$$\begin{aligned} & \textit{W}_{crew} \coloneqq 200 \text{ lbf} & \textit{n}_{max} \coloneqq 7 & \textit{V}_{max_sl_wo} \coloneqq 400 \text{ kn} \\ & \textit{W}_{gun} \coloneqq 2000 \text{ lbf} & \textit{ROC}_{sl} \coloneqq 10000 \frac{\text{ft}}{\text{min}} & \textit{V}_{slp} \coloneqq 375 \text{ kn} \\ & \textit{W}_{ammo} \coloneqq 2000 \text{ lbf} & \textit{V}_{stall_sl} \coloneqq 95 \text{ kn} & \textit{C}_{L\ max} \coloneqq 2.8 \end{aligned} \qquad \begin{aligned} & 21 \text{ Jun } 2025 \text{ 17:39:50 - Raymond_Initial_Sizing_Methodology.sm} \\ & \textit{V}_{itr_sl} \coloneqq 30 \frac{\text{deg}}{\text{s}} & \textit{S}_{takeoff_50ft} \coloneqq 1400 \text{ ft} \\ & \textit{S}_{landing_50ft} \coloneqq 1900 \text{ ft} \\ & \textit{V}_{slp} \coloneqq 375 \text{ kn} & \textit{M}_{cruise} \coloneqq 0.5 \end{aligned}$$

$$AR_{wet} := \frac{AR}{Swet Sref} = 3.0952$$

$$\begin{aligned} \textit{KLD} &:= 14 & & & & & & & & & \\ \textit{L}_\textit{D}_{max} &:= \textit{KLD} \cdot \sqrt{\textit{AR}_{wet}} &= 24.6306 & & & & & & & \\ \textit{C}_{fe} &:= .0035 & & & & & \\ \textit{L}_\textit{D}_{max} &:= \textit{KLD} \cdot \sqrt{\textit{AR}_{wet}} &= 24.6306 & & & & \\ \textit{C}_{D0} &:= \textit{C}_{fe} \cdot \textit{Swet}_\textit{Sref} &= 0.0074 & & \\ \end{aligned}$$

$$e_{\textit{Oswald}} := \frac{4 \cdot C_{\textit{D0}} \cdot L_{-}D_{\textit{max}}^{}}{\textit{AR} \cdot \mathbf{\pi}} = 0.8734 \qquad \qquad K := \frac{1}{\mathbf{\pi} \cdot \textit{AR} \cdot e_{\textit{Oswald}}} = 0.0561$$

State: Sea Level

$$\rho_{sl} \coloneqq 23.77 \cdot 10^{-4} \frac{\text{slug}}{\text{ft}} \ a_{sl} \coloneqq 661 \text{ kn}$$

$$V_{cruise_sl} \coloneqq M_{cruise} \cdot a_{sl} = 330.5 \text{ kn}$$

$$M_{max} \coloneqq \frac{V_{max_sl_wo}}{a_{sl}} = 0.6051$$

$$\begin{split} & \underline{W_S_{stall}} := \frac{1}{2} \cdot \rho_{sl} \cdot \left[V_{stall_sl} \right] \cdot C_{\underline{L_max}} = 85.556 \text{ psf} \\ & V_{corner} := \frac{g_e \cdot \sqrt{n_{max}} - 1}{\Psi_{itr_sl}} = 252.2345 \text{ km} \end{split}$$

$$q_{itr_sl} \coloneqq \frac{1}{2} \cdot \rho_{sl} \cdot V_{cruise_sl}^2 = 369.8183 \text{ psf}$$

$$W_{S_{itr_sl}} := \frac{q_{itr_sl} \cdot c_{L_max}}{n_{max}} = 147.9273 \frac{lbf}{ft}$$

Landing

$$S_{Landing} := 1900 \text{ ft}$$

$$S_a := 450 \text{ ft}$$

$$W_{_S_{landing}} := \left(S_{Landing} - S_a\right) \cdot \frac{C_{L_{_max}}}{80 \frac{\text{ft}}{\text{psf}}} = 50.75 \text{ psf}$$

$$\alpha := 0.648$$

$$C := 0.594$$

$$T_{\underline{W}_{max}} := \alpha \cdot M_{max} = 0.4808$$

$$T_{-}W_{max} := \alpha \cdot M_{Max}^{C} = 0.4956$$

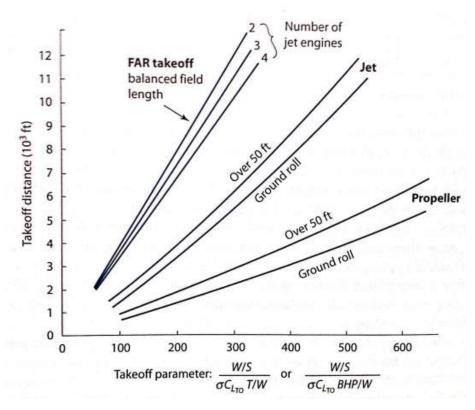
$$S_a := 450 \text{ ft}$$

$$W_{S_{takeoff}} := \left(S_{takeoff_50ft} - S_a\right) \cdot \frac{C_{L_max}}{80 \frac{ft}{psf}} = 33$$

$$a_{30k} := 589 \text{ km}$$

$$M_{slp.30k} := \frac{V_{slp}}{a_{30k}} = 0.6367$$

$$M_{\text{Max}} := M_{\text{slp.30k}}$$



$$\mathit{TOP} := 75 \ \frac{\texttt{lbf}}{\texttt{ft}} \qquad C_{\mathit{LTO}} := \frac{C_{\mathit{L_max}}}{\texttt{1.21}}$$

$$T_{W_{takeoff}} := \frac{W_{S}}{C_{LTO} \cdot TOP} = 0.2924$$

$$C_L := \frac{2 \cdot W_S}{\rho_{sl} \cdot V_{cruise \ sl}} = 0.1372$$

$$C_D := C_{DO} + K \cdot C_L^2 = 0.0084$$

$$L_{-}D := \frac{C_{L}}{C_{D}}$$

$$T_{-}W_{ROC} := \frac{1}{L_{-}D} + \frac{ROC_{sl}}{V_{cruise_sl}} = 0.36$$

Service Ceiling

$$a_{35} := 573 \text{ km}$$

$$V_{cruise_35} := M_{cruise} \cdot a_{35} = 286.5 \text{ km}$$

 $\rho_{35k} := 8.89 \cdot 10^{-4} \frac{\text{slug}}{\text{ft}}$

$$C_{L_35} := \frac{2 \cdot W_S}{\rho_{35k} \cdot V_{cruise_35}} = 0.4883$$

$$C_{D-35}^- := C_{D0}^- + K \cdot C_{L-35}^- = 0.0347$$

$$L_D_{35} := \frac{C_{L_35}}{C_{D_35}}$$

$$T_{-}W_{35} := \frac{1}{L_{-}D_{35}} + \frac{100 \frac{\text{ft}}{\text{min}}}{V_{cruise_35}} = 0.0746$$

$$T_{W_{s1}_{35}} := T_{W_{35}} \cdot \frac{\rho_{s1}}{\rho_{35k}} = 0.1994$$

$$\boxed{T_W_{ofc} := \max\left(\left[\begin{array}{cc} T_W_{s1_35} & T_W_{ROC} & T_W_{takeoff} & T_W_{max} \end{array}\right]\right) = 0.4956}$$

$$W_S_{ofc} := \min \left(\left[W_S_{itr_sl} \ W_S_{landing} \ W_S_{stall} \right] \right) = 50.75 \text{ psf}$$

$$W_{\text{quess}} := 39900 \text{ lbf}$$

$$T_{sl} := T_{ofc} \cdot W_{quess} = 19773.0648$$
 lb:

$$\overline{W_{guess}} := 39900 \text{ lbf}$$

$$\overline{T_{sl}} := \overline{T_{wofc}} \cdot \overline{W_{guess}} = 19773.0648 \text{ lbf}$$

$$S_{ref} := \frac{\overline{W_{guess}}}{\overline{W_{sofc}}} = 786.2069 \text{ ft}$$

 $D_{sl} := \frac{W_1}{\frac{C_{L_wg}}{C_{D_{slock}}}} = 10837.9556 \text{ N}$

Mission:

1. Warmup and Takeoff:

$$W_1 := W_{guess} - (10 \text{ min} \cdot 10 \% + 1 \text{ min} \cdot 100 \%) \cdot T_{sl} \cdot 0.75 \frac{1 \text{bf}}{1 \text{bf hr}} = 39405.6734 \text{ lbf}$$

2. Climb

$$C_{L_wg} := \frac{2 \cdot W_1}{\rho_{sl} \cdot V_{cruise_sl}^2 \cdot S_{ref}} = 0.1355$$

$$C_{D_{wg}} := C_{D0} + K \cdot C_{L_{wg}}^{2} = 0.0084$$

$$RC_{sl} := V_{cruise_sl} \cdot \left[T_{-}W_{ofc} - \frac{C_{D_wg}}{C_{L_wg}} \right] = 143.3495 \text{ kn}$$

$$\rho_{30k} := 10.97 \cdot 10^{-4} \frac{\text{slug}}{3}$$

$$a_{30k} := 589 \text{ kn}$$

$$V_{30k} := M_{cruise} \cdot a_{30k} = 294.5 \text{ km}$$

$$V_{30k} := M_{cruise} \cdot a_{30k} = 294.5 \text{ kn}$$

$$C_{L_wg} := \frac{2 \cdot W_1}{\rho_{30k} \cdot V_{30k}^2 \cdot S_{ref}} = 0.3699$$

$$C_{D_{_wg}} := C_{D0} + K \cdot C_{L_{_wg}}^{} ^{2} = 0.015$$

$$RC_{30k} := V_{30k} \cdot \left[T_{-}W_{ofc} \cdot \frac{\rho_{30k}}{\rho_{sl}} - \frac{C_{D_{-}wg}}{C_{L_{-}wg}} \right] = 55.3947 \text{ km}$$

$$a := \frac{RC_{30k} - RC_{sl}}{30000 \text{ ft}} = -0.0049 \text{ Hz}$$

$$t_{climb30k} := \frac{1}{a} \cdot \ln \left(\frac{RC_{30k}}{RC_{sl}} \right) = 192.1448 \text{ s}$$

$$D_{30k} := \frac{W_1}{\frac{C_{L_wg}}{C_{D_wg}}} = 7118.1692 \text{ N}$$

$$R_{\textit{climb30k}} := \frac{t_{\textit{climb30k}}}{2} \cdot \left[V_{\textit{cruise_sl}} \cdot \left[\cos \left(\text{asin} \left(\frac{RC_{sl}}{V_{\textit{cruise_sl}}} \right) \right) \right] + V_{30k} \cdot \left[\cos \left(\left(\text{asin} \left(\frac{RC_{30k}}{V_{30k}} \right) \right) \right) \right) \right] = 15.6661$$

$$W_2 := W_1 - \left(0.6 \frac{\text{lbf}}{\text{lbf hr}}\right) \cdot \left(\frac{D_{s1} + D_{30k}}{2}\right) \cdot t_{climb30k} = 39341.0375 \text{ lbf}$$

3. Cruise Out: $R_{CruiseOut} := 400 \text{ nmi}$

$$C_{L_{_wg}} := \frac{2 \cdot W_2}{\rho_{30k} \cdot V_{30k}^2 \cdot S_{ref}} = 0.3692$$

$$C_{D_wg} := C_{D0} + K \cdot C_{L_wg}^{} ^{2} = 0.015$$

$$-\left(\frac{\left(R_{CruiseOut} - R_{climb30k}\right) \cdot 0.48 \frac{\text{lbf}}{\text{lbf hr}}}{V_{30k} \cdot \frac{C_{L_wg}}{C_{D_wg}}}\right) = 3$$

4.1. Conduct Sea Level Penetration for 50NM at 375 kts.

$$M_{slp.30k} := \frac{V_{slp}}{a_{30k}} = 0.6367$$
 $M_{slp.sl} := \frac{V_{slp}}{a_{sl}} = 0.5673$

$$M_{\text{Max}} := M_{\text{slp.30k}}$$

$$T_{\underline{W}_{\max}} := \alpha \cdot M_{\underline{Max}} \overset{C}{=} 0.4956$$

$$C_{L_wg} := \frac{2 \cdot W_3}{\rho_{30k} \cdot V_{slp}^2 \cdot S_{ref}}$$

$$C_{D \ wg} := C_{D0} + K \cdot C_{L \ wg}^{2} = 0.0101$$

$$SR_{30k} := V_{slp} \cdot \left(T_{-}W_{ofc} \cdot \frac{\rho_{30k}}{\rho_{sl}} - \frac{C_{D_{-}wg}}{C_{L_{-}wg}} \right) = 68.6823 \text{ km}$$

$$C_{L_wg} := \frac{2 \cdot W_3}{\rho_{sl} \cdot V_{slp}^2 \cdot S_{ref}} = 0.1025$$

$$C_{DW\alpha} := C_{D0} + K \cdot C_{LW\alpha}^2 = 0.0079$$

$$D_{30k} := \frac{W_1}{\frac{C_{L_wg}}{C_{D_wg}}} = 3053.151 \, \mathrm{lbf}$$

$$SR_{sl} := V_{slp} \cdot \left(T_{-}W_{ofc} - \frac{C_{D_{-}wg}}{C_{L_{-}wg}} \right) = 156.7821 \text{ km}$$

$$a := \frac{SR_{s1} - SR_{30k}}{30000 \text{ ft}} = 0.005 \text{ Hz}$$

$$t_{slp} := \frac{1}{a} \cdot \ln \left(\frac{SR_{sl}}{SR_{30k}} \right) = 166.5212 \text{ s}$$

$$R_{slp} := \frac{t_{slp}}{2} \cdot \left[V_{slp} \cdot \left[\cos \left[\left(\operatorname{asin} \left(\frac{SR_{30k}}{V_{slp}} \right) \right) \right] + V_{slp} \cdot \left[\cos \left(\operatorname{asin} \left(\frac{SR_{sl}}{V_{slp}} \right) \right) \right] \right] = 16.4049 \; \mathrm{nmison}$$

$$-\left(\frac{(50 \text{ nmi}) \cdot 0.38 \frac{\text{lbf}}{\text{lbf hr}}}{V_{slp} \cdot \frac{C_{L_{wg}}}{C_{D_{wg}}}}\right) - 30000 \text{ for }$$

$$W_{_{\mathcal{I}}}:=W_{_{\mathcal{I}}}\cdot\mathbf{e}$$

4.2. Combat:

$$W_4 := W_4 - (15 \text{ min}) \cdot T_{sl} \cdot 1 \frac{\text{lbf}}{\text{lbf hr}} = 33259.3913 \text{ lbf}$$

5. Fire All:

$$W_5 := W_4 - W_{ammo} = 31259.3913$$
 lbf

6. Climb back again 35

$$V_{35k} := M_{cruise} \cdot a_{35} = 286.5 \text{ km}$$

 $D_{sl} := \frac{W_5}{\frac{C_{L_wg}}{C_{r}}} = 10267.2658 \text{ N}$

$$C_{L_wg} := \frac{2 \cdot W_5}{\rho_{sl} \cdot V_{cruise_sl}} = 0.1075$$

$$C_{D_{_Wg}} := C_{D0} + K \cdot C_{L_{_Wg}}^{2} = 0.008$$

$$RC_{sl} := V_{cruise_sl} \cdot \left(T_{_W_{ofc}} - \frac{C_{D_wg}}{C_{L_{wg}}} \right) = 139.1977 \text{ km}$$

$$C_{L_{_wg}} := \frac{2 \cdot W_5}{\rho_{35k} \cdot V_{35k}^2 \cdot S_{ref}} = 0.3825$$

$$C_{D_{_Wg}} := C_{D0} + K \cdot C_{L_{_Wg}}^{2} = 0.0156$$

$$RC_{35k} := V_{35k} \cdot \left(T_{_W_{ofc}} \cdot \frac{\rho_{35k}}{\rho_{sl}} - \frac{C_{D_wg}}{C_{L_wg}} \right) = 41.451 \text{ kn}$$

$$a := \frac{RC_{35k} - RC_{s1}}{35000 \text{ ft}} = -0.0047 \text{ Hz}$$

$$t_{climb35k} := \frac{1}{a} \cdot \ln \left(\frac{RC_{35k}}{RC_{sl}} \right) = 256.9948 \text{ s}$$

$$D_{35k} := \frac{W_5}{\frac{C_{L_wg}}{C_{D_wg}}} = 5653.9021 \text{ N}$$

$$R_{climb35k} := \frac{t_{climb35k}}{2} \cdot \left[V_{cruise_sl} \cdot \left[\cos \left(\left[a sin \left(\frac{RC_{sl}}{V_{cruise_sl}} \right] \right] \right) \right] + V_{35k} \cdot \left[\cos \left[a sin \left(\frac{RC_{35k}}{V_{35k}} \right] \right] \right] \right] = 20.818$$

$$W_6 := W_5 - \left[0.6 \frac{\text{lbf}}{\text{lbf hr}}\right] \cdot \left[\frac{D_{s1} + D_{35k}}{2}\right] \cdot t_{climb35k} = 31182.7379 \text{ lbf}$$

Cruise back

$$C_{L_{_wg}} := \frac{2 \cdot W_6}{\rho_{35k} \cdot V_{35k}^2 \cdot S_{ref}} = 0.3816$$

$$C_{D\ wg} := C_{D0} + K \cdot C_{L\ wg}^{2} = 0.0155$$

$$-\left(\frac{\left(R_{CruiseOut}-R_{climb35k}\right)\cdot 0.4\frac{1\mathrm{bf}}{1\mathrm{bf}\,\mathrm{hr}}}{V_{35k}\cdot \frac{C_{L_wg}}{C_{D_wg}}}\right)=30518.7558\,\mathrm{lb}$$

8. Loiter
$$E := 30 \text{ min}$$

$$\left(-\frac{E \cdot 0.25 \frac{\text{lbf}}{\text{lbf hr}}}{L_{D_{max}}} \right) = 30364.2658 \text{ lbf}$$

Empty Weight:

$$W_{empty} := W_8 - W_{gun} - W_{crew} = 28164.2658 \text{ lbf}$$

$$W_{Empty} := 95 \% \cdot W_{empty} = 26756.0525$$
 lbf

$$K_{_{VS}} := 1.00$$

$$W_{e} := W_{guess} \cdot \left[-.02 + 2.16 \cdot \left(\frac{W_{guess}}{1 \text{bf}} \right)^{-.1} \cdot AR^{.2} \cdot T_{-}W_{ofc} \cdot 04 \cdot \left(\frac{W_{-}S_{ofc}}{psf} \right)^{-.1} \cdot M_{Max}^{.08} \right] \cdot K_{vs} = 26711.69$$

$$\% ERROR := \left| \frac{W_{Empty} - W_{e}}{W_{e}} \right| \cdot 100 = 0.1661$$

$$W_{fuel} := W_0 - W_{Empty} = 13143.9475 \text{ lbf}$$

$$\frac{W_{fuel}}{W_{O}} = 0.3294$$

 $W_0 := W_{guess} = 39900 \text{ lbf}$

· Geometry sizing of the fuselage (starting point):

Length = aW_0^C (ft or $\{m\}$)	а	C
Sailplane—unpowered	0.86 {0.383}	0.48
Sailplane—powered	0.71 {0.316}	0.48
Homebuilt—metal/wood	3.68 {1.35}	0.23
Homebuilt—composite	3.50 {1.28}	0.23
General aviation—single engine	4.37 {1.6}	0.23
General aviation—twin engine	0.86 {0.366}	0.42
Agricultural aircraft	4.04 {1.48}	0.23
Twin turboprop	0.37 {0.169}	0.51
Flying boat	1.05 {0.439}	0.40
Jet trainer	0.79 {0.333}	0.41
Jet fighter	0.93 {0.389}	0.39
Military cargo/bomber	0.23 {0.104}	0.50
Jet transport	0.67 {0.287}	0.43

$$L_{f} := \left[0.93 \text{ ft} \cdot \left(\frac{W_{guess}}{1 \text{ bf}}\right)^{0.39}\right] = 57.9245 \text{ ft}$$

$$\boxed{W_{Eng} := 3700 \text{ lbf}}$$

$$\boxed{ENGINE := GE_CF34_10E}$$

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Created 21 Jun 2025 17:39:50 - Raymond Initial Sizing Methodology.sm (Created using a ree version of Swath Studio C_{nasa\_sc2} := 6 \text{ m} = 19.685 \text{ ft}
```

$$\begin{aligned} & \textit{W}_{\textit{Bod}} \coloneqq \texttt{0.44} \cdot \left(\textit{W}_{\textit{Empty}} - \textit{W}_{\textit{Eng}} \right) = \texttt{10144.6631 \, lbf} \\ & \textit{W}_{\textit{Wing}} \coloneqq \texttt{0.34} \cdot \left(\textit{W}_{\textit{Empty}} - \textit{W}_{\textit{Eng}} \right) = \texttt{7839.0579 \, lbf} \\ & \textit{W}_{\textit{Tail}} \coloneqq \texttt{0.12} \cdot \left(\textit{W}_{\textit{Empty}} - \textit{W}_{\textit{Eng}} \right) = \texttt{2766.7263 \, lbf} \end{aligned} \qquad \begin{aligned} & c_{\textit{nasa_sc2}} \coloneqq \texttt{6 \, m} = \texttt{19.685 \, ft} \\ & \textit{wing_cg}_{\textit{nasa_sc2}} \coloneqq \texttt{0.40} \cdot c_{\textit{nasa_sc2}} = \texttt{7.874 \, ft} \\ & \textit{W}_{\textit{Tail}} \coloneqq \texttt{0.12} \cdot \left(\textit{W}_{\textit{Empty}} - \textit{W}_{\textit{Eng}} \right) = \texttt{2766.7263 \, lbf} \end{aligned}$$

$$ScaleFactor := \frac{\textit{W}_{\textit{0}}}{\left(\textit{W}_{\textit{Bod}} + \textit{W}_{\textit{Wing}} + \textit{W}_{\textit{Tail}} + \textit{W}_{\textit{Eng}} + \textit{W}_{\textit{LG}} + \textit{W}_{\textit{fuel}}\right)} = 1$$

$$X_{Gun} := 11 \% \cdot L_f = 6.3717 \text{ ft}$$

$$X_{Crew} := 13.8 \% \cdot L_f = 7.9936 \text{ ft}$$

 $W_{LG} := 0.1 \cdot (W_{Empty} - W_{Eng}) = 2305.6053 \text{ lbf}$

$$X_{Amm0} := 20.8 \% \cdot L_f = 12.0483 \text{ ft}$$

$$X_{Bod} := 39 \% \cdot L_f = 22.5906 \text{ ft}$$

$$X_{Wing} := 55.9 \% \cdot L_f = 32.3798 \text{ ft}$$

$$X_{Tail} := 89.9 \% \cdot L_f = 52.0741 \text{ ft}$$

$$X_{Enq} := 87 \% \cdot L_f = 50.3943 \text{ ft}$$

$$X_{Fuel} := 34.1 \; \% \cdot L_f = 19.7523 \; \mathrm{ft}$$

$$X_{LG1} := 20 \% \cdot L_f = 11.5849 \text{ ft}$$

$$X_{LG2} := 65 \% \cdot L_f = 37.6509 \text{ ft}$$

$$\mathbf{x}_{cg_wo} := \frac{\left(\mathbf{W}_{crew} \right) \cdot \left(\mathbf{X}_{Crew} \right) + \mathbf{W}_{ammo} \cdot \left(\mathbf{X}_{Amm0} \right) + \mathbf{W}_{Bod} \cdot \left(\mathbf{X}_{Bod} \right) + \mathbf{W}_{Wing} \cdot \left(\mathbf{X}_{Wing} \right) + \mathbf{W}_{Tail} \cdot \left(\mathbf{X}_{Tail} \right) + \mathbf{W}_{Eng} \cdot \left(\mathbf{X}_{Eng} \right) - \mathbf{W}_{Crew} \cdot \left(\mathbf{X}_{Crew} \right) + \mathbf{W}_{ammo} \cdot \left(\mathbf{X}_{Eng} \right) - \mathbf{W}_{Crew} \cdot \left(\mathbf{X}_{Crew} \right) + \mathbf{W}_{Crew} \cdot \left(\mathbf{X}_{Eng} \right) - \mathbf{W}_{Eng} \cdot \left(\mathbf{X}_{Eng} \right) - \mathbf{W}_{Crew} \cdot \left(\mathbf{X}_{Eng} \right) - \mathbf{W}_{Eng} \cdot \left(\mathbf{X}_{Eng} \right)$$

$$x_{cg_wo} = 26.7204 \text{ ft}$$

$$\frac{x_{\rm CG_WO}}{L_{\rm f}} = 46.1298~\%$$

$$Z_{Crew} := 5.87 \text{ ft}$$

$$Z_{Gun} := 1.58 \text{ ft}$$

$$Z_{Ammo} := 2.57 \text{ ft}$$

$$Z_{Bod} := 2.8 \text{ ft}$$

$$Z_{LG} := 1.22 \text{ ft}$$

$$Z_{Fuel} := 2.90 ft$$

$$Z_{Wing} := 2.30 \text{ ft}$$

$$Z_{Eng} := 7.43 \text{ ft}$$

$$Z_{HT} := 3.49 \text{ ft}$$

$$Z_{VT} := 5.87 \text{ ft}$$

$$x_{cg_wo} - X_{Wing} = -5.6594 \text{ ft}$$

$$z_{cg_wo} \coloneqq \frac{\left(\textit{W}_{\textit{crew}} \right) \cdot \left(\textit{Z}_{\textit{Crew}} \right) + \textit{W}_{\textit{ammo}} \cdot \left(\textit{Z}_{\textit{Ammo}} \right) + \textit{W}_{\textit{Bod}} \cdot \left(\textit{Z}_{\textit{Bod}} \right) + \textit{W}_{\textit{Wing}} \cdot \left(\textit{Z}_{\textit{Wing}} \right) + \frac{\textit{W}_{\textit{Tail}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \textit{W}_{\textit{Eng}} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \textit{W}_{\textit{Eng}} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{Wing}} \right) + \frac{\textit{W}_{\textit{Tail}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \textit{W}_{\textit{Eng}} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Crew}}}{2} \cdot \left(\textit{Z}_{\textit{HT}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{Eng}} \right) + \frac{\textit{W}_{\textit{Eng}}}{2} \cdot \left(\textit{Z}_{\textit{E$$

$$MAC_{1} = \overline{c}_{1} = \frac{2}{3}c_{R_{1}} \frac{(1 + \lambda_{1} + \lambda_{1}^{2})}{(1 + \lambda_{1})}, \quad MAC_{2} = \overline{c}_{2} = \frac{2}{3}c_{R_{2}} \frac{(1 + \lambda_{2} + \lambda_{2}^{2})}{(1 + \lambda_{2})}$$
$$MAC = \overline{c} = \frac{(\overline{c}_{1} \cdot S_{1}) + (\overline{c}_{2} \cdot S_{2})}{S}$$

$$b_1 := 24 \text{ ft}$$
 $b_2 := 22 \text{ ft}$

$$c_{T1} := 18 \text{ ft}$$
 $c_{T2} := 16 \text{ ft}$

$$c_{\pi 2} := 16 \text{ ft}$$

$$C_T := C_{T}$$

$$b := b_1 + b_2 = 46 \text{ ft}$$

$$\boldsymbol{c}_{R1} := \boldsymbol{c}_{T1}$$

$$c_{R1} := c_{T1}$$
 $c_{R2} := c_{R1} = 18 \text{ ft}$

$$\Lambda_{LE1} := 0 \deg$$

$$\lambda_1 := \frac{c_{T1}}{c_{R1}} = 1$$
 $\lambda_2 := \frac{c_{T2}}{c_{R2}} = 0.8889$

$$\Lambda_{LE2} := \operatorname{atan}\left(\frac{2 \text{ ft}}{16 \text{ ft}}\right) = 7.125 \text{ deg}$$
 $\lambda_{ht} := 1$

$$S_1 := \frac{b_1}{2} \cdot c_{R1} \cdot (1 + \lambda_1) = 432 \text{ ft}^2$$

$$S_2 := \frac{b_2}{2} \cdot c_{R2} \cdot (1 + \lambda_2) = 374 \text{ ft}^2$$

$$S := S_1 + S_2 = 806 \text{ ft}^2$$
 $S_{ref} = 786.2069 \text{ ft}^2$

$$S > S_{ref} = 1$$

$$S > S_{ref} = 1$$

$$\lambda := \text{solve} \left(\frac{2 \cdot S}{b \cdot c_T} - \left(\frac{1}{\lambda} + 1 \right), \lambda, 0.01, 1.0 \right) = 0.8402$$

$$AR_{act} := \frac{b}{S} = 2.6253$$

$$c_R := \frac{c_T}{\lambda} = 19.0435 \text{ ft}$$

$$\Lambda_{LE} := \operatorname{atan} \left(\frac{\operatorname{tan} \left(\Lambda_{LE1} \right) \cdot S_1 + \operatorname{tan} \left(\Lambda_{LE2} \right) \cdot S_2}{S} \right) = 3.3196 \operatorname{deg} \left[c_{bar.2} := \frac{2}{3} \cdot c_{R2} \cdot \left(\frac{1 + \lambda_2 + \lambda_2}{1 + \lambda_2} \right) \right] = 17.0196 \operatorname{ft}$$

$$c_{bar} := \frac{2}{3} \cdot c_R \cdot \left(\frac{1 + \lambda + \lambda^2}{1 + \lambda} \right) = 17.5658 \text{ ft}$$

$$y_{\textit{mac}} := \frac{b}{6} \cdot \left(\frac{1 + 2 \cdot \lambda}{1 + \lambda} \right) = 11.1671 \text{ ft}$$

$$AR_{act} := \frac{b^2}{S} = 2.6253$$

$$c_{bar.1} \coloneqq \frac{2}{3} \cdot c_{RI} \cdot \left(\frac{1 + \lambda_1 + \lambda_1^2}{1 + \lambda_1}\right) = 18 \text{ ft}$$

$$c_{bar.2} := \frac{2}{3} \cdot c_{R2} \cdot \left(\frac{1 + \lambda_2 + \lambda_2^{2}}{1 + \lambda_2} \right) = 17.0196 \text{ ft}$$

$$c_{bar.0} \coloneqq \frac{c_{bar.1} \cdot s_1 + c_{bar.2} \cdot s_2}{s} = 17.5451 \; \text{ft}$$

$$l_{H} := X_{Tail} - X_{CQWO} = 25.3537 \text{ ft}$$

$$C_{RH} := 8 \text{ ft}$$

$$C_{TH} := C_{RH} = 8 \text{ ft}$$

$$S_{H} := \frac{0.3 \cdot S_{ref} \cdot (Y_{mac})}{I_{H}} = 103.8859 \text{ ft}^{2}$$

$$b_{H} := \frac{S_{H}}{C_{RH}} = 12.9857 \text{ ft}$$

$$c_{bar_ht} := \frac{2}{3} \cdot c_{RH} \cdot \left(\frac{1 + \lambda_{ht} + \lambda_{ht}^{2}}{1 + \lambda_{ht}} \right) = 8 \text{ ft}$$

$$y_{mac_ht} := \frac{b_H}{6} \cdot \left(\frac{1 + 2 \cdot \lambda_{ht}}{1 + \lambda_{ht}} \right) = 3.2464 \text{ ft}$$

$$\mathbf{x}_{\mathit{mac_ht}} := \mathbf{y}_{\mathit{mac}} \cdot \mathrm{tan} \left(\mathbf{\Lambda}_{\mathit{LE}} \right) = \mathrm{0.6477 \ ft}$$

$$V_{H} := \frac{S_{H} \cdot l_{H}}{S_{ref} \cdot \left(\frac{c_{T1} + c_{T2}}{2}\right)} = 0.1971$$

$$x_{ac} := x_{mac} + .25 \cdot c_{bar} = 5.0392 \text{ ft}$$

$$x_{nose2_LE} := 47 \% \cdot L_f = 27.2245 \text{ ft}$$

$$x_{ac} := x_{ac} + x_{nose2_LE} = 32.2637 \text{ ft}$$

$$\frac{x_ac}{L_f} = 55.6995 \%$$
 $\frac{x_{cg_wo}}{L_f} = 46.1298 \%$

$$x_{cg\ wo} - x_{ac} = -5.5432 \text{ ft}$$

$$static_margen_{withAmmo} := \left| \frac{x_{cg_wo} - x_ac}{c_{bar}} \right| = 31.557 \%$$

$$x_{cg}_{noammo} := \frac{\left(\textit{W}_{\textit{crew}} \right) \cdot \left(\textit{X}_{\textit{Crew}} \right) + \textit{W}_{\textit{Bod}} \cdot \left(\textit{X}_{\textit{Bod}} \right) + \textit{W}_{\textit{Wing}} \cdot \left(\textit{X}_{\textit{Wing}} \right) + \textit{W}_{\textit{Tail}} \cdot \left(\textit{X}_{\textit{Tail}} \right) + \textit{W}_{\textit{Eng}} \cdot \left(\textit{X}_{\textit{Eng}} \right) + \textit{W}_{\textit{fuel}} \cdot \left(\textit{X}_{\textit{Fing}} \right) + \textit{W}_{\textit{Crew}} + \textit{W}_{\textit{gun}} + \textit{W}_{\textit{gun}} + \textit{W}_{\textit{gun}} + \textit{W}_{\textit{Crew}} + \textit{W}_{\textit{gun}} + \textit{W}_{\textit{Crew}} + \textit{W}_{\textit{gun}} + \textit{W}_{\textit{Crew}} + \textit{Crew} + \textit{W}_{\textit{Crew}} + \textit{Crew} + \textit{Cre$$

$$x_cg_{noammo} - x_ac = -4.8462 \text{ ft}$$

$$Z_{ac} := \frac{Z_{Wing} \cdot S + Z_{HT} \cdot S_{H}}{S + S_{H}} = 2.4359 \text{ ft}$$

$$1_v := X_{Tail} - X_{cg_wo} = 25.3537 \text{ ft}$$

$$S_v := 0.15 \cdot S_H = 15.5829 \text{ ft}^2$$

$$V_{v} := \frac{S_{v} \cdot I_{v}}{S_{vof} \cdot b} = 0.0109$$

$$x_{cg}_{NoAmo_NoFuel} := \frac{\left(\textit{W}_{\textit{crew}} \right) \cdot \left(\textit{X}_{\textit{Crew}} \right) + \textit{W}_{\textit{Bod}} \cdot \left(\textit{X}_{\textit{Bod}} \right) + \textit{W}_{\textit{Wing}} \cdot \left(\textit{X}_{\textit{Wing}} \right) + \textit{W}_{\textit{Tail}} \cdot \left(\textit{X}_{\textit{Tail}} \right) + \textit{W}_{\textit{Eng}} \cdot \left(\textit{X}_{\textit{Eng}} \right) + \left(\frac{1}{3} \cdot \textit{W}_{\textit{Crew}} \right) +$$

$$x_cg_{NoAmo_NoFuel} - x_ac = -1.3668 ft$$

$$static_margen_{withOutAmmoNoFuel} := \left| \frac{x_cg_{NoAmo_NoFuel} - x_ac}{c_{bar}} \right| = 7.781 \%$$