

Assignment - 2 Solution
Flight Mechanics AE 321A

Question - 1

Solution

Given data -

A Jet airplane

$$W = 20000 \text{ N}$$

$$W/S = 1000 \text{ N/m}^2$$

$$T_0 = 2000 \text{ N} @ \text{sea level}$$

$$T = T_0 \sigma^{0.8} @ \text{an altitude}$$

$$C_D = 0.015$$

$$K = 0.024$$

$$G_{\max} = 1.4$$

Absolute and service ceiling problems can be solved graphically.

Steps to plot the absolute and service ceiling properties

① Calculate $\sigma @ \text{altitude } h$

② Calculate $S = S_0 \cdot \sigma$

③ Calculate $T = T_0 \sigma^{0.8}$

④ Calculate $V = \sqrt{\frac{1}{3S C_D}} \cdot \sqrt{T + \sqrt{T^2 + 12k G_0 W^2}}$

$$⑤ C_L = \frac{2W}{\rho S V^2}$$

$$⑥ T_R = \frac{1}{2} \rho S V^2 (C_0 + k C_L^2)$$

$$⑦ R/C_{max} = \frac{(T - T_R) \cdot V}{W}$$

Plot h vs R/C_{max} , V vs R/C_{max} and C_L vs R/C_{max} to find out required quantities.

From the plots -

(a)

Absolute ceiling ≈ 10.95 km

Velocity at absolute ceiling ≈ 83.2592 m/s

Lift coefficient at absolute ceiling ≈ 0.79

(b)

Service ceiling ≈ 9.35 km

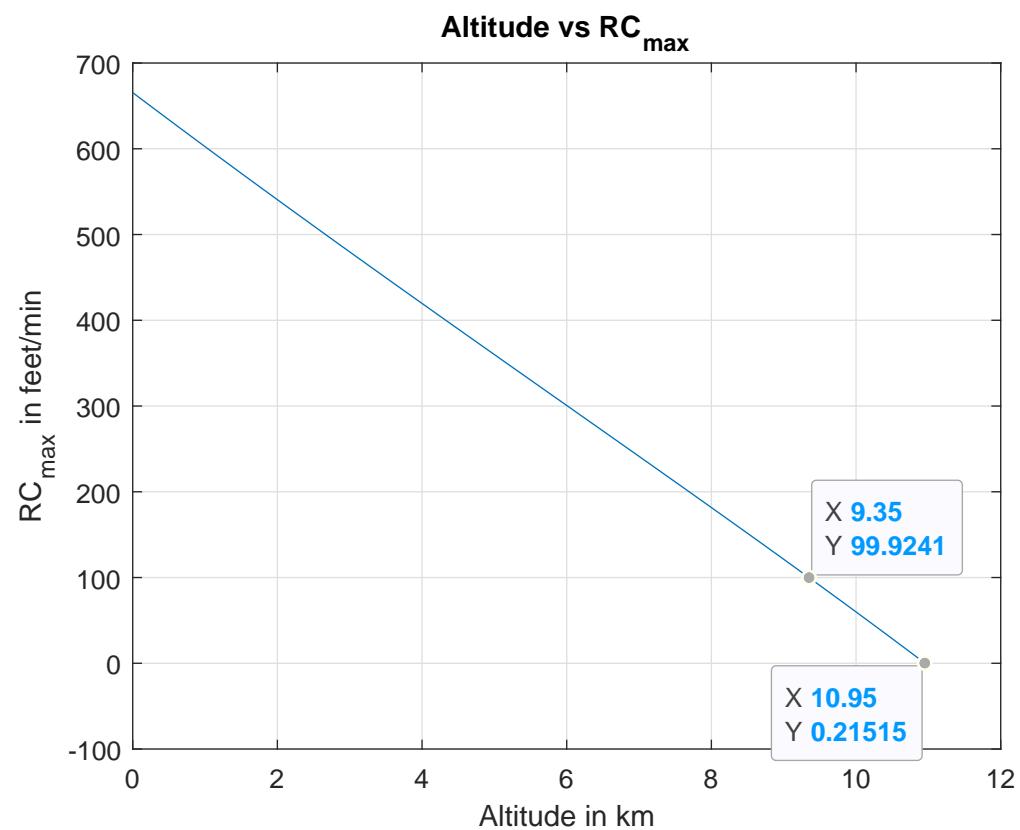
Velocity at service ceiling ≈ 78.63 m/s

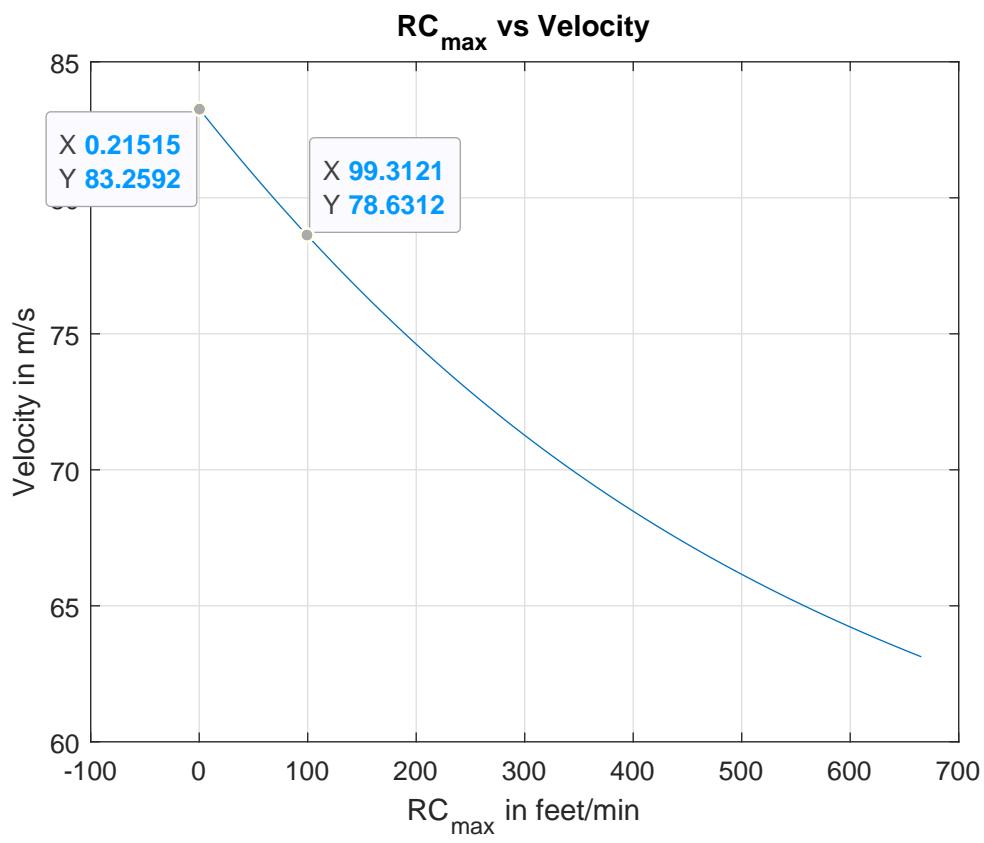
Lift coefficient at service ceiling ≈ 0.726

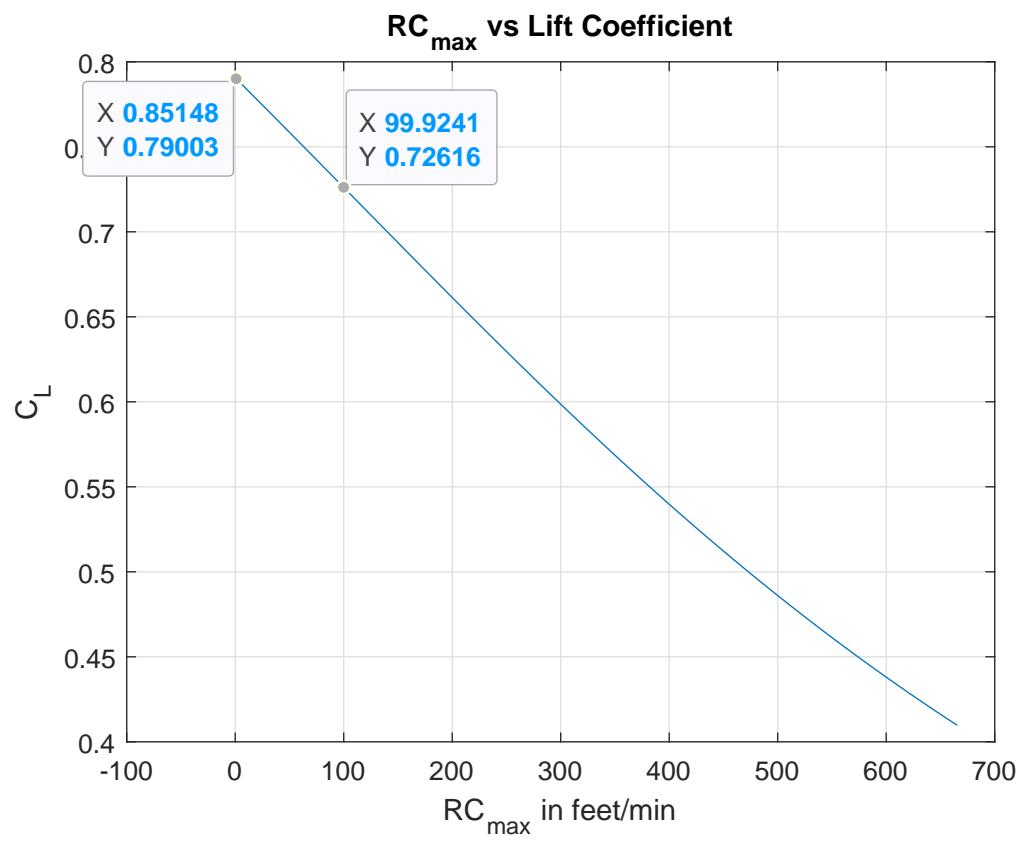
Accepted answers -

(a) $h_{abs} \in [10.40, 11.5]$ km, $V \in [79.1, 87.4]$ m/s
 $C_L \in [0.75, 0.83]$

(b) $h_{service} \in [8.9, 9.8]$ km, $V \in [74.7, 82.6]$ m/s
 $C_L \in [0.69, 0.76]$







Question - 2Solution

Given data -

A piston-prop aircraft.

$$W/S = 1400 \text{ N/m}^2$$

$$S = 24 \text{ m}^2$$

$$C_{D_0} = 0.025$$

$$\tau_2 = 0.05$$

$$C_{L\max} = 1.5$$

$$P_0 = 250 \text{ kW} \quad @ \text{ sea level}$$

$$P = P_0 \sigma \quad @ \text{ an altitude}$$

$$\eta_p = 0.85$$

This problem can be solved graphically.

Steps to plot the characteristics are as follows -

$$\textcircled{1} \quad \sigma @ \text{ an altitude}$$

$$\textcircled{2} \quad f = \sigma \cdot f_0$$

$$\textcircled{3} \quad P = P_0 \sigma$$

$$\textcircled{4} \quad P_a = P \cdot \eta_p \quad \sqrt{\frac{2 W^3}{g S}} \cdot \left(\frac{\tau_2^3 C_{D_0}}{27} \right)^{\frac{1}{4}}$$

$$\textcircled{5} \quad P_{R\min} = 4 \cdot \sqrt{\frac{2 W}{g S}} \cdot \left(\frac{\tau_2}{3 C_{D_0}} \right)^{\frac{1}{4}}$$

$$\textcircled{6} \quad V = \sqrt{\frac{2 W}{g S}} \cdot \left(\frac{\tau_2}{3 C_{D_0}} \right)^{\frac{1}{4}}$$

$$\textcircled{7} \quad C_L = \sqrt{\frac{3 C_{D_0}}{\tau_2}}$$

$$\textcircled{8} \quad R/C_{\max} = \frac{(P_a - P_{R\min})}{W}$$

(4)

Plot h vs R/C_{max} , V vs R/C_{max} and C_L vs R/C_{max} to get the required quantities.

From the plots -

(a) Absolute ceiling ≈ 3.86 km

Velocity at absolute ceiling ≈ 52.47 m/s

Lift coefficient at absolute ceiling ≈ 1.225

(b) Service ceiling ≈ 3.12 km

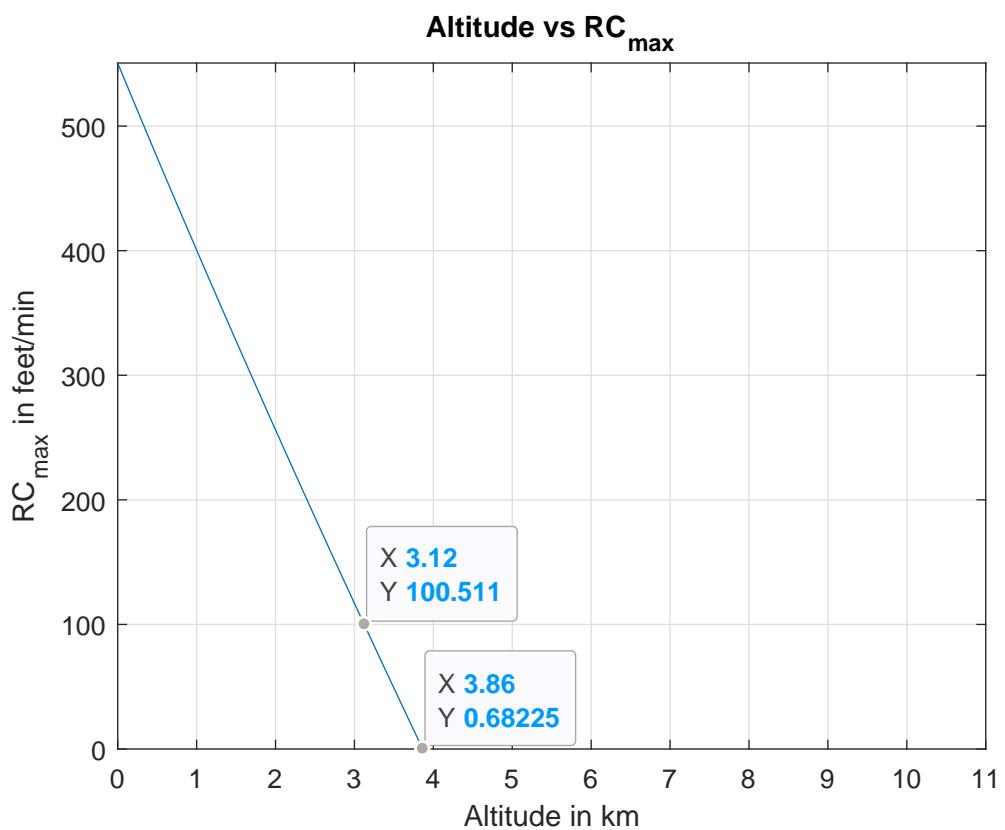
Velocity at service ceiling ≈ 50.5 m/s

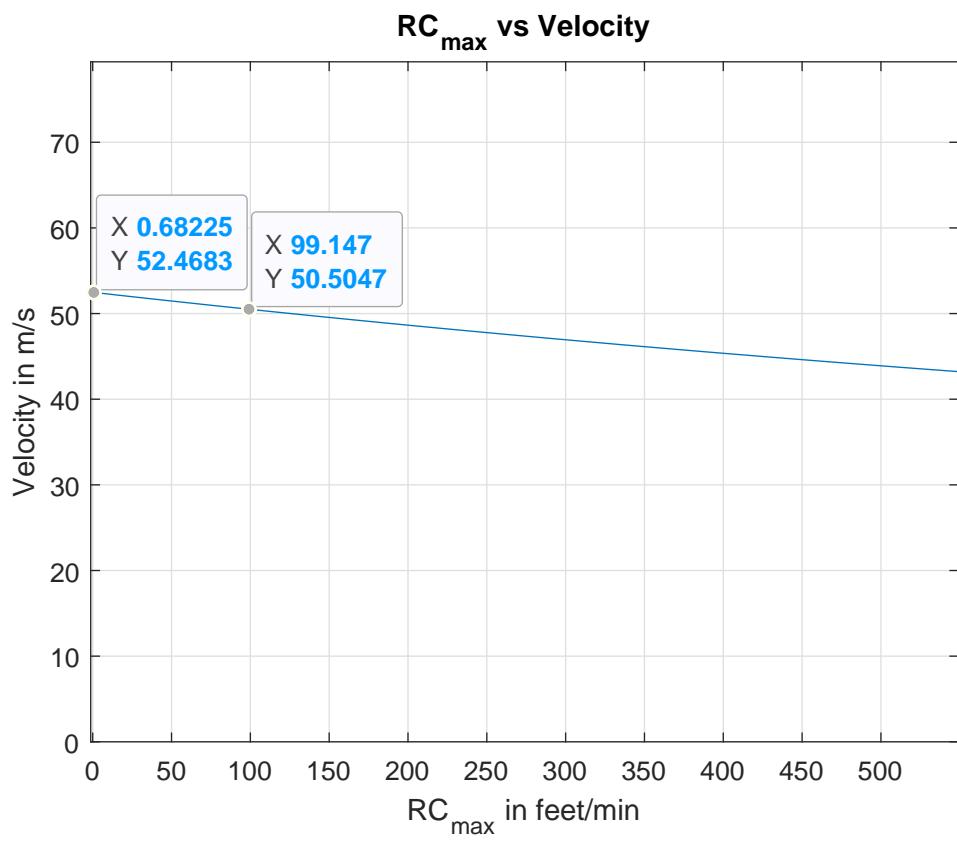
Lift coefficient at service ceiling ≈ 1.225

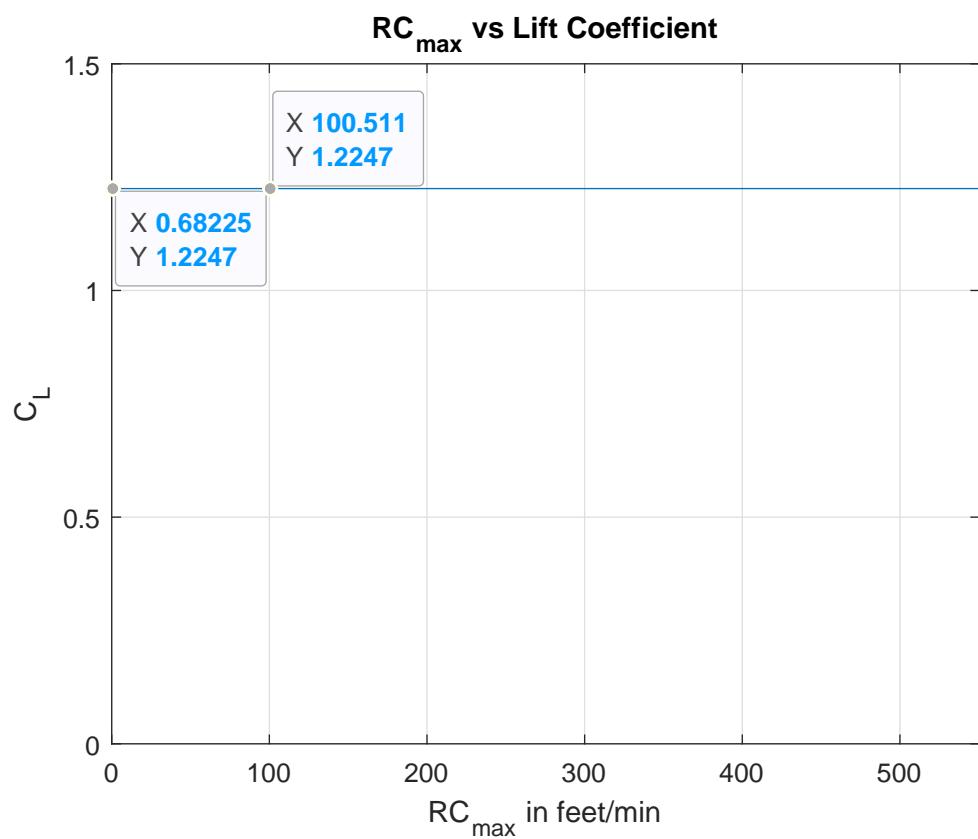
Accepted Answers

(a) $h_{abs} \in [3.7, 4.1]$ km, $V \in [49.8, 55.1]$ m/s
 $C_L \in [1.225]$

(b) $h_{service} \in [2.96, 3.28]$ km, $V \in [47.98, 53.03]$ m/s
 $C_L \in [1.225]$







Question - 3Solution

A propeller aircraft

$$W = 35000 \text{ N}$$

$$S = 21.8 \text{ m}^2$$

$$C_{D_0} = 0.021$$

$$k = 0.045$$

$$C_{L\max} = 1.5$$

$$P_s = 700 \text{ kW}$$

$$\eta_p = 0.85$$

$$n_{lim} = 3.0$$

(a)

at fastest sustained turn rate - (MSTR)

it can be solved graphically.

The deciding parameters of fastest sustained turn rate are

$$n \leq n_{lim}$$

$$\text{and } C_L \leq C_{L\max}$$

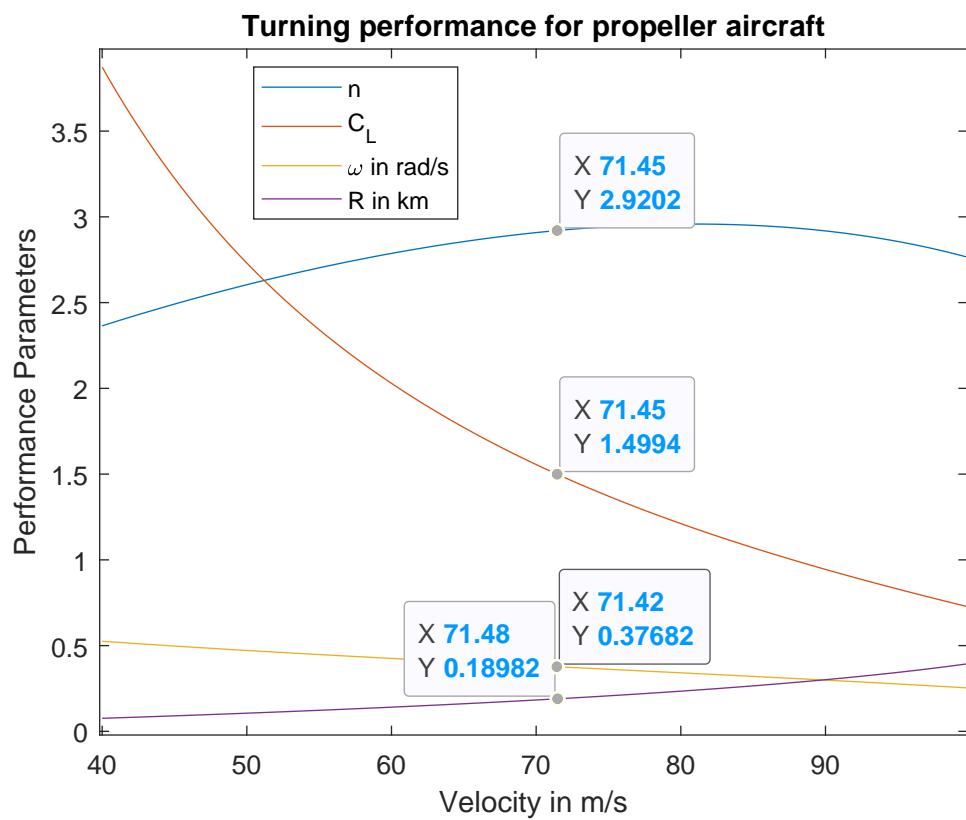
From the figure, we can see that n always remains less than the limiting load factor.

Hence, C_L will be the deciding parameter for this case.

$$\textcircled{a} \quad \underset{\text{MSTR}}{C_L} = C_{L\max}, \quad \underset{\text{MSTR}}{V} \approx 71.45 \text{ m/s}$$

$$\underset{\text{MSTR}}{\omega} \approx 0.377 \text{ rad/sec}, \quad \underset{\text{MSTR}}{R} \approx 189.82 \text{ m}$$

$$\underset{\text{MSTR}}{n} \approx 2.92$$



Accepted Answers -

$$n_{MSTR} \in [2.8, 3.0], V_{MSTR} \in [67.8, 75.0] \text{ mys}$$

$$\omega_{MSTR} \in [0.358, 0.396] \text{ rad/sec} \quad R_{MSTR} \in [180.33, 199.31] \text{ m}$$

- ⑥ Sharpest sustained turn (SST) -
It can be solved graphically.

From figure we can see that as velocity increases radius of turn is increasing.

In this case, C_{max} will also be the deciding parameter. Hence, all the performance parameters will be the same.

- ⑦ Maximum load factor turn -

$$E_m = \frac{1}{\sqrt{4 + k_2 C_{D0}}} = \frac{1}{\sqrt{4 \times 0.045 \times 0.021}} = 16.265$$

$$n_{max} = \frac{0.687 \times S}{W} \cdot \left(\frac{P_a^2 / E_m}{k S^2} \right)^{\frac{1}{3}}$$

$$= \frac{0.687 \times 21.8}{35000} \left(\frac{(595 \times 10^3)^2 \times 1.225 \times 16.265}{0.045 \times 21.8^2} \right)^{\frac{1}{3}}$$

$$\boxed{P_a = P_s n_p \\ = 595 \text{ kW}}$$

$$= 2.96$$

$$V_{n_{\max}} = \left(\frac{P_a}{2 \rho S C_D} \right)^{\frac{1}{3}}$$

$$= \left(\frac{595000}{2 \times 1.225 \times 21.8 \times 0.021} \right)^{\frac{1}{3}}$$

$$= 80.95 \text{ m/s}$$

$$\omega_{n_{\max}} = \frac{g \sqrt{n_{\max}^2 - 1}}{V_{n_{\max}}}$$

$$= \frac{9.81 \times \sqrt{2.96^2 - 1}}{80.95}$$

$$= 0.3372 \text{ rad/sec}$$

$$R_{n_{\max}} = \frac{V_{n_{\max}}^2}{g \sqrt{n_{\max}^2 - 1}}$$

$$= \frac{80.95^2}{9.81 \sqrt{2.96^2 - 1}}$$

$$= 240.1 \text{ m}$$

Accepted Answers —

$$n_{\max} \in [2.8, 3.0] , V_{n_{\max}} \in [76.9, 84.9] \text{ m/s}$$

$$\omega_{n_{\max}} \in [0.32, 0.354] \text{ rad/sec} , R_{n_{\max}} \in [228.1, 252.1] \text{ m}$$

Question - 4Solution

A jet aircraft

$$W = 60000 \text{ N}$$

$$T = 22500$$

$$C_{Lx} = 5 \text{ per radian}$$

$$\alpha_{C_{Lx}} = -2^\circ$$

$$C_{L\max} = 1.5$$

$$S = 18.75 \text{ m}^2$$

$$C_{D_0} = 0.018$$

$$\frac{1}{k} = 0.08$$

$$n_{lim} = 6.0$$

$$h = 1.5 \text{ km}$$

$$\rho = 1.058 \text{ kg/m}^3$$

$$E_m = \frac{1}{\sqrt{4 \frac{1}{k} C_{D_0}}} = \sqrt{\frac{1}{4 \times 0.08 \times 0.018}} \\ = 13.1762$$

$$Z = \frac{T E_m}{W} = \frac{22500 \times 13.1762}{60000} \\ = 4.9411$$

$$C_L^* = \sqrt{\frac{C_{D_0}}{\frac{1}{k}}} = \sqrt{\frac{0.018}{0.08}} = 0.4743$$

$$V_R = \sqrt{\frac{2W}{SS C_L^*}} = \sqrt{\frac{2 \times 60000}{1.225 \times 18.75 \times 0.4743}} \\ = 112.928 \text{ m/s}$$

(a) Fastest sustained turn rate (MSTR) -

$$n_{MSTR} = \sqrt{2Z - 1} = \sqrt{2 \times 4.9411 - 1} = 2.98$$

$$V_{MSTR} = V_R = 112.928 \text{ m/s}$$

$$\omega_{MSTR} = \frac{2 \sqrt{2Z - 2}}{V_R} = \frac{2 \sqrt{2 \times 4.9411 - 2}}{112.928} = 0.2438 \text{ rad/sec}$$

$$R_{MSTR} = \frac{V_{MSTR}^2}{2 \sqrt{n_{MSTR}^2 - 1}} = \frac{112.928^2}{2 \sqrt{2.98^2 - 1}} \\ = 463.03 \text{ m}$$

⑨

Accepted answers -

$$n_{MSTR} \in [2.83, 3.13] , V_{MSTR} \in [107.28, 118.57] \text{ m/s}$$

$$\omega_{MSTR} \in [0.23, 0.256] \text{ rad/sec} , R_{MSTR} \in [439.88, 486.18] \text{ m}$$

(b) Sharpest sustained turn (SST) -

$$n_{SST} = \frac{\sqrt{2z^2 - 1}}{z} = \frac{\sqrt{2 \times 4.9411^2 - 1}}{4.9411} = 1.399$$

$$V_{SST} = \frac{V_R}{\sqrt{z}} = \frac{112.928}{\sqrt{4.9411}} = 50.8 \text{ m/s}$$

$$\begin{aligned} \omega_{SST} &= \frac{g}{V_R} \cdot \sqrt{\frac{z^2 - 1}{z}} \\ &= \frac{9.81}{112.928} \cdot \sqrt{\frac{4.9411^2 - 1}{4.9411}} = 0.189 \text{ rad/s} \end{aligned}$$

$$R_{SST} = \frac{V_{SST}^2}{g \sqrt{n_{SST}^2 - 1}} = \frac{50.8^2}{9.81 \sqrt{1.399^2 - 1}} = 268.66 \text{ m}$$

Accepted answers -

$$n_{SST} \in [1.32, 1.47] , V_{SST} \in [48.26, 53.34] \text{ m/s}$$

$$\omega_{SST} \in [0.179, 0.198] \text{ rad/sec} , R_{SST} \in [255.2, 282.1] \text{ m}$$

(C) Turn with maximum load factor -

$$n_{\max} = Z = 4.94$$

$$V_{n_{\max}} = \sqrt{Z} V_R = \sqrt{4.94} \cdot 112.928 \\ = 251.02 \text{ m/s}$$

$$\omega_{n_{\max}} = \frac{2 \sqrt{n_{\max}^2 - 1}}{V_{n_{\max}}} = \frac{9.81 \times \sqrt{4.94^2 - 1}}{251.02} \\ = 0.189 \text{ rad/sec}$$

$$R_{n_{\max}} = \frac{V_{n_{\max}}^2}{2 \sqrt{n_{\max}^2 - 1}} = \frac{251.02^2}{9.81 \sqrt{4.94^2 - 1}} \\ = 1327.44 \text{ m}$$

Accepted answers -

$$n_{\max} \in [4.69, 5.19], V_{n_{\max}} \in [238.4, 263.6] \text{ m/s}$$

$$\omega_{n_{\max}} \in [0.179, 0.198] \text{ rad/sec}, R_{n_{\max}} \in [1261.06, 1393.8] \text{ m}$$

Question - 5Solution

A light turbojet

$$W = 20000 \text{ N}$$

$$W/S = 1000 \text{ N/m}^2$$

$$T_0 = 2000 \text{ N} \quad @ \text{ sea level}$$

$$T = T_0 e^{-0.8} \quad @ \text{ an altitude}$$

$$C_{D_0} = 0.015$$

$$k = 0.024$$

$$C_{L_{\max}} = 1.4$$

$$C_{L_{\min}} = -0.5$$

$$n_p = 6.0 \quad [\text{Positive limiting load factor}]$$

$$n_s = 3.0 \quad [\text{Negative limiting load factor}]$$

V-n diagram is shown in figure.

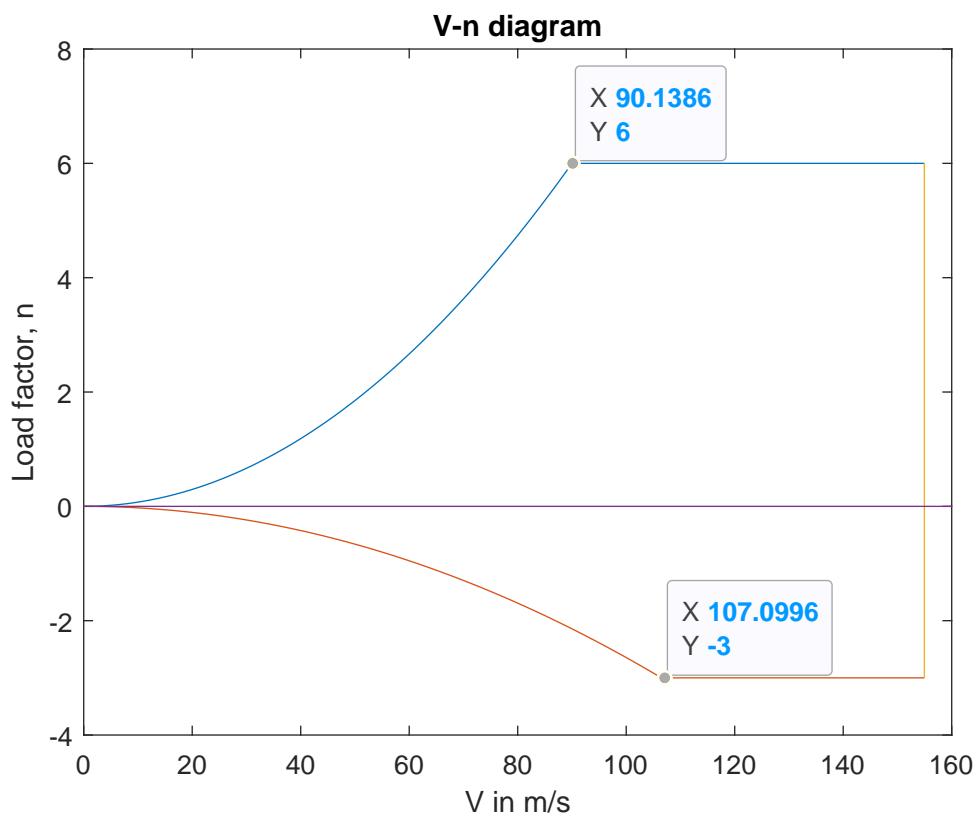
$$V_{lim} = 1.5 V_{max}$$

$$V_{max} = V_R \sqrt{z + \sqrt{z^2 - 1}}$$

$$\text{where } V_R = \sqrt{\frac{2W}{SS}} \cdot \left(\frac{k}{C_{D_0}}\right)^{\frac{1}{4}}$$

$$z = \frac{T E_m}{W}$$

$$@ \text{ Corner velocity } V_c = \sqrt{\frac{2 n_i (W/S)}{S C_{L_{\max}}}} = \sqrt{\frac{2 \times 6 \times 10000}{1.058 \times 1.4}} = 90.0 \text{ m/s}$$



b) Corner radius of turn

$$C_D = C_{D_0} + \frac{1}{2} C_{L_{max}}^2$$

$$= 0.015 + 0.024 \times 1.4^2$$

$$= 0.062$$

$$D = \frac{1}{2} \gamma S C_D V_c^2$$

$$= \frac{1}{2} \times 1.058 \times 20 \times 0.062 \times 90^2$$

$$= 5317.7 \text{ N}$$

$$T_a = T_0 \sigma^{0.8}$$

$$= 2000 \left(\frac{1.058}{1.225} \right)^{0.8} = 1778.7 \text{ N}$$

$$\gamma_c = \sin^{-1} \left(\frac{T_a - D}{W} \right)$$

$$= \sin^{-1} \left(\frac{1778.7 - 5317.7}{20000} \right)$$

$$= -0.1779 \text{ rad} = -10.19^\circ$$

$$R_c = \frac{(V_c \cdot \cos \gamma_c)^2}{2 \sqrt{n_i^2 - (\cos \gamma_c)^2}}$$

$$= \frac{(90 \times \cos(-10.19^\circ))^2}{9.81 \sqrt{6^2 - (\cos(-10.19^\circ))^2}}$$

$$= 135.16 \text{ m}$$

$$w_c = \frac{V_c \cos(\gamma_c)}{R_c} = \frac{90 \times \cos(-10.19^\circ)}{135.16}$$

$$= 0.655 \text{ rad/sec}$$

$$t_{\pi} = \frac{\pi}{\omega_c}$$

$$= \frac{\pi}{0.655} = 4.79 \text{ sec}$$

Accepted answers -

$$V_c \in [85.5, 94.5] \text{ m/s}, R_c = [128.4, 141.9] \text{ m}$$

$$\omega_c \in [0.622, 0.687] \text{ rad/s}, t \in [4.5, 5.03] \text{ sec}$$

Question - 6

Solution

given data -

$$W = 10000 \text{ N}$$

$$S = 3.4 \text{ m}^2$$

$$T = 2500 \text{ N}$$

$$C_D = 0.021$$

$$f_2 = 0.045$$

$$C_{L_{\max}} = 1.8$$

$$\mu = 0.05$$

① minimum ground run will occur when

$$C_L^* = \frac{\mu}{2f_2} = \frac{0.05}{2 \times 0.045} = 0.556$$

(14)

$$V_{stall} = \sqrt{\frac{2W}{\rho S C_{Lmax}}} = \sqrt{\frac{2 \times 10000}{1.225 \times 3.4 \times 1.8}} = \\ = 51.65 \text{ m/s}$$

$$V_i = 1.2 V_{stall} \\ = 1.2 \times 51.65 \\ = 61.98 \text{ m/s}$$

$$F_0 = T - \mu W \\ = 2500 - 0.05 \times 10000 \\ = 2000 \text{ N}$$

$$F_i^* = T - \frac{1}{2} \rho S V_i^2 (C_D + \frac{1}{2} C_L^*) \\ = 2500 - \frac{1}{2} \times 1.225 \times 3.4 \times 61.98^2 (0.021 + 0.045 \times 0.556) \\ = 2220.9 \text{ N}$$

a

$$S_i = \frac{W}{2g} \times \frac{V_i^2}{F_0 - F_i^*} \ln \left(\frac{F_0}{F_i^*} \right) \\ = \frac{10000}{2 \times 9.81} \times \frac{61.98^2}{2000 - 2220.9} \ln \left(\frac{2000}{2220.9} \right) \\ = 928.6 \text{ m}$$

(b) time to ground run

$$A = F_0 = 2000$$

$$B = \frac{F_i^* - F_0}{V_i^2} = \frac{2220.9 - 2000}{61.98^2} \\ = 0.0575$$

(15)

Since $A > 0 \& B > 0$

$$t_1 = \frac{W}{2\sqrt{AB}} \cdot \tan^{-1} \left(\sqrt{\frac{B}{A}} V_1 \right)$$

$$= \frac{10000}{9.81 \sqrt{2000 \times 0.0575}} \cdot \tan^{-1} \left(\sqrt{\frac{0.0575}{2000} \times 61.98} \right)$$

$$= 30.49 \text{ sec}$$

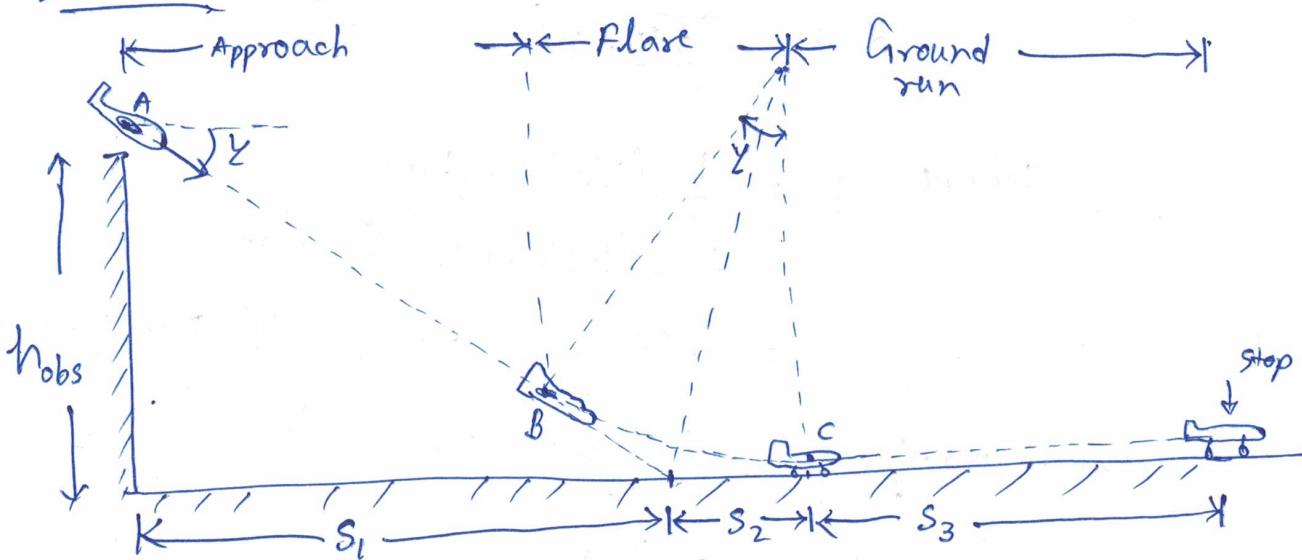
Accepted answers -

$$s_1 \in [882.17, 975.0] \text{ m}$$

$$t_1 \in [28.97, 32.0] \text{ sec}$$

Question - 7

Solution



from figure -

$$\frac{h_{obs}}{S_1} = \tan \gamma$$

$$S_1 = \frac{h_{obs}}{\tan \gamma}$$

$$t_1 = \frac{S_1}{V_A \cos \gamma}$$

$$V_A = \text{Approach velocity}$$

$$= 1.3 V_{stall}$$

$$= V_1$$

from equations of motion -

$$L - W \cos \gamma = \frac{W V_A^2}{R g} \quad \text{--- (1)}$$

$$T - D - W \sin \gamma = 0 \quad \text{--- (2)}$$

$$\sin \gamma = \frac{T - D}{W} \quad \text{--- (3)}$$

Assuming γ is small, from equation (1), we can write -

$$R = \frac{W V_A^2}{g(L - W)} \quad \text{--- (4)}$$

where $L = \frac{1}{2} \delta V_A^2 S C_{lmax}$

$$= \frac{1}{2} \delta (1.3 V_{stall})^2 S C_{lmax}$$

$$= 1.69 W \quad \text{--- (5)} \quad \because L = W = \frac{1}{2} \delta S C_{lmax} V_{stall}^2$$

From equation (4) & (5), we can write -

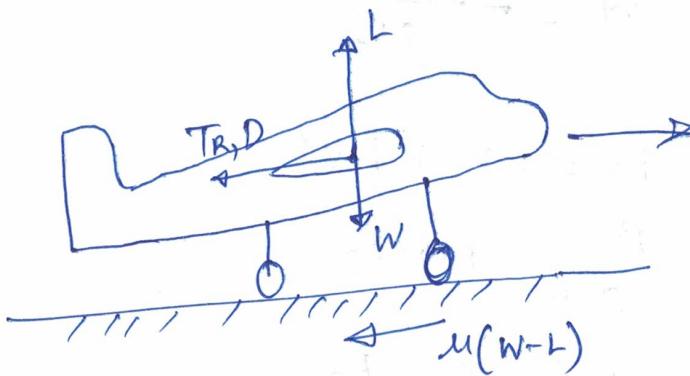
$$R = \frac{V_A^2}{0.699 \delta}$$

(17)

$$S_2 \approx \frac{1}{2} R Y$$

$$t_2 = \frac{S_2}{V_A Y}$$

ground run -



net deaccelerating force -

$$F_a = T_R + D + \mu(W-L) \quad \text{--- (6)}$$

where T_R is the thrust reversal.

$$\frac{W}{g} V \frac{dV}{ds} = -F_a$$

$$ds = -\frac{W dV^2}{2g F_a}$$

$$F_a = F_0 + \frac{F_1 - F_0}{V_i^2} V^2$$

$$\int_0^{S_3} ds = -\frac{W}{2g} \int_{V_i}^0 \frac{dV^2}{F_0 + \frac{F_1 - F_0}{V_i^2}}$$

$$S_3 = \frac{W}{2g} \left(\frac{V_i^2}{F_1 - F_0} \right) \ln \left(\frac{F_1}{F_0} \right)$$

where, $F_1 = T_R + D$

$$F_0 = T_R + \mu W$$

* For minimum ground run $C_L^* = \frac{\mu}{2k}$

$$\frac{W}{g} \frac{dV}{dt} = -F_a$$

$$dt = -\frac{W dV}{g F_a}$$

$$F_a = a + b V^2$$

$$a = \cancel{F_0}$$

$$b = \frac{F_1 - F_0}{V_1^2}$$

$$\int_0^{t_3} dt = - \int_{V_1}^0 \frac{W}{g} \cdot \frac{dV}{a + b V^2}$$

$$t_3 = \frac{W}{g \sqrt{ab}} \tan^{-1} \left(\sqrt{\frac{b}{a}} V_1 \right) [a > 0, b > 0]$$

$$t_3 = \frac{W}{2g \sqrt{ab_1}} \ln \left(\frac{\sqrt{a} + \sqrt{b_1} V_1}{\sqrt{a} - \sqrt{b_1} V_1} \right) [a > 0, b < 0]$$

where, $b_1 = |b|$

Question - 8

(9)

Solution

Given data -

$$W = 62784 \text{ N}$$

$$S = 20 \text{ m}^2$$

$$C_D = 0.0254$$

$$\frac{1}{k} = 0.178$$

$$G_{\max} = 0.95$$

$$\sigma = 0.9074$$

$$\mu = 0.02$$

$$\gamma = 3.5^\circ = 3.5 \times \frac{\pi}{180} = 0.0611 \text{ rad}$$

$$h_{\text{obs}} = 15 \text{ m}$$

a) Airborne distance (including flare) = $s_1 + s_2$

$$s_1 = \frac{h_{\text{obs}}}{\tan(\gamma)}$$

$$= \frac{15}{\tan(3.5^\circ)} = 245.25 \text{ m}$$

$$s_2 = \frac{1}{2} R \gamma$$

$$V_1 = 1.3 V_{\text{stall}} = 1.3 \times \sqrt{\frac{2W}{\rho S G_{\max}}}$$

$$= 1.3 \times \sqrt{\frac{2 \times 62784}{1.1116 \times 20 \times 0.95}} = 100.24 \text{ m/s}$$

$$L = \frac{1}{2} \rho S V_1^2 G_{\max} = \frac{1}{2} \times 1.1116 \times 20 \times 100.24^2 \times 0.95$$

$$= 1.061 \times 10^5 \text{ N}$$

$$\begin{aligned}
 R &= \frac{w v_i^2}{g(L - w \cos\gamma)} \\
 &= \frac{62784 \times 100.24^2}{9.81(1.061 \times 10^5 - 62784 \cos(3.5^\circ))} \\
 &= 1.4804 \times 10^3 \text{ m} \\
 &= 1480.4 \text{ m}
 \end{aligned}$$

$$\begin{aligned}
 \text{or } R &= \frac{v_i^2}{0.669 g} = \frac{100.24^2}{0.669 \times 9.81} \\
 &= 1531.04 \text{ m}
 \end{aligned}$$

$$\begin{aligned}
 S_2 &= \frac{1}{2} R \gamma \\
 &\approx \frac{1}{2} \times 1480.4 \times 0.0611 = 45.22 \text{ m} \\
 \text{or } &\approx \frac{1}{2} \times 1531.04 \times 0.0611 = 46.77 \text{ m}
 \end{aligned}$$

$$\begin{aligned}
 \text{Airborne distance} &= S_1 + S_2 \\
 &= 245.25 + 45.22 \\
 &= 290.46 \text{ m}
 \end{aligned}$$

Accepted answer -

$$\text{Airborne distance } \in [275.9, 304.9] \text{ m}$$

(b) ground run (S_3) ~~is 11.63 m and = 0~~

① Case -

$$C_L^* = \frac{\mu}{2f_k} = \frac{0.02}{2 \times 0.178}$$

$$= 0.95$$

$$F_0 = \mu w$$

$[T_R = 0]$ no thrust reversal.

$$= 0.02 \times 62784$$

$$= 1255.7 \text{ N}$$

$$F_I^* = \frac{1}{2} \rho S V_I^2 (C_D + \frac{1}{4} C_L^{*2})$$

$$= \frac{1}{2} \times 1.116 \times 20 \times 100.24^2 (0.0254 + 0.178 \times 0.95^2)$$

$$= 2899.7 \text{ N}$$

$$S_3 = \frac{w}{2g} \cdot \frac{V_I^2}{F_0 + F_I^*} \ln\left(\frac{F_0}{F_I^*}\right)$$

$$= \frac{62784}{2 \times 9.81} \times \frac{100.24^2}{1255.7 + 2899.7} \ln\left(\frac{1255.7}{2899.7}\right)$$

$$= 1636.90 \text{ m}$$

Accepted Answer -

~~S_3~~

Second Case

$$\text{when } C_L^* = C_{L\max}$$

$$F_0 = \mu w = 1255.7 \text{ N}$$

$$F_I = 20779 \text{ N}$$

$$\underline{S_3 = 4621.66 \text{ m}}$$

$G = G_{\max}$ will give the minimum ground run.

$$(S_3)_{\min} = 4621.66 \text{ m}$$

* It requires very large ground run because there is no thrust reversal system.

Accepted answers

① Case $S_3 \in [15550, 17187] \text{ m}$

② Case $S_3 \in [4390.5, 4852.7] \text{ m}$