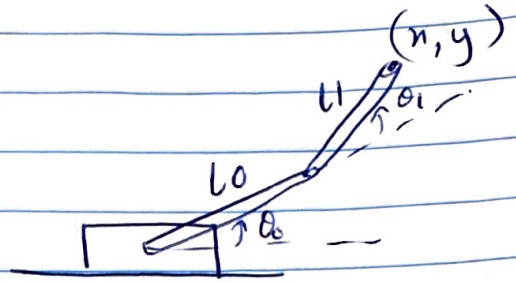


## Part 1

### A) Forward Model



$$l_0 = 0.1 \quad , \quad l_1 = 0.11$$

$$\begin{aligned} n &= l_0 \cos(\theta_0) + l_1 \cos(\theta_0 + \theta_1) \\ y &= l_0 \sin(\theta_0) + l_1 \sin(\theta_0 + \theta_1) \end{aligned} \quad \left. \vphantom{\begin{aligned} n &= l_0 \cos(\theta_0) + l_1 \cos(\theta_0 + \theta_1) \\ y &= l_0 \sin(\theta_0) + l_1 \sin(\theta_0 + \theta_1) \end{aligned}} \right\} \begin{array}{l} \text{End effector} \\ \text{position} \end{array}$$

### B) Jacobian Formula

~~$$J = \frac{\partial d(\theta)}{\partial \theta} = \begin{bmatrix} \frac{\partial n}{\partial \theta_0} & \frac{\partial n}{\partial \theta_1} \\ \frac{\partial y}{\partial \theta_0} & \frac{\partial y}{\partial \theta_1} \end{bmatrix}$$~~

$$J = \frac{\partial d(\theta)}{\partial \theta} = \begin{bmatrix} \frac{\partial n}{\partial \theta_0} & \frac{\partial n}{\partial \theta_1} \\ \frac{\partial y}{\partial \theta_0} & \frac{\partial y}{\partial \theta_1} \end{bmatrix}$$

$$J(\theta) = \begin{bmatrix} -l_0 \sin(\theta_0) - l_1 \sin(\theta_0 + \theta_1) & -l_1 \sin(\theta_0 + \theta_1) \\ l_0 \cos(\theta_0) + l_1 \cos(\theta_0 + \theta_1) & l_1 \cos(\theta_0 + \theta_1) \end{bmatrix}$$

c) Algorithm for Inverse

$$dx = J(\theta) d\theta$$

$$\Rightarrow \Delta x = J(\theta) \Delta \theta$$

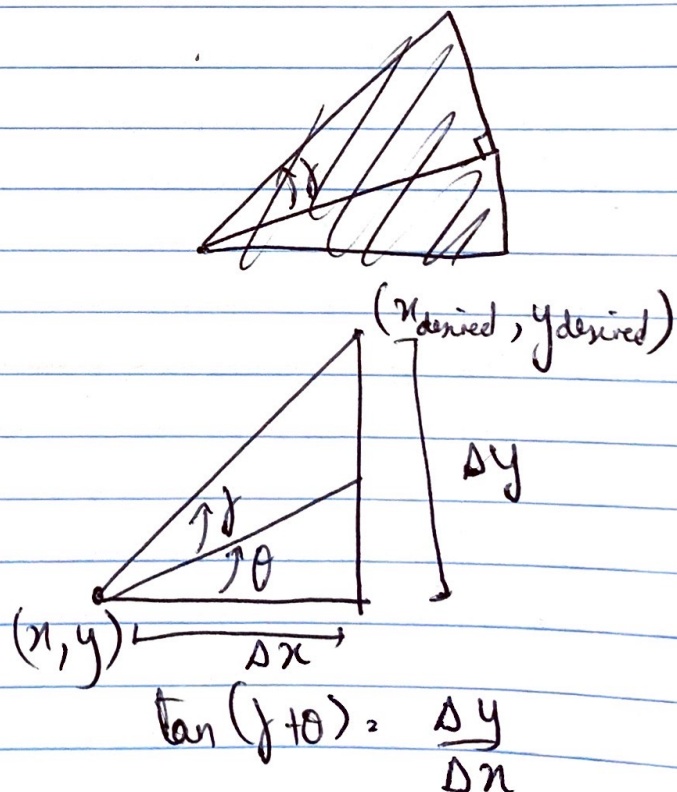
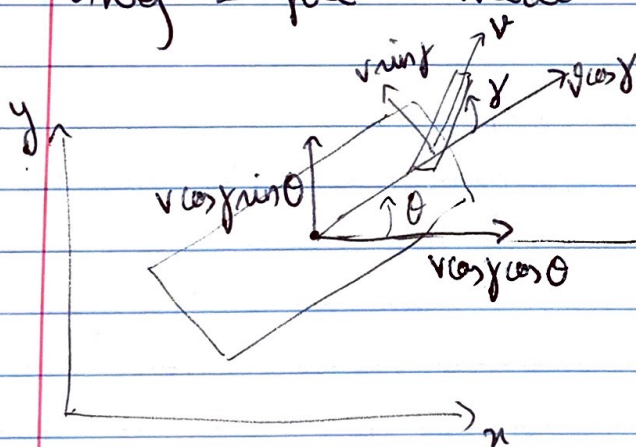
$$\Rightarrow \Delta \theta = J^{-1}(\theta) \Delta x$$

To avoid singularities with  $J^{-1}(\theta)$ , use pseudoinverse

$$\Rightarrow \Delta \theta = J^{\dagger}(\theta) \Delta x$$

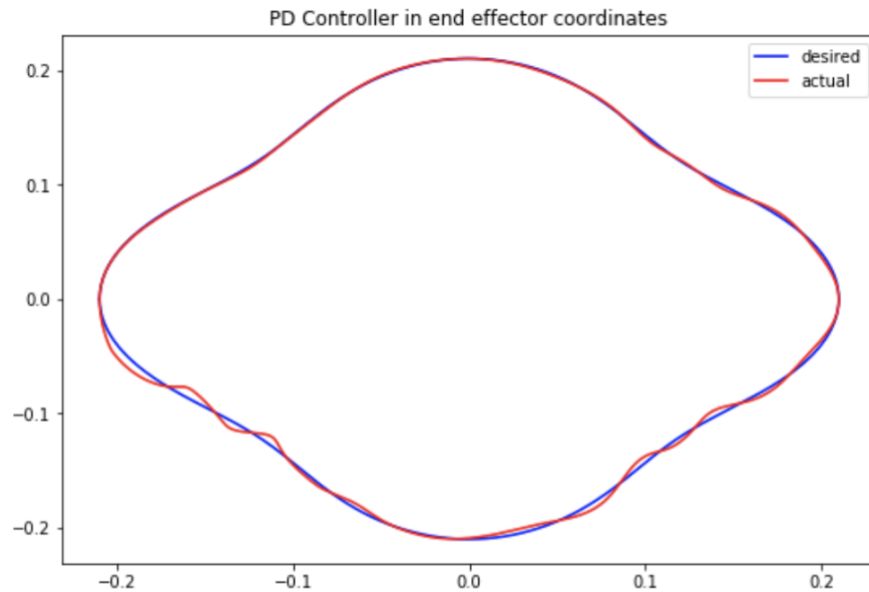
## PART 2

Using bicycle model:



## Part 1

**D)** Graph of actual and desired robot trajectory with using error in end effector as input

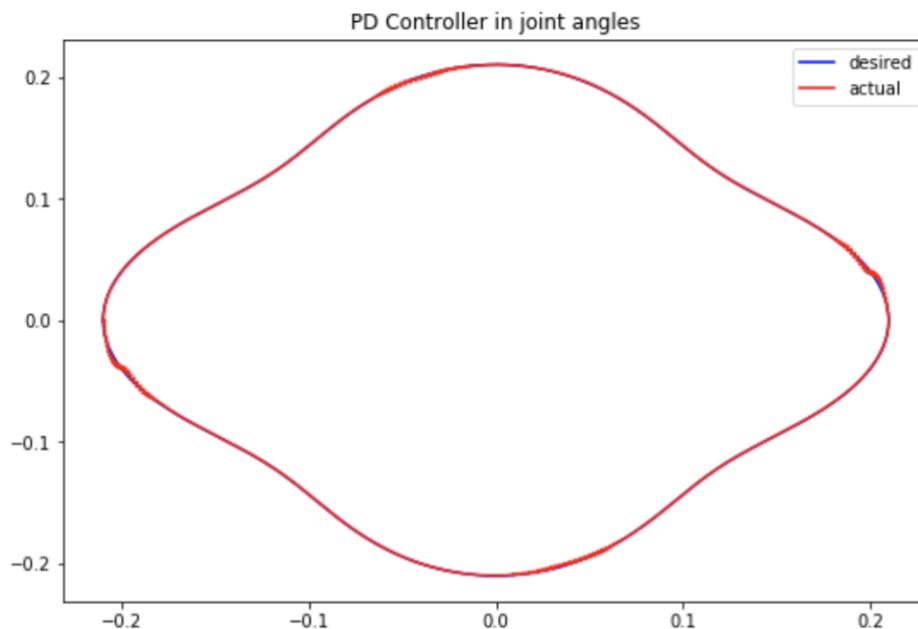


MSE =  $8.468949988734487e-06$   
Gains used -->  $K_p = 2.4$ ,  $K_d = 0.15$

**Gains used:**  $K_p = 2.4$ ,  $K_d = 0.15$

**MSE:**  $8.47 \times 10^{-6}$

**E)** Graph of actual and desired robot trajectory with using error in joint angles as input



MSE =  $4.29363859003678e-06$   
Gains used -->  $K_p = 8.0$ ,  $K_d = 0.18$

**Gains used:**  $K_p = 8.0$ ,  $K_d = 0.18$

**MSE:**  $4.29 \times 10^{-6}$

## Part 2

### A) Controller

A PD controller similar to part 1 was used to control the thrust. No controller was used to control the wheel angle given by  $\gamma$ . That is calculated definitively and fed in as an input.

$Thrust = [K_p \times \sqrt{(\Delta x^2 + \Delta y^2)}] + [K_d \times (v_{desired} - v_{current})]$ , where

$$v_{current} = \sqrt{(v_x^2 + v_y^2)} \quad v_{desired} = \sqrt{\frac{(\Delta x^2 + \Delta y^2)}{\cos^2 \gamma}} \quad \gamma = \tan^{-1}\left(\frac{\Delta y}{\Delta x}\right) - \theta$$

$$\Delta y = y_{desired} - y_{current} \quad \Delta x = x_{desired} - x_{current}$$

$K_p = \text{Proportional gain}$ ,  $K_d = \text{Differential gain}$

$x_{desired}$ ,  $y_{desired}$ ,  $x_{current}$ ,  $y_{current}$ ,  $v_x$ ,  $v_y$ ,  $\theta$  are read from the observation.

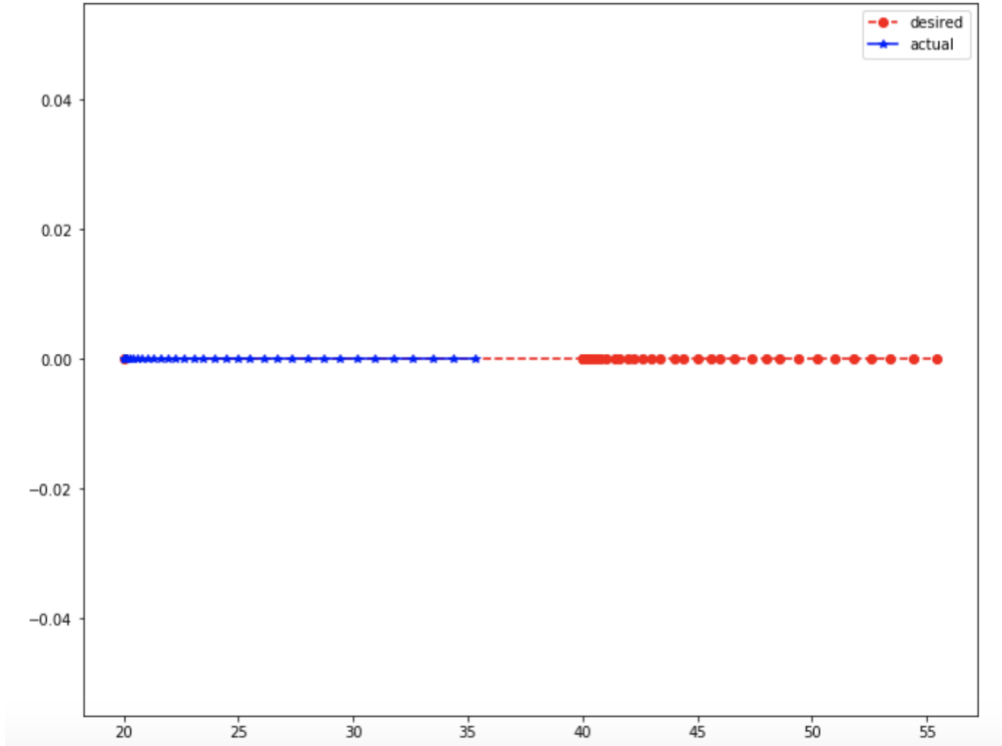
### B) Results

For gain of  $K_p = 1.05$ ,  $K_d = 0.33$ , the plots are:

#### 1) Linear Track

Steps taken = 34

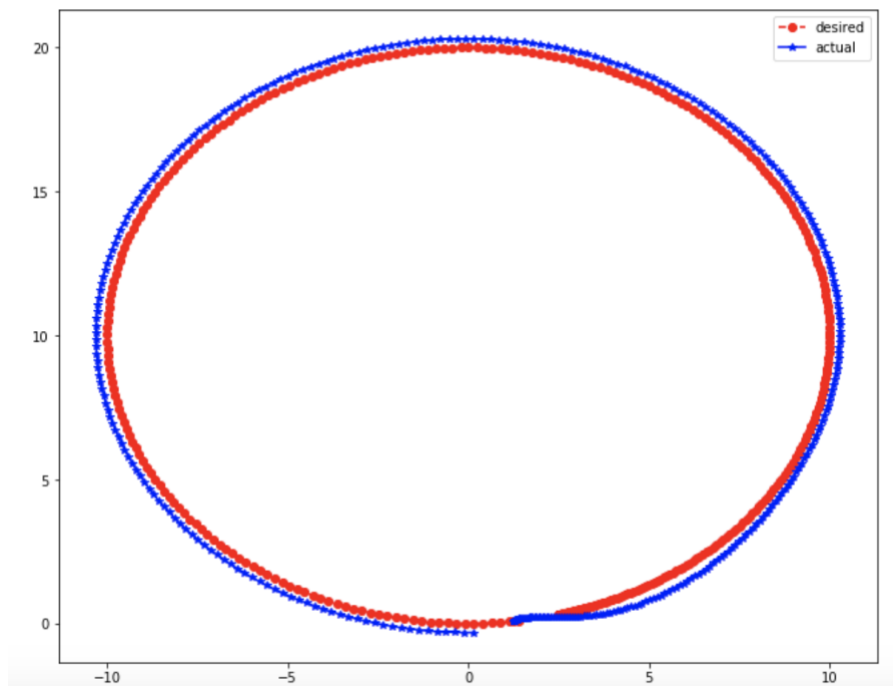
MSE between actual and desired trajectories = 388.36986321483533



## 2) Circle Track

Steps taken = 342

MSE between actual and desired trajectories = 1.7063010753262253

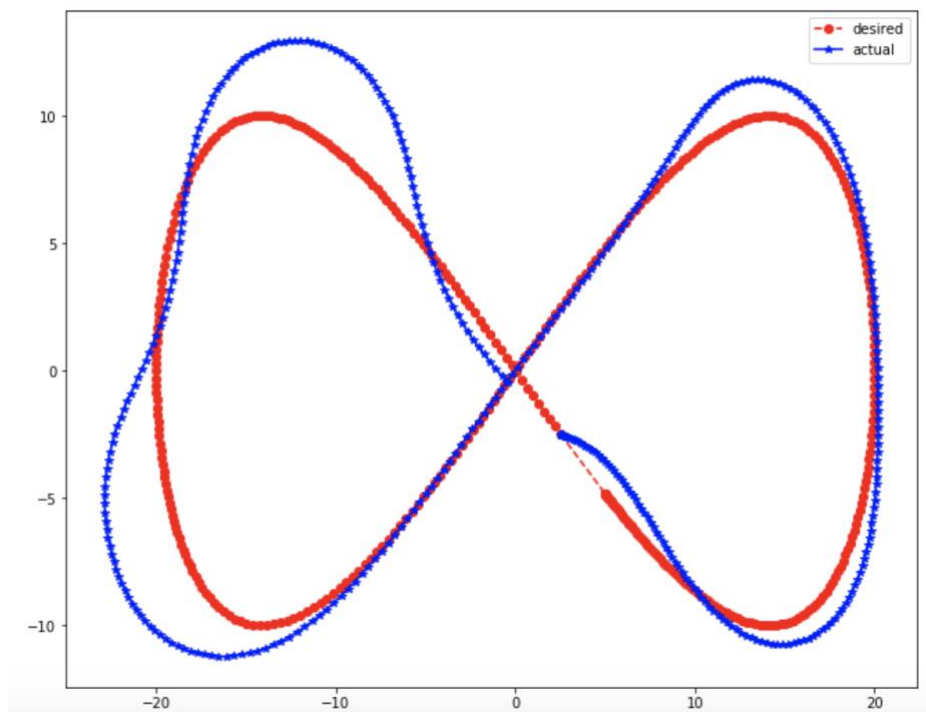


Steps taken = 342, MSE = 1.70

## 3) FigureEight Track

Steps taken = 403

MSE between actual and desired trajectories = 9.361375979211653



Steps taken = 403, MSE = 9.36

Although the controller is able to make the car stay almost on track, the error can be completely eliminated by using an integral controller too. This is reserved for future work.