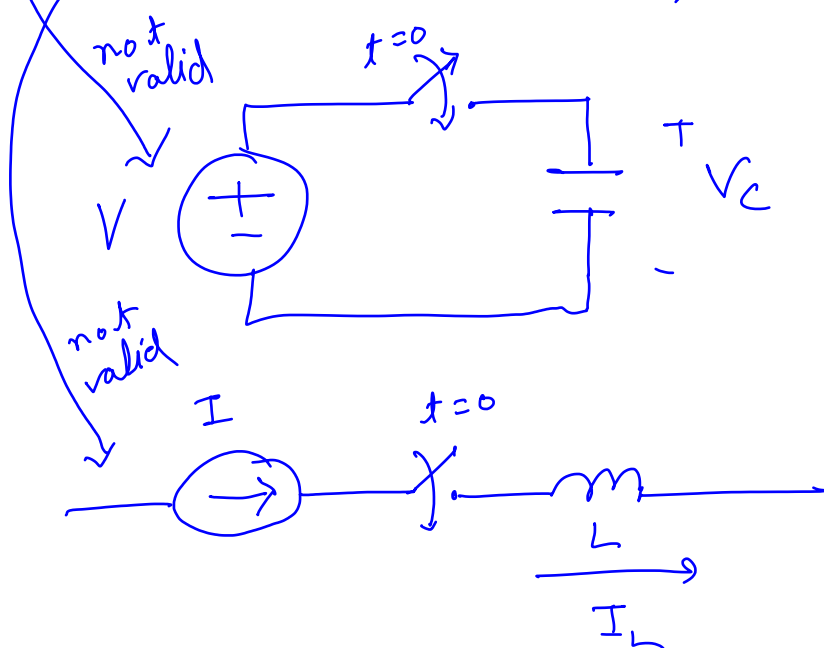


Quick Recap

$$V_C(t^-) = V_C(t^+) \text{ , provided } I_C(t) \neq \infty$$

$$I_L(t^-) = I_L(t^+) \text{ , provided } V_L(t) \neq \infty$$



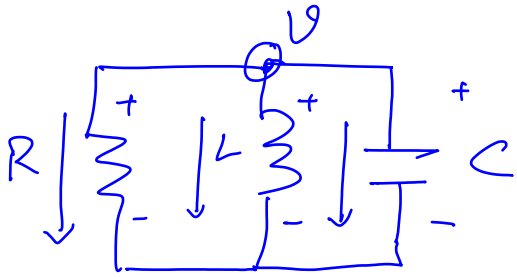
circuits involving dc sources

$$I_C(\infty) = 0 \quad \left(\lim_{t \rightarrow \infty} I_C(t) = 0 \right)$$

$$V_L(\infty) = 0$$

RLC circuit (parallel)

↳ natural response { overdamped
underdamped
critically damped



$$V_C(0) = V_0$$

$$I_L(0) = I_0$$

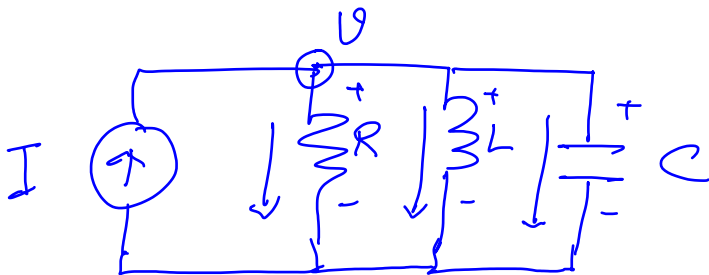
natural response,

$$V(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t} \quad (\text{overdamped})$$

$$V(t) = e^{-\alpha t} (A_d \sin \omega_d t + B_d \cos \omega_d t) \quad (\text{underdamped})$$

$$V(t) = A_1 e^{s^* t} + A_2 e^{s^* t} = e^{s^* t} (A_1 t + A_2) \quad (\text{critically damped system})$$

Forced Response of RLC circuit,



$$\left. \begin{aligned} V_C(0) &= V_0 \\ I_L(0) &= I_0 \end{aligned} \right\}$$

$$V(t) = \underset{\approx}{V_f(t)} + \underset{\approx}{V_n(t)}$$

$$\frac{d^2 V}{dt^2} + 2\alpha \frac{dV}{dt} + \omega_0^2 V = \bar{V}$$

$$\left. \begin{aligned} V(0) &= \underline{V_0} \\ \frac{dV(0)}{dt} &= \underline{\dot{V}_0} \end{aligned} \right\}$$

$$\frac{d^2 V_f}{dt^2} + 2\alpha \frac{dV_f}{dt} + \omega_0^2 V_f = \bar{V}$$

$$V_f(0) = 0$$

$$\frac{dV_f(0)}{dt} = 0$$

$$\checkmark \quad \frac{d^2 V_n}{dt^2} + 2\alpha \frac{dV_n}{dt} + \omega_0^2 V_n = 0$$

$$V_n(0) = V_0$$

$$\frac{dV_n(0)}{dt} = \dot{V}_0$$

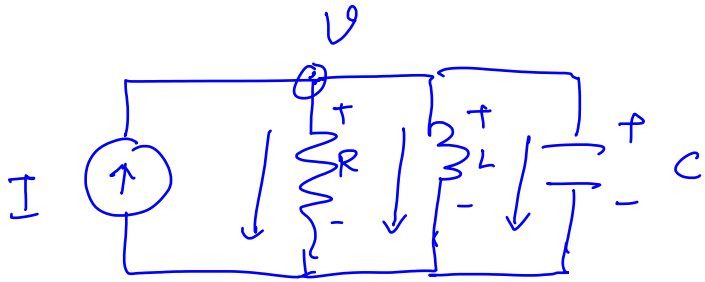
$$V(t) = V_f(t) + V_n(t)$$

$$= V_{SS} + \underbrace{V_T(t)}$$

$$\left\{ \begin{aligned} &A_1 e^{s_1 t} + A_2 e^{s_2 t} \\ &A_1 t e^{s^* t} + A_2 e^{s^* t} \\ &\vdots \end{aligned} \right.$$

$$\underline{V(t) = V_{SS} + A_1 e^{s_1 t} + A_2 e^{s_2 t}} \quad (\text{overdamped case})$$

✓ $V_{SS} = 0$ since $(\underline{V(\infty) = 0})$



$$\left. \begin{aligned} V_C(0) &= V_0 \\ I_L(0) &= I_0 \end{aligned} \right\}$$

$$I = I_R(t) + I_L(t) + I_C(t) \quad \forall t \geq 0$$

$$= \frac{V(t)}{R} + \frac{1}{L} \int_0^t V(\tau) d\tau + I_L(0) + C \frac{dV}{dt}$$

$$0 = \frac{1}{R} \frac{dV}{dt} + \frac{1}{L} V + C \frac{d^2 V}{dt^2}$$

$$\Rightarrow V_{SS} = 0$$

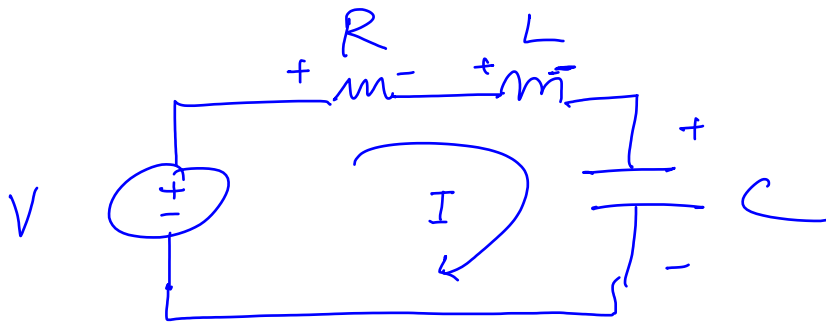
Total response, (general structure)

$$V(t) = V_{SS} + A_1 e^{s_1 t} + A_2 e^{s_2 t} \quad (\text{overdamped})$$

$$= V_{SS} + e^{-\alpha t} (A_d \sin \omega_d t + B_d \cos \omega_d t) \quad (\text{underdamped})$$

$$= V_{SS} + e^{-\alpha t} (A_1 t + A_2) \quad (\text{critically damped})$$

Series RLC circuit



$$V_C(0) = V_0$$

$$I_L(0) = I_0$$

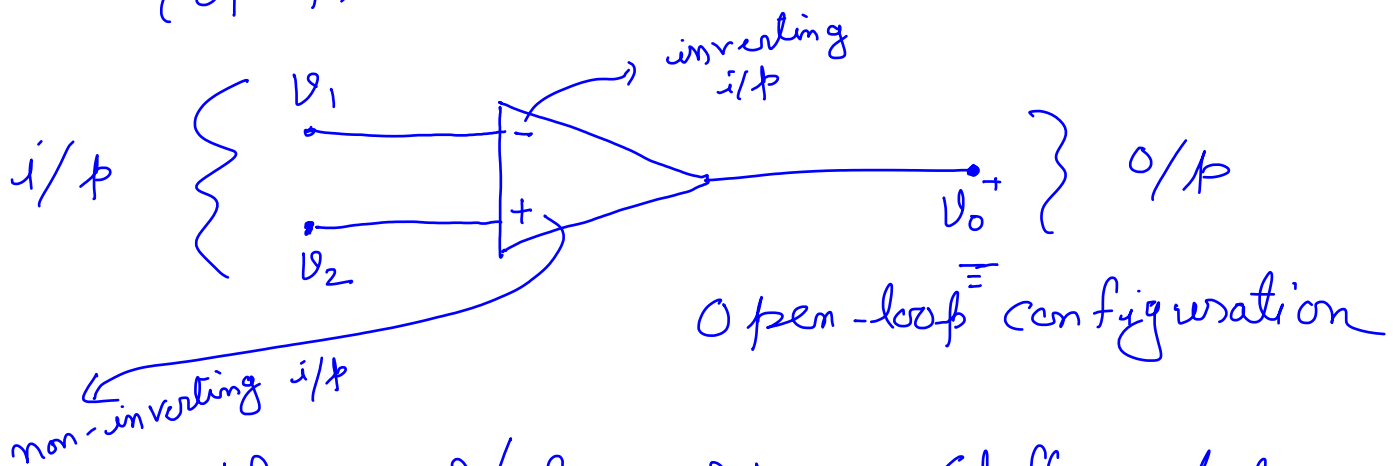
$$V = V_R(t) + V_L(t) + V_C(t) \quad \forall t \geq 0$$

$$I_C(t) = I_L(t) = I_R(t) = I(t)$$

$$V = I(t)R + L \frac{dI(t)}{dt} + \frac{1}{C} \int_0^t I(\tau) d\tau + V_C(0)$$

$$0 = \frac{dI}{dt} R + L \frac{d^2 I}{dt^2} + \frac{1}{C} I$$

Operational Amplifiers (Active element) (OpAmp)



$$V_0 = A(V_2 - V_1)$$

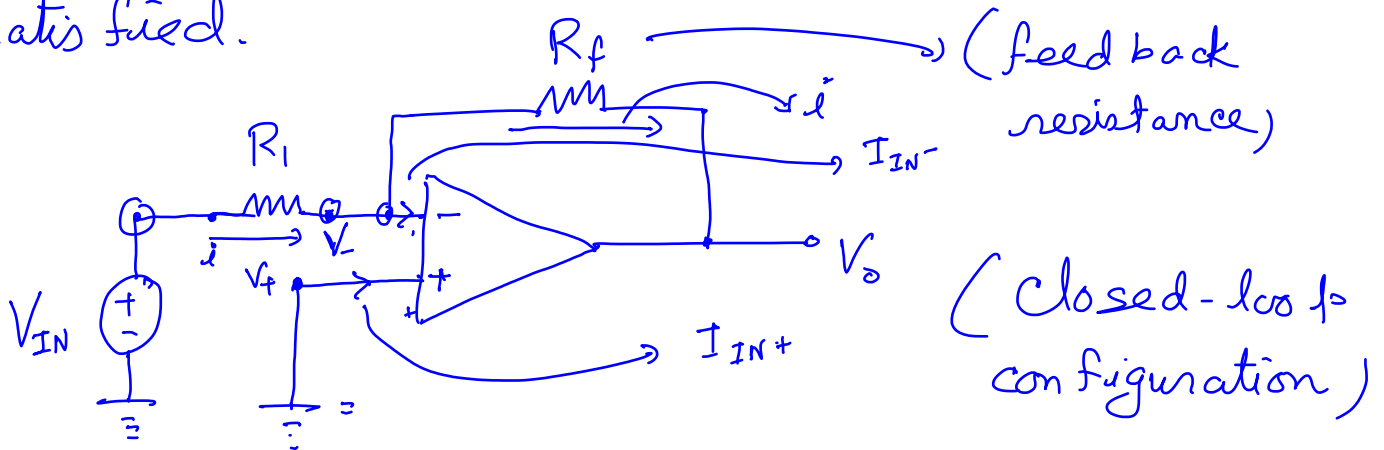
(differential amplifiers)

(linear property, only valid in a certain range of operating condition)

For an ideal OpAmp ($A \xrightarrow{\underline{\underline{\infty}}}$)

$$(V_2 - V_1) \approx 0$$

In closed-loop, this property is automatically satisfied.



In closed-loop, an ideal OpAmp follows the subsequently defined properties.

1) $V_+ = V_-$ (virtual short circuit)

2) $I_{IN-} = I_{IN+} = 0$

$V_+ = 0 = V_-$

$$i = \frac{V_{IN}}{R_i} = \frac{-V_o}{R_f}$$



$$V_o = -\frac{R_f}{R_i} V_{IN}$$

(Inverting amplifiers)

