

# Info-gap robustness assessment of reliability evaluations using several OpenTURNS features

## OpenTURNS User's Day

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# Scientific context

## ■ Uncertainty framework

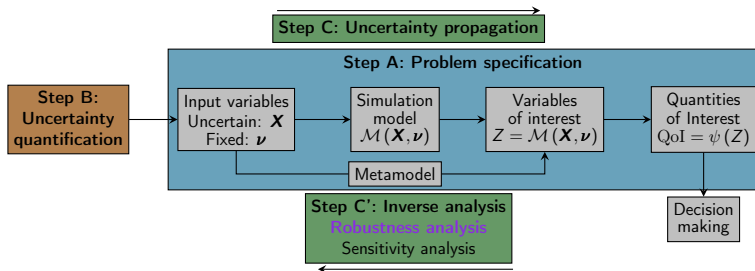


Figure 1: General uncertainty quantification and propagation framework.

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- 2 Hybrid reliability analysis
- 3 Industrial application
- 4 Robustness of the reliability assessment of penstocks
- 5 Conclusion

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# Info-gap applied to reliability analysis

## ■ Robustness curves (Ben-Haïm, 2006):

decision 1

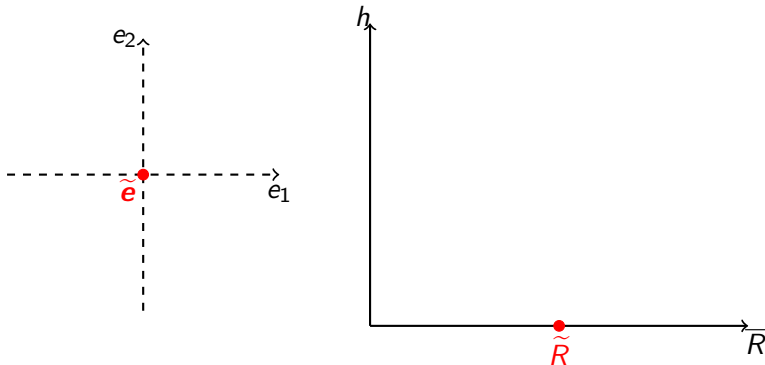


Figure 2: Nested convex sets with robustness curves.

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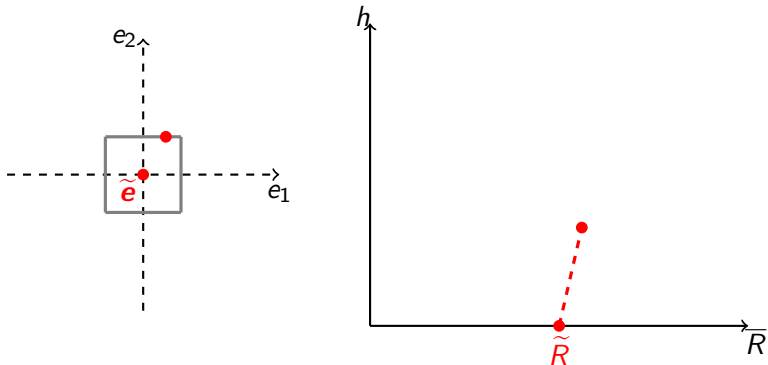


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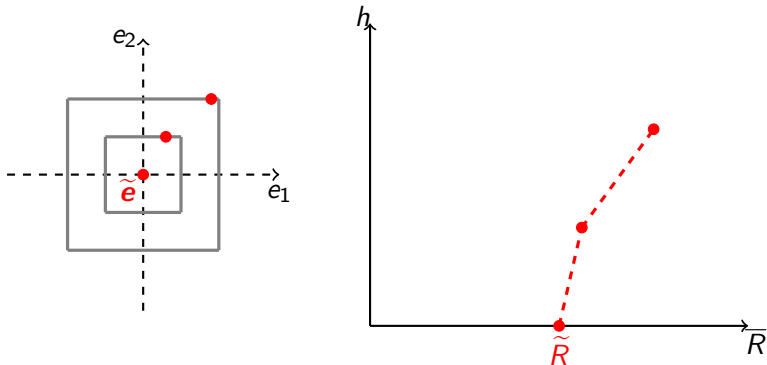


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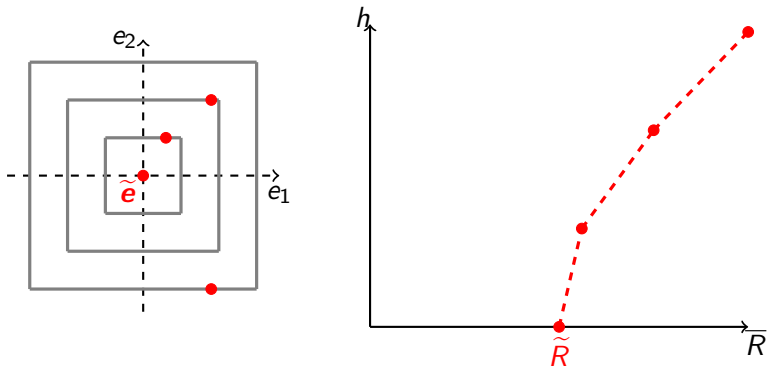


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# Info-gap applied to reliability analysis

■ Robustness curves (*Ben-Haïm, 2006*):

decision 1 vs decision 2

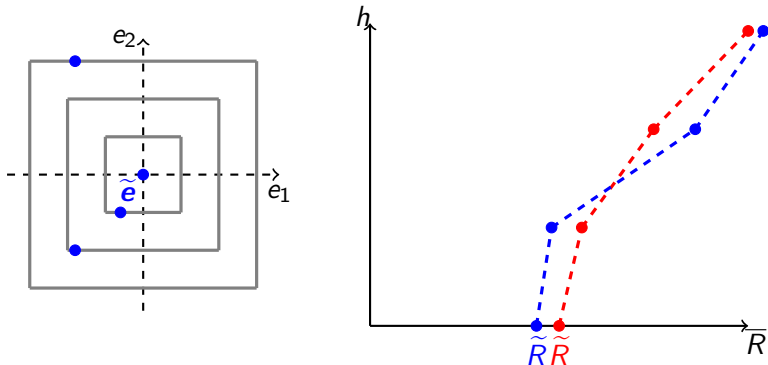


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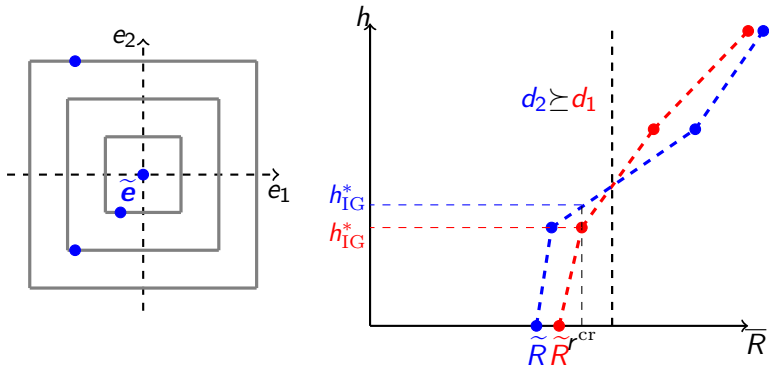


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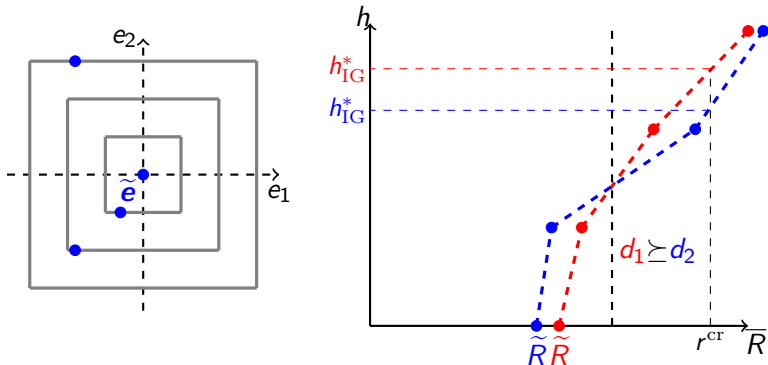


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# Info-gap applied to reliability analysis

## ■ Robustness of reliability evaluations

$$h_{IG}^* = \max_h \left\{ \max_{\mathbf{e} \in U(h, \tilde{\mathbf{e}})} \text{QoI}(\mathbf{d}, \mathbf{e}) \leq \text{QoI}^{cr} \right\} \quad (1)$$

- ▶ QoI: (small) failure probability, (high-order) quantile, superquantile ...
- ▶  $\mathbf{e}$ : input variables, hyperparameters of a probability distribution, model errors, ...

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**Q1** How to apply IG uncertainty models to the reliability framework?

# Info-gap applied to reliability analysis

## ■ Robustness of reliability evaluations

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- ▶ QoI: (small) failure probability, (high-order) quantile, superquantile ...
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**Q2** How to propagate hybrid uncertainty (aleatory and epistemic) in order to estimate the bounds of the QoI?

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## ■ Robustness of reliability evaluations

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- ▶ QoI: (small) failure probability, (high-order) quantile, superquantile ...
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**Q3** How to efficiently reduce the computational burden induced by both the QoI estimator and the IG formulation?

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## 2 – Hybrid reliability analysis

### ■ Failure probability estimation under aleatory uncertainty

$$P_f = \Pr [g(\mathbf{X}) \leq 0] = \int_{g(\mathbf{x}) \leq 0} f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} = \int_{\mathbb{R}^{n_{\mathbf{X}}}} 1_{g(\mathbf{x}) \leq 0} f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} \quad (2)$$

### ■ Failure probability estimation under hybrid uncertainty

$$P_f = \Pr [g(\mathbf{X}, \mathbf{Y}) \leq 0] \quad (3)$$

- ▷ Random vector  $\mathbf{X} \sim f_{\mathbf{X}}$
- ▷ Epistemic vector  $\mathbf{Y}$ : intervals, convex sets, possibility distribution, Dempster-Shafer structures, p-boxes, probability distribution ...
- ▷ Only the bounds  $\left[ \underline{P}_f, \overline{P}_f \right]$  of the failure probability can be estimated
- ▷ Need for a common framework for estimating and comparing these bounds





## 2 – Hybrid reliability analysis

### ■ Random sets as a unifying framework (*Alvarez, 2006*)

- ▷ With  $\Omega = [0, 1]^{n_X + n_Y}$  and  $\alpha_{Y_i} \sim U(0, 1)$ , one retrieves several uncertainty representations:

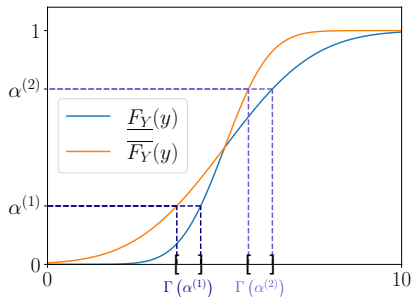


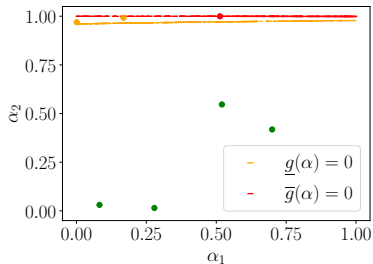
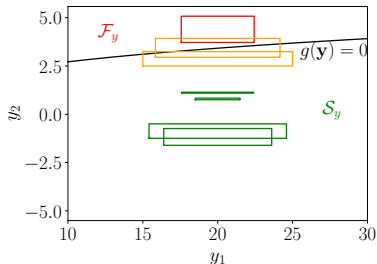
Figure 5: Random set with a p-box.

## 2 – Hybrid reliability analysis

### ■ Random sets in the reliability framework (*Alvarez et al., 2018*)

$$\overline{P}_f = \Pr \left[ \min_{\Gamma(\alpha)} g(\alpha) \leq 0 \right] = \int_{\Omega} \mathbb{1}_{\underline{g}(\alpha) \leq 0} d\alpha \quad (5a)$$

$$\underline{P}_f = \Pr \left[ \max_{\Gamma(\alpha)} g(\alpha) \leq 0 \right] = \int_{\Omega} \mathbb{1}_{\overline{g}(\alpha) \leq 0} d\alpha \quad (5b)$$



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### 3 – Reliability of penstocks



Figure 6: Example of a penstock operated by EDF.

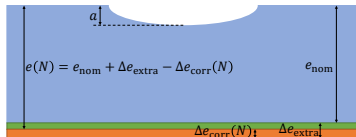


Figure 7: illustration of a penstock presenting a planar flaw of height  $a$ .

## 3 – Reliability of penstocks

### ■ Main characteristics (*Ardillon et al., 2022*)

- ▷ **Failure mode** (*Step A*): brittle failure affecting welds due to corrosion and the presence of a default
- ▷ **Simulation model** (*Step A*): analytical expressions → fast to compute
- ▷ **QoI** (*Steps A and C*): small failure probability

$$P_f = \Pr(\{G_{N+1}(\mathbf{X}, \mathbf{Y}) \leq 0\} \cap \{G_N(\mathbf{X}, \mathbf{Y}) > 0\} \cap \{G_{\text{HPT}}(\mathbf{X}, \mathbf{Y}) > 0\}) \quad (6)$$

- ▷ **Uncertain inputs dimension** (*Step A*):  $n_X + n_Y = 6$
- ▷ **IG motivation** (*Step C'*): are there some nominal configurations of penstocks more robust than others?
- ▷ **Challenge** (*Step C*): complexity of the failure domain and of the failure probability estimation



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## 4 – Robustness of the reliability assessment of penstocks

### ■ IG uncertainty model (Step B)

Variable $X_i$	Distribution	Param. 1	Param. 2	Param. 3
$X_1 = R_m$ (MPa)	Lognormal	480	24	-
$X_2 = \varepsilon$ (MPa)	Normal	0	16.816	-
$Y_1 = \Delta e_{\text{extra}}$ (mm)	Normal	$\theta_1$	0.25	-
$Y_2 = \Delta e_{\text{corr}}$ (mm) (mm)	Normal	$\theta_2$	0.4	-
$Y_3 = a$ (mm)	Uniform	0	$\theta_3$	-
$Y_4 = K_{IC}$ (MPa. $\sqrt{\text{m}}$ )	Weibull Min	$\theta_4$	4	20

Table 1: Input probabilistic modeling of  $\mathbf{X}$  for the penstock use-case.

- ▶ Parametric p-box uncertainty model

$$D_{\theta} \left( h, \tilde{\theta} \right) = \bigotimes_{i=1}^4 l_{\theta_i}(h) \text{ with } \begin{cases} l_{\theta_i}(h) = \left[ \tilde{\theta}_i (1 - h), \tilde{\theta}_i (1 + h) \right] & \text{if } \tilde{\theta}_i > 0 \\ l_{\theta_i}(h) = [-h, h] & \text{if } \tilde{\theta}_i = 0 \end{cases} \quad (7)$$

- ▶ Robustness function

$$h_{IG}^* = \max_h \left\{ \max_{\theta \in D_{\theta}(h, \tilde{\theta})} P_f(\theta) \leq P_f^{\text{cr}} \right\} \quad (8)$$

## 4 – Robustness of the reliability assessment of penstocks

### ■ Failure probability estimator (*Step C*)

- ▷ **FISSTAR**: FORM-IS-Tested Automatically-Rapid seaRch: current algorithm used for the failure probability estimations
- ▷ **Line sampling**: directional technique investigated in order to better target the restricted failure domain

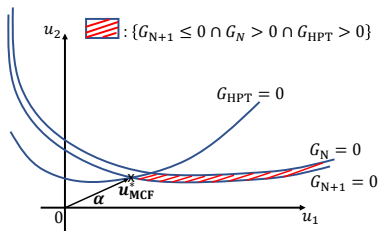


Figure 8: Illustration of the failure domain for the reliability of penstocks.

## 4 – Robustness of the reliability assessment of penstocks

### ■ “Standard” Line Sampling (*Koutsourelakis, 2004*)

$$\triangleright \mathbf{u} = u^{\parallel} \boldsymbol{\alpha} + \mathbf{u}^{\perp}$$

$$\begin{aligned} P_f &= \mathbb{E}_{\varphi_{\mathbf{u}^{\perp}}} \left[ \int_{G(u^{\parallel} \boldsymbol{\alpha} + \mathbf{u}^{\perp}) \leq 0} \varphi(u^{\parallel}) du^{\parallel} \right] \\ &= \mathbb{E}_{\varphi_{\mathbf{u}^{\perp}}} \left[ \Phi \left( -r(\mathbf{u}^{\perp}) \right) \right] \end{aligned} \quad (9)$$

▷ LS estimator:

$$\mathbf{u}^{\perp, (i)} = \mathbf{u}^{(i)} - (\mathbf{u}^{(i)} \boldsymbol{\alpha}) \boldsymbol{\alpha}^{\top}$$

$$\begin{aligned} \hat{P}_f &= \frac{1}{n_{\text{LS}}} \sum_{i=1}^{n_{\text{LS}}} \Phi \left( -r(\mathbf{u}^{\perp, (i)}) \right) \\ &= \frac{1}{n_{\text{LS}}} \sum_{i=1}^{n_{\text{LS}}} p_f^{(i)} \end{aligned} \quad (10)$$

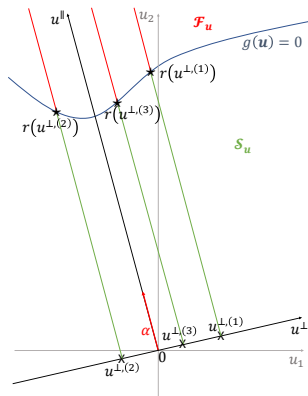


Figure 9: LS illustration.



## 4 – Robustness of the reliability assessment of penstocks

### ■ Adapted LS algorithms for each formulation $E_i$

$$\triangleright E_3 = \{G_{N+1} \leq 0 \cap G_N > 0 \cap G_{\text{HPT}} > 0\}$$

$A_{E_3}$
Find $r_1$ s.t. $G_{N+1}^\perp(r_1) = 0$
If $G_{\text{HPT}}^\perp(r_1) > 0$ then
Find $r_2$ s.t. $G_N^\perp(r_2) = 0$
If $G_{\text{HPT}}^\perp(r_2) < 0$ then
Find $r_2$ s.t. $G_{\text{HPT}}^\perp(r_2) = 0$
Else:
no roots

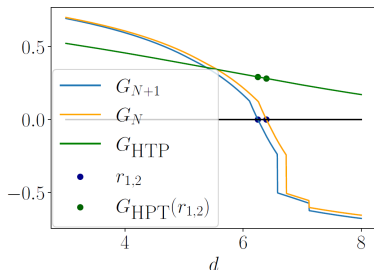


Figure 11: Roots search on  $E_3$

## 4 – Robustness of the reliability assessment of penstocks

### ■ Application of the methodology for the robustness evaluation (*Step C'*)

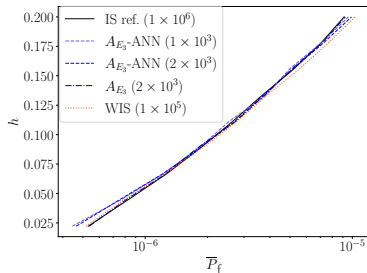


Figure 12: Comparison of robustness curves.

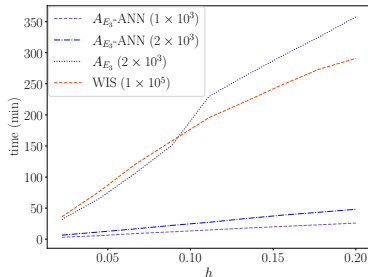


Figure 13: Comparison of the cumulative time needed for the robustness assessment.

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# Conclusion : thank you OpenTURN

- **Data analysis**

- ...

- **Probabilistic modeling**

- Standard parametric models
  - Copulas
  - Convex sets, possibility distributions, DS structures, p-boxes, random sets

- **Meta modeling**

- Artificial neural networks (Keras)

- **Reliability, sensitivity**

- MC, FORM, IS, SS
  - Line Sampling

- **Numerical methods**

- Uniform Random Generator
  - Distribution realizations + random set realizations
  - Optimization Algorithms : NLOpt (DIRECT) + root search (scipy)
  - Isoprobabilistic transformation

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