

# Fluid Mechanics: Assignment #1

Due on 2nd September, 2018

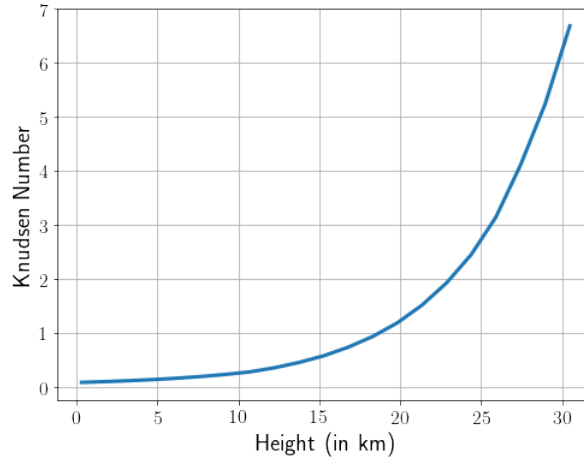
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## Problem 1

The *Knudsen Number* is given by,

$$\text{Kn} = \frac{\lambda}{L} = \frac{k_B T}{\sqrt{2} \pi d^2 p L}$$

where  $L$  is the characteristic length scale, and  $T$  and  $p$  are the temperature and pressure respectively. We can take some approximations for the variations of  $T$  and  $p$ , but we note that data for the variation of  $T$  and  $p$  is also available publicly [http://www.hyvac.com/tech\\_support/atmosphere%20vs%20pressure%202.htm](http://www.hyvac.com/tech_support/atmosphere%20vs%20pressure%202.htm). We import that data and use it to do our calculations. We also assume some standard values for all the other parameters.



## Problem 2

$$\frac{dC}{d\eta} = \kappa \exp\left(\frac{-\eta^2}{4D}\right)$$

where  $\eta = x/\sqrt{t}$ . Performing the indefinite integral and substituting for  $\eta$ , one gets,

$$C(\eta) = \sqrt{D\pi}\kappa \operatorname{erf}\left(\frac{\eta}{2\sqrt{D}}\right) + \alpha = \sqrt{D\pi}\kappa \operatorname{erf}\left(\frac{x}{2\sqrt{D}\sqrt{t}}\right) + \alpha$$

where  $\alpha$  is some integration constant. We now go ahead and impose boundary conditions

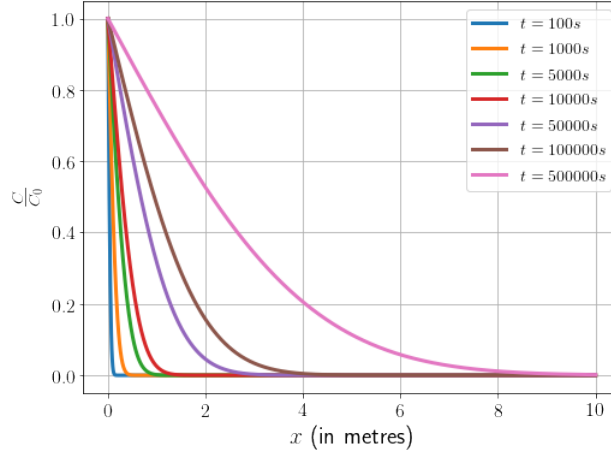
- The concentration at the flower ( $x = 0$ ) is assumed to be a constant  $C_0$  at all times. As  $\operatorname{erf}(0) = 0$ ,  $\alpha = C_0$

- At  $t = 0$ , any  $x$  would have zero concentration. As  $\text{erf}(x \rightarrow \infty) = 1$ , We get the condition that  $\sqrt{D\pi}\kappa + C_0 = 0$  ie.  $\kappa = -C_0/\sqrt{D\pi}$

Therefore, the final solution is,

$$C(x, t) = C_0 \left[ 1 - \text{erf} \left( \frac{x}{2\sqrt{D}\sqrt{t}} \right) \right]$$

The function is plotted below for different  $t$  using standard value of diffusivity  $D \approx 10^{-5} \text{ m}^2/\text{s}$ ,



### Problem 3

#### Part (a)

The continuity equation ( $\nabla \cdot \vec{v} = 0$ ) in cylindrical coordinates is given by,

$$\frac{1}{\rho} \frac{\partial v_\rho}{\partial \rho} + \frac{1}{\rho} \frac{\partial v_\theta}{\partial \theta} + \frac{\partial v_z}{\partial z} = 0$$

For flows symmetric about the  $\phi$  direction, this can be written as,

$$\frac{1}{\rho} \frac{\partial v_\rho}{\partial \rho} + \frac{\partial v_z}{\partial z} = 0$$

The stream function  $\psi$  should be such that,

$$d\psi = \frac{\partial \psi}{\partial \rho} d\rho + \frac{\partial \psi}{\partial z} dz = M d\rho + N dz \implies \frac{\partial M}{\partial z} = \frac{\partial N}{\partial \rho}$$

Comparing the forms of the last two equations, one can infer,

$$M = \frac{\partial \psi}{\partial \rho} = \rho v_z \text{ and } N = \frac{\partial \psi}{\partial z} = \rho v_\rho$$

Therefore, the stream function  $\psi$  is given by,

$$\psi = \int \rho v_z d\rho + \int \rho v_\rho dz$$

The streamlines for a cone are plotted in the figure below.

#### Part (b)

The velocity fields at the respective locations of the stream functions as shown in the figure will be  $v_1 =$

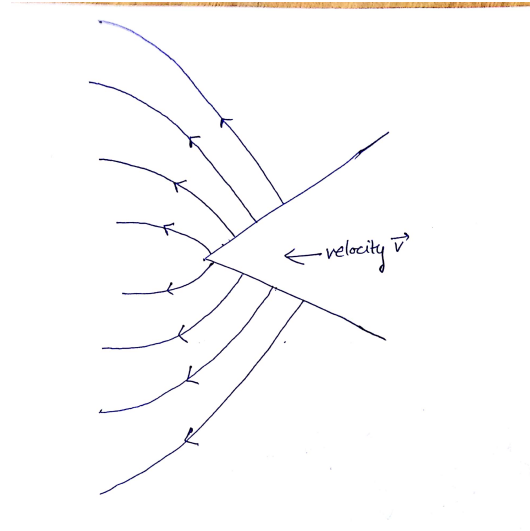


Figure 1: Flow past moving cone, assuming slip

$\nabla \times \vec{\psi}_1$  and  $v_2 = \nabla \times \vec{\psi}_2$ , where  $\vec{\psi}_1 = (0, 0, \psi_1)$  and  $\vec{\psi}_2 = (0, 0, \psi_2)$ . The streamlines for this flow will meet somewhere in between (because there cannot be two directions of velocity at a single point). For example, such a flow can be generated by two moving infinite plates inclined at an acute angle, and having the no-slip boundary condition.

## Problem 4

$$\nabla u = e_{ij} + \Omega_{ij}$$

We can do the above decomposition of  $\nabla u$  into a symmetric and antisymmetric tensor.  $\Omega_{ij}$  **represents pure rotation**. The symmetric part can be written and the divergence of some  $\phi$ .

Let the principle axes in the problem be  $x, y$  and  $z$  (different from the coordinate axes). For some constants  $a, b, c$ ,  $\phi$  can be written as (in three dimensions),

$$\begin{aligned} \phi &= \frac{1}{2}(ax^2 + by^2 + cz^2) \\ &= \frac{1}{2} \left[ \frac{a+b+c}{3}(x^2 + y^2 + z^2) + \frac{2a-b-c}{3}x^2 + \frac{2b-a-c}{3}y^2 + \frac{2c-b-a}{3}z^2 \right] \\ &= \frac{1}{2} [\alpha(x^2 + y^2 + z^2) + \alpha_1 x^2 + \alpha_2 y^2 + \alpha_3 z^2] \end{aligned}$$

We note that  $\alpha_1 + \alpha_2 + \alpha_3 = 0$ . Then,

$$\begin{aligned} \phi &= \frac{1}{2} [\alpha(x^2 + y^2 + z^2) + \alpha_1 x^2 + \alpha_2 y^2 - (\alpha_1 + \alpha_2)z^2] \\ &= \frac{1}{2} [\alpha(x^2 + y^2 + z^2) + \alpha_1(x^2 - z^2) + \alpha_2(y^2 - z^2)] \end{aligned}$$

We see that the first term is symmetric in the coordinates, and hence we remark that it is the pure expansion/contraction term. Similarly, the other two terms are antisymmetric under exchange of coordinates, hence they are pure strain terms. One can make a rotation of coordinates such that

$$x^2 - y^2 \rightarrow xy \text{ and } y^2 - z^2 \rightarrow yz$$

One can now make the interpretation of the last two terms as shear strain terms in the rotated coordinates. **So, we have successfully decomposed the  $e_{ij}$  into shear strain + pure expansion/contraction.**