

Aircraft Design : Solved Example

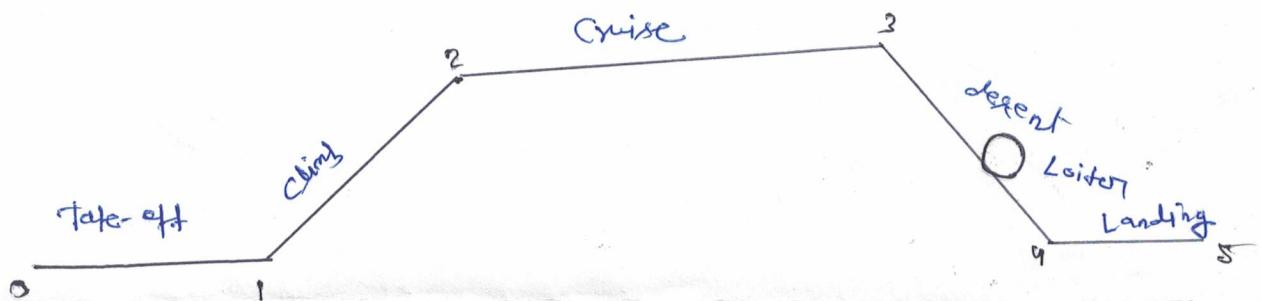
Let us say we have been given the following mission requirement to design the light weight aircraft.

MISSION REQUIREMENTS

1. Weight of the aircraft: $\leq 3000 \text{ kg}$
2. Four passenger + 1 crew
3. Maximum Range: 1000 km
4. Service Ceiling: 7 km
5. Flight Altitude: mean sea level to $10,000 \text{ ft}$
6. Design cruise speed: go to 110 m/s
7. Rate of climb: $5 \text{ to } 6 \text{ m/s}$ (At sea level)
8. Take-off distance: $50^{\circ} \text{ to } 60^{\circ} \text{ m}$
9. Landing distance: $500 \text{ to } 600 \text{ m}$

STEP . 1

Draw the mission profile



Take-off :	0 to 1
Climb :	1 to 2
Cruise :	2 to 3
Descent :	3 to 4
Landing :	4 to 5

STEP : 2 \Rightarrow Weight Estimation of Aircraft

An Aircraft can have the following types of weight \Rightarrow

$w_c = w_{\text{crew}} = \text{Weight of the crew}$

$w_p = w_{\text{payload}} = \text{Weight of the payload}$

$w_f = w_{\text{fuel}} = \text{Weight of the fuel}$

$w_e = w_{\text{empty}} = \text{Empty weight}$

If total weight of the Aircraft is w_0 then -

$$w_0 = w_c + w_p + w_f + w_e$$

we have
manipulation

doing the mathematical

$$\left[w_0 = \frac{w_c + w_p}{1 - \frac{w_f}{w_0} - \frac{w_e}{w_0}} \right] - \textcircled{1}$$

It can be noticed that in Eq.(1)

$\frac{w_f}{w_0}$ and $\frac{w_e}{w_0}$ are required to find the total weight of the aircraft.

⇒ Estimation of empty weight fraction (w_e/w_0)
From the literature survey for weight class -
 $2000 - 3000 \text{ kg}$ Empty weight fraction (w_e/w_0)

$$18 \quad 0.62$$

$$\boxed{\frac{w_e}{w_0} = 0.62}$$

for more information please refer the Fig. 1

⇒ Estimation of fuel weight fraction (w_f/w_0)

If $R =$ Range of Aircraft

$\frac{L}{D} =$ Lift to drag ratio

$h_{pr} =$ propeller efficiency

$c =$ specific fuel consumption

then, Range can be written as -

$$R = \frac{h_{pr}}{c} \left(\frac{L}{D} \right) \ln \left(\frac{w_2}{w_3} \right) \quad \text{--- (2)}$$

for the present case \Rightarrow

$$R_{max} = 1000 \text{ km}$$

$$(L/D)_{max} = 13 \quad (\text{Assumed})$$

$$h_{pr} = 0.85$$

$$C = \frac{0.4 \times 9.81}{246 \times 3600} \left(\frac{1}{\rho} \right)$$

$$= 1.4611 \times 10^{-6} \left(\frac{1}{\rho} \right)$$

From Eq. (2) \Rightarrow

(recirculating engine)

$$1000 \times 10^3 = \frac{0.85}{1.4611 \times 10^{-6}} \times 13 \text{ J} \cdot \frac{\omega_2}{\omega_1}$$

$$\frac{\omega_2}{\omega_1} = 1.14136$$

$$\boxed{\frac{\omega_3}{\omega_2} = 0.87614}$$

and

$$\boxed{\frac{\omega_4}{\omega_1} = 1} \rightarrow$$

Fuel consumption in descent = 0

$$\boxed{\frac{\omega_5}{\omega_4} = 0.995} \rightarrow$$

Amount of fuel used in landing is small

From the mission profile \Rightarrow

$$\frac{\omega_5}{\omega_0} = \frac{\omega_1}{\omega_2} \cdot \frac{\omega_2}{\omega_1} \cdot \frac{\omega_3}{\omega_2} \cdot \frac{\omega_4}{\omega_3} \cdot \frac{\omega_5}{\omega_4} \quad \leftarrow (3)$$

and

$$\omega_f = \omega_0 - \omega_5 \quad \leftarrow (4)$$

6*

$$\frac{w_f}{w_0} = \left(1 - \frac{w_f}{w_0} \right)$$

$$\frac{w_f}{w_0} = 1.06 \left(1 - \frac{w_f}{w_0} \right) \quad | \begin{array}{l} 6\% \text{ fuel} \\ \text{is required} \end{array}$$

← (5)

for take-off ($c = 1$)

$$\frac{w_f}{w_0} = 0.97$$

climb ($c = 2$)

$$\frac{w_c}{w_i} = 0.985$$

So, till now, we have, $\frac{w_1}{w_0}, \frac{w_c}{w_1}, \frac{w_3}{w_2}, \frac{w_4}{w_1}$ and

$$\frac{w_5}{w_4}$$

inserting the values of these fractions in

Eq. (3) we have,

$$\frac{w_5}{w_0} = \frac{w_1}{w_0} \cdot \frac{w_2}{w_1} \cdot \frac{w_3}{w_2} \cdot \frac{w_4}{w_3} \cdot \frac{w_5}{w_4}$$

$$= 0.97 \times 0.985 \times 0.87617 \times 1 \times 0.925$$

$$\frac{w_5}{w_0} = 0.8322$$

Inserting $\frac{w_f}{w_s}$ in Eq. (1) we get,

$$\frac{w_f}{w_s} = 1.06 (1 - 0.8332c_2)$$

$$\boxed{\frac{w_f}{w_s} = 0.1771}$$

it can be noticed that to find the total weight of the aircraft (w_s). We have found out

w_c and w_p are.

w_c and $\frac{w_f}{w_s}$. However,

to find w_s .

required

$$w_c = 80 \text{ kg}$$

(Average weight of
a human)

As we know there are four passengers

So, passenger weight will be = 4×80

$$= 320 \text{ kg}$$

10 kg extra weight carried by each one

total payload weight will be -

80 + 320 + 520

$$w_p =$$

$$\boxed{w_p = 320 \text{ kg}}$$

From Eq. (1)

$$W_0 = \frac{W_c + W_f}{1 - \frac{W_f}{W_0} \cdot \frac{W_e}{W_0}}$$

$$= \frac{80 + 370}{1 - 0.1771 \times 0.62}$$

Total Weight of

Aircraft.

$$W_0 = 2217.84 \text{ kg}$$

Fuel weight, now, can be found as -

$$W_f = \frac{W_f}{W_0} \cdot W_0 = 0.1771 \times 2217.84$$

$$W_f = 392.77 \text{ kg}$$

STEP - 3

~~Wing Sizing of Wing~~

Till now, we have estimated the total weight of the aircraft. This weight will lift by the wing of the Aircraft. In this section, we will design the wing.

for a Steady-Straight-level flight

$$\text{Weight} = \text{lift} -$$
$$W = \frac{1}{2} \rho v^2 S C_L$$

or

$$W_S = \frac{1}{2} \rho V^2 C_L - \textcircled{1}$$

where

W_S = wing loading

ρ = density of air

V = flight velocity

C_L = lift coefficient

Further,

$$W_S = \frac{1}{2} \rho V_{\text{stall}}^2 C_{L_{\text{max}}} \textcircled{2}$$

$$\begin{aligned} W_S &= \frac{1}{2} \times 1.225 \times (30)^2 \times 2.3 \\ &= 1268.4 \text{ N/m}^2 \end{aligned}$$

$$W_S = 126.84 \text{ kg/m}^2$$

at
 $C_L = C_{L_{\text{max}}} = 2.3$

$V = V_{\text{stall}}$
= 30 m/s

Note:
 $C_{L_{\text{max}}}$ is at
take-off with
flap deflection

wing loading calculation of desired cruise speed and lift coefficient

Let say our desire cruise speed ie
 70 m/s and lift coefficient ie 0.4

From Eq. \textcircled{1}

$$W_S = \frac{1}{2} \times 1.225 \times (70)^2 \times 0.4$$

$$W_S = 1201.688 = 122.435 \text{ kg/m}^2$$

Wing Loading calculation when Landing distance is specified \Rightarrow

Using the relation

$$S_g = jN \sqrt{\frac{2}{\rho_\infty} \left(\frac{W}{S}\right) \frac{1}{C_{L_{max}}}} + \frac{j^2 \left(\frac{W}{S}\right)}{\rho g (C_{L_{max}}) S_f}$$

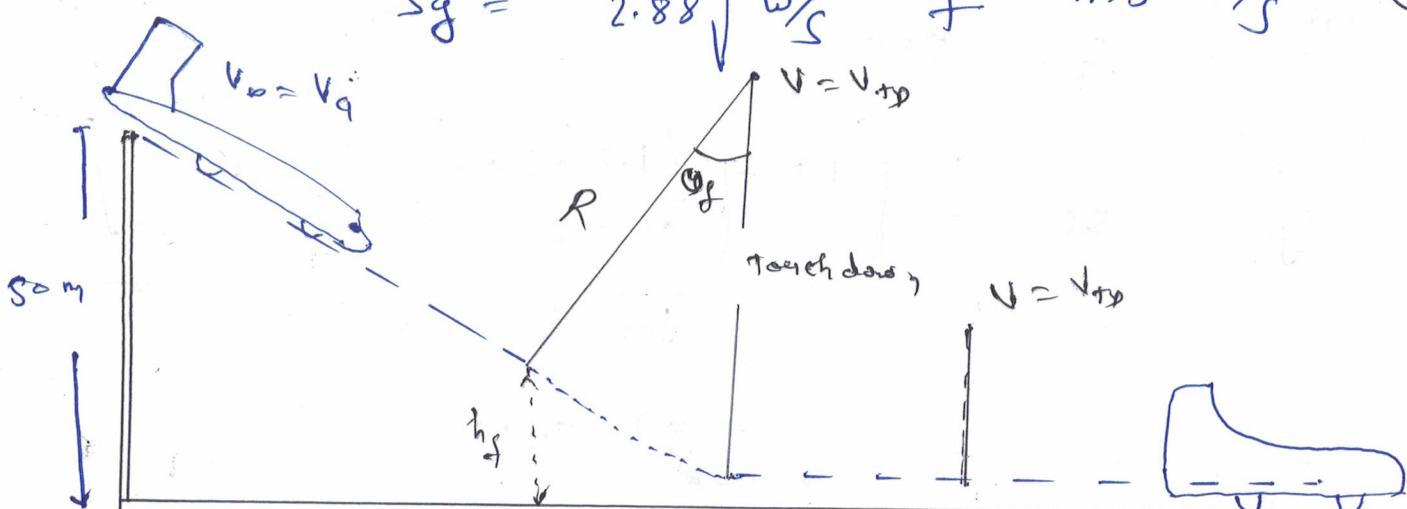
for considered aircraft

$$j = 1.15$$

$$N = 3$$

Eq.(8) becomes

$$S_g = 2.88 \sqrt{\frac{W/S}{\rho}} + 0.1175 \frac{W/S}{\rho} - \textcircled{9}$$



$$S_g = S_a + S_f + S_g$$

S_a = Approach distance, V_a = Approach velocity

$\Phi_f = \Phi_a =$ Approach Angle

S_f = flare distance

S_g = Period roll distance

$$S_g = S_a + S_f + S_g$$

Hence

$$S_g = S_L - S_a - S_f$$

$$S_g = S_L - \left(\frac{15 - h_f}{\tan \alpha_a} \right) - R \sin \alpha_a$$

$$= S_L - \left[15 - \frac{R(1 - \cos \alpha_a)}{\tan \alpha_a} \right] - R \sin \alpha_a \quad \begin{cases} v_f = 1.23 \\ \times v_{\text{Stead}} \end{cases}$$

$$S_g = S_L - \left[15 - \frac{15 - \left[\frac{v_f^2}{0.2g} (1 - \cos \alpha_a) \right]}{\tan \alpha_a} \right] - \left[\frac{\frac{v_f^2}{0.2g} (1 - \cos \alpha_a)}{\tan \alpha_a} \right]$$

if the total landing is specified as 500 to 600

Let

$$S_L = 550$$

$$S_g = 550 - \left[15 - \left[\frac{(1.23 + 30)^2}{0.2 + 9.81} (1 - \cos 3^\circ) \right] \right] - \frac{(1.23 + 30)^2}{0.2 + 9.81} \sin 3^\circ$$

$$= 550 - 268.064 - 36.32$$

$$\boxed{S_g = 245.61 \text{ m}}$$

Inserting the value in Eq. (8) -

$$245.61 = 2.88 \sqrt{\omega_s} + 0.1125 \omega_s$$

Let $\omega_s = x^2$

$$\Rightarrow 245.61 = 2.88x + 0.1125x^2$$

$$0.1125x^2 + 2.88x - 245.61 = 0$$

$$x = \frac{-2.88 \pm \sqrt{(2.88)^2 - 4 \times 0.1125 \times (-245.61)}}{2 \times 0.1125}$$

$$x = \frac{-2.88 \pm 11.123}{2 \times 0.1125}$$

$$x = 35.025$$

$$x^2 = 1237.501$$

$$\omega_s = 1237.501 \text{ rad/sec}$$

$$\boxed{\omega_s = 125.433 \text{ rad/sec}}$$

It can be noticed that -

1. ω_s (from Stall velocity approach)
(take-off)

$$= \underbrace{127.301}_{\text{kg/m}^2} \text{ kg/m}^2$$

2. ω_s (from cruise velocity
approach)

$$= \underbrace{122.435}_{\text{kg/m}^2} \text{ kg/m}^2$$

3. ω_s (from landing approach)

$$= \underbrace{125.433}_{\text{kg/m}^2} \text{ kg/m}^2$$

All three are very much
close to each other

Now, Area of the wing can be found as-

$$S = \frac{W}{C_S}$$

$$= \frac{2217.84}{122.435}$$

$$[S = 18.11 \text{ m}^2]$$

Let the Aspect ratio of wing is chosen to

be 10

$$AR = 10$$

$$\Rightarrow AR = \frac{b^2}{S}$$

$$b = \sqrt{AR \cdot S}$$

$$= \sqrt{10 \times 18.11}$$

wing span

$$b = 13.45 \text{ m}$$

wing chord
(for rectangular)

wing)

$$\bar{c} = \frac{b}{AR} = \frac{13.45}{10}$$

$$\bar{c} = 1.345$$

Engine Selection \Rightarrow [Step - 4]

Estimation of thrust to weight ratio:

let us consider the take-off distance. [Ground roll distance]

$$S_g = \frac{1.21 (W/S)}{g S_{\text{roll}} C_{L_{\max}} (T/W)} \quad - (10)$$

$$= \frac{1.21 \times 122.425 \times 9.8}{9.81 \times 1.225 \times 2 \times (T/W)}$$

$$S_g = \frac{\frac{60.43}{9.81 \times 1.225}}{(T/W)} = \frac{60.43}{T/W} \quad - (11)$$

for $C_{L_{\max}} = 2$

$$V_{\text{Street}} = \sqrt{\frac{2 W/S}{g S_{\text{roll}} C_{L_{\max}}}}$$

$$= 31.3 \text{ m/s}$$

[take-off velocity]

$$V_{L_0} = 1.1 V_{\text{Street}} = 34.435$$

$$R = \frac{6.98 V_s^2}{g} = \frac{6.98 \times (31.3)^2}{9.81}$$

$$R = 697.66 \text{ m}$$

Induced flight path

Angle i.e.

$$\Theta_{iB} = \cos^{-1} \left(1 - \frac{h_{iB}}{R} \right)$$

$$= \cos^{-1} \left(1 - \frac{15}{697.66} \right) = 11.9^\circ$$

Airborn distance

$$S_a = R \cdot S_{g_2} = 697.06 \times \sin(11.9^\circ) \\ = 143.82 \text{ m}$$

If take-off distance is specified as

$$600 \text{ m}$$

then

$$600 = S_g + S_a \quad \rightarrow \text{Eq. 12}$$

From Eq. 11

$$600 = \frac{60.43}{(\tau/\omega)} + 143.82$$

$$\frac{1}{\tau/\omega} = \frac{600 - 143.82}{60.43}$$

$$\frac{1}{\tau/\omega} = 7.548 \times$$

$$\boxed{\tau/\omega = 0.13246}$$

or

$$\boxed{\left(\frac{1}{\tau/\omega}\right)_{0.7 V_L} = 0.13246}$$

$$V_{L0} = 0.7 V_L = 0.7 \times 34.435$$

$$\boxed{V_{L0} = 24.1045 \text{ m/s}}$$

V_{L0} = take-off

velocity

Power required \Rightarrow

$$P_F = T V_o$$

$$= (\frac{1}{\omega}) W_s \cdot V_o$$

$$= 0.1324 \times 2212.84 \times 24.10 \\ \times 9.81$$

$$= 69454.13 \text{ (Watt)}$$

$$P_R = \frac{82.954}{93.06} \text{ (hp)}$$

Power Available \Rightarrow

$$P_A = \frac{P_R}{h} \quad | h = 0.8$$

$$= \frac{82.954}{0.8}$$

$$P_A = 103.7 \text{ hp}$$

$$P_A = 116.4 \text{ hp}$$

To satisfy the take-off constraint, the total power must be at least

$$P \geq 116.4 \text{ hp}$$

Next

Power available calculation to
perform the job (rate of doing)

using

$$\frac{h_p \times P}{\omega} = (P/C)_{max} + \left[\frac{2}{S_{00}} \sqrt{\frac{K}{3C_{b0}}} \left(\frac{\omega}{J} \right) \right]^{1/2}$$

$$= 5 + \left[\frac{2}{1.2256} \sqrt{\frac{0.0422}{3 \times 0.035}} \cdot 122.435 \times 9.81 \right]^{1/2}$$

$$= 5 + \left[\frac{1.155}{1.3} \right]^{1/2}$$

Induced drag factor

$$f = \frac{1}{4C_{b0}(L_D)^2}$$

Assume

$$\frac{h_p \times P}{\omega} = 8.133$$

$$C_{b0} = 0.035$$

(zero lift drag coeff.)

$$P = \frac{8.133 \times \omega}{h_p} = \frac{8.133 \times 2217.84 + 9.81}{0.8}$$

$$= 22198.2165 \text{ watt}$$

$$P = 296.5 h_p$$

To satisfy the constraint on rate of climb, the power must be

$$P \geq 296.5 \text{ hp}$$

Let us summarize the findings

Total weight, $w_0 = 2212.84 \text{ kg}$

Fuel weight, $w_f = 392.77 \text{ kg}$

Wing Area, $S = 18.11 \text{ m}^2$

Span, $l = 13.45 \text{ m}$

Wing chord, $c = 1.345$

AR (Aspect ratio) = 10

Maximum lift loading ratio - $(l/b)_{max} = 13$

Wing loading = 122.435 kg/m^2

Power loading = 7.48 (kg/hp)

(W/P)

Induced drag coefficient factor, $K = 0.0422$

Zero-drag coefficient, $C_D = 0.035$