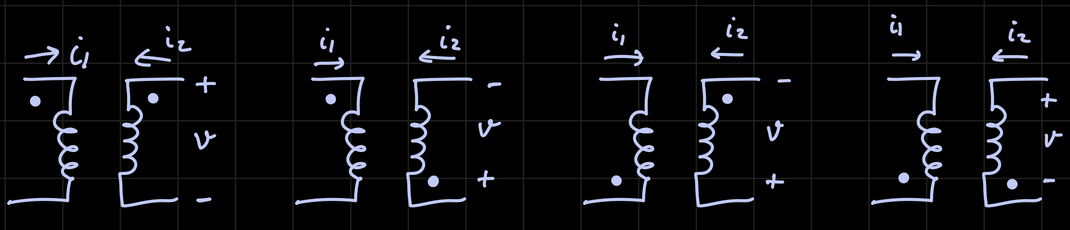
$$v_2 = L\frac{di_2}{dt} + M\frac{di_1}{dt}$$



$$v_2 = L\frac{di_2}{dt} - M\frac{di_1}{dt}$$

• Dotted Notation

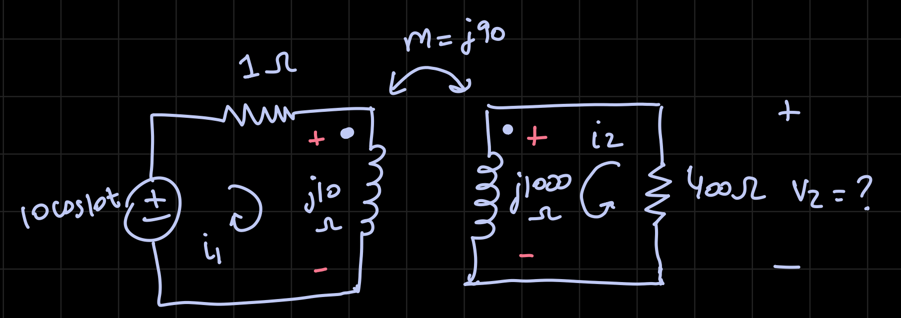
current entering _ terminal means +ve voltage reference at _
(dotted/undotted)



$v = L_1\frac{di}{dt} + M\frac{di_2}{dt}$ time domain

$V = j\omega L_1 I_1 + j\omega M I_2$ phasor domain

eg3



① $-10\angle 0° + I_1 + j10\, I_1 + j90\, I_2 = 0$

$I_1(1 + j10) + I_2(j90) = 10$

② $400 I_2 + j1000\, I_2 + j90\, I_1 = 0$

$I_1(j90) + I_2(400 + j1000) = 0$

CRAMMERS :

$$\Delta = \begin{vmatrix} 1+j10 & j1000 \\ j90 & 400+j1000 \end{vmatrix}$$

$= (1+j10)(400+j1000) + 90000$

$= 400 + j1000 + j4000 - 10.000 + 90.000$

$= j5000 + 80,400 = 80555\angle 3.55°$

$$\Delta_1 = \begin{vmatrix} j1000 & 10 \\ 400+j1000 & 0 \end{vmatrix} = -4000 - j10.000 = 10770\angle -111.8°$$

$$\Delta_2 = \begin{vmatrix} 10 & 1+j10 \\ 0 & j90 \end{vmatrix} = j900 = 900\angle 90°$$

$I_1 = \frac{\Delta}{\Delta_1} = -3.2 + 6.75j$

full cramers part wrong because I took $M = L_2 = j1000$ above

$$D_0 = \begin{vmatrix} 1+j10 & j90 \\ j90 & 400+j1000 \end{vmatrix}$$

$= 400 + j1000 + j4000 - 10.000 + 8100$

$= j5000 - 1500 = 5220\angle 106.69°$

---

energy stored in the circuit

$$w(t) = \frac{1}{2}L_1 i_1(t)^2 + \frac{1}{2}L_2 i_2(t)^2 \pm M i_1(t) i_2(t)$$

+ : current entering same : • and • OR _ and _

− : current entering different : • and _ OR _ and •

COUPLING COEFFICIENT (K)

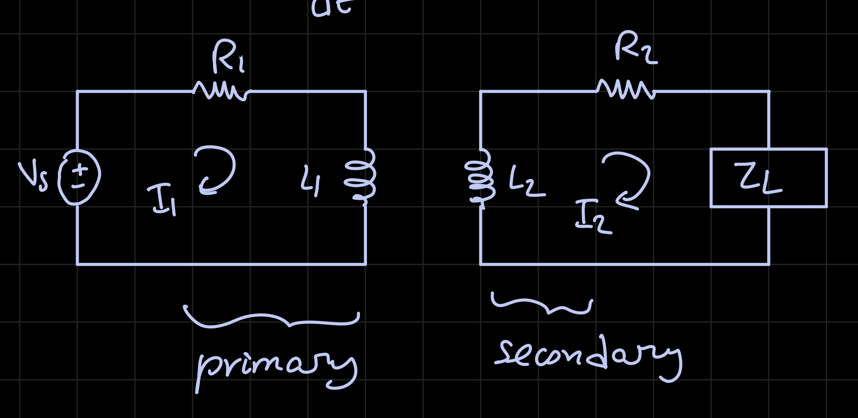
$K = \frac{M}{\sqrt{L_1 L_2}}$: note ∴ $M \leq \sqrt{L_1 L_2}$

So, $0 \leq K \leq 1$

* lecture 13 25/09/24

- **LINEAR TRANSFORMER**

when $v \propto \frac{di}{dt}$ ⇒ no magnetic core



$$-V_s + I_1R_1 + (j\omega L_1)I_1 - (j\omega M)I_2 = 0$$
$$(j\omega L_2)I_2 + R_2I_2 + Z_LI_2 - (j\omega M)I_1 = 0$$

$$\Rightarrow \quad V_s = \underbrace{(R_1 + j\omega L_1)}_{Z_{11}} I_1 - j\omega M I_2$$
$$0 = (-j\omega M)I_1 + \underbrace{(R_2 + j\omega L_2 + Z_L)}_{Z_{22}} I_2$$

$$V_s = Z_{11}I_1 - j\omega M I_2$$
$$0 = (-j\omega M)I_1 + Z_{22}I_2 \Big\} \Rightarrow \frac{I_2}{I_1} = \frac{j\omega M}{Z_{22}}$$

Input Impedance : $Z_{in} = \frac{V_s}{I_1} = Z_{11} - j\omega M \frac{I_2}{I_1}$

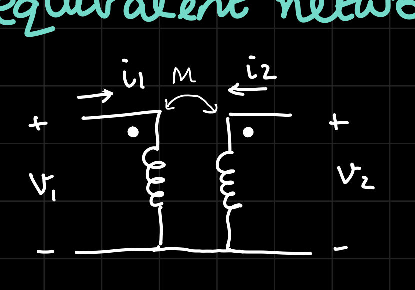
$$\boxed{Z_{in} = Z_{11} + \underbrace{\frac{\omega^2 M^2}{Z_{22}}}_{\text{Reflective Impedance}}}$$

where

$$Z_{11} = R_1 + j\omega L_1 \quad , \quad Z_{22} = R_2 + j\omega L_2 + Z_L$$

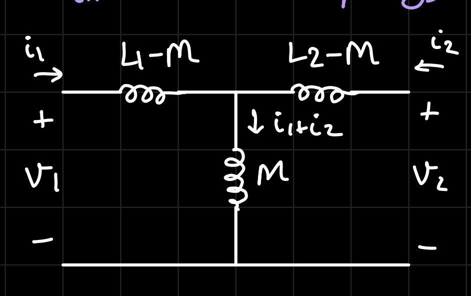
- if $K = \frac{M}{\sqrt{L_1L_2}} = 0 \Rightarrow Z_{in} = Z_{11}$ i.e. no coupling

- **T equivalent network**



≡

(no mutual coupling)



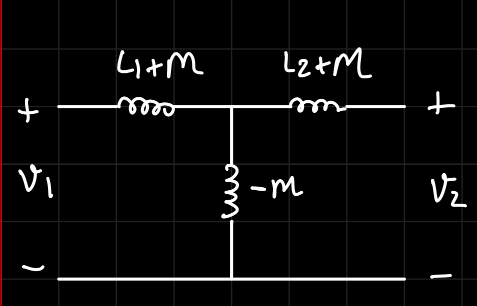
$$V_1 = L_1\frac{di_1}{dt} + M\frac{di_2}{dt}$$
$$V_2 = L_2\frac{di_2}{dt} + M\frac{di_1}{dt}$$

Note: no mutual coupling since there is no arrow for it

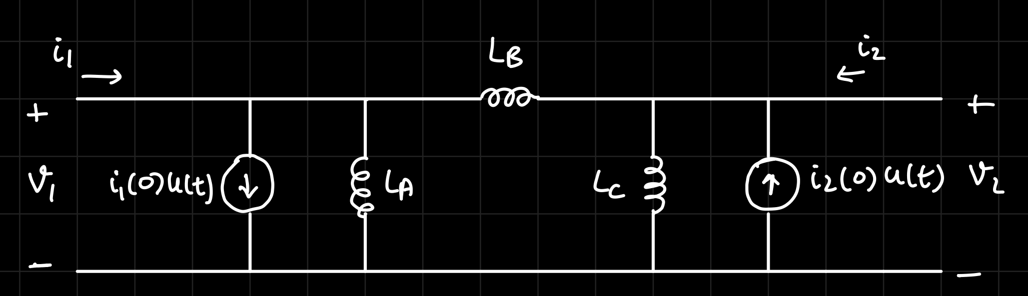
$$V_1 = (L_1 - M)\frac{di_1}{dt} + M\left(\frac{di_1}{dt} + \frac{di_2}{dt}\right)$$
$$V_1 = L_1\frac{di_1}{dt} + M\frac{di_2}{dt}$$

similarly, we get V_2 same as we got in the left circuit. Hence, both circuits are equivalent.

Note: if dots are on opposite sides, replace M with −M



- **π EQUIVALENT NETWORK**



$$L_A = \frac{L_1L_2 - M^2}{L_2 - M}$$

$$L_B = \frac{L_1L_2 - M^2}{M}$$

$$L_C = \frac{L_1L_2 - M^2}{L_1 - M}$$

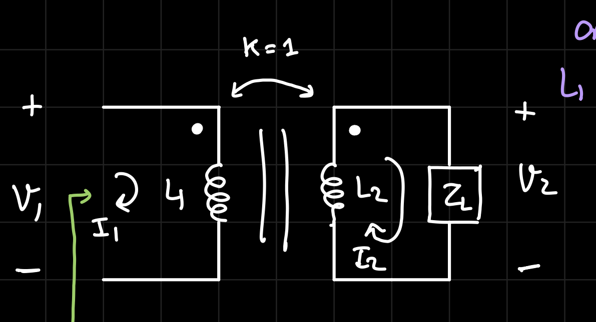
use nodal analysis to prove this

$$v = L\frac{di}{dt} \Rightarrow i = \frac{1}{L}\int_{-\infty}^{t} v\,dt$$
$$i = i(0)u(t) + \frac{1}{L}\int_{-\infty}^{t} v\,dt$$

if dots are on opposite side: $M \to -M$

- **Ideal Transformer**

$K = 1$ ⇒ achieved only with ferrite core (iron)
and
$L_1 \,\&\, L_2 \gg Z_L$



$$V_1 = j\omega L_1 I_1 - j\omega M I_2$$
$$0 = -j\omega M I_1 + (j\omega L_2 + Z_2)I_2$$

$$Z_{in} = \frac{V_1}{I_1} = j\omega L_1 + \frac{\omega^2 M^2}{Z_L + j\omega L_2}$$

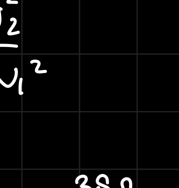
$$Z_{in} = \frac{Z_L}{\left(\frac{Z_L}{j\omega L_1}\right) + a^2}$$ and since $j\omega L_1 \gg Z_L$ ⇒

$$Z_{in} = \frac{Z_L}{a^2}$$

Current ratio : $\frac{I_2}{I_1} = \frac{1}{a}$
Voltage ratio : $\frac{V_2}{V_1} = a$
} replace a by −a if dots are on opp. side

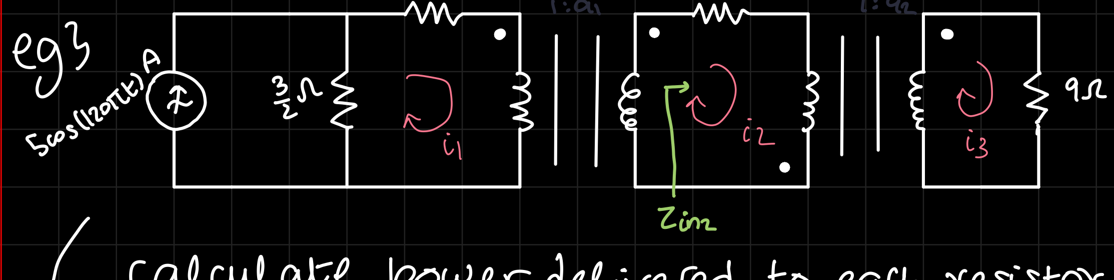
- **TURN RATIO**

let it be 1:a
then



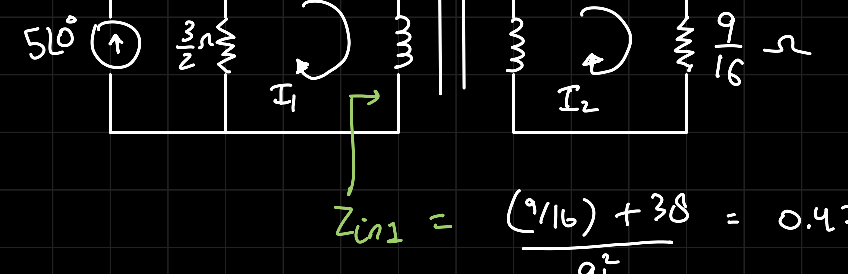
$$a = \frac{L_2}{L_1} = \frac{N_2^2}{N_1^2}$$

eg3

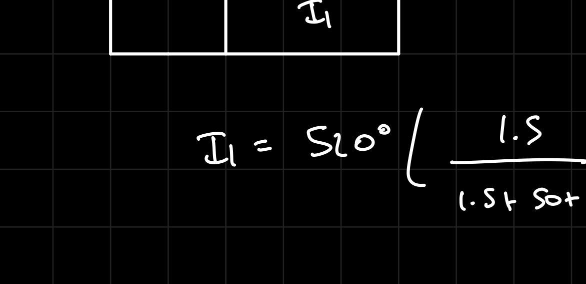


calculate power delivered to each resistor

$$Z_{in2} = \frac{Z_L}{a^2} = \frac{9}{16}\,\Omega$$



$$Z_{in1} = \frac{(9/16) + 38}{a_1^2} = 0.476\,\Omega$$



$$I_1 = 5\angle 0^\circ \left(\frac{1.5}{1.5 + 50 + 0.476}\right) = 0.144\angle 0^\circ A$$

We know $\frac{I_1}{I_2} = \frac{1}{a_1} \Rightarrow I_2 = \frac{0.144\angle 0^\circ}{9} = 0.016\angle 0^\circ A$

$$\frac{I_3}{I_2} = \frac{-1}{a_2} \Rightarrow I_3 = -\frac{0.016\angle 0^\circ}{4} = -4\angle 0^\circ mA$$

$$P_{avg\ 1.5\Omega} = \frac{1}{2}(5 - 0.144)^2 \times 1.5 = 17.67W$$

$$P_{avg\ 50\Omega} = \frac{1}{2}(0.144)^2 \times 50 = 0.518W$$

$$P_{avg\ 38\Omega} = \frac{1}{2}(0.016)^2 \times 38 = 0.0048W$$

$$P_{avg\ 9\Omega} = \frac{1}{2}(-4)^2 \times 10^{-6} \times 9 = 72 \times 10^{-6} W$$

* lecture : 14

• module : 6 → Circuit Analysis in S-domain
(textbook Chp 14)

$$V_m \cos(\omega t+\theta) = Re\{V_m e^{j\omega t+\theta}\}$$

⇓

to phasor how?

↓ Remove Re{ }, $e^{j\omega t}$

$$V_m e^{j\theta} = V_m \angle\theta$$

in phasor form, we can eliminate the differential equations and converted to algebraic equations

we cannot use phasors if not sinusoidal signals ??

let $v(t) = V_m e^{\sigma t}\cos(\omega t+\theta)$

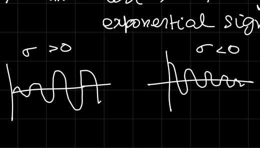
V(t) is not sinusoidal because extra term but we can write in phasor form using laplace transform

put $\sigma = 0,\ \omega = 0 \Rightarrow v(t) = V_m$ DC source

$\sigma = 0,\ \omega \neq 0 \Rightarrow v(t) = V_m\cos(\omega t+\theta)$ AC source sinusoidally varying ✓

$\sigma \neq 0,\ \omega = 0 \Rightarrow v(t) = V_m e^{\sigma t}\cos(\theta) = V_1 e^{\sigma t}$ exponential signal

$\sigma \neq 0,\ \omega \neq 0 \Rightarrow$ $\sigma > 0$ $\sigma < 0$



$$v(t) = V_m e^{\sigma t}\cos(\omega t+\theta)$$

$$= V_m e^{\sigma t}\left[\frac{e^{j(\omega t+\theta)} + e^{-j(\omega t+\theta)}}{2}\right]$$

$$= \frac{V_m}{2} e^{j\theta}\left[e^{\overbrace{(\sigma+j\omega)}^{s}t} + e^{\overbrace{(\sigma-j\omega)}^{s^*}t}\right]$$

$S \equiv$ complex frequency

$S = \sigma + j\omega$

σ = Neper Frequency (neper/sec)
ω = Radian frequency $= 2\pi f$ (rad/s)

• Laplace Transform

$$f(t) \longrightarrow \boxed{\text{Laplace Transform}} \longrightarrow F(S)$$

LT : invertible ✓

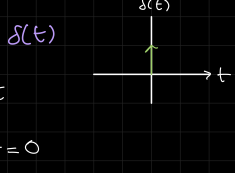
$$F(S) \xrightarrow[\text{Transform}]{\text{Laplace}} f(t)$$

one sided laplace transform $F(S) = \mathcal{L}(f(t)) = \int_{0^-}^{\infty} e^{-st} f(t)\,dt$

$$f(t) = \frac{1}{2\pi j}\int_{\sigma_0 - j\infty}^{\sigma_0 + j\infty} e^{st} F(S)\,ds$$

$$f(t) \Longleftrightarrow F(S)$$

• Unit step function : u(t)



$$\mathcal{L}(u(t)) = \int_{0^-}^{\infty} e^{-st} u(t)\,dt$$

$$= \int_{0}^{\infty} e^{-st}\,dt = \left[\frac{e^{-st}}{-s}\right]_0^{\infty} = -\frac{e^{-\infty}}{s} + \frac{e^{0}}{s}$$

$$= \frac{1}{s}\ ✓$$

$$\boxed{u(t) \rightleftharpoons \frac{1}{s}}$$

note : $\frac{1}{s+5} \Leftrightarrow e^{-5t}u(t)$

* Unit Impulse function $\delta(t)$

$$\mathcal{L}(\delta(t)) = \int_{0^-}^{\infty} e^{-st}\delta(t)\,dt$$

$\delta(t) = 1$ at $t = 0$

$$\boxed{\delta(t) \rightleftharpoons 1}$$

* Exponential

$$e^{-\alpha t}u(t) \Longleftrightarrow \frac{1}{s+\alpha}$$

$$te^{-\alpha t}u(t) \Longleftrightarrow \frac{1}{(s+\alpha)^2}$$

• Laplace Transform Theorems

① linearity theorems

$$\mathcal{L}\{f_1(t)+f_2(t)\} = \mathcal{L}\{f_1(t)\} + \mathcal{L}\{f_2(t)\}$$

summation in time domain ≡ summation in phasor domain

$$\mathcal{L}\{kf(t)\} = k\,\mathcal{L}\{f(t)\}$$

k is a constant
multiplication in time ≡ multiplication in phasor

eg} $V(S) = \frac{7}{s} - \frac{31}{s+17}$ find $v(t) = ?$

$$v(t) = \mathcal{L}^{-1}\{V(S)\} = 7\mathcal{L}^{-1}\left\{\frac{1}{s}\right\} - 31\,\mathcal{L}^{-1}\left\{\frac{1}{s+17}\right\}$$

$$v(t) = 7u(t) - 31e^{-17t}u(t) = (7 - 31e^{-17t})\,u(t)$$

• ZEROES & POLES

for some functions : $V(S) = \frac{N(S)}{D(S)}$

zeroes : values of S that lead to numerator, $N(S) = 0$

Poles : values of S that lead to denominator, $D(S) = 0$

eg : $V(S) = \frac{S-3}{S(S+6)}$

Zeroes : $S = 3$
Poles : $S = 0, -6$

eg} $V(S) = \frac{1}{(S+\alpha)(S+\beta)}$ find $v(t)$

convert to : $V(S) = \frac{A}{S+\alpha} + \frac{B}{S+\beta}$
↳ method of residue

$$\frac{1}{(S+\alpha)(S+\beta)} = \frac{A}{S+\alpha} + \frac{B}{S+\beta}$$

$$1 = A(S+\beta) + B(S+\alpha)$$

when $S = -\alpha \Rightarrow$ $1 = A(\beta-\alpha)$

$$A = \frac{1}{\beta-\alpha}$$

when $S = -\beta \Rightarrow$ $1 = B(\alpha-\beta)$

$$B = \frac{-1}{\beta-\alpha}$$

$$V(S) = \left(\frac{\frac{1}{\beta-\alpha}}{S+\alpha}\right) + \left(\frac{\frac{-1}{\beta-\alpha}}{S+\beta}\right)$$

$$v(t) = \frac{1}{(\beta-\alpha)}e^{-\alpha t}u(t) - \frac{1}{(\beta-\alpha)}e^{-\beta t}u(t)$$

$$= \frac{1}{(\beta-\alpha)}\left(e^{-\alpha t} - e^{-\beta t}\right)u(t)$$

eg} $I(S) = \frac{7s+5}{s^2+s}$ $i(t) = ?$

zeroes : $\frac{-5}{7}$

poles : $0, -1$

$$I(S) = \frac{7S+5}{S(S+1)} = \frac{A}{S} + \frac{B}{S+1}$$

$$A = \frac{1}{\beta-\alpha} = \frac{1}{1},\quad B = \frac{-1}{\beta-\alpha} = -1$$

$$7S+5 = A(S+1) + B(S)$$

$$7s+5 = (A+B)s + A$$

$A+B = 7 \Rightarrow B = 2$
$A = 5$

$$I(S) = \frac{5}{S} + \frac{2}{S+1}$$

$$\mathcal{L}^{-1}(I(S)) = 5u(t) + 2e^{-t}u(t)$$

⇒ Repeated Poles

$$F(S) = \frac{2}{S^3 + 12S^2 + 36S} = \frac{2}{S(S^2+12S+36)}$$

$$F(S) = \frac{2}{S(S+2)^2}$$

$$F(S) = \frac{A}{S} + \frac{B}{S+2} + \frac{C}{S+2}$$

if we try to solve like earlier, we get inconsistent eqns like $2 = 0$

for repeated poles :

$$V(S) = \frac{N(S)}{(S-p)^n}$$

$$V(S) = \frac{a_n}{(S-p)^n} + \frac{a_{n-1}}{(S-p)^{n-1}} + \frac{a_{n-2}}{(S-p)^{n-2}} + \dots \frac{a_1}{(S-p)}$$

$$F(S) = \frac{A}{S} + \frac{B}{(S+6)^2} + \frac{C}{(S+6)}$$

$$2 = A(S+6)^2 + B(S) + C(S)(S+6)$$

when $S = 0 \Rightarrow 2 = 36A \Rightarrow A = \frac{1}{18}$

when $S = -6 \Rightarrow 2 = -6B \Rightarrow B = -\frac{1}{3}$

differentiate to find C

$$2 = A(S+6)^2 + BS + C\,S(S+6)$$

$$\frac{d(2)}{ds} \Rightarrow 0 = 2A(S+6) + B + C(S+6) + CS$$

$\Rightarrow S = -6 \Rightarrow$ $0 = B + C(-6)$

$$C = \frac{B}{6} = \frac{-1}{18}$$

So, $A = \frac{1}{18},\ B = \frac{-1}{3},\ C = \frac{-1}{18}$

$$F(t) = \frac{1}{18}u(t) - \frac{1}{3}\left(te^{-6t}u(t)\right) - \frac{1}{18}e^{-6t}u(t)$$

• THEOREMS :

① Time differentiation theorem

$$f(t) \rightleftharpoons F(S)$$

$$\boxed{\frac{d}{dt}f(t) \rightleftharpoons sF(S) - f(0^-)}$$

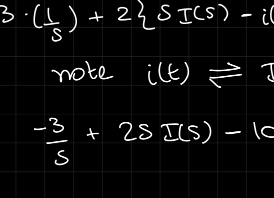
$L\frac{di}{dt} \rightarrow j\omega L I = SLI$
↳ when $\sigma = 0$

② Time Integration theorem

$$f(t) \rightleftharpoons F(S)$$

$$\int_{0^-}^{t} f(t)\,dt \rightleftharpoons \frac{F(S)}{S}$$

eg}



$i(t) = ?$

DC src + switch

$i(0^-) = 5A$

KVL? $\Rightarrow$ $-3u(t) + 2\frac{di}{dt} + 4i(t) = 0$

then integrate
but better way → Laplace

we cant use phasors because source ≠ sinusoidal
and we have a transient from $i(0^-) = 5A$

$$\Rightarrow -3\cdot\left(\frac{1}{s}\right) + 2\{sI(S) - i(0^-)\} + 4I(S) = 0$$

note $i(t) \rightleftharpoons I(S)$

$$-\frac{3}{s} + 2sI(S) - 10 + 4I(S) = 0$$

$$I(S) = \frac{\frac{3}{s}+10}{2s+4} = \frac{10s+3}{2s^2+4s}$$

$$= \frac{A}{2s} + \frac{B}{s+2}$$

$$10s+3 = As + 2A + 2Bs$$

$$10s+3 = s(A+2B) + 2A$$

$A = \frac{3}{2}$, $A + 2B = 10$

$$B = \frac{17}{4}$$

$$\Rightarrow I(S) = \frac{3/2}{2s} + \frac{17/4}{s+2} \Rightarrow i(t) = ?$$

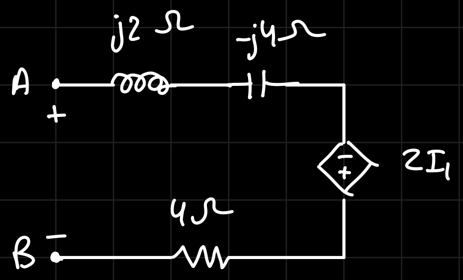
$$i(t) = \frac{3}{4}u(t) + \frac{17}{4}e^{-2t}u(t)\ ✓$$

* CTD Practice

① Quiz : 1 (Set A)

mesh analysis: current
nodal analysis: voltage

• midsem : 2023

② 

thevenin's voltage :

* lecture 15

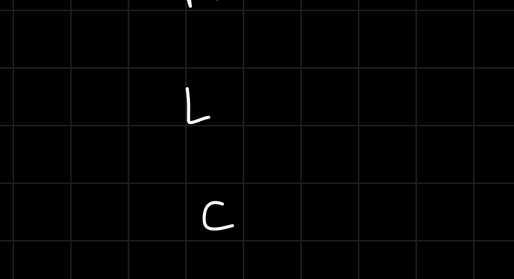
13/10/24

• Phasor vs S-domain

Assumptions:
zero initial conditions
sinusoidally varying source
"steady state"

time domain	freq. domain
$v(t) = V_m \cos(\omega t + \theta) = Re\{V_m e^{j\omega t} e^{j\theta}\}$	$V = V_m e^{j\theta}$
$v(t) = V_m e^{\sigma t}\cos(\omega t+\theta) = Re\{V_m e^{\sigma t} e^{j\theta} e^{j\omega t}\}$	$V = V_m e^{j\theta}$ where $s = \sigma + j\omega$ complex frequency
R	R
L	$L(\sigma + j\omega) = sL$
C	$\frac{1}{(\sigma+j\omega)C} = \frac{1}{sC}$

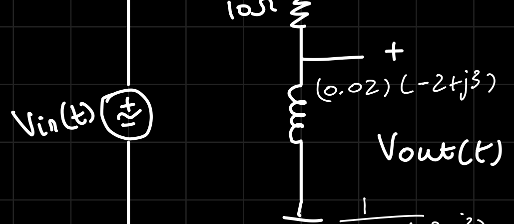
eg}



$V_{in}(t) = 5e^{-2t}\cos(3t + 45°)$

$s = \sigma + j\omega$
$s = -2 + j3$

$V_{in} = 5e^{j45} = 5\angle 45° \text{ V}$



Voltage divider for finding Vout

$$V_{out} = \frac{5\angle 45° \times (0.02)(-2+j3) \times \frac{1}{(0.01)(-2+j3)}}{10 + (0.02)(-2+j3) + \frac{1}{(0.01)(-2+j3)}}$$
$$= 5.86 \angle -24.4$$

$$V_{out}(t) = Re\{5.86 e^{j(-24.4)} e^{(\sigma + j\omega)t}\}$$
$$= 5.86 e^{-2t}\cos(3t - 24.4) \text{ V}$$

for zero initial condition, we can use phasors for $e^{\sigma t}\cos(\omega t + \theta)$

Can we still use phasors for $\delta(t)$, $u(t)$, $\sin(\omega t)u(t)$
NO
but laplace transform works ✓

$$\mathcal{L}\{f(t)\} = \int_{0^-}^{\infty} e^{-st} f(t)\,dt \Rightarrow F(s)$$
variable ✓

$\delta(t)$	1	$f_1(t) \pm f_2(t)$	$F_1(t) \pm F_2(t)$
$u(t)$	$1/s$	$kf(t)$	$KF(t)$
$tu(t)$	$1/s^2$	$\frac{d}{dt}f(t)$	$sF(s) - f(0^-)$
$e^{-at}u(t)$	$1/(s+a)$		
$te^{-at}u(t)$	$\frac{1}{(s+a)^2}$	$\int_{0^-}^{t} f(t)dt$	$F(s)/s$
$\sin(\omega t)u(t)$	$\frac{\omega}{s^2+\omega^2}$	$f_1(t) * f_2(t)$	$F_1(t)\cdot F_2(t)$
$\cos(\omega t)u(t)$	$\frac{s}{s^2+\omega^2}$	$f(t-a)u(t-a)$	$e^{-as}F(s)$
$e^{-at}\sin(\omega t)u(t)$	$\frac{\omega}{(s+a)^2+\omega^2}$	$f(t)e^{-at}$	$F(s+a)$

$$e^{-at}\cos(\omega t)u(t) = \frac{s}{(s+a)^2+\omega^2}$$

Initial and final value theorems

$$f(0^+) = \lim_{s\to\infty} sF(s)$$
$$f(\infty) = \lim_{s\to 0} sF(s)$$
all poles of sF(s) lie in left half plane

proof: $\mathcal{L}\{\sin(\omega t)u(t)\}$

$$= \int_{0^-}^{\infty} e^{-st}\left\{\frac{1}{2j}\left(e^{j\omega t} - e^{-j\omega t}\right)u(t)\right\}dt$$
$$= \frac{1}{2j}\int_{0^-}^{\infty} e^{t(j\omega - \sigma - j\omega)}u(t) - e^{-t(j\omega - \sigma - j\omega)}\,dt$$
$$= \frac{1}{2j}\int_{0^-}^{\infty} e^{-\sigma t}u(t) - e^{\sigma t}u(t)\,dt$$
$$= \frac{1}{2j}\mathcal{L}\{e^{j\omega t}\} - \mathcal{L}\{e^{-j\omega t}\}$$
$$= \frac{1}{2j}\left[\left(\frac{1}{s-j\omega}\right) - \left(\frac{1}{s+j\omega}\right)\right]$$
$$= \frac{1}{2j}\frac{2j\omega}{s^2+\omega^2} = \frac{\omega}{s^2+\omega^2}$$

example

① find $f(0^+)$ and $f(\infty)$ for $F(s) = \frac{4e^{-2s}(s+50)}{s}$

$$f(0^+) = \lim_{s\to\infty} sF(s) = \lim_{s\to\infty} \frac{4e^{-2s}(s+50)\cancel{s}}{\cancel{s}}$$
$$= \lim_{s\to\infty}\frac{4(s+50)}{e^{2s}}$$
$\frac{\infty}{\infty}$ form

use L'Hôpital's rule

$$\lim_{x\to\infty}\frac{f(x)}{g(x)} = \lim_{x\to\infty}\frac{f'(x)}{g'(x)}$$

$$\Rightarrow f(0^+) = \lim_{s\to\infty}\frac{4}{2e^{2s}} = \frac{1}{\infty} \text{ form} = \underline{\underline{0}}$$

final value : $f(\infty) = \lim_{s\to 0} 4e^{-2s}(s+50)$
$= 4(50) = \underline{\underline{200}}$

② find $f(0^+)$ for $F(s) = \frac{5s^2+10}{2s(s^2+3s+5)}$

$$\Rightarrow f(0^+) = \lim_{s\to\infty} sF(s) = \frac{5s^2+10}{2s^2+6s+10}$$

$$\lim_{s\to\infty}\frac{10s}{4s+6} \Rightarrow \lim_{s\to\infty} = \frac{10}{4} = \frac{5}{2}$$

$$f(\infty) = \lim_{s\to 0}\frac{5s^2+10}{2(s^2+3s+5)} = 1$$

example : find ILT of $F(s) = \frac{s^2+6}{s^2+7}$

$$F(s) = 1 - \frac{1}{s^2+7} = 1 - \frac{\sqrt{7}}{\sqrt{7}(s^2+(\sqrt{7})^2)}$$

$$f(t) = \delta(t) - \frac{1}{\sqrt{7}}\sin(\sqrt{7}t)u(t)$$

eg} find ILT of $\frac{s+2}{s^2+2s+4}$

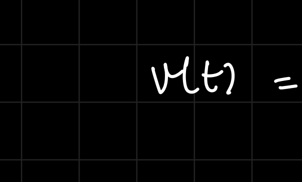
$$\Rightarrow \frac{1}{s+2} \Rightarrow f(t) = e^{-2t}u(t) \quad \times$$

$$\Rightarrow \frac{(s+1)+1}{(s+1)^2+(\sqrt{3})^2} \Rightarrow \frac{s+1}{(s+1)^2+(\sqrt{3})^2} + \frac{1}{s^2+s+5}$$
$\Downarrow$
$\cos(\sqrt{3}t)u(t)$

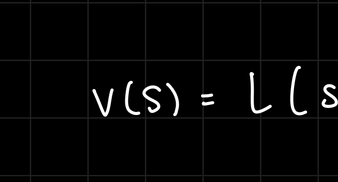
$s^2 + 2s + 4$
$\Downarrow$
$s = -1 \pm j\sqrt{3}$

Impedances in S-domain

Resistor :



$v(t) = iR$



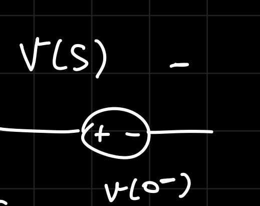
$V(s) = I(s)R$

Inductor :

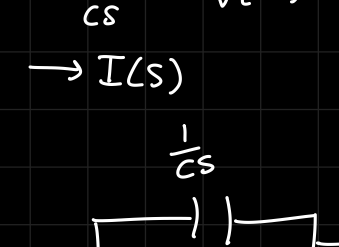
$$v(t) = L\frac{di(t)}{dt}$$

$$V(s) = L(sI(s) - i(0^-))$$
$$V(s) = sL\,I(s) - L\,i(0^-)$$

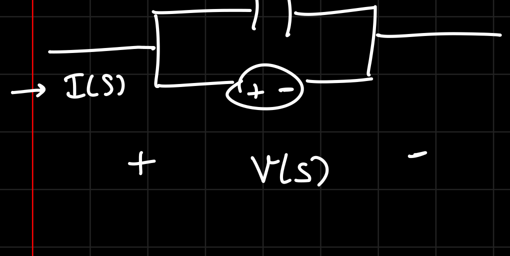
Capacitor :



$$i(t) = C\frac{dv}{dt}$$



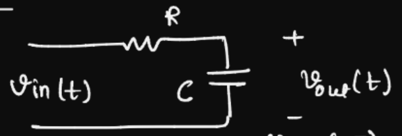
$$I(s) = C[sV(s) - v(0^-)]$$
$$I(s) = CsV(s) - Cv(0^-)$$
$$V(s) = \frac{1}{Cs}I(s) + \frac{v(0^-)}{s}$$



* Lecture 16 {missed}

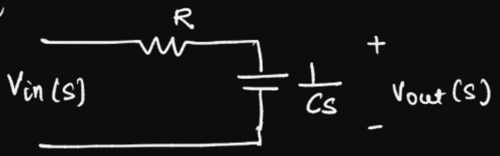
Transfer function :

Lets consider :



$v_{out}(0^-) = 0$

Freq. domain



$$V_{out}(s) = \frac{1/Cs}{R + 1/Cs} V_{in}(s)$$

$$\Rightarrow \underbrace{\frac{V_{out}(s)}{V_{in}(s)}}_{\text{transfer function } H(s)} = \frac{1}{sRC+1}$$

$$v_{out}(t) = \mathcal{L}^{-1}\{V_{out}(s)\} = \mathcal{L}^{-1}\{\underbrace{H(s)}_{\text{defines the system.}} \cdot V_{in}(s)\}$$

* lecture: 17

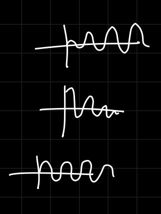
21/10/24

• Stability

Stable: bounded o/p for bounded i/p
unstable: unbounded o/p for bounded i/p
marginally stable: oscillating OR bounded offset

let : $e^{\sigma t}\cos(\omega_o t)\,u(t)$

① $\sigma > 0$: unstable
② $\sigma < 0$: stable
③ $\sigma = 0$: marginally stable

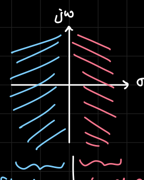


* **Stability Criterion**

System transfer fn $H(s) = k\dfrac{(s-z_1)(s-z_2)(s-z_3)\cdots(s-z_m)}{(s-p_1)(s-p_2)(s-p_3)\cdots(s-p_n)}$

- System is stable if
  All poles of $sH(s)$ lie on LHS of complex plane
- Marginally stable if
  1st order pole at $s=0$ OR 1st order complex conjugate pole pair at $j\omega$-axis
- Unstable system if
  All other cases
  → Any poles on RHS OR
  → 2nd or higher order pole at $s=0$ OR
  → 2nd or higher order conjugate pole pair at $j\omega$-axis

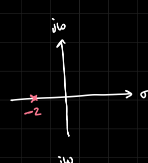
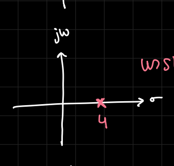
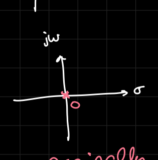
order of poles ≡ order of s ($s = \sigma + j\omega$)



stable | unstable

at jw axis:
could be unstable
or marginally stable

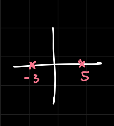
	$f(t)$	$sF(s)$	
①	$e^{-2t}u(t)$	$s\cdot\frac{1}{s+2}$	stable
②	$e^{4t}u(t)$	$s\,\frac{1}{s-4}$	unstable
③	$u(t)$	$s\cdot\frac{1}{s}$	marginally stable

(③) don't cancel, we have one zero and one pole

④ $e^{-3t}u(t) + e^{+5t}u(t)$ $\quad s\left\{\frac{1}{s+3} + \frac{1}{s-5}\right\}$

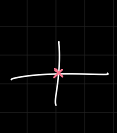
unstable



⑤ $s\cdot\dfrac{8}{(s+1)(s+2)(s+3)}$ stable

⑥ $s\cdot\dfrac{14}{(s+1-\sqrt{2})(s-1+\sqrt{2})}$ unstable

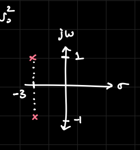
⑦ $tu(t)$ $\quad \dfrac{1}{s^2}$
↳ poles = 2
2nd order pole at $s=0$
unstable



⑧ $e^{-3t}\sin(\omega_o t)\,u(t)$ $\quad s\,\dfrac{\omega_o}{(s+3)^2+\omega_o^2}$

stable

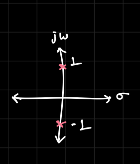
poles:
$(s+3)^2+\omega_o^2 = 0$
$(s+3)^2 = -\omega_o^2$
$s+3 = \pm\sqrt{-1}\,\omega_o$
$s = -3 \pm j\omega_o$



⑨ $\sin(\omega_o t)\,u(t)$ $\quad s\cdot\dfrac{\omega_o}{s^2+\omega_o^2}$

marginally stable

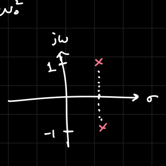
$s^2 = -\omega_o^2$
$s = \pm j\omega_o$



⑩ $e^{3t}\sin(\omega_o t)\,u(t)$ $\quad s\cdot\dfrac{\omega_o}{(s-3)^2+\omega_o^2}$

unstable (RHS)

$s-3 = \pm j\omega_o$
$s = 3 \pm j\omega_o$



⑪ $t\cos(\omega_o t)\,u(t)$

note: $f(t) \rightleftharpoons F(s)$
$tf(t) \rightleftharpoons -\frac{d}{ds}F(s)$

$\cos(\omega_o t)u(t) \Rightarrow \dfrac{s}{s^2+\omega_o^2} = s(s^2+\omega_o^2)^{-1}$

$\dfrac{d}{ds} = (s^2+\omega_o^2)^{-1} - s(s^2+\omega_o^2)^{-2}(2s)$

$= \dfrac{1}{s^2+\omega_o^2} - \dfrac{2s^2}{(s^2+\omega_o^2)^2}$

$= \dfrac{s^2+\omega_o^2-2s^2}{(s^2+\omega_o^2)^2} = \dfrac{\omega_o^2-s^2}{(s^2+\omega_o^2)^2}$

$s = \pm j\omega_o$ (2nd order)

unstable

• Final Value Theorem

$f(t\to\infty) = \lim_{s\to 0} sF(s)$
↳ when all poles are on LHS (condition)

• Initial value theorem

$f(0) = \lim_{s\to\infty} sF(s)$ (no condition)

eg} $f(t) = \sin(\omega_o t)\,u(t)$

final value: $f(\infty) = \lim_{s\to 0} sF(s)$

$= \lim_{s\to 0} s\,\dfrac{\omega_o}{\omega_o^2+s^2} = 0$ ✗

indeterminant because condition not met
(all poles are not on LHS)

• Chapter 15 {frequency response}

assuming zero initial conditions:

capicitor impedance $= Z_C = \dfrac{1}{sC}$

where $s = \sigma + j\omega$

we represent capacitor as open circuit in case of DC input voltage

Transfer function:

$H(s) = \dfrac{V_{out}(s)}{V_{in}(s)} \Rightarrow V_{out}(s) = \underbrace{V_{in}(s)}_{\text{input}}\cdot\underbrace{H(s)}_{\text{system}}$

let $\sigma = 0$ since we are only considering frequency
$\Rightarrow s = j\omega$

$H(j\omega) = \dfrac{V_{out}(j\omega)}{V_{in}(j\omega)}$ Voltage gain V/V

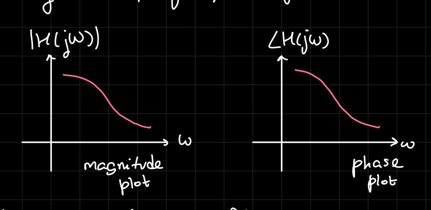
$H(j\omega) = \dfrac{I_{out}(j\omega)}{I_{in}(j\omega)}$ current gain A/A

$H(j\omega) = \dfrac{V_{out}(j\omega)}{I_{in}(j\omega)}$ transfer impedance $\frac{V}{A}$ or Ω

$H(j\omega) = \dfrac{I_{out}(j\omega)}{V_{in}(j\omega)}$ transfer admittance $\frac{A}{V}$ or Ω^{-1}

note: currents and voltages here are in freq. domain and since we have assumed $\sigma = 0$ i.e. $s = j\omega$, they are phasors ⇒ complex numbers ✓

$H(j\omega) = |H(j\omega)|\,\angle H(j\omega)$



here these are low pass filters

• DECIBELS SCALE (dB)

$H_{dB} = 20\log_{10}|H(j\omega)|$

note: $\log_{10}1 = 0$
$\log_{10}10 = 1$
$\log_{10}2 = 0.3$
$\log_{10}(0.1) = -1$
$\log_{10}(10^{-k}) = -k$
$\log_{10}(0) =$ undefined

find H_{dB} at $\omega = 146$ rad/s if $H(s) = 20(s+100)$

⇒ $H_{dB} = 20\log_{10}|H(j\omega)|$
$= 20\log_{10}|20j\omega + 2000|$
$= 20\log_{10}\left(20\sqrt{\omega^2+100^2}\right)$ ↳ $\omega = 146$
$= 70.97$ dB

---

let ....
$H(s) = K\dfrac{(s-z_1)(s-z_2)\cdots(s-z_m)}{(s-p_1)(s-p_2)\cdots(s-p_n)}$

$H_{dB} = 20\log|K| + 20\log|s-z_1| + 20\log|s-z_2| + \cdots 20\log|s-z_m| - 20\log|s-p_1| - 20\log|s-p_2| - \cdots 20\log|s-p_n|$

let $H(j\omega) = H_1(j\omega)\cdot H_2(j\omega)$

$20\log_{10}|H(j\omega)| = 20\log_{10}|H_1(j\omega)| + 20\log|H_2(j\omega)|$

$\angle H(j\omega) = \angle H_1(j\omega) + \angle H_2(j\omega)$

⇒ consider: $H(s) = 1 + \dfrac{s}{a}$ → simple zero

$H(j\omega) = 1 + \dfrac{j\omega}{a}$

$H_{dB} = 20\log_{10}\left|1 + j\left(\frac{\omega}{a}\right)\right|$
$= 20\log_{10}\left(\sqrt{1^2 + \frac{\omega^2}{a^2}}\right)$

① let $\omega \lll a$
⇒ $\frac{\omega}{a}$ → negligible
$H_{dB} = 20\log_{10}(1) = \underline{0\text{ dB}}$

② if $\omega \ggg a$
⇒ 1^2 term becomes negligible
$\underline{H_{dB} = 20\log_{10}\left(\frac{\omega}{a}\right)\text{ dB}}$

③ if $\omega = 10a$
$H_{dB} = 20\log(10) = 20$ dB

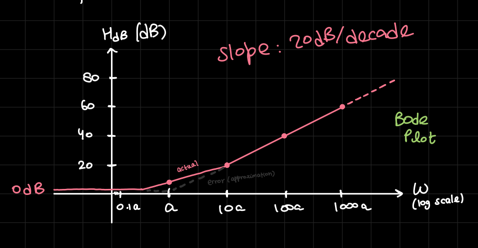
④ $\omega = 100a$
$H_{dB} = 20\log(100) = 40$ dB

⑤ $\omega = 1000a$
$H_{dB} = 60$ dB

⑥ $\omega = 10000a$
$H_{dB} = 80$ dB

Observation: $\omega \times 10 \to H_{dB} + 20$ dB

Using log scale instead of ω directly



Semilog graph because only one axis is in logarithmic scale (x-axis here is linear)

now let $\omega = a \Rightarrow H_{dB} = 20\log_{10}(\sqrt{2})$
$= 20\times\frac{1}{2}\log_{10}(2)$
$= 3$ dB

corner frequency / break freq at $\omega = a$

- Lecture 18 {Bode Plots} Missed

23/10/24

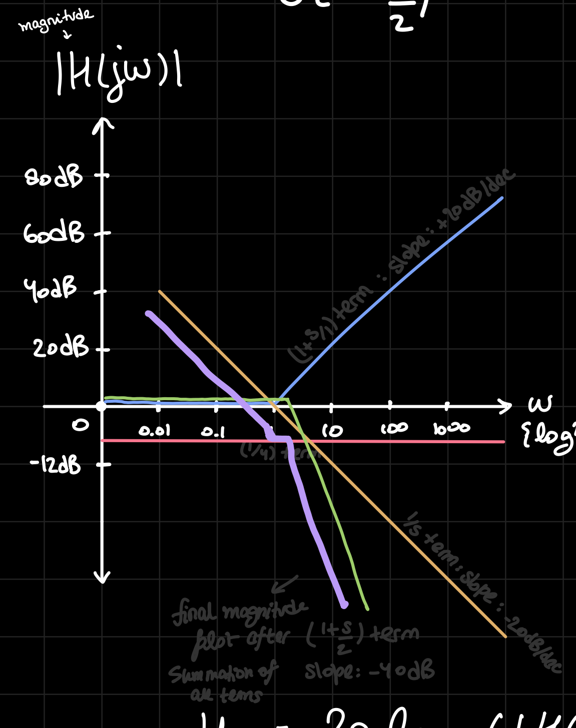
- Lecture 19 04/11/24

eg3 draw bode plots of $H(s) = \frac{s+1}{s(s+2)^2}$

zeroes: 1 → $s=-1$
poles: 3 → $s = 0, -2, -2$

$$H(s) = \frac{(1+s/1)}{s(1+\frac{s}{2})^2 \cdot 4} = \frac{1}{4}\cdot\frac{1}{s}\cdot\left(1+\frac{s}{1}\right)\cdot\frac{1}{(1+\frac{s}{2})^2}$$

simple pole case so, we have corner frequency at $w=a$ i.e. at $w=1$ & $w=2$ respectively



$$H_{dB} = 20\log_{10}(|H(jw)|)$$

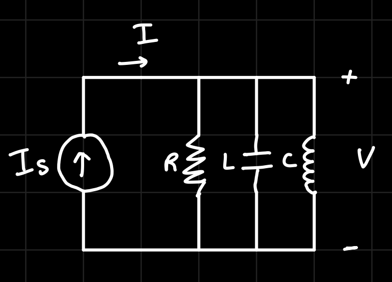
$$= 20\log_{10}\left(\frac{1}{4}\right) + 20\log_{10}\left(\left|\frac{1}{jw}\right|\right)$$

-20 log(w) straight line no break frequency

$$20\log_{10}\left(1+\frac{s}{1}\right) + 40\log_{10}\left(1+\frac{s}{2}\right)$$

todo: phase plot for ↑

- **Resonance** : A network is in resonance when V and I at network input terminals are in phase



① Assume: $I_s = I_0 \cos(wt+\phi)$

$$Y(jw) = \frac{1}{Z(jw)} = \frac{1}{R} + jwC + \frac{1}{jwL}$$

$$= \frac{1}{R} + j\left(wC - \frac{1}{wL}\right)$$

for resonance ⇒ V and I are in phase (purely resistive circuits)

i.e. $wC - \frac{1}{wL} = 0$

⇒ $w = \frac{1}{\sqrt{LC}} = w_0$ "resonant frequency"

② Assume $I_s = I_0 e^{\sigma t}\cos(wt+\phi)$

$$Y(s) = \frac{1}{Z(s)} = \frac{1}{R} + sC + \frac{1}{sL}$$

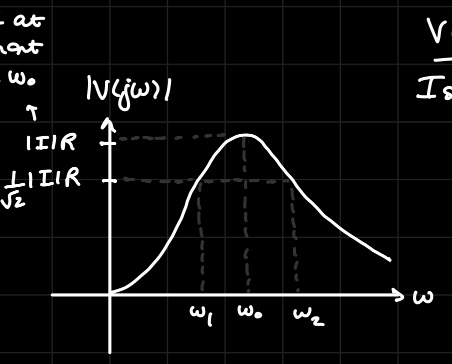
$$= \frac{s^2 + s(1/RC) + (1/LC)}{(1/C)s}$$

$V_{out} = V$
$I_{in} = I_s$ ⇒ transfer function?

$$\frac{V(s)}{I_s(s)} = Z(s) = \frac{1}{Y(s)}$$

transfer impedance

max at resonant freq. w_0



w_1, w_2 : half power frequency

height of this curve depends only on value of Resistance (R)

Width of the curve depends on L & C as well

There will be some current flowing in capacitor & inductor but it is equal and opposite so it cancels out and net total current flows only through the resistor

At resonance :

$I_s = I_R$
$I_C = -I_L$ ⇒ $I_C + I_L = 0$

quality factor

$$Q = 2\pi \frac{\text{max. energy stored}}{\text{total energy lost per time period}}$$

$$= 2\pi \frac{[w_L(t) + w_C(t)]_{max}}{P_R \cdot T}$$

P_R: avg power lost in resistor
$= \frac{1}{2}|I|^2 R$ WATTS

T : time period (sec)
$w_L(t)$: $\frac{1}{2}Li_L^2(t)$ (J)
$w_C(t)$: $\frac{1}{2}Cv_C^2(t)$ (J)

$$Q = w_0 RC = R\sqrt{\frac{C}{L}}$$

$$\alpha = \text{damping factor} = \frac{1}{2RC} = \frac{w_0}{2Q_0}$$

$$w_d : \text{damped frequency} = \sqrt{w_0^2 - \alpha^2}$$

$$= w_0\sqrt{1-\left(\frac{1}{2Q_0}\right)^2}$$

- **HALF POWER BANDWIDTH (BW)**

$$BW = w_2 - w_1 = \frac{w_0}{Q_0}$$

where $w_0 = \sqrt{w_1 w_2}$

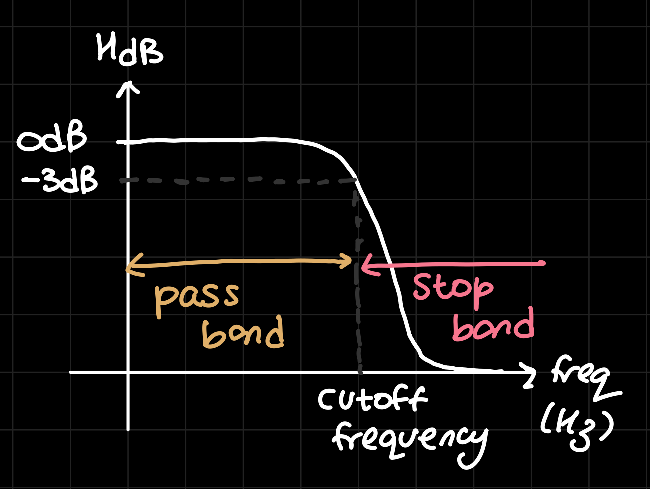
note: $BW \propto \frac{1}{Q_0}$

note: if $Q_0 > 5$: high-Q circuit

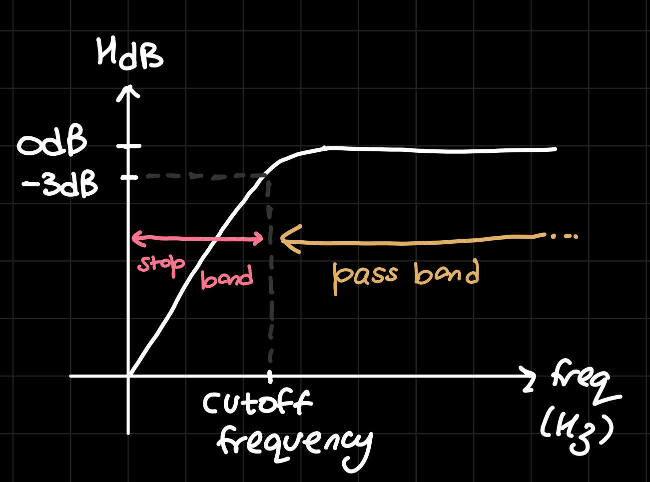
• Lecture 20 06/11/24

→ FILTER DESIGN

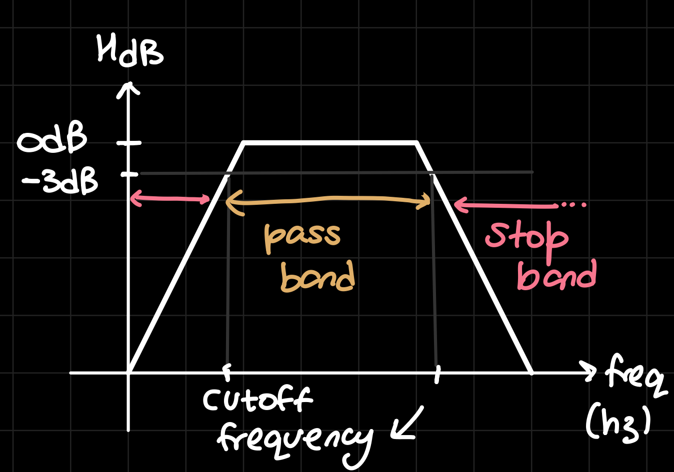
① Low Pass filter



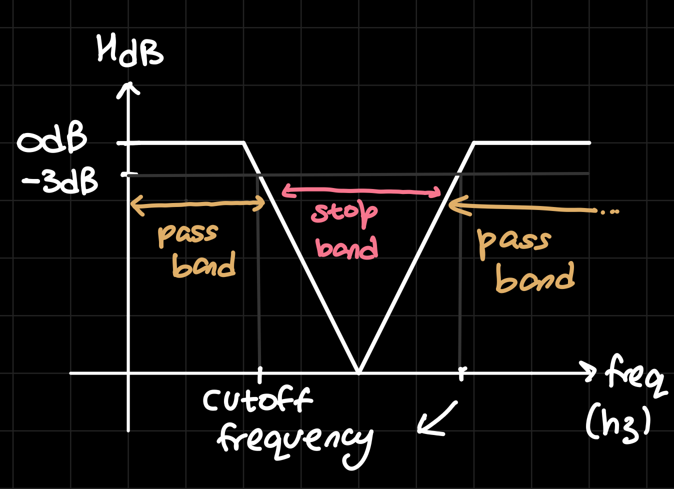
② High Pass filter



③ Band Pass Filter



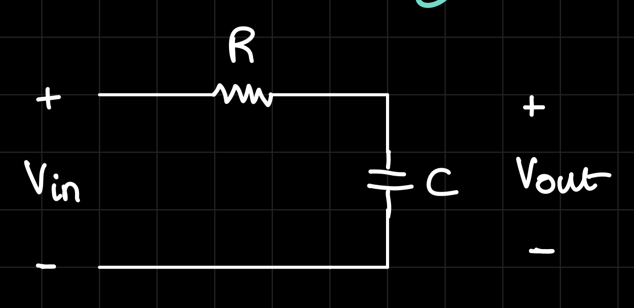
④ Band Pass Filter



• Passive filters : Gain ≤ 1 ⇒ $H_{dB} \leq 0dB$
↳ using R,L,C

• Active filters : Gain can be more than 1
here ⇒ $H_{dB} \geq 0$
↳ using opAmp + R,L,C

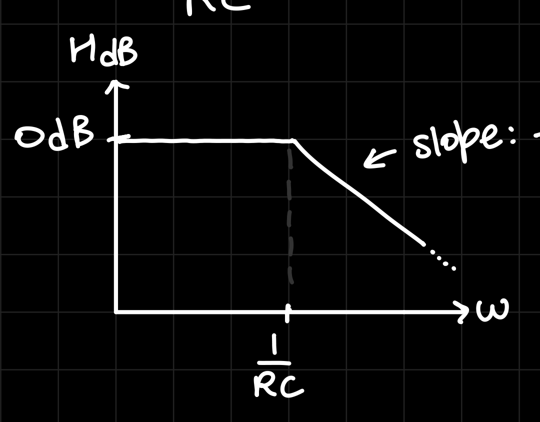
• 1st order LPF using R,L,C



$$\frac{V_{out}(s)}{V_{in}(s)} = \frac{1/Cs}{1/Cs + R} = \frac{1}{1+RCs}$$

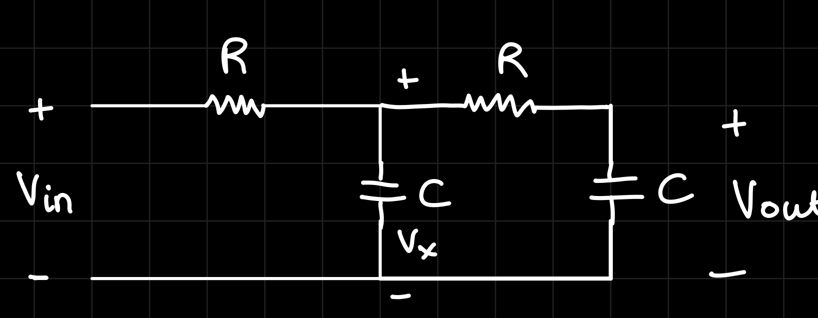
$$= \frac{1}{1+\frac{s}{(1/RC)}}$$

$$W_C = \frac{1}{RC}$$



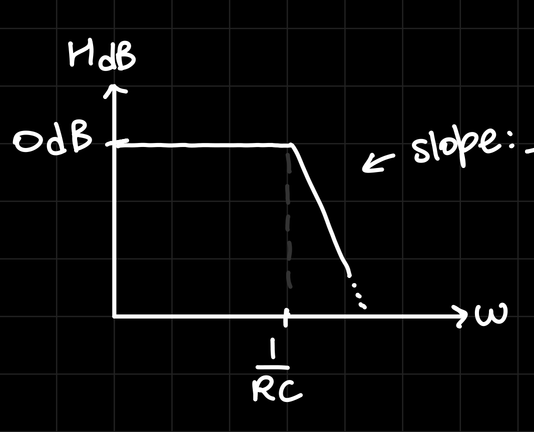
not a good filter because

• 2nd order LPF :



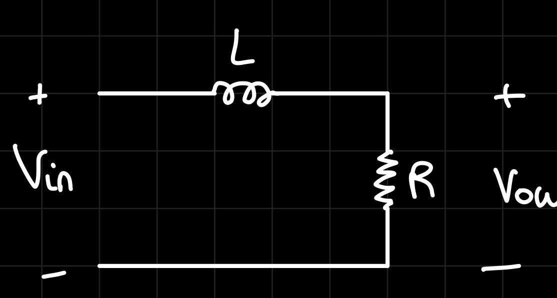
$$H(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{V_{out}(s)}{V_x} \cdot \frac{V_x}{V_{in}(s)}$$

$$H(s) = \frac{1}{1+\frac{s}{\left(\frac{1}{RC}\right)}} \cdot \frac{1}{1+\frac{s}{\left(\frac{1}{RC}\right)}}$$



cascading
↓
better filter ✓

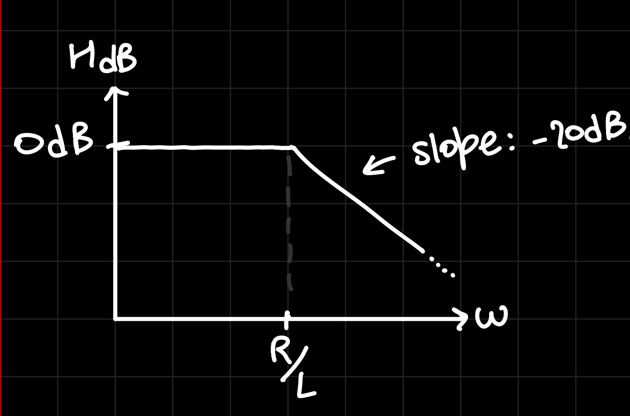
• Another 1st order LPF

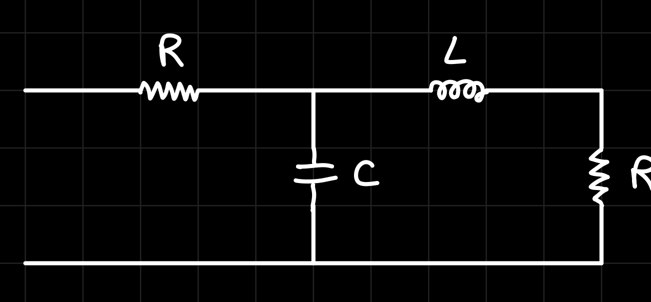


$$H(s) = \frac{V_{out}(s)}{V_{in}(s)}$$

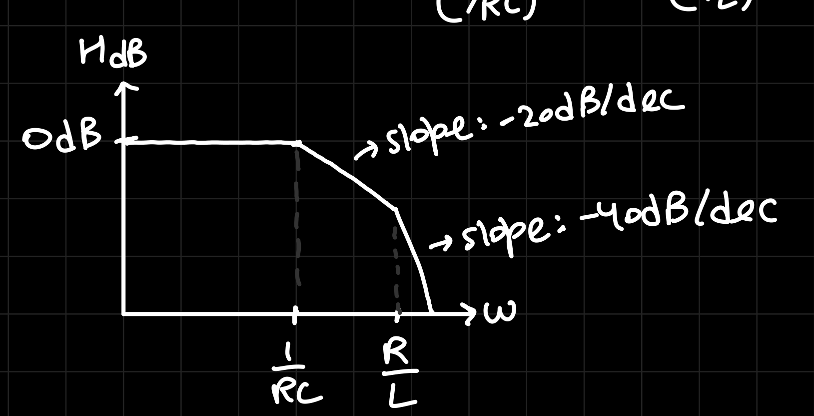
$$= \frac{R}{R+sL}$$

$$= \frac{1}{1+\frac{s}{(R/L)}}$$

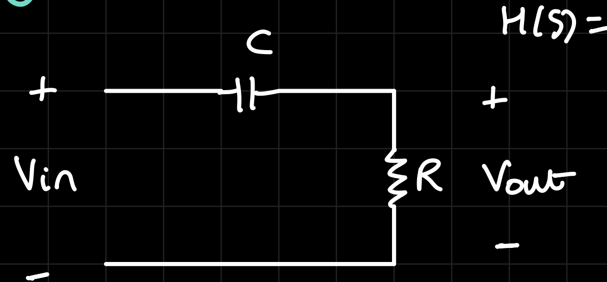




$$H(s) = \frac{1}{1+\frac{s}{(1/RC)}} \cdot \frac{1}{1+\frac{s}{(R/L)}}$$



• High Pass Filter

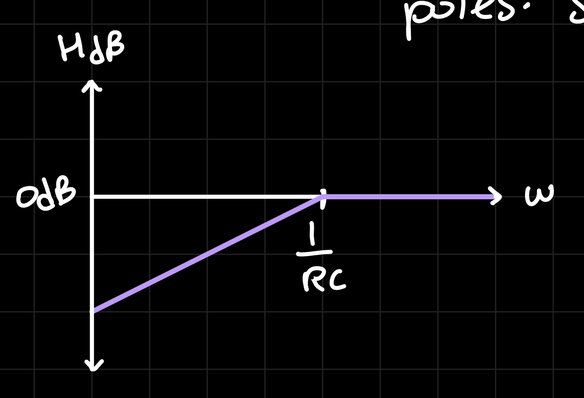


$$H(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{R}{R+\frac{1}{sC}}$$

$$= \frac{RCs}{RCs+1}$$

$$H(s) = \frac{\frac{s}{(1/RC)}}{1+\frac{s}{(1/RC)}}$$

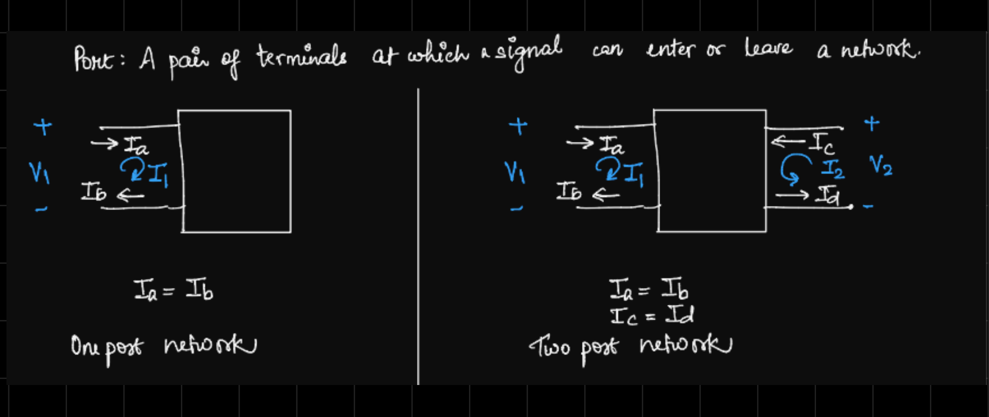
zero: $s = 0$
poles: $s = \frac{-1}{RC}$



lecture 22

13/11/24

port : a pair of terminals where a signal can enter or exit



The network ("box") can have only 1st order elements and dependent sources. (R, L, C)

Parameters

① Y parameter ② Z parameter

③ h parameter (hybrid) ③ t parameter (transmission or ABCD)

These parameters are independent of the i/p or o/p

remember y-parameter {unit : S / Ω^{-1}}

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

short circuit Y-parameter

$$Y_{12} = \left.\frac{I_1}{V_2}\right|_{V_1=0} \qquad Y_{22} = \left.\frac{I_2}{V_2}\right|_{V_1=0}$$

$$Y_{11} = \left.\frac{I_1}{V_1}\right|_{V_2=0} \qquad Y_{21} = \left.\frac{I_2}{V_1}\right|_{V_2=0}$$

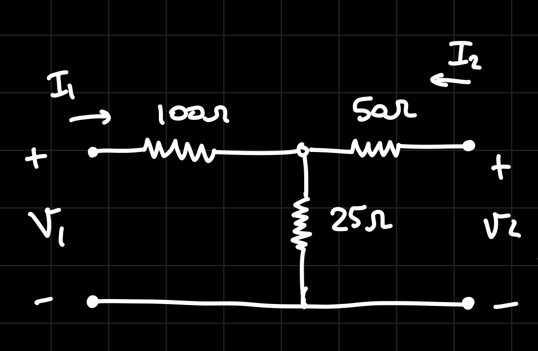
Z parameter {unit : Ω}

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$
$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

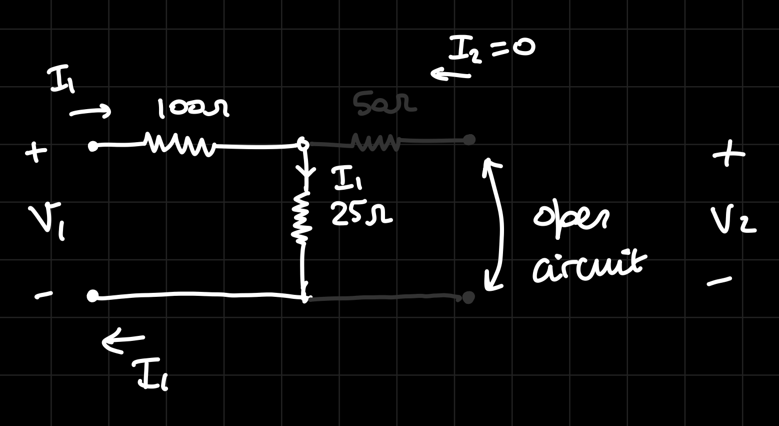
$$\underbrace{Z_{11} = \left.\frac{V_1}{I_1}\right|_{I_2=0} \qquad Z_{12} = \left.\frac{V_1}{I_2}\right|_{I_1=0} \qquad Z_{21} = \left.\frac{V_2}{I_1}\right|_{I_2=0} \qquad Z_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0}}_{\text{open circuit Z parameters}}$$

eg}



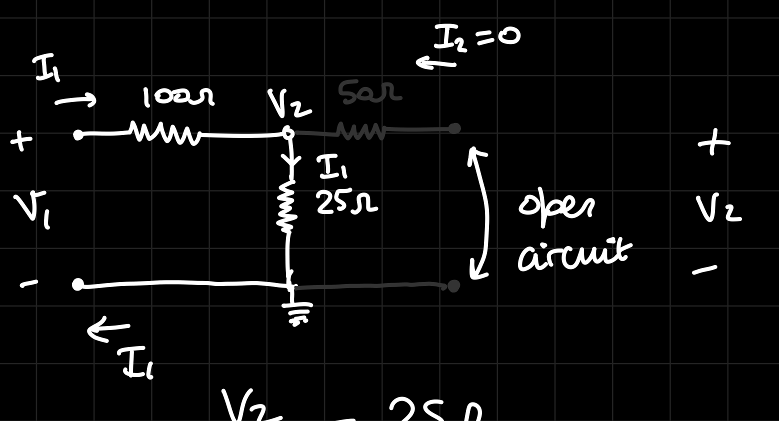
find z parameter

$$Z_{11} = \left.\frac{V_1}{I_1}\right|_{I_2=0}$$



$$V_1 = I_1(125)$$
$$Z_{11} = 125$$

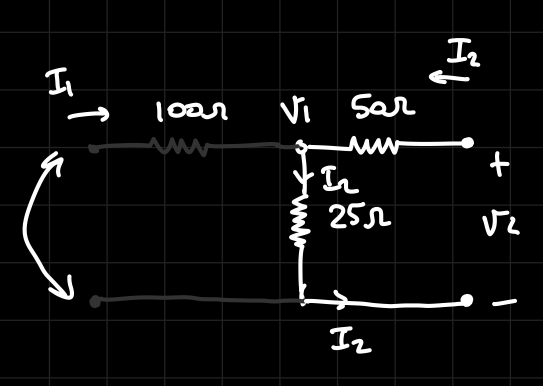
$$Z_{21} = \left.\frac{V_2}{I_1}\right|_{I_2=0}$$



$$Z_{21} = \frac{V_2}{I_1} = 25\Omega$$

$$Z_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0}$$

OC



$$Z_{22} = 75\Omega$$

$$Z_{12} = 25\Omega$$

observation: $Z_{21} = Z_{12}$

Reciprocal / Bilateral network

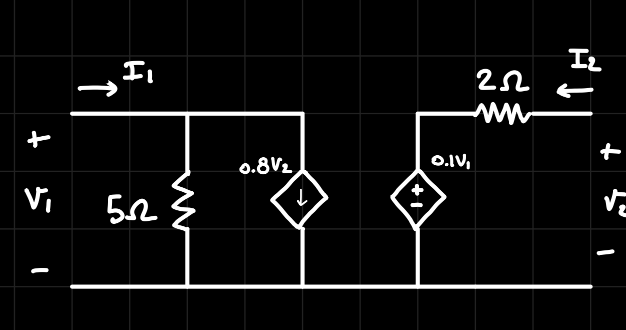
HYBRID PARAMETER (h)

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$h_{11} = \left.\frac{V_1}{I_1}\right|_{V_2=0} \ \Omega \ \text{(SC)} \qquad h_{12} = \left.\frac{V_1}{V_2}\right|_{I_1=0} \ V/V \ \text{(OC)}$$

$$h_{21} = \left.\frac{I_2}{I_1}\right|_{V_2=0} \ \frac{V}{V} \ \text{(OC)} \qquad h_{22} = \left.\frac{I_2}{V_2}\right|_{I_1=0} \ \Omega \ \text{(SC)}$$

eg}



$$I_1 = 0.8V_2 + \frac{V_1}{5} \quad ; \quad I_2 = \frac{V_2 - 0.1V_1}{2}$$

① $h_{11} = \left.\frac{V_1}{I_1}\right|_{V_2=0}$

$I_1 = \frac{V_1}{5} \Rightarrow h_{11} = 5\Omega$

② $h_{12} = \left.\frac{V_1}{V_2}\right|_{I_1=0} = -4 \frac{V}{V}$

③ $h_{21} = \left.\frac{V_2}{V_1}\right|_{I_2=0} = 0.1 \frac{V}{V}$

④ $h_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0} \Rightarrow 4V_2 + V_1 = 0$

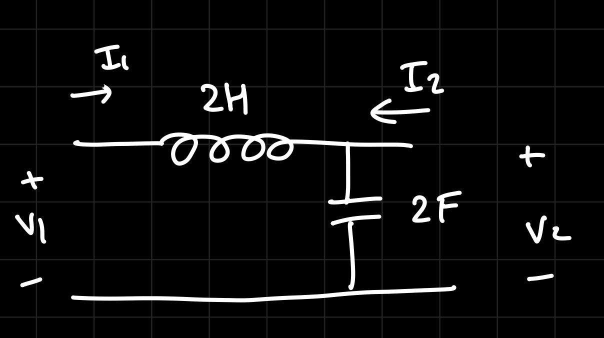
$V_1 = -4V_2$

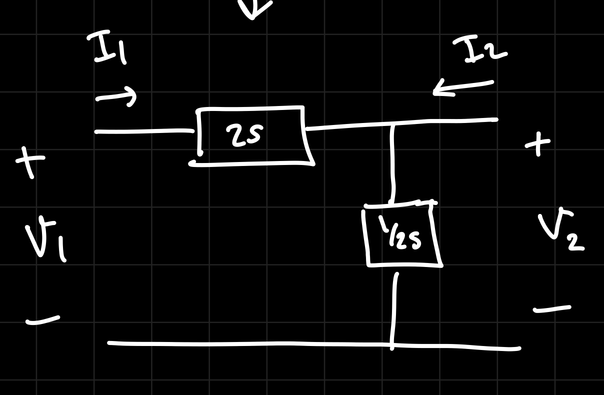
$I_2 = \frac{V_2 - 0.4V_2}{2}$

$h_{22} = 3.33\ \Omega$

$\Rightarrow \frac{V_2}{I_2} = \frac{2}{0.6} = \frac{10}{3}$

eg}





$$h_{11} = \left.\frac{V_1}{I_1}\right|_{V_2=0} =$$

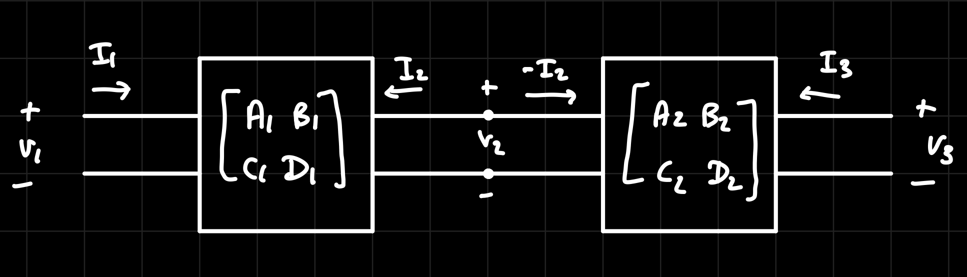
$$h_{22} = \left.\frac{V_2}{I_2}\right|_{I_1=0} = \frac{1}{2s}$$

$$h_{12} = \frac{V_1}{I_2} \qquad [h] = \begin{bmatrix} 2s\Omega & 1\ V/V \\ 1\ A/A & 2s\Omega \end{bmatrix}$$

Transmission parameter (ABCD)

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

Cascading :



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \begin{bmatrix} V_3 \\ -I_3 \end{bmatrix}$$

eg)

(admittance)
- Y Parameters {unit: S / Ω^{-1}}

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$I_1 = Y_{11}V_1 + Y_{12}V_2$
$I_2 = Y_{21}V_1 + Y_{22}V_2$

$Y_{11} = \frac{I_1}{V_1}\Big|_{V_2=0}$ $\quad Y_{12} = \frac{I_1}{V_2}\Big|_{V_1=0}$

$Y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0}$ $\quad Y_{22} = \frac{I_2}{V_2}\Big|_{V_1=0}$

(impedance)
- Z parameter {unit: Ω}

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$V_1 = Z_{11}I_1 + Z_{12}I_2$
$V_2 = Z_{21}I_1 + Z_{22}I_2$

$Z_{11} = \frac{V_1}{I_1}\Big|_{I_2=0}$ $\quad Z_{12} = \frac{V_1}{I_2}\Big|_{I_1=0}$

$Z_{21} = \frac{V_2}{I_1}\Big|_{I_2=0}$ $\quad Z_{22} = \frac{V_2}{I_2}\Big|_{I_1=0}$

if $Z_{12} = Z_{21}$ then network is called bilateral/reciprocal network

- H Parameter
(H ≡ hybrid)

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$V_1 = h_{11}I_1 + h_{12}V_2$
$I_2 = h_{21}I_1 + h_{22}V_2$

$h_{11} = \frac{V_1}{I_1}\Big|_{V_2=0}$ Ω $\quad h_{12} = \frac{V_1}{V_2}\Big|_{I_1=0}$ V/V

$h_{21} = \frac{I_2}{I_1}\Big|_{V_2=0}$ A/A $\quad h_{22} = \frac{I_2}{V_2}\Big|_{I_1=0}$ Ω^{-1}

- T Parameter (ABCD)
(T ≡ transmission)

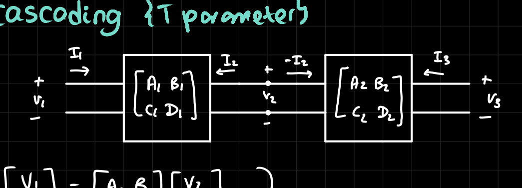
$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$V_1 = AV_2 - BI_2$
$I_1 = CV_2 - DI_2$

$A = \frac{V_1}{V_2}\Big|_{I_2=0}$ $\quad B = \frac{-V_1}{I_2}\Big|_{V_2=0}$

$C = \frac{I_1}{V_2}\Big|_{I_2=0}$ $\quad D = \frac{-I_1}{I_2}\Big|_{V_2=0}$

- cascoding {T parameter}

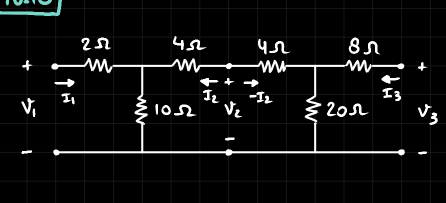


$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$
$$\begin{bmatrix} V_2 \\ -I_2 \end{bmatrix} = \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \begin{bmatrix} V_3 \\ -I_3 \end{bmatrix}$$
$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \begin{bmatrix} V_3 \\ -I_3 \end{bmatrix}$$

The coefficients are multiplied (matrix multiplication)

- Examples

16.10

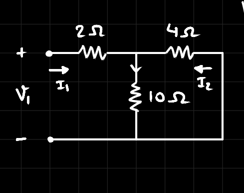


$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$A_1 = \frac{V_1}{V_2}\Big|_{I_2=0} \Rightarrow \frac{V_1}{I_1} = 12$ & $\frac{V_2}{I_1} = 10$

$\frac{V_1}{V_2} = 1.2$ V/V

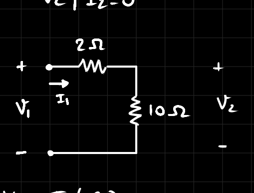
$B_1 = \frac{-V_1}{I_2}\Big|_{V_2=0}$



$V_1 = 2I_1 + 10I_1 + 10I_2$
$V_1 = 12I_1 + 10I_2$
$V_1 = 2I_1 - 4I_2$

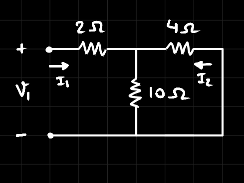
$5V_1 = -34I_2$
$\frac{-V_1}{I_2} = \frac{34}{5} = 6.8\Omega$

$C_1 = \frac{I_1}{V_2}\Big|_{I_2=0} = 0.1\ \Omega^{-1}$



$V_1 = I_1(12)$
$V_2 = I_1(10)$
$\frac{I_1}{V_2} = \frac{1}{10}$

$D_1 = \frac{-I_1}{I_2}\Big|_{V_2=0} = 1.4$ A/A



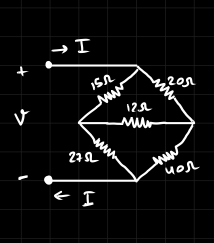
$V_1 = 12I_1 + 10I_2$
$V_1 = 2I_1 - 4I_2$
$I_1 - 2I_2 = 6I_1 + 5I_2$
$5I_1 = -7I_2$
$\frac{-I_1}{I_2} = \frac{7}{5}$

- Questions

16.3 (21)

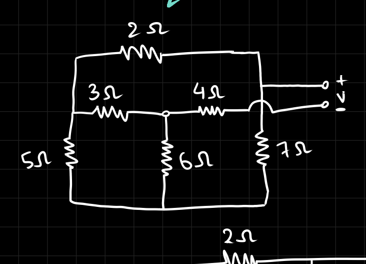
Zin?

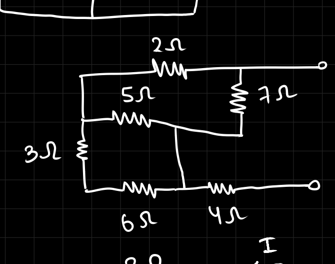
$Z_{in} = \frac{V}{I}$

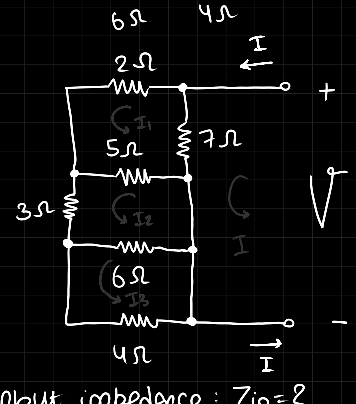


- Tutorial 11 questions

①







input impedance : Zin = ?

$Z_{in} = \frac{\Delta_Z}{\Delta_{11}}$

$-V + 7(I - I_1) = 0$
① $7I - 7I_1 = V$

$2I_1 + 5I_1 - 5I_2 + 7I_1 - 7I = 0$
② $-7I + 14I_1 - 5I_2 = 0$

$3I_2 + 6I_2 - 6I_3 + 5I_2 - 5I_1 = 0$
③ $-5I_1 + 14I_2 - 6I_3 = 0$

$4I_3 + 6I_3 - 6I_2 = 0$
④ $-6I_2 + 10I_3 = 0$

conclusion:

$$\begin{bmatrix} V \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 7 & -7 & 0 & 0 \\ -7 & 14 & -5 & 0 \\ 0 & -5 & 14 & -6 \\ 0 & 0 & -6 & 10 \end{bmatrix} \begin{bmatrix} I \\ I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

$$Z_{in} = \frac{\Delta_Z}{\Delta_{11}} = \frac{\begin{vmatrix} 7 & -7 & 0 & 0 \\ -7 & 14 & -5 & 0 \\ 0 & -5 & 14 & -6 \\ 0 & 0 & -6 & 10 \end{vmatrix}}{\begin{vmatrix} 14 & -5 & 0 \\ -5 & 14 & -6 \\ 0 & -6 & 10 \end{vmatrix}}$$

$$= \frac{7\begin{vmatrix} 14 & -5 & 0 \\ -5 & 14 & -6 \\ 0 & -6 & 10 \end{vmatrix} - 7\begin{vmatrix} -7 & -5 & 0 \\ 0 & 14 & -6 \\ 0 & -6 & 10 \end{vmatrix}}{\begin{vmatrix} 14 & -5 & 0 \\ -5 & 14 & -6 \\ 0 & -6 & 10 \end{vmatrix}}$$

$\Rightarrow 14(140 - 36) + 5(-50) = 14(104) - 250$
$= 1456 - 250 = 1206$

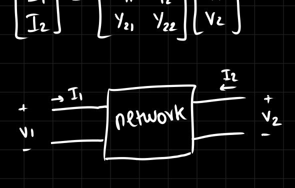
$\Rightarrow -7(140 - 36) = -7(104) = -728$

$Z_{in} = \frac{7(1206) + 7(728)}{1206} = \frac{7(1934)}{1206}$

$\approx 11.22\ \Omega$

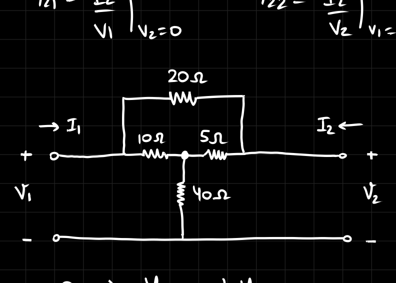
②

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$



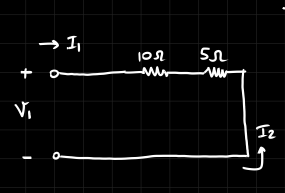
$Y_{11} = \frac{I_1}{V_1}\Big|_{V_2=0}$ $\quad Y_{12} = \frac{I_1}{V_2}\Big|_{V_1=0}$

$Y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0}$ $\quad Y_{22} = \frac{I_2}{V_2}\Big|_{V_1=0}$



① $V_2 = 0 \Rightarrow Y_{11}$ and Y_{21}

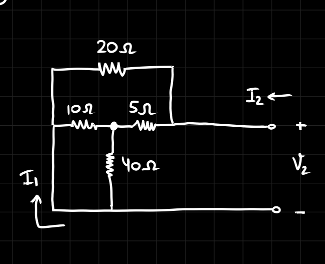
$I_2 = -I_1$



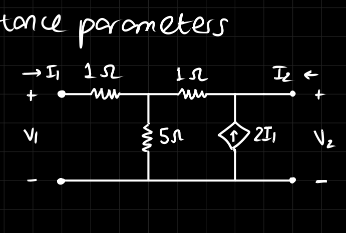
$V_1 = I_1(15)$
$\frac{I_1}{V_1} = \frac{1}{15}$
$\frac{I_2}{V_1} = \frac{-1}{15}$

$Y_{11} = \frac{1}{15}$, $Y_{21} = \frac{-1}{15}$

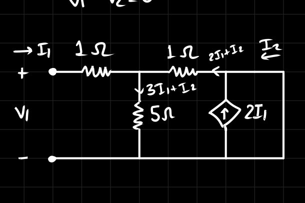
② $V_1 = 0$



③ admittance parameters

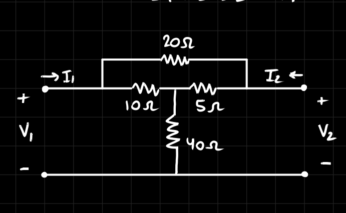


① $V_2 = 0$ $\quad Y_{11} = \frac{I_1}{V_1}\Big|_{V_2=0}$ $\quad Y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0}$

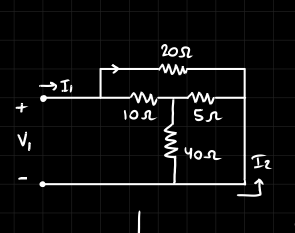


$-V_1 + I_1 + 10I_1 + 5I_2 = 0$
$9I_1 + 5I_2 = V_1$

②

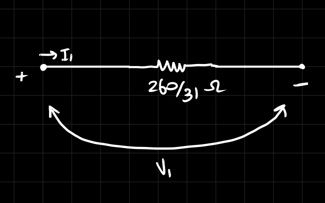


$V_2 = 0$



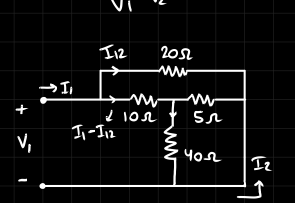
$\frac{9}{130} + \frac{1}{20}$

$\frac{260}{31}$

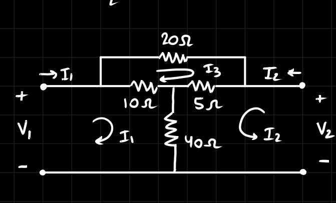


$Y_{11} = \frac{I_1}{V_1} = \frac{31}{260}\ \Omega^{-1}$ ✓

$Y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0}$



how about finding parameters using KVL equations



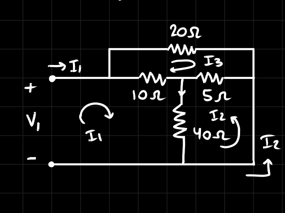
$-V_1 + 10I_1 - 10I_3 + 40I_1 + 40I_2 = 0$
$50I_1 + 40I_2 - 10I_3 = V_1$

$-V_2 + 5I_2 + 5I_3 + 40I_2 + 40I_1 = 0$
$40I_1 + 45I_2 + 5I_3 = V_2$

$20I_3 + 5I_3 + 5I_2 + 10I_3 - 10I_1 = 0$
$-10I_1 + 5I_2 + 35I_3 = 0$

$$\begin{bmatrix} V_1 \\ V_2 \\ 0 \end{bmatrix} = \begin{bmatrix} 50 & 40 & -10 \\ 40 & 45 & 5 \\ -10 & 5 & 35 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

this technique not working



$-V_1 + 10I_1 - 10I_3 + 40I_1 + 40I_2 = 0$
$30I_1 + 40I_2 - 10I_3 = V_1$

$20I_3 + 5I_3 + 5I_2 + 10I_3 - 10I_1 = 0$
$-10I_1 + 5I_2 + 35I_3 = 0$

$5I_2 + 5I_3 + 40I_2 + 40I_1 = 0$
$40I_1 + 45I_2 + 5I_3 = 0$

$$\begin{bmatrix} V_1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 30 & 40 & -10 \\ -10 & 5 & 35 \\ 40 & 45 & 5 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

$\Delta =$

$\Delta_1 = \begin{vmatrix} 40 & -10 & V_1 \\ 5 & 35 & 0 \\ 45 & 5 & 0 \end{vmatrix} = V_1(25 - 45 \cdot 35)$

$\Delta = 30(25 - 1575) - 40(-50 - 1400)$
$-10(-450 - 800)$

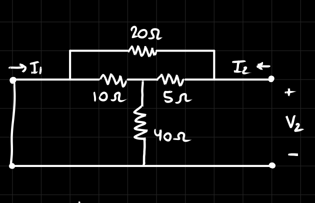
$= 30(-1550) + 40(1450) + 10(1250)$
$= -46500 + 58000 + 12500$
$= 58000 - 34000 = 24000$

$\Delta_2 = \begin{vmatrix} 30 & -10 & V_1 \\ -10 & 35 & 0 \\ 40 & 5 & 0 \end{vmatrix} = V_1(-50 - 1400)$
$= V_1(-1450)$

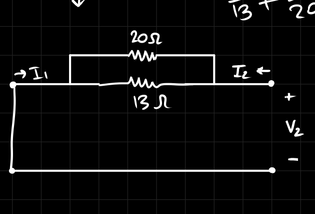
$I_2 = \frac{\Delta_2}{\Delta} = \frac{V_1(-1450)}{24000}$

$\frac{I_2}{V_1} = \frac{-145}{2400} = \frac{-29}{480}$

$V_1 = 0$}

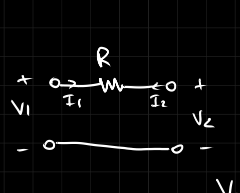


$\frac{1}{13} + \frac{1}{20}$ $\quad \frac{260}{33}$ $\quad \frac{33}{260}$



$Y_{22} = \frac{33}{260} = 0.1269\ \Omega^{-1}$

④ (a)



$I_2 = -I_1$

$\frac{V_2 - V_1}{R} = -I_1$

$V_2 - V_1 + I_1R = 0$
$V_2 - V_1 - I_2R = 0$
$V_1 + I_2R = 0$

$Y_{11} = \frac{I_1}{V_1}\Big|_{V_2=0} = \frac{1}{R}$

$Y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0} = \frac{-1}{R}$

$Y_{12} = \frac{I_1}{V_2}\Big|_{V_1=0} = \frac{-1}{R}$

$Y_{22} = \frac{I_2}{V_2}\Big|_{V_1=0} = \frac{1}{R}$

$Z_{11} = \frac{V_1}{I_1}\Big|_{I_2=0} = \infty$

$Z_{21} = \frac{V_2}{I_1}\Big|_{I_2=0} = \infty$

$Z_{12} = \frac{V_1}{I_2}\Big|_{I_1=0} = \infty$

$Z_{22} = \frac{V_2}{I_2}\Big|_{I_1=0} = \infty$