# **Basics of Electrical and Electronic Circuits**

## **Experiment 7**

Voltage amplifiers using Op-Amp

Spring 2025

An ideal voltage amplifier is a VCVS, generating an output voltage with a waveform which is a magnified replica of the input voltage waveform, irrespective of the current that the amplifier has to supply to any load connected to its output. All amplifiers are necessarily linear and time-invariant, and are studied in terms of their sinusoidal steady state behavior using phasor equivalents. Let the input and output voltages of an amplifier be denoted by

 $V_1 = V_{1m} \sin(\omega t)$  and  $V_2 = V_{2m} \sin(\omega t + \theta)$ . Then the phasors are given by  $V_1 = V_{1m}$  and  $V_2 = V_{2m} \angle \theta$  and the voltage gain is given by  $A_V = V_2 / V_1 = A_{Vm} \angle \theta$ , where  $A_{vm} = V_{2m} / V_{1m}$  denotes the magnitude of the voltage gain.

The most important property that characterizes a voltage amplifier is its frequency response, given by the graph of  $G_{\nu}$  vs **frequency** on a logarithmic scale, where  $G_{\nu} = 20 \log_{10} A_{\nu m}$ .

Any practical voltage amplifier will behave like an ideal one only as long as the voltage and current at the

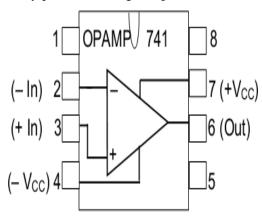


Fig. 1 Pin Connection of OPAMP 741

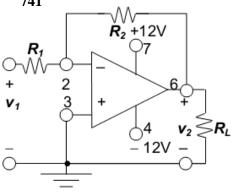


Fig. 2 Inverting Amplifier

output and the frequency are within prescribed limits. We will examine these limits for two amplifier circuits using an Operational amplifier (OPAMP): The Inverting Amplifier for the **limits on the output voltage and current**, and the Noninverting Amplifier for the **limit on frequency**.

An OPAMP is an integrated circuit (IC) consisting of number of transistors and resistors inside the chip. The opamp we will use in this course is the extremely popular 741, which has the pin connection given in **Fig. 1**. (– In) and (+In) are two input terminals, (Out) is the output terminal and (+VCC) and ( – VCC) indicate two power supply terminals where **equal and opposite d-c** voltages have to be connected to the opamp for its normal operation. The exact values of these voltages are flexible, but they must be equal in magnitude (range 6-15V) and opposite in sign.

## A. **Inverting Amplifier**

The circuit of an Inverting Amplifier is shown in **Fig. 2**. If the opamp can be considered to be ideal, i.e. it has no limitations with regard to voltage, current or frequency, the voltage gain of this amplifier is given by

$$A_v = -R_2/R_1$$

We will study in this experiment the limitations imposed on the output voltage by the d-c power supply voltages used by the opamp as well as the limitations imposed on the output current by virtue of the protection feature incorporated in the opamp by design.

**1.** Build the circuit of Fig. 2 on bread board. Use general purpose OPAMP IC-741.

- 2. Set up the Inverting Amplifier with  $R_I = 1.00 \text{k}\Omega$ ,  $R_2 = 10.0 \text{k}\Omega$  and  $R_L = 1.80 \text{k}\Omega$ . Apply the input voltage  $v_I$  from the voltage source and set it at 1kHz sinusoidal voltage with peak-to-peak value 0.2V. Display the input and output voltage waveforms on the DSO and measure the **peak-to-peak** voltages. Measure the output voltage  $v_2$  for  $R_2$ . Note that  $v_2$  is opposite in phase with respect to input  $v_I$
- 3. Repeat step 2 for  $R_2 = 82.0 \text{k}\Omega$ . Justify the use of direct measurement based on your observations. Tabulate the magnitude of the voltage gain against the theoretically expected value of Av for the given values of  $R_2$ . This establishes that the Inverting Amplifier behaves like a VCVS with a constant voltage gain for a fairly wide range of load resistances.

#### **Observation Table 1**

$R_2$	$v_{I}$	$v_2$	$A_{V}$	Theoretical $A_v = -R_2/R_{I.}$
10.0kΩ				
82.0kΩ				

- **4.** Keeping  $R_2 = 82.0 \text{k}\Omega$ , increase amplitude of  $v_I$  until the waveform of v becomes flat both at the top and at the bottom. These flat levels correspond to the output **voltage saturation levels**  $V_{O+}$  and  $V_{O-}$  of the OpAmp for the d-c power supply voltages used. Find  $V_{O+}$  and  $V_{O-}$  by using direct measurement of the **Max** and **Min** levels and verify that increase in  $v_I$  widens the flat levels, but not their values.
- 5. Set  $v_I$  back to 0.2V peak to peak, keeping  $R_2 = 82.0 k\Omega$ , and observe the waveform of  $v_2$  with  $R_L = 330\Omega$ ,  $220\Omega$  and  $100\Omega$ . Note the flattening of the waveform both at the top and at the bottom, and measure the values of these two levels for each  $R_L$ , using direct measurement of the **Max** and **Min** levels. Note that these levels are NOT the same as the voltage saturation levels  $V_{O_+}$  and  $V_{O_-}$ , but are given by  $R_L I_{O_+}$  and  $R_L I_{O_-}$ , where  $I_{O_+}$  and  $I_{O_-}$  are the **current limits imposed by design** for positive and negative values of  $v_O$  respectively. Calculate the values of  $I_{O_+}$  and  $I_{O_-}$  for each value of  $R_L$ .

## **B.** Non-inverting Amplifier

In this experiment, we will study the **frequency limitation** on OpAmp-based circuits by measuring the Frequency Response of the Non-inverting Amplifier, another popular voltage amplifier using OpAmp.

- 1. Set up the Non-inverting Amplifier shown in Fig. 3(a), with  $R_I = 2.00 \text{k}\Omega$  and set the voltage source at 100 Hz sinusoidal voltage with peak-to-peak value 0.2V. Display the input and output voltage waveforms on the waveform viewer and measure the **peak-to-peak** voltages.
- **2.** With  $R_2 = 18.0 \text{k}\Omega$ , measure  $v_2$  for frequencies in the 1-2-5 sequence: f = 0.1, 0.2, 0.5, 1, 2, 5, 10, 20, 50, 100, 200 and 500 kHz, maintaining the peak-to-peak value of  $v_I$  at 0.2V.

### **Observation Table 2**

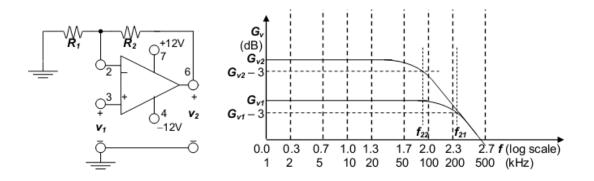
Observation Table 2					
Frequency	$v_1$	$v_2$	$A_{vm} = V_{2m} / V_{1m}$	$G_{v}=20\log_{10}A_{vm}$	Theoretical
					$A_{vm}=1+R_2/R_1.$
	0.2				
	0.2				

**3.** Repeat step **B.2** with  $R_2 = 56.0 \text{k}\Omega$ 

#### Observation Table 3

Frequency	$v_1$	$v_2$	$A_{vm} = V_{2m} / V_{Im}$	$G_v = 20 \log_{10} A_{vm}$	Theoretical
		-	, <u>2</u>		$A_{vm} = 1 + R_2 / R_1.$
	0.2				
	0.2				

- **4.** Calculate and plot the dB gain Gv against f for all values of  $R_2$  on the **same scale** by choosing the log scale.
- 5. Note the low-pass nature of the frequency response and determine the values of  $G_{vI}$  and  $G_{v2}$  from the flat regions of the graphs corresponding to  $R_2 = 18.0 \text{k}\Omega$ , and  $56.0 \text{k}\Omega$  respectively. Compare these values with the values expected from the theoretical expression  $A_{vm} = 1 + R_2 / R_I$ .



(a) Circuit Diagram (b) Frequency Response (for two cases)

Fig.3 Non-inverting Amplifier

## C. Integrator Circuit

The ideal circuit of an integrator is shown in figure 4.1, assuming the opamp to be ideal.

$$i = v_1/R_1, v_2 = -(\int idt)/C = -(\int v_1 dt)/(CR_1)$$

Thus, the output voltage v2 is proportional to the integral of the input voltage v1 with a constant of proportionality given by the input voltage v1 with a constant of proportionality given by the values of circuit elements.

If 
$$v_1=V_{1m} \sin \omega t$$
,  $v_2=V_{2m} \sin \omega t$ , where  $V_{2m}=V_{1m}/(\omega CR_1)$ 

implying that a sinusoidal input gives a sinusoidal output with a voltage  $Gain = 1/(\omega CR_1)$ , and a phase shift of 90 degree.

A more interesting way of checking the operation of an integrator is to use a symmetrical square wave input, which results in an output voltage having a triangular waveform, as shown in **figure 4.2**. This is easy to show by taking the areas under the different segments of the square wave that

$$V_{2p} = V_{1p} T / (4CR_1)$$

Unfortunately, this circuit will never work in practice, because any non-zero average (DC) value of v1, as well as the very small but nonzero current flowing into the opamp input terminals will lead to a continuous change in the

output voltage, eventually forcing the opamp to go into voltage saturation. So practical integrators include a second resistor in parallel with the capacitor s shown in **figure 4.3**.

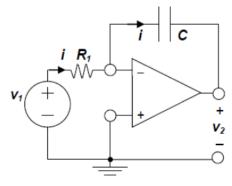


Fig. 4.1 Ideal Integrator

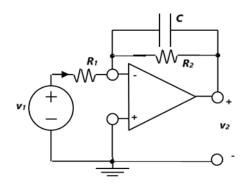


Fig. 4.3 Practical Integrator

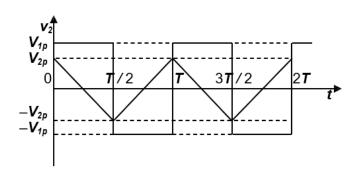


Fig. 4.2 Ideal Integrator Waveforms

- 1. Set up the practical integrator shown in Fig. 4.3,with  $R_1 = 2.00 \text{k}\Omega$ ,  $R_2 = 200 \text{k}\Omega$  and  $C = 0.01 \mu\text{F}$ . Follow the standard opamp pin connection for assembling the circuit, including the connections to the d-c power supply (not shown here).
- 2. Apply a 2kHz square wave input voltage v<sub>1</sub> with peak-to-peak value 0.8V from the Wavegen. Observe the waveforms of v<sub>1</sub> and v<sub>2</sub> on the DSO, triggering the DSO by the Wavegen output. Adjust the vertical scales of CH-1 and CH-2 so that the peak-to-peak swings of v<sub>1</sub> and v<sub>2</sub> as seen on the DSO are exactly equal. Find the value of V<sub>2p</sub> / V<sub>1p</sub> by taking the ratio of the scales of CH-2 and CH-1.
- 3. Compare the measured value of  $V_{2p} / V_{1p}$  with its theoretically expected value  $T / (4R_1C)$ .
- **4.** Change  $v_1$  to a sine wave with all other settings of the Wavegen as before. Note the phase difference between the two waveforms and measure the ratio  $v_{2m} / v_{1m}$  of their peak-to-peak values as done in step **A.1** above. Compare the measured value with the theoretically expected value  $v_{2m} / v_{1m} = 1/(\omega CR_1)$  as given above for sinusoidal voltages.

#### **Observation Table 4**

Wave shape	$v_{1p} Or v_{1m}$	$v_{2p} Or v_{2m}$	$v_{2p}/v_{1p}$ Or $v_{2m}/v_{1m}$	Theoretical T/ (4CR <sub>1</sub> ) or 1/ ( $\omega$ CR <sub>1</sub> )
Square				
Sine				

#### **Results:**

**Conclusion**: It must be in your words and be based on your understanding/learning in the experiment.