Multidisciplinary Topology Optimization of Hot Structures Subject to Random Engine Acoustic Loading

Topic Area: RQ16-36: Aerothermoelastic Analysis Methodologies for Aircraft Design AFRL POC: Dr. Philip S. Beran

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Problem Statement

Ever since the advent of turbine engines, acoustic loading of the neighboring structures has been noted as a significant source of fatigue damage that tends to reduce the intended life cycle of affected components. As early as 1950's, random acoustic loading was identified as a critical parameter that warrants consideration in the early design of aircraft. Despite this observation, acoustic loads have received little attention in preliminary design concepts due to the complex nature of the dynamic problem that is inherent in an acoustic related analysis, which can make analysis both computationally and time demanding. Additionally, acoustic loads are considered low in magnitude with respect to structure loads imposed by aerodynamic and thermal effects. Regardless of small loading magnitude, severity of acoustics is amplified by multi-physical nature of aircraft loading environment, which is not typically considered in preliminary design stage. As a result, over the past 70 years, there have been notable fatigue related issues as a direct consequence of poor acoustic considerations. To remedy the impact of these early failures, substantial monetary and time expenditures are required in terms of unplanned inspection and repair intervals.

As aircraft designs become increasingly complex due to stealth and high-speed flight requirements, the role of acoustics will increase and must be treated with a novel and multidisciplinary approach in conjunction with aerodynamic and thermal loads. This is especially true for tailless Efficient Supersonic Air Vehicles (ESAV) and the accompanying Engine Exhaust Washed Structure (EEWS), which is often found in embedded engine aircraft design. These structures are exposed to random acoustic and thermal loading that cause a non-linear structural response comprising of local and global buckled modes, which are not well understood. Lack of physics in early analysis lead to early skin failures on the upper wing section of the F-15 fighter, which is a generation 4 aircraft. It is only natural that this issue is propagated to later generation aircraft such as the B-2 spirit stealth bomber, where aft-deck of the embedded exhaust structure fails prematurely due to a combination of acoustic and thermal loads. Above examples clearly demonstrate a need to develop a better physical understanding of the loading interactions within the embedded exhaust structure. More specifically, work proposed herein aims to employ a coupled fluid-structure model of the exhaust structure to accomplish following tasks:

- Incorporate heat transfer analysis of the coupled fluid-structure EEWS model to ascertain the temporal distribution throughout the structure.
- Use the temperature distribution results to obtain thermal response of the EEWS structure. Following this, perform modal analysis on the fluid-structure model in order to

- determine dynamic response and the coupling nature of the fluid and structure components. At this stage fidelity levels of the model are also investigated.
- Utilize modal analysis results in conjunction with periodic and random loading to investigate fatigue implications of the structure due to panel buckling phenomena.
- Investigate use of stress response for topology optimization in conjunction with continuum sensitivity analysis.

Accomplishing tasks above will further the understanding of acoustic and thermal interactions. It is especially interesting to study the effects thermal buckling has on random acoustic loading within the exhaust structure, which can have a profound impact on fatigue performance of individual panels that comprise the complete system. The methods developed by the proposed work will give rise to novel design configurations that otherwise would not be immediately discernible by conventional design practices. Consequently, this advanced and creative treatment of the acoustic loading effects will serve to reduce unexpected failure occurrences due to lack of physics in the preliminary design phase. This will, in turn, reduce unexpected repair costs and schedule delays for future aircraft platforms.

Background

As stated in the prior section, random acoustic vibrations became a significant source of loading, which the aircraft has to sustain during operation. This was the result of incorporating jet engines into the mainstream aircraft design in the 1950's. In these very early inceptions of jet engines, it became quickly evident that secondary structures in the vicinity of the jet engine experienced fatigue failures [1]. As these types of failures became more frequent, government agencies of the time such as National Advisory Committee for Aeronautics (NACA, today known as NASA) began to study random acoustic effects of jet engine noise on surrounding components [1-3]. The majority of failures experienced were in the aircraft skin and exhaust structures near the outlet [2]. Acoustic loading driven by the jet engine noise is typically occurring in high-frequency ranges that are as high as 1000 Hz [4]. This translates to more than a million fatigue cycles in a single flight. Since acoustic loading is a high cycle fatigue phenomenon, the majority of fatigue life is spent in initiating a crack. This is followed by a shorter period of crack growth until the defect is discovered or failure occurs [5]. If, however, a damage site is already present due aerodynamic and/or thermal loads, then acoustic fatigue life is drastically shortened since little to no operational life of the aircraft is spent initiating a damage site. This deleterious multi-loading interaction can cause panels to fail less than 10% into the service life [6]. These sort of fatigue cases lead NACA even in the 1950's to call for acoustic analysis incorporation in the preliminary design process. Failure to do so was attributed to extensive rework and repair of the affected areas, which often carried a heavy price tag [7].

Design challenges for the modern aircraft have become more daunting and influence of acoustic loads has become increasingly prominent as engines become more powerful. This is mainly driven by the need to develop aircraft that have reduced radar, infrared, and visual signatures. Additionally, there is interest in developing more efficient airframes, which are capable of sustained supersonic and hypersonic flight. Programs such as these fall under the scope of tailless ESAV concept as seen in Figure 1 [8, 9]. The pictured configuration employs an embedded engine design along with the exhaust duct work seen in the expanded view of Figure 1, which is subject to acoustic and thermal loads generated by the power plant. Embedded engine configurations have become a staple of 5th generation aircraft design and is only seen to gain

popularity in the future. As a result, loading characteristics of modern aircraft are highly multidisciplinary in nature and possess many coupled interactions that are hard to quantify using conventional design tools [10]. Additionally, the severity of the operating conditions cause a non-linear response within the structure. Modeling becomes even more difficult since material and dynamic properties of the structure are load and temperature dependent [10, 11]. Couple these challenges with the complex shapes required for EEWS in order to ensure low visibility characteristics renders the design space open for manipulation very minimal. Conventional practices such as increasing panel thicknesses may reduce deformation due to acoustic loading but is detrimental to the thermal performance of the structure. Additionally, added weight is typically not welcome in high-performance designs. Given the interplay of loading mechanisms coupled with complex and restrictive shape requirements, new and creative modeling techniques need to be developed in order to ensure robust designs.

During usual operation of the embedded engine aircraft, the exhaust structure will experience loading that is mainly driven by the power plant. These loads are a combination of random acoustic and thermal loads seen in Figure 2. In general, thermal loads can be considered quasi-static while acoustic loads are dynamic and cause the structure to react through a band of mode shapes and frequencies as directed by the acoustic nature of the turbine engine [7]. Depending on the severity of the thermal loads, the structure will experience expansion, which is resisted by surrounding structure and, as a result, thermal stresses are generated. These stresses, can in worst cases, buckle selected panels of the EEWS. Static effects of thermal loading can modify the dynamic response of the exhaust structure through deflections imparted via material expansion. Material properties are also subject to change, which will have profound effects on the dynamic response [10]. Acoustic experiments performed on heated aluminum panels show that the natural frequencies of the test articles are reduced. Furthermore, stiffness and damping characteristics are also changed, which can lead to increased deformations due to acoustic loads. Stiffness tends to go down until buckling occurs, which then increases stiffness since the panel takes on a new shape [12]. Panels exposed to acoustic loading have three modes of vibration in a thermal environment. Before buckling occurs the panel will oscillate about its neutral point. When buckling occurs two forms of vibratory response can take place. If acoustic energy is sufficiently high, it can 'push' the panel from one buckled mode to the other. This is known as snap-through [4,12,13]. Conversely, if acoustic energy is not high enough for snap though to occur, the panel will vibrate about one of the buckled points. Instances of these behaviors can be seen in Figure 3 [13]. Each one of the modes shown in Figure 3 will have a certain effect on the stress response and is critical if meaningful predictions about fatigue performance are to be made.

Based on the discussion above, determining the influence of thermal loading on the dynamic response of the structure is an integral part of the posed solution to the acoustic problem. As such thermal analysis is necessary to infer the spatial temperature distribution of the exhaust structure as shown in Figure 4. Temporal values are used to evaluate the thermal stress within the structure, which in turn is used to study the dynamic response of the coupled fluid-structure system. To the knowledge of the author this sort of analysis has not been carried out on EEWS. Since acoustic and thermal interactions are not well understood, the possibility of suboptimal design selection is likely. Therefore, to ensure sound design practices for future aircraft designs, whose requirements will only become more demanding, a good understanding of acoustic and thermal interactions is integral to success.

Technical Development and Proposed Work

Multidisciplinary nature of the proposed work will require discretization of efforts that will build upon each other to produce a complete body of work. The first step will include the thermal analysis in order to determine the temperature distribution throughout the exhaust structure. This will be necessary to quantify temperature effects on the material and dynamic properties of the model, which must be accounted for to maintain proper fidelity. Once thermal contributions have been identified, modal analysis is carried out to calculate the resonant frequencies and critical modes shapes that will dominate the dynamic response of the structure. At this time non-linear effects are investigated. Modal analysis is used in conjunction with a dynamic excitation force (periodic/random) to estimate displacements and stresses within the structure. Finally, topology optimization using stress results shall be investigated.

Following thermal analysis, one of the most critical aspects of the proposed work will be the accurate dynamic response of the coupled fluid-structure EEWS model. Modal analysis has been carried out within our research group on simple EEWS representations at room temperature. Work done by Vogel [10] extensively investigated the fluid-structure interactions of the EEWS model. Simulation results show that coupling interactions played a significant role in the modal response of the system. Failure to account for the exhaust volume inside the EEWS cavity affected the modal shapes and natural frequencies significantly enough to impact proper stress response of the model under dynamic loading. Given this conclusion, the plan is to utilize similar modeling techniques with included thermal effects. This method of analysis will make it easier to identify thermal contributions on the modal response of the system. Effects such a buckling, frequency shifting, stiffness impacts, and modal shape changes should be clearly identifiable. Once thermal effects on the modal response have been fully characterized, the plan is to move to a more representative EEWS model, which will be comprised of complex shapes indicative of real world EEWS designs as seen in Figure 2. Shape complexity may induce more pronounced fluid-structure interactions. Furthermore, curved structures tend to have higher coupling tendencies between flexural and membrane modes. These effects will be investigated accordingly.

As turbine engine pressure ratios increase with each design iteration so will the accompanying nonlinear response of the surrounding structures. These nonlinearities were evident in the panel tests carried out by Lassiter and Hess [3], where frequency response functions developed skewed response shapes with increasing sound pressure levels (SPL) seen in Figure 5. Asymmetric peaks were contributed to increase/decrease in panel stiffness. Additional effects of nonlinearity are response broadening and frequency shifting to higher values as pointed out by [6, 7]. Curve broadening is attributed to change in damping of the system while curve peak shift is credited to stiffness changes within the structure. Additionally, strain response is typically over-predicted if linear analysis is used in the nonlinear regime. All the aforementioned influences are seen in Figure 6. The nonlinear impact to frequency and strain response will have significant effects on fatigue performance of the acoustically loaded structure. Therefore it is noteworthy to investigate nonlinear impact to the proposed work. Presently, reduced order modeling is highly utilized to perform nonlinear modal analysis while maintaining computational times to reasonable levels [4,6,14,22]. Such a method or equivalent can be investigated herein to study impacts of modal nonlinearities.

Following the modal analysis and verification, the results can be used to simulate displacement and stress response of the models proposed above. Initially, a simple periodic loading condition will be implemented. This will lend itself to an easier interpretation of the

results at the initial stage. Subsequently, random loading inputs shall be implemented to compare and contrast the response of the structure with respect to the periodic loading case. An attempt will be made to acquire random acoustic loading generated by a jet engine. Furthermore, tests are planned at AFRL which are intended for investigating the acoustic response of airframe panels. If available, loading histories from the test can be utilized for model simulations. Moreover, any future test results can be used to verify the accuracy of the multi-physics models developed.

Use of simulated stress results for topology optimization is investigated next. By definition topology optimization is characterized by a systematic method that seeks to find the best material distribution within the defined boundary [15]. Topology optimization is considered an iterative technique where the material is either added or removed until an optimum design is achieved based on a cost function and supporting problem constraints. Many topology optimization techniques exist in the literature which include but are not limited to; Solid Isotropic Material with Penalization (SIMP), homogenization method, level set method, and cellular division method [16-19]. Each of the aforementioned methods have advantages and drawbacks, which have been effectively summarized by Deaton and Grandhi [20]. In work done by Vogel [10], modal results were used in conjunction with a periodic loading sequence to perform a panel thickness optimization on the EEWS model. Due to the spatial and multi-modal considerations, the design space may have multiple local optima which make the optimal solution dependent on the initial design configuration. To circumvent this problem, a hybrid optimization technique was implemented, which combines global and local search algorithms in order to obtain an optimum design. Similar techniques may be required for topology optimization in the proposed work and shall be investigated. One of the research goals is to utilize already developed design packages such as Multidisciplinary-design Adaptation and Sensitivity Toolkit (MAST) since optimization methodologies are included within the software. Additionally, it is advantageous to study MAST capabilities on acoustic related problems, which to author knowledge has not been done.

In prior works, adjoint sensitivity analysis formulations were successfully used for stress based topology optimization of thermally loaded structures [11]. Additional progress in continuum sensitivity analysis was achieved by Gobal et. al. [21] for fluid-structure interaction problems (FSI). Aforementioned sensitivity formulations are superior to their numerical counterparts such as finite difference schemes in terms of both accuracy and computational time. Therefore, work proposed herein shall pursue investigation of analytical based sensitivity methods for the proposed topology optimization.

Relevance to Previous Work

Work proposed herein plans to significantly expand on previous work done on the acoustic problem within our research group [10]. In the past, fluid-structure interactions were studied and found to be significant. However, interactions between thermal effects and random acoustic loading are still to be analyzed. Ultimate goal is to unify acoustic and thermal analysis under a single multidisciplinary approach. Additionally, a significant amount of effort has been expended within our group on the thermoelastic problem of EEWS [9, 10, 11]. Furthermore, my advisor, Dr. Ramana Grandhi is a published leader in the optimization community with over 200 authored papers. Given the past experience and expertise, our team is well suited to work on and tackle the problem presented by acoustic and thermal interactions.

Timeline

Timeframe below outlines the schedule of the proposed work. Throughout the course of the project, I expect a great deal of collaboration between Dr. Grandhi, AFRL scientists, and myself. Because I am domiciled within the Dayton area, I will be readily available to meet with the AFRL team throughout the entirety of the research project. Furthermore, I am accustomed to working within a team setting due to more than five years of industry experience in aerospace and automotive fields. Since this work is performed at the Ph.D. level schedule details are provided beyond the first year.

2016 Q1: Incorporate thermal analysis in the fluid-structure acoustic model to obtain thermal response the structure.

2016 Q2: Perform modal analysis on the simplified EEWS model to ascertain thermal effects on the dynamic response of the structure. The results will be used to fully characterize thermal influence by contrasting the results with prior work, which did not possess thermal inputs.

2016 Q3 (summer): Intent is to spend the summer working full time at the AFRL. While there, lessons learned from the simplified fluid-solid model are used to perform thermal and modal analysis on more representative complex shape EEWS model. Effects of structure complexities with respect to thermal effects will be fully investigated.

2016 Q4: Investigate non-linear modal effects due to loading conditions. This may be performed by reduced order modeling techniques or equivalent method.

2017 Q1: Modal analysis results will be used in conjunction with periodic and random loading signals to generate displacement and stress results from the simple and complex shape models.

2017 Q2: Investigate the use of stress results from the fluid-solid coupled EEWS model to perform topology optimization of the EEWS. Results will be documented and methodologies delivered to AFRL.

2017 Q3: Since modeling and analysis will be well defined at this stage, efforts can be shifted to study uncertainty quantification of the acoustic loading envelope and material properties of the model.

2017 Q4: Work outlined above can be utilized to generate stress spectra for the EEWS. These spectra can be converted into loading block cycles via rainflow counting methods and be used for fatigue life estimation.

Expected Results and Significance

At the end of the project, it is expected to obtain significant findings on random acoustic and thermal interactions that govern lifecycle limits of EEWS. Results of this work will provide multiphysics modeling techniques and tools to be used in design and simulation of aircraft components. This not only applies to embedded exhaust structures but has the potential to be modified for use on hypersonic vehicle skin analysis, where acoustic and thermal loading due to high-speed airflow are significant. The newly gained knowledge can help save the Air Force millions of dollars by preventing inadequate designs from reaching maturity only to fail soon after service life begins.

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Figures

Tailless Efficient Supersonic Air Vehicle (ESAV)

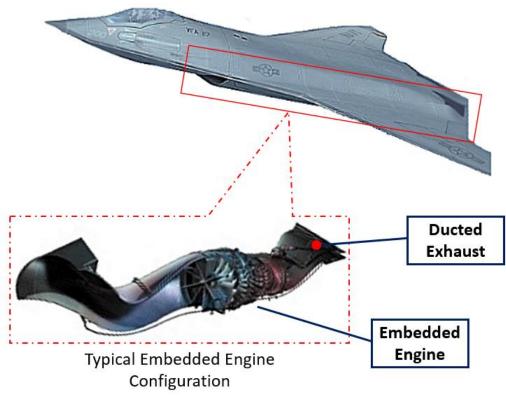


Figure 1: Tailless embedded engine configuration for a typical ESAV configuration. Expanded view shows the embedded engine configuration in more detail.

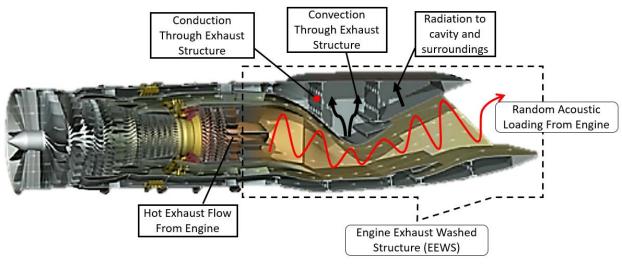


Figure 2: Acoustic and thermal loading environments often present in embedded engine configuration, which acts on the exhaust washed structure (EEWS)

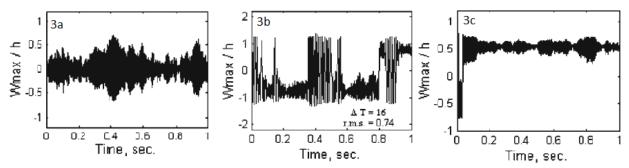


Figure 3: Dynamic response of aluminum panels subjected to thermal loading. 3a) non-buckled panel subject to acoustic loading. 3b) Post-buckled panel showing snap-though. 3c) Post-buckled panel vibrating about a buckled position.

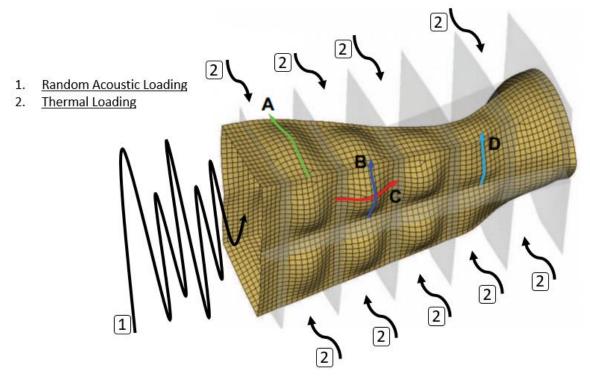


Figure 4: Deformation of the EEWS structure due to thermal expansion. Superimposed random acoustic loads with excite the thermally expanded structure, which drive a dynamics response at numerous excitation frequencies.

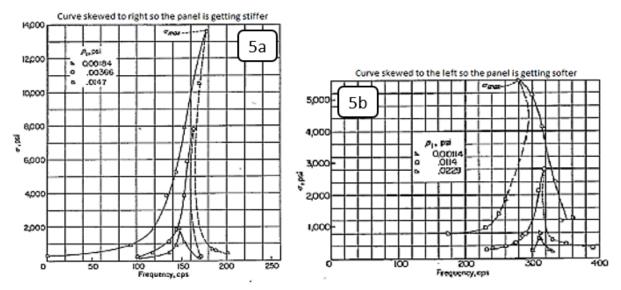


Figure 5: Asymmetric frequency response cures due to increased sound pressure levels. Figure on the left (5a) shows a response with increasing stiffness. Figure on the right shows a response with decreasing stiffness (5b)

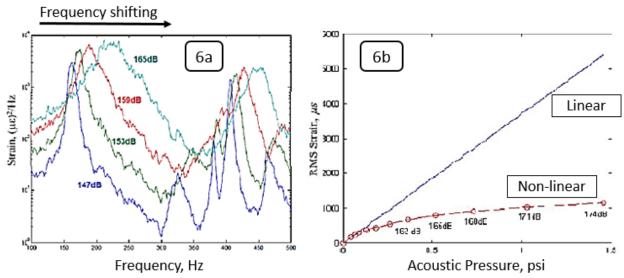


Figure 6: Frequency response function peak shifts and broadening due to nonlinear effects. Figure 6a shows non-linear effects on the frequency response. Figure 6b shows non-linear effects on strain estimations.