

ME7690 - Vibration Testing and Machine Health Monitoring

Impact of Fixture Rigidity on Cantilever Beam Vibration Response

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INTRODUCTION

There are many factors to consider during the set up phase of any experiment, which will ultimately determine the accuracy of the results. These factors include but are not limited to fixture stability, sensor health, settings of the data recorder, human factors, and surrounding noise. The goal of this study is to determine the impact of fixture stability on the vibratory response of the cantilever beam system pictured in Figure 1.



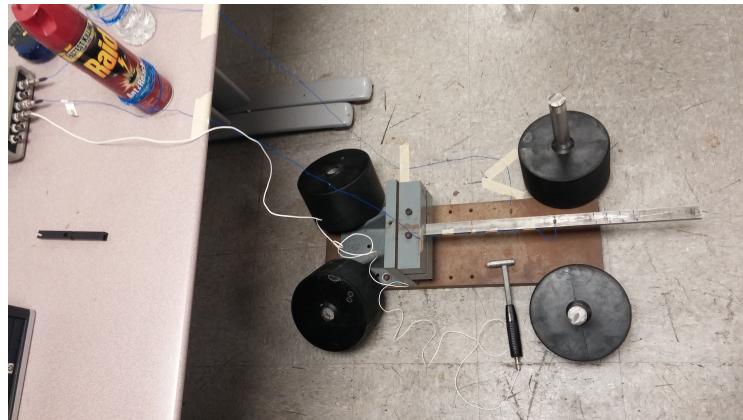
Figure 1: Cantilever Beam Setup

The Figure shows a beam that is clamped to a fixture. In order to have proper cantilever beam response, the fixture must be very stiff. Applying this concept to Finite Element Analysis (FEA), the clamped end of the beam is simulated by applying a fixed constraint. This implies infinite stiffness at the boundary, which is never true in the real world but will agree well with the experimental results if the fixture is indeed stiff and has limited movement. Of course there are experimental cases where the boundary is not assumed to be rigid and it is important to capture this behavior in FEA with proper boundary treatments. In general, the goal is for the FEA is to match the experimental set-up and not vice versa.

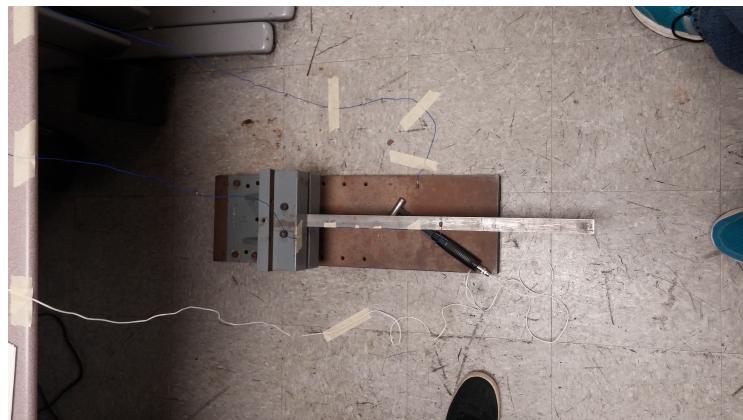
The following sections will discuss two experiments. The first experiments ensures that the fixture is made rigid. Data from this experiment will be identified by the term FIXED. The second experimental set-up deliberately makes the fixture unstable by ensuring the ground contact is not stable and even. This in turn will allow for significant motion in the fixture during testing. The second experimental set-up will be termed LOOSE. Results from the two experiments will be discussed and compared to each other in order to determine the impact of poor base fixivity.

EXPERIMENTAL SETUP

Experimental set-up for the two cases can be seen in Figure 2. In Figure 2(a) the fixture is restrained by adding 50 pound weights on each corner of the base. Conversely, the set-up in Figure 2(b) has the weight removed. In addition to this the base was placed on the section of the floor that is quite uneven, which further destabilized the base. It is also worth noting that the sensor cables were taped down to minimize noise due to cable movement.



(a) Fixed cantilevered beam setup



(b) Loose cantilevered beam setup

Figure 2: Experimental setup for the two cases

Three signals were recorded during each experiment (1 input and 2 output). Signal definitions can be seen in the Table 1 below.

Channel 1	Hammer
Channel 2	Beam Accelerometer
Channel 4	Base Accelerometer

Table 1: Channel Assignments

Channel assignments and sensor locations remained the same for both experiments in order to minimize errors due to set-up variation. For each case (FIXED and LOOSE) a total of 10 data sets were obtained. Five samples were obtained using hammer excitation at the base of the beam. The remaining five samples were obtained exciting the beam at location 4. For simplicity with further discussions, excitation locations will be termed base and LOC4. Sensing and excitation locations are illustrated in Figure 3 below.

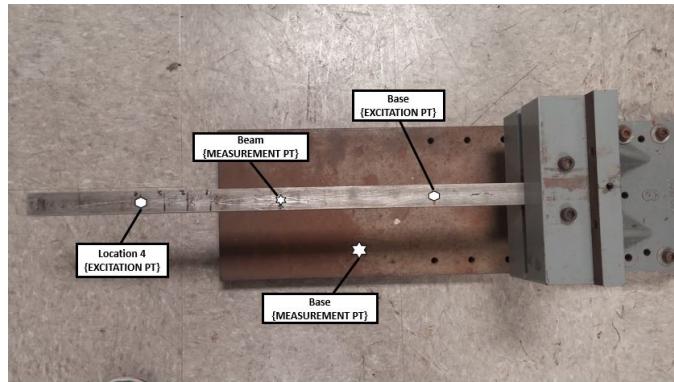


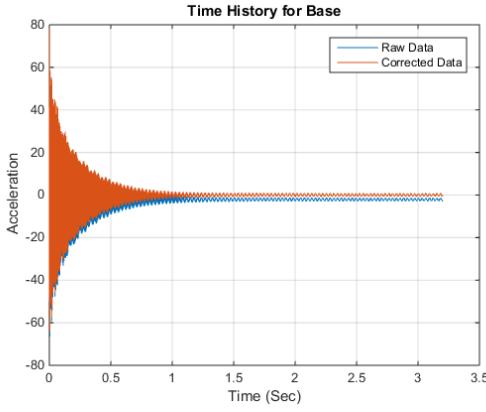
Figure 3: Cantilever beam setup

Time duration for each data sample gathered is 3.2 seconds. There is no particular reason for the choice of the period. Rather it was simply the default setting in the data acquisition system. In hindsight, it would have been wise to try longer time periods to confirm that 3.2 seconds was sufficiently long. Effort will be made in future labs to accomplish this task. Additionally, it was discovered at a later time that the beam sensor was mounted upside down, which inverted the acceleration response. This, however, does not render the data useless. It is possible to invert the time history manually during the post-process stage. Another acceptable practice is to simply swap the operational order of input and output time histories when calculating cross spectrum densities (CSD) and frequency response functions (FRF).

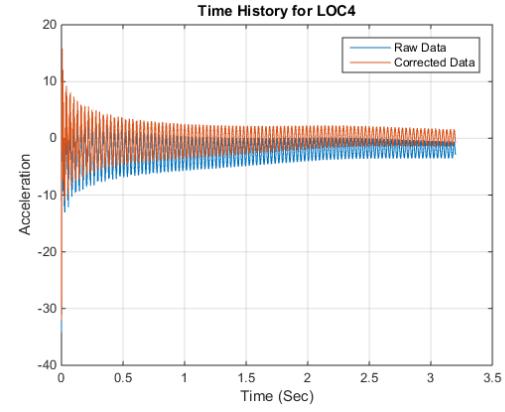
In addition to the input and output data collected, two data series were obtained for the hammer and sensors while they were resting in their respective boxes. Intention for this data is to modify the response signals during the post process phase in an attempt to reduce noise and channel drift before calculating CSD's and FRF's.

DATA INSPECTION

Input and output time histories were plotted to confirm proper response characteristics. In general the response behaved in an expected manner when compared to other cantilever beam data. For both base and LOC4 beam responses, there was a vertical shift in the data, which prevented symmetric oscillation about the x-axis. This shift was observed in the response data of the hammer and sensors while they were resting in their boxes. For this case the decision was made to use box data in order to shift the beam responses closer to the x-axis. Results of this operation can be seen in the Figure 4 below for the FIXED base condition.



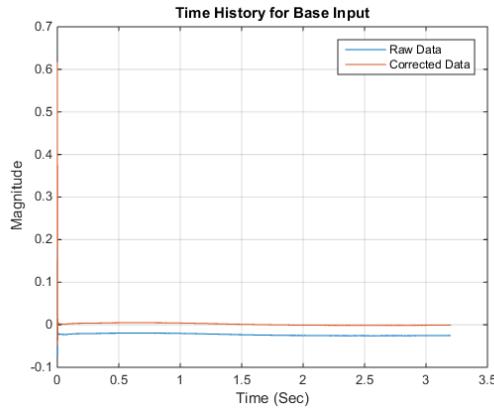
(a) Base excitation response for the FIXED fixture



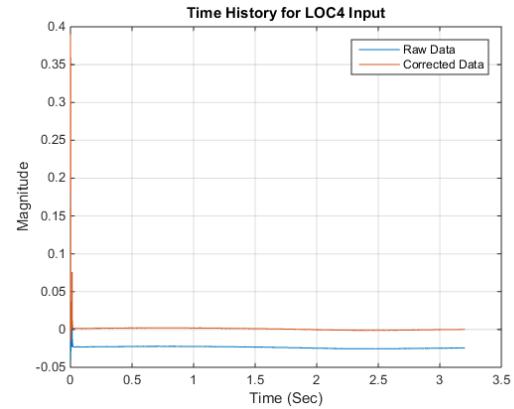
(b) LOC4 excitation response for the FIXED fixture

Figure 4: Raw and shifted response histories for the cantilever beam (FIXED)

Observing the response in Figure 4(b) it becomes evident that the beam sensor is indeed inverted since the highest amplitude occurs in the negative half of the plot. It is also evident that the modified data now looks more symmetric about the x-axis. In similar manner the input time response possessed the vertical shift, which was removed from the data using the raw input signal from the hammer while it was sitting in its respective box. The results for the shifted input signal can be seen in Figure 5.



(a) Input signal for base excitation

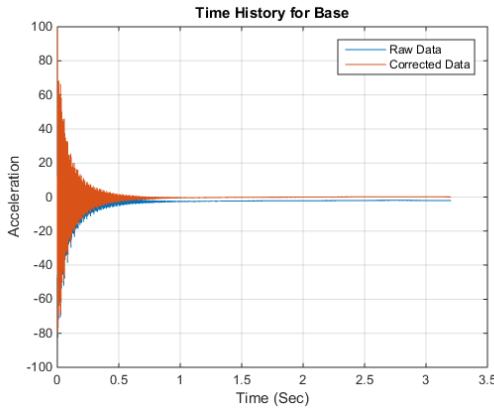


(b) Input signal for LOC4 excitation

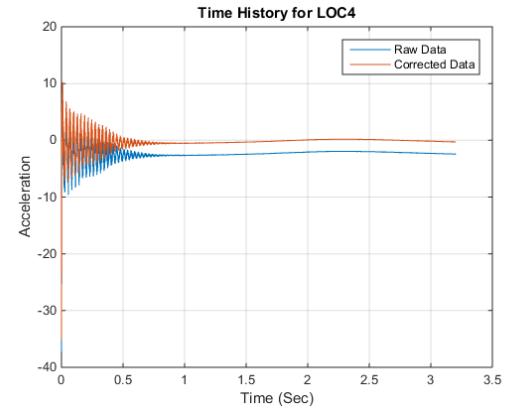
Figure 5: Raw and shifted input signals (FIXED)

The hammer strike appears well defined for both the base and LOC4 excitation. There is, however, a small double strike that consistently occurred while exciting LOC4.

In the next subsection similar plots are presented for the LOOSE condition. One thing that is quite apparent is the fact that the system damping is significantly higher because the response dies off in about 1.0-1.5 seconds. This is mainly due to pronounced fixture movement, which acts to remove energy from the system. This effect along with vertical shift of the data can be seen in Figure 6 below.



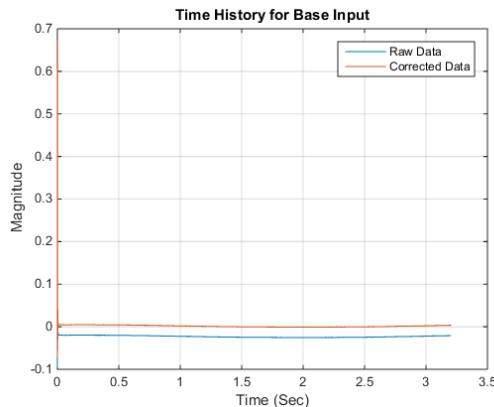
(a) Base excitation response for the LOOSE fixture



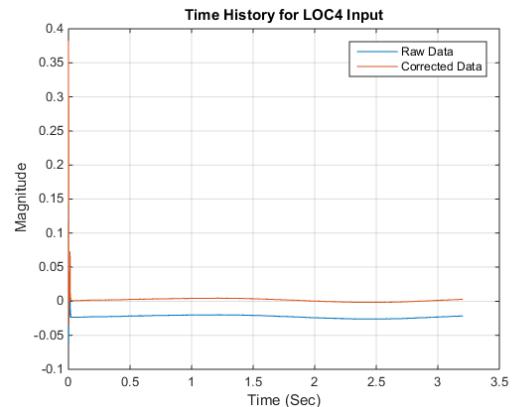
(b) LOC4 excitation response for the LOOSE fixture

Figure 6: Raw and shifted response histories for the cantilever beam (LOOSE)

The input signals did not exhibit any notable differences when compared to the FIXED base condition. Input signal for LOC4 shows a double strike feature, which was also noted for the input signal of the FIXED base experiments. Input signals for the LOOSE condition were also shifted and those results can be seen in Figure 7.



(a) Input signal for base excitation



(b) Input signal for LOC4 excitation

Figure 7: Raw and shifted input signals (LOOSE)

In the next section both shifted and raw time data were used to generate FRF's for the FIXED and LOOSE fixture conditions.

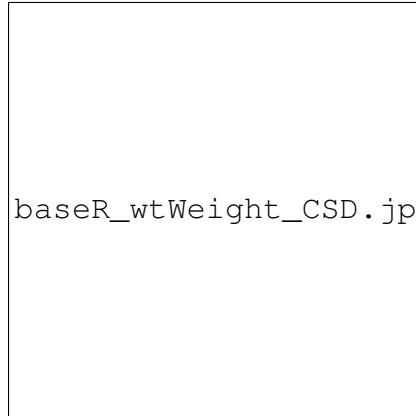
DATA ANALYSIS

In this section vibration toolbox was used to calculate all the items listed in Table 2. Both raw and shifted data were used from both experimental setups. In general, shifting the data did not change the calculations to any significant degree. The effect of the LOOSE fixture condition seems to be more pronounced when the beam is excited at LOC4. Each calculation performed in Matlab used 5 data samples.

Calculation	Number of Samples
Cross Spectrum Density (CSD)	5 samples
Auto Spectrum Density (input) (ASD)	5 samples
Auto Spectrum Density (output) (ASD)	5 samples
Frequency Response Function (H1, H2)	5 samples
Coherence	5 samples

Table 2: Performed calculations

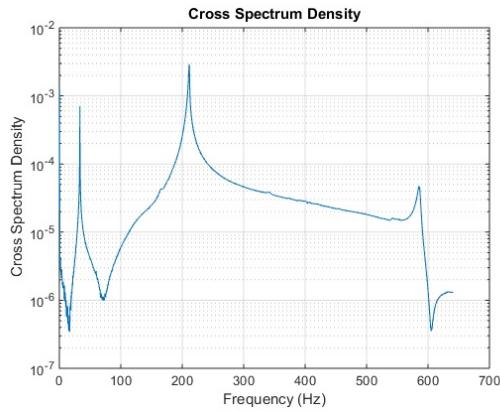
For the sake of brevity only pertinent plots will be shown in this section. The remaining plots can be found in the Appendix. First set of plots shown pertain to the base excitation. Starting with the plots of the CSD, Figure 8 shows the impact of two different fixture settings along with data correction effects.



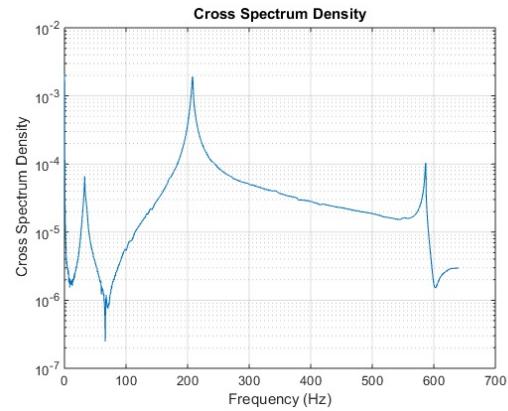
(a) CSD for base excitation using raw data (FIXED)



(b) CSD for base excitation using raw data (LOOSE)



(c) CSD for base excitation using corrected data (FIXED)

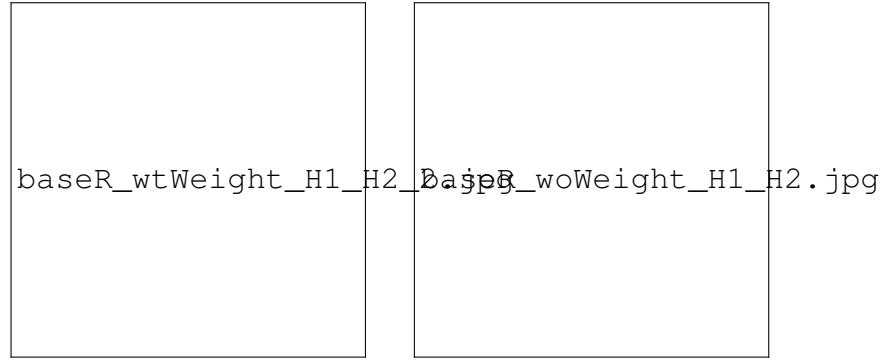


(d) CSD for base excitation using corrected data (LOOSE)

Figure 8: CSD plots for base excitation. Results shown for FIXED and LOOSE condition.

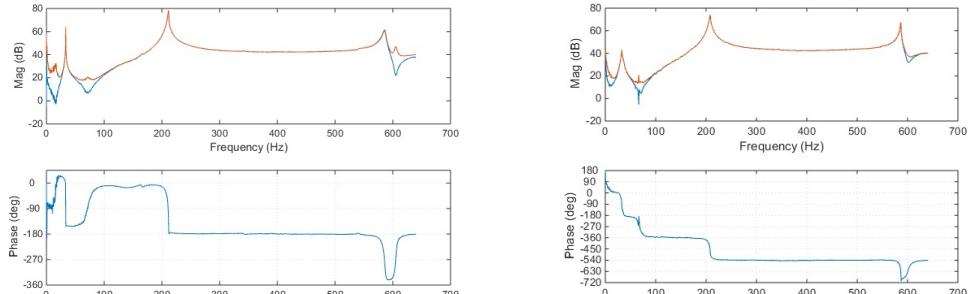
Shifting the data had no appreciable impact on the CSD plots when comparing Figures 8(a), 8(c) and 8(b), 8(d). On the other hand, fixture setting did show additional noise for the LOOSE condition. This noise is especially evident at the zero located near 75 Hz. Even with the additional noise the poles are well defined for all cases. There appears to be no shift in the natural frequency locations.

Figure 9 shows the H1 and H2 FRF estimations along with the phase plots.



(a) H1 and H2 for base excitation using raw data (FIXED)

(b) H1 and H2 for base excitation using raw data (LOOSE)



(c) H1 and H2 for base excitation using corrected data (FIXED)

(d) H1 and H2 for base excitation using corrected data (LOOSE)

Figure 9: H1 and H2 plots for base excitation. Results shown for FIXED and LOOSE condition.

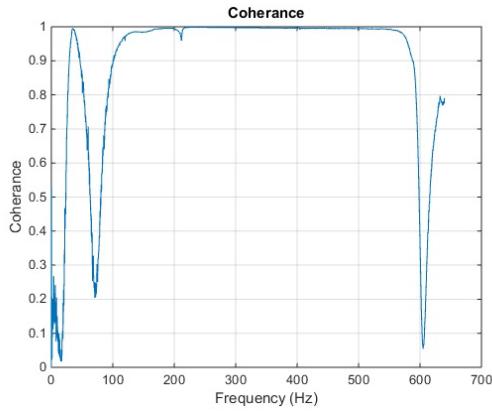
As was the case for the CSD plots in Figure 8 there is additional noise present near the zero located at 75 Hz. The additional noise impact can be clearly seen when looking at the phase plots of Figures 9(a), 9(b), 9(c), and 9(d). For the FIXED case there is a positive phase shift at the 75 Hz zero location. Conversely, for the LOOSE case the additional noise causes the calculation to think there is an additional pole at 75 Hz. As a result, the phase diagram shows a negative phase shift at 75 Hz. At the zero location, system displacement is very low and can be susceptible to noise errors. For the LOOSE case it is possible that the instability of the fixture caused the error floor to be in the same amplitude range as the actual zero measurement from the beam. This could lead to the discrepancy witnessed in the phase diagrams.

Finally the coherence plots are shown in Figure 10 below.

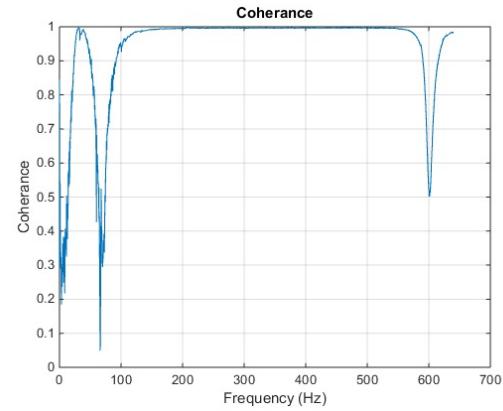


(a) Coherence for base excitation using raw data (FIXED)

(b) Coherence for base excitation using raw data (LOOSE)



(c) Coherence for base excitation using corrected data (FIXED)

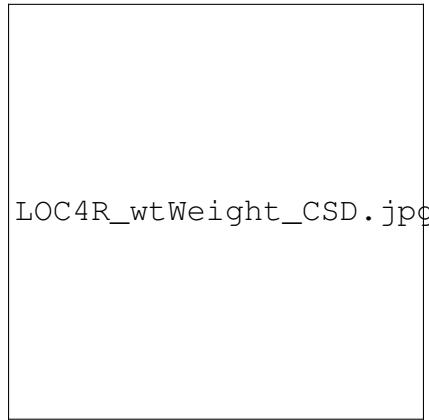


(d) Coherence for base excitation using corrected data(LOOSE)

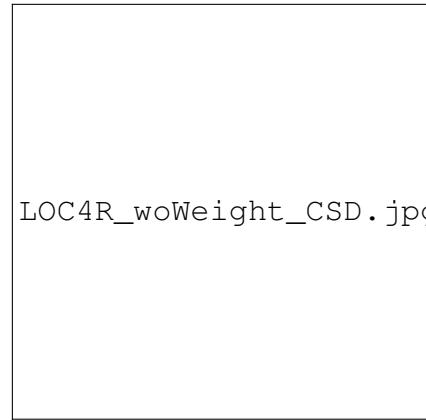
Figure 10: Coherence plots for base excitation. Results shown for FIXED and LOOSE condition.

Coherence plots for all the cases look similar with respect to each other. Very good coherence is obtained from 100-500 Hz. Remaining frequency range is not considered in the analysis as it is the last 20% of the frequency bandwidth.

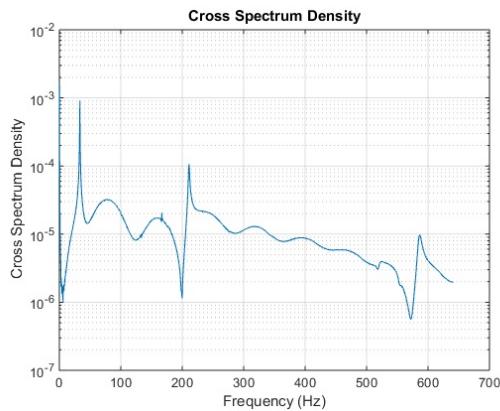
In the following subsection same plots are provided for the beam response when excited at LOC4. Figure 11 below shows plots for the CSD's.



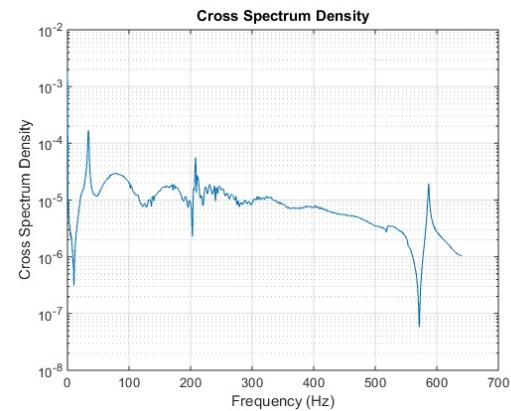
(a) CSD for LOC4 excitation using raw data (FIXED)



(b) CSD for LOC4 excitation using raw data (LOOSE)



(c) CSD for LOC4 excitation using raw data (FIXED)



(d) CSD for LOC4 excitation using raw data(LOOSE)

Figure 11: CSD plots for LOC4 excitation. Results shown for FIXED and LOOSE condition.

At the 200 Hz location there is almost a pole/zero cancellation. All the plots show this property but the LOOSE plots have significant amount of noise in this region. If no FIXED data was available for comparison this aspect of the system response can be easily missed. Comparing Figure 11 to Figure 8 there is noticeable waviness in Figure 11. This can be attributed to the over-damped type response for the LOOSE time data. Since the response dies off relatively fast (in about 1 second) there is not enough time data to get sufficient frequency resolution. In turn there appears to be leakage to surrounding frequency values.

Next set of plots show the H1 and H2 FRF estimates for the LOC4 excitation.

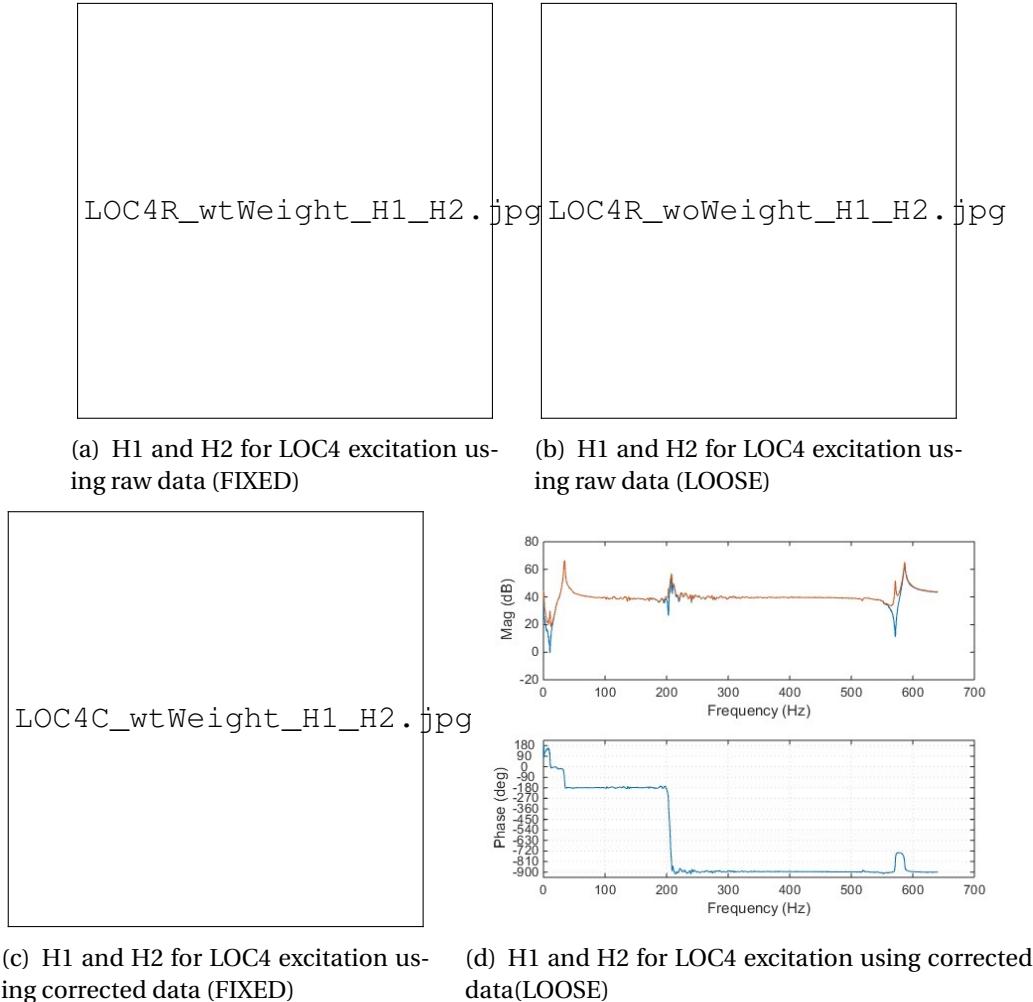


Figure 12: H1 and H2 plots for LOC4 excitation. Results shown for FIXED and LOOSE condition.

The phase diagrams of Figures 12(a) and 12(c) show just how close the FRF was to having a pole/zero cancellation. Additionally, when looking at the FRF and phase plots of the LOOSE response (12(b), 12(d)) the zero is completely masked by the noise. Furthermore, it appears from the plots that there are two closely spaced poles, which is not be the case.

Finally the coherence plots for the LOC4 excitation are shown in Figure 13.

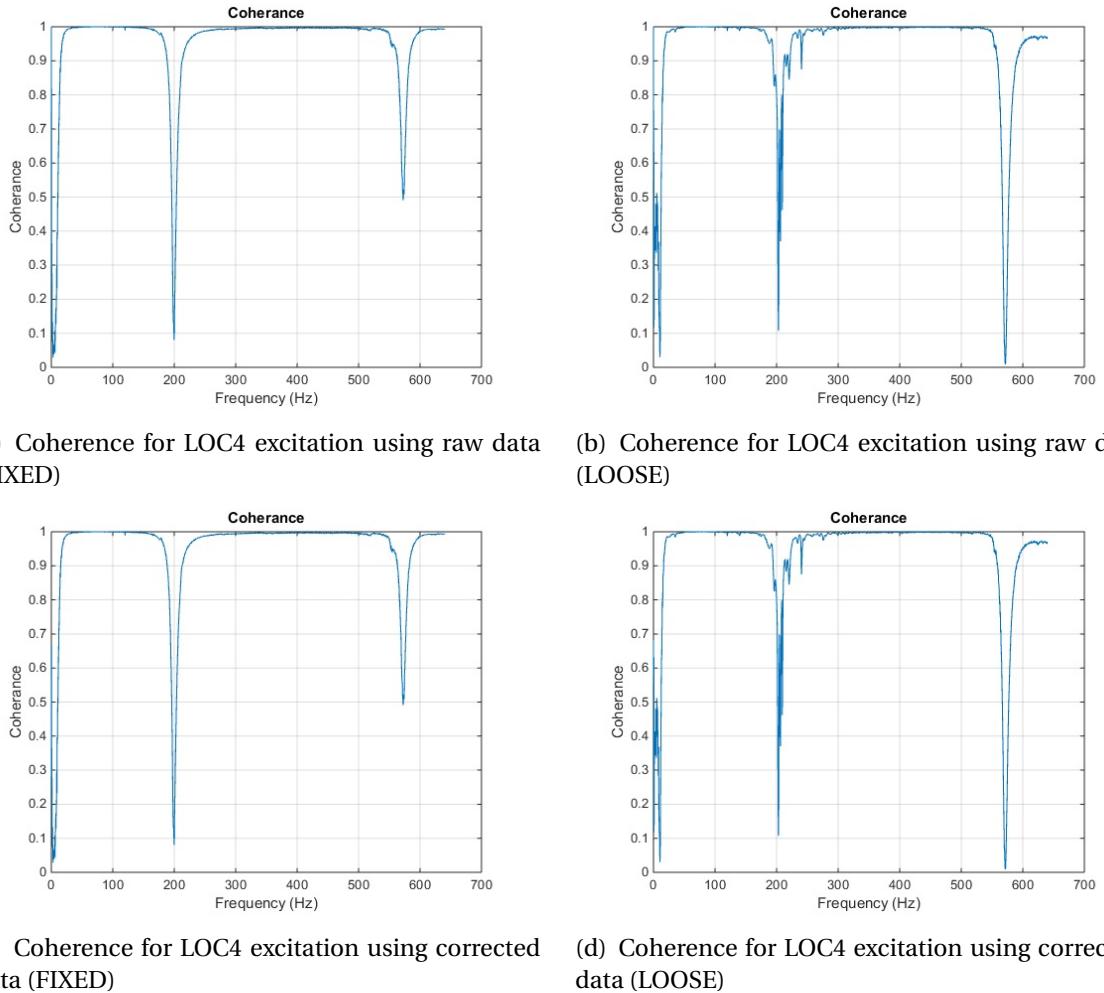


Figure 13: Coherence plots for LOC4 excitation. Results shown for FIXED and LOOSE condition.

The coherence plots show excellent behavior across the entire frequency range. Drops observed at the pole locations are to be expected. Plots in Figures 13(b) and 13(d) have noisy behavior, which is due to the LOOSE condition of the fixture.

SUMMARY

Experiments were conducted using two distinct fixture set-ups. For the first experimental set-up the fixture was well grounded and additionally supported by adding 50 pound weights on each corner. This condition was dubbed as "FIXED". For the second set-up, the weights were not used. Additionally, the fixture for the second case was purposefully placed on the uneven area of the floor, which further exacerbated fixture instability. This case was dubbed as "LOOSE".

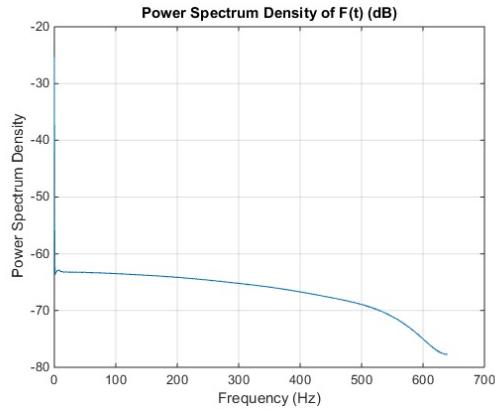
For both cases, sensors and excitation locations remained the same and are depicted in Figure 3. Beam was excited at the base and LOC4. For each of the four combinations, 5 experiments were conducted. This resulted in a total of 20 data sets for analysis. The goal of the study is to ascertain the impact of poor fixture stability on the beam response. In addition, a secondary goal was to determine the significance of shifting data to account for the drift in the input and sensor signals.

Experimental data was post-processed and the respective responses plotted with the help of the vibration toolbox. Both raw and corrected data sets were evaluated. Correcting the data for the sensor drift had no significant impact on the structure of the CSD, FRF, and coherence plots. Therefore, for this case the exercise was superfluous.

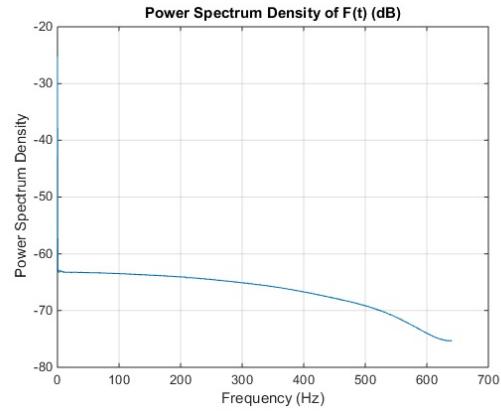
Influence of fixture stability did have a profound impact on the beam response and its respective FRF estimations. For base and LOC4 data sets the zero definitions were 'smeared' by the additional noise generated by the unstable fixture. Phase diagrams for all LOOSE calculations failed to identify the zero locations. Moreover, it also seems to add an artificial pole at the zero location. For the LOC4 FRF estimates, there was a near pole/zero calculation, which is evident in the phase diagrams of the FIXED data sets. The coherence plots were of very good quality even for the LOOSE data sets. However, they did appear more noisy near the pole locations. In conclusion ensuring good fixture grounding is quite essential to obtaining accurate system response of the cantilever beam. If FIXED data was not available for comparison, it would have been very easy to miss the zero location of the system. Additionally, LOOSE data seems to have an artificial pole in the zero region. Surprisingly the natural frequency peaks did not have any significant shift between FIXED and LOOSE data.

Appendix contains the auto spectrum density plots for all cases to serve as reference.

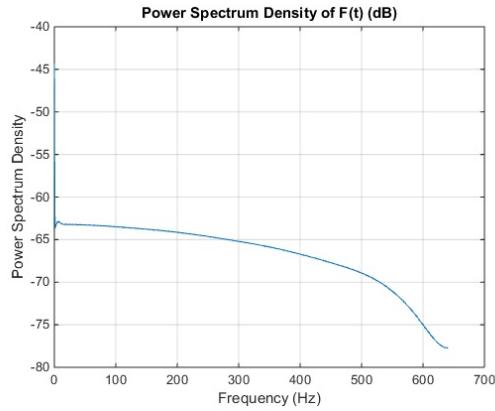
APPENDIX



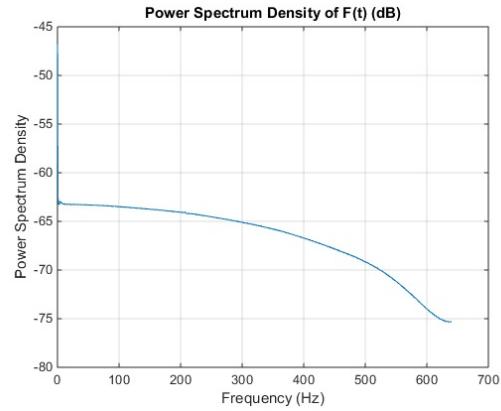
(a) Input ASD for base excitation using raw data (FIXED)



(b) Input ASD for base excitation using raw data (LOOSE)

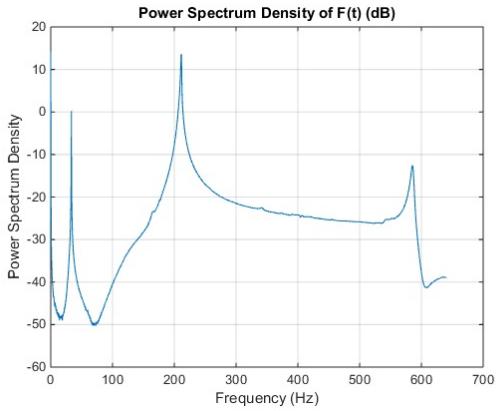


(c) Input ASD for base excitation using corrected data (FIXED)

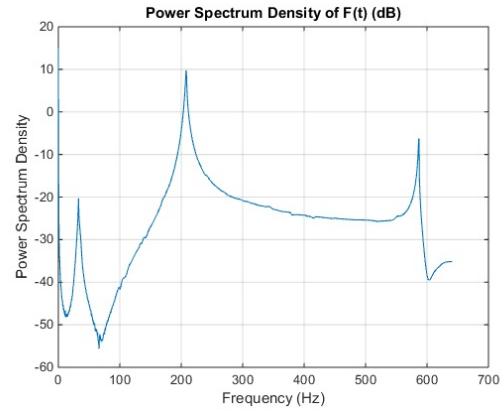


(d) Input ASD for base excitation using corrected data (LOOSE)

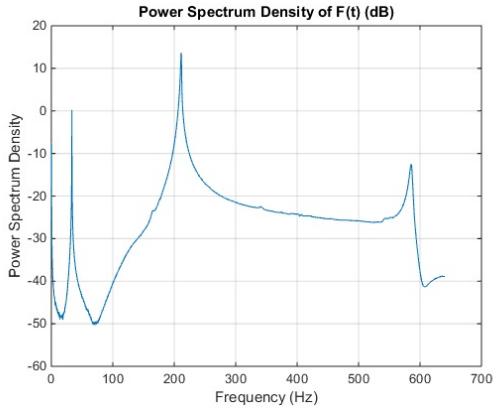
Figure 14: Input ASD plots for base excitation. Results shown for FIXED and LOOSE condition.



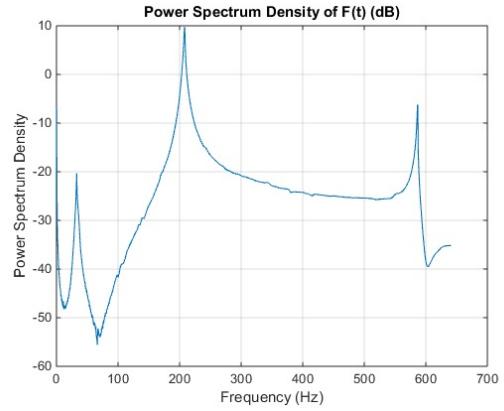
(a) Output ASD for base excitation using raw data (FIXED)



(b) Output ASD for base excitation using raw data (LOOSE)

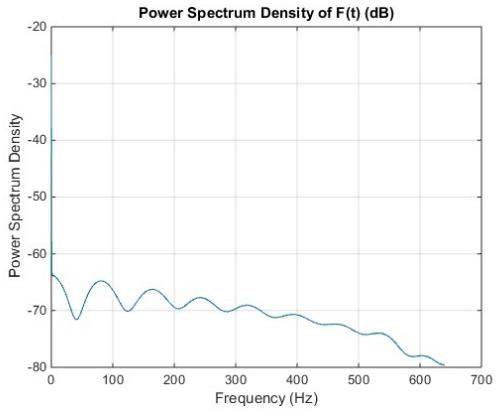


(c) Output ASD for base excitation using corrected data (FIXED)

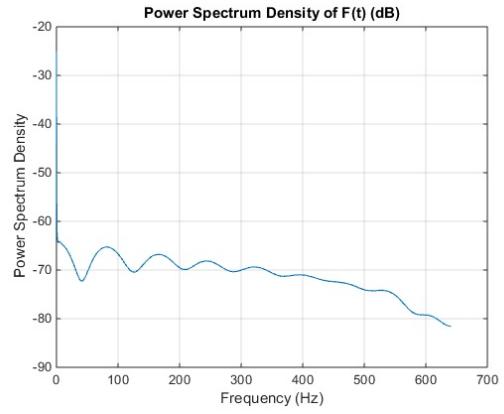


(d) Output ASD for base excitation using corrected data (LOOSE)

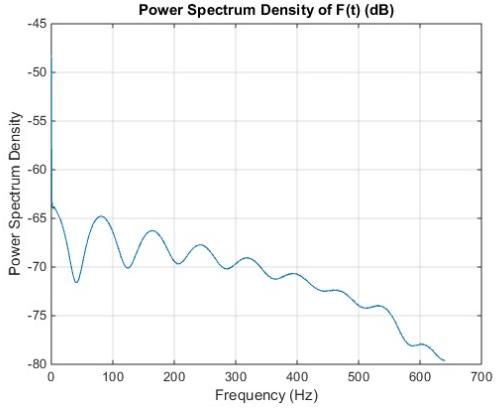
Figure 15: Output ASD plots for base excitation. Results shown for FIXED and LOOSE condition.



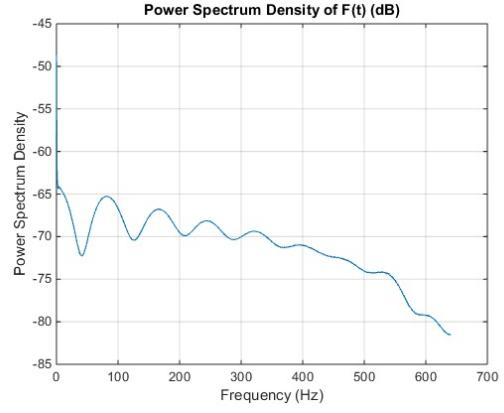
(a) Input ASD for LOC4 excitation using raw data (FIXED)



(b) Input ASD for LOC4 excitation using raw data (LOOSE)

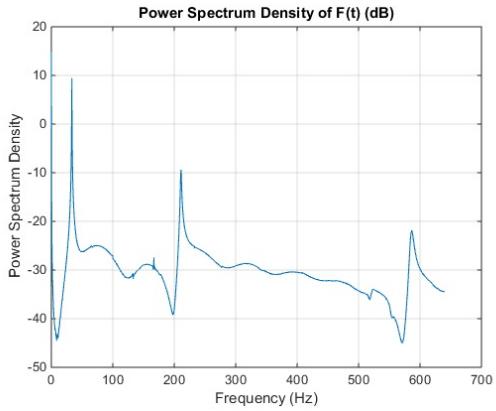


(c) Input ASD for LOC4 excitation using corrected data (FIXED)

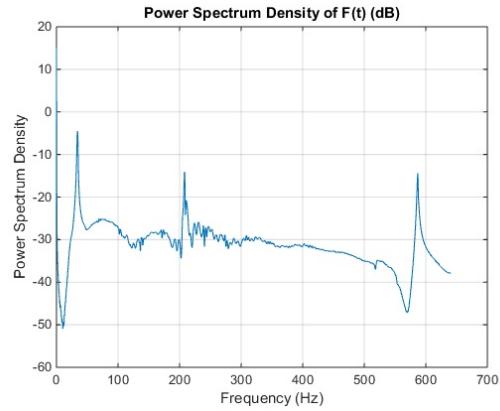


(d) Input ASD for LOC4 excitation using corrected data (LOOSE)

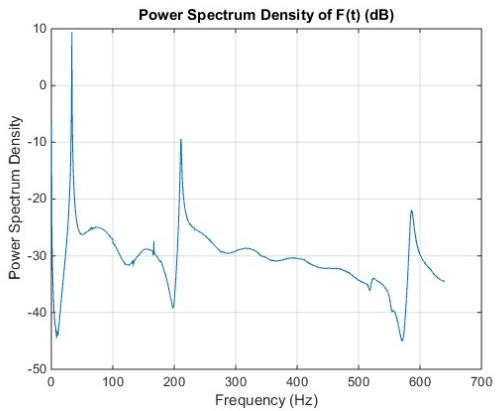
Figure 16: Input ASD plots for LOC4 excitation. Results shown for FIXED and LOOSE condition.



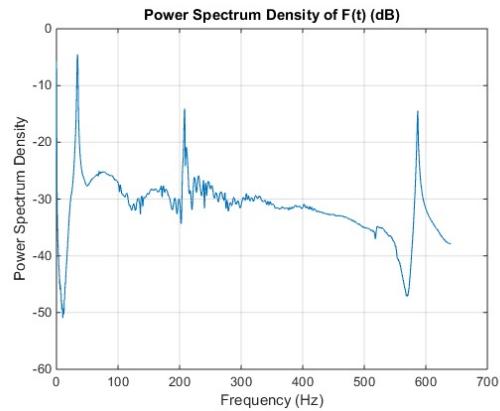
(a) Output ASD for LOC4 excitation using raw data (FIXED)



(b) Output ASD for LOC4 excitation using raw data (LOOSE)



(c) Output ASD for LOC4 excitation using corrected data (FIXED)



(d) Output ASD for LOC4 excitation using corrected data (LOOSE)

Figure 17: Output ASD plots for LOC4 excitation. Results shown for FIXED and LOOSE condition.