ME 441: FEM Homework Assignment 3

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December 2023

Problem 1

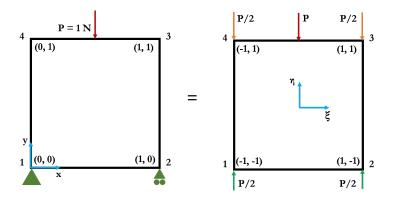


Figure 1: Q4 element

Here,

$$\begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ x_3 & y_3 \\ x_4 & y_4 \end{bmatrix}_{4 \times 2} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 1 & 1 \\ 0 & 1 \end{bmatrix}_{4 \times 2}$$

Jacobian Matrix,
$$[J]_{2\times 2} = \frac{1}{4} \begin{bmatrix} -(1-\eta) & (1-\eta) & (1+\eta) & -(1+\eta) \\ -(1-\xi) & -(1+\xi) & (1+\xi) & (1-\xi) \end{bmatrix}_{2\times 4} \begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ x_3 & y_3 \\ x_4 & y_4 \end{bmatrix}_{4\times 2}$$

$$=\frac{1}{4}\begin{bmatrix} -(1-\eta) & (1-\eta) & (1+\eta) & -(1+\eta) \\ -(1-\xi) & -(1+\xi) & (1+\xi) & (1-\xi) \end{bmatrix} \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 1 & 1 \\ 0 & 1 \end{bmatrix}$$

 $[J]_{2\times 2} = \begin{bmatrix} 0.5 & 0 \\ 0 & 0.5 \end{bmatrix}$ Now,

$$[\mathbf{J}]_{2\times 2}^{-1} = \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix} \quad \text{and} \quad |J| = \frac{1}{4}$$

$$[\alpha]_{3\times 4} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 1 & 1 & 0 \end{bmatrix}$$

$$[\beta]_{4\times 4} = \begin{bmatrix} [J]_{2\times 2}^{-1} & [0]_{2\times 2} \\ [0]_{2\times 2} & [J]_{2\times 2}^{-1} \end{bmatrix}$$

$$[\gamma]_{4\times 8} = \frac{1}{4} \begin{bmatrix} -1+\eta & 0 & 1-\eta & 0 & 1+\eta & 0 & -1-\eta & 0 \\ -1+\xi & 0 & -1-\xi & 0 & 1+\xi & 0 & 1-\xi & 0 \\ 0 & -1+\eta & 0 & 1-\eta & 0 & 1+\eta & 0 & -1-\eta \\ -0 & -1+\xi & 0 & -1-\xi & 0 & 1+\xi & 0 & 1-\xi \end{bmatrix}$$

$$[\mathbf{B}]_{3\times 8} = [\alpha]_{3\times 4} [\beta]_{4\times 4} [\gamma]_{4\times 8} \qquad [K]_{8\times 8} = \int_{-1}^{1} [B]_{8\times 3}^{T} [E]_{3\times 3} [B]_{3\times 8} t |J| \, d\xi d\eta$$

$$[B]_{3\times8} = \begin{bmatrix} \frac{\eta}{2} - \frac{1}{2} & 0 & \frac{1}{2} - \frac{\eta}{2} & 0 & \frac{\eta}{2} + \frac{1}{2} & 0 & -\frac{\eta}{2} - \frac{1}{2} & 0 \\ 0 & \frac{\xi}{2} - \frac{1}{2} & 0 & -\frac{\xi}{2} - \frac{1}{2} & 0 & \frac{\xi}{2} + \frac{1}{2} & 0 & \frac{1}{2} - \frac{\xi}{2} \\ \frac{\xi}{2} - \frac{1}{2} & \frac{\eta}{2} - \frac{1}{2} & -\frac{\xi}{2} - \frac{1}{2} & \frac{1}{2} - \frac{\eta}{2} & \frac{\xi}{2} + \frac{1}{2} & \frac{\eta}{2} + \frac{1}{2} & \frac{1}{2} - \frac{\xi}{2} & -\frac{\eta}{2} - \frac{1}{2} \end{bmatrix}$$

$$[\mathbf{K}]_{8\times 8} = \int_{-1}^{1} [B]_{8\times 3}^{T} [E]_{3\times 3} [B]_{3\times 8} t |J| \, d\xi d\eta = \int_{-1}^{1} [\mathrm{integrand}]_{8\times 8} \, d\xi d\eta$$

Using 2nd order Gauss Quadrature to solve the integral:

$$[K]_{8\times8} = \begin{pmatrix} \frac{5000}{9} & 250 & -\frac{3500}{9} & \frac{250}{3} & -\frac{2500}{9} & -250 & \frac{1000}{9} & -\frac{250}{3} \\ 250 & \frac{5000}{9} & -\frac{250}{3} & \frac{1000}{9} & -250 & -\frac{2500}{9} & \frac{250}{3} & -\frac{3500}{9} \\ -\frac{3500}{3} & -\frac{250}{3} & \frac{5000}{9} & -250 & \frac{1000}{9} & \frac{250}{3} & -\frac{2500}{9} & 250 \\ \frac{250}{3} & \frac{1000}{9} & -250 & \frac{5000}{9} & -\frac{250}{3} & -\frac{3500}{9} & 250 & -\frac{2500}{9} \\ -\frac{2500}{9} & -250 & \frac{1000}{9} & -\frac{250}{3} & \frac{5000}{9} & 250 & -\frac{3500}{9} & \frac{250}{3} \\ -250 & -\frac{2500}{9} & \frac{250}{3} & -\frac{3500}{9} & 250 & \frac{5000}{9} & -\frac{250}{3} & \frac{1000}{9} & -\frac{250}{3} & \frac{5000}{9} & -\frac{250}{3} & \frac{5000}{9} & -\frac{250}{3} \end{pmatrix}_{8\times8}$$

Now,

$$[K]_{8\times8}\{d\}_{8\times1} = \{F\}_{8\times1}$$

Applying boundary conditions,

$$[\mathbf{K}]_{8\times 8} \xrightarrow{\mathrm{apply \ BC}} [K]_{5\times 5}$$
 (eliminating rows and columns to match with $\{d\} and \{F\})$

$$\{d\}_{5\times 1} = [K]_{5\times 5}^{-1} \{F\}_{5\times 1}$$

$$\begin{cases} u_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{cases} = \begin{cases} 0.0005 \\ 0.0005 \\ -0.001 \\ 0 \\ -0.001 \end{cases}$$

Listing 1: Nodal displacements of a Q4 element with one mesh

```
%% FEM, HW 3, Problem 1
  %% Afnan Mostafa
%% 11/28/2023
3
4
5
6
  clc
   c \, l \, e \, a \, r
   close all
   rng('shuffle')
  14
   E_0 = 1e6;
   nu = 0.5;
16
17
   t = 0.001;
  18
   syms n e x y u2 u3 v3 u4 v4
  %%
  %%%%%%%%
26
27
28
29
30
31
             #1
  %%%%%%
33
34
35
36
  38
  xyMat = [0 \ 0; \ 1 \ 0; \ 1 \ 1; \ 0 \ 1];
39
  40
41
  \% \ \text{xyMat} \ = \ [\, -0.5 \ \ -0.5; \ \ 0.5 \ \ \ -0.5; \ \ 0.5 \ \ 0.5; \ \ -0.5 \ \ 0.5 \,]\,;
42
44
  45
   \begin{array}{lll} J &=& 1/4* \big[ -(1-n) & (1-n) & (1+n) & -(1+n) \, ; \\ & & -(1-e) & -(1+e) & (1+e) & (1-e) \, \big] * xyMat \, ; \\ inv J &=& inv \, (J) \, ; \end{array}
46
47
49
50
   Zer = zeros(size(invJ));
   alphaMat = [1 \ 0 \ 0 \ 0; \ 0 \ 0 \ 1; \ 0 \ 1 \ 1 \ 0];
  56
   betaMat = [[invJ] [Zer]; [Zer] [invJ]];
```

```
62
       0 -1+n 0 1-n 0 1+n 0 -1-n;
63
       0 - 1 + e \ 0 - 1 - e \ 0 \ 1 + e \ 0 \ 1 - e \ ];
   B = alphaMat*betaMat*gammaMat;
69
    B_{-t} = transpose(B);
   E = (E_0/(1-(nu)^2))*[1 nu 0; nu 1 0; 0 0 (1-nu)/2];
   76
77
78
79
    integrand = eval(B_t*E*B*t*det(J));
   80
81
    gaussPoints = [-1/sqrt(3) -1/sqrt(3);
       1/sqrt(3) -1/sqrt(3)
1/sqrt(3) 1/sqrt(3)
82
83
84
       -1/sqrt(3) 1/sqrt(3);
85
86
    for i=1:length(integrand)
87
       for j=1:length(integrand)
88
           func = integrand(i,j);
89
           c = 0;
90
           for k=1:4
             e = gaussPoints(k,1);
n = gaussPoints(k,2);
gq(k) = eval(subs(func));
93
94
           integral(i,j) = gq(1)+gq(2)+gq(3)+gq(4);
96
97
   end
98
99
   100
    disp = [0;0;u2;0;u3;v3;u4;v4];
    force = [0;0.5;0;0.5;0;-0.5;0;-0.5];
   \begin{array}{l} {\rm disp\_BC} = \, [\, u2\,; u3\,; v3\,; u4\,; v4\,]\,; \\ {\rm force\_BC} \, = \, [\, 0\,; 0\,; -0\,.5\,; 0\,; -0\,.5\,]; \\ {\rm new\_integral} \, = \, {\rm integral}\,; \end{array}
106
   new_integral(:,1) =
113
    new_integral(:,1) =
114
    new\_integral(:,2) =
    new\_integral(1,:) =
    new_integral(1,:) =
    new_integral(2,:) =
118
119
   120
    nod_disp = inv(new_integral)*force_BC;
    allDisp = [
       0 0; nod_disp(1) 0; nod_disp(2) nod_disp(3); nod_disp(4) nod_disp(5)
          ];
    \begin{array}{l} [\,id\_v\,] \ = \ find\,(ismember\,(abs\,(allDisp\,(:\,,2)\,)\,), \ max\,(abs\,(allDisp\,(:\,,2)\,)))); \\ [\,id\_u\,] \ = \ find\,(ismember\,(abs\,(allDisp\,(:\,,1)\,)\,), \ max\,(abs\,(allDisp\,(:\,,1)\,)))); \end{array} 
128
   sprintf('Max Vertical displacement occurs at node %d: %0.4f units', id_v
```

```
, allDisp(id_v ,2)) sprintf('Max Horizontal displacement occurs at node %d: %0.4f units', id_u, allDisp(id_u,1))
134
        %%
        %
%
136
       %%%%%%
138
140
                              #1
141
       %
%
       %
%
146
147
148
       \%\% %%%%%%%%%% plot original and deformed systems \%\%\%\%\%\%\%\%\%
        plotDeform\!=\!1;
        if plotDeform
               hold on
              hold on
% plots the original system
11 = line([0,1],[0,0], 'LineWidth',3,'Color','k');
line([1,1],[0,1],'LineWidth',3,'Color','k');
line([0,0],[0,1],'LineWidth',3,'Color','k');
line([1,0],[1,1],'LineWidth',3,'Color','k');
x = [0; 1; 1; 0; 0];
y = [0; 0; 1; 1; 0];
disp y = [0, 0; 1; 1]; ellDisp(2,1); ellDisp(3,1);
158
               \operatorname{disp\_u} = [\operatorname{allDisp}(1,1); \operatorname{allDisp}(2,1); \operatorname{allDisp}(3,1); \operatorname{allDisp}(4,1);
                      allDisp (1,1)]
               disp_v = [allDisp(1,2); allDisp(2,2); allDisp(3,2); allDisp(4,2);
                       allDisp (1,2);
164
               defX = x + disp_u;
               defY = y + disp_v;
               box on
               % plots the deformed system
              % plots the deformed system
p1 = plot(defX, defY, 'r-', 'LineWidth', 1.5);
set(gca, 'FontName', 'Garamond', 'FontSize', 18, 'FontWeight', 'bold',...
'LineWidth', 2, 'XMinorTick', 'off',...
'YMinorTick', 'off', 'GridAlpha', 0.07,...
'GridLineStyle', '--', 'LineWidth', 2);
title('Deformation Plot in Real Space (global coordinate system)');
whele (YY).
169
               xlabel('X');
ylabel('Y');
               legend ([l1 p1], { 'Original System', 'Deformed System'}, 'Location', '
                      southeast',...
'Color',[0.941176470588235 0.941176470588235 0.941176470588235])
178
               % set(gcf, 'units', 'points', 'position', [100,100,1024,700])
        end
180
181
```

Output of the code:

Max Vertical displacement occurs at nodes 3 and 4: -0.001 units. Max Horizontal displacement occurs at nodes 2 and 3: 0.0005 units

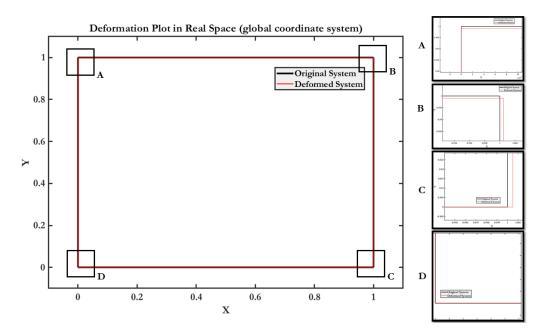


Figure 2: Deformation Plot of Q4 single element

Problem 2

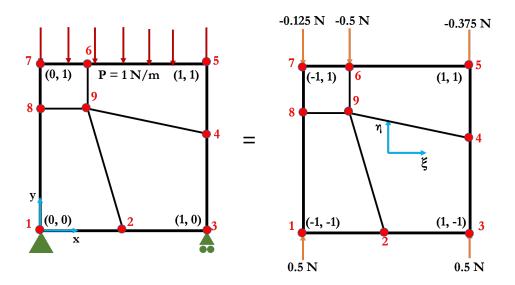


Figure 3: Q4 element with 4 meshes

Algorithm for solving for displacements when 4 Q4 elements are considered:

1. Get $[J]_{2\times 2}$ for each element using:

$$[J]_{2\times 2} = \frac{1}{4} \begin{bmatrix} -(1-\eta) & (1-\eta) & (1+\eta) & -(1+\eta) \\ -(1-\xi) & -(1+\xi) & (1+\xi) & (1-\xi) \end{bmatrix}_{2\times 4} \begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ x_3 & y_3 \\ x_4 & y_4 \end{bmatrix}_{4\times 2},$$

where $\begin{bmatrix} x & y \end{bmatrix}$ is different for each element.

2. Solve for integrand using **IntegrandStiffMatQ4.m** (see Appendix B) function (for each element),

$$[B]_{8\times3}^T[E]_{3\times3}[B]_{3\times8}|J|t = [\text{integrand}]_{8\times8}$$

3. Use Gauss Quadrature (GaussQuadQ4.m) (see Appendix C) to get the integral (or elemental stiffness matrix) for each element:

$$[K]_{8\times 8} = \int_{-1}^{1} [B]_{8\times 3}^{T} [E]_{3\times 3} [B]_{3\times 8} t |J| \, d\xi d\eta = \int_{-1}^{1} [\text{integrand}]_{8\times 8} \, d\xi d\eta$$

4. Globalize element stiffness matrices, $[K_i]_{8\times 8}$; i=1,2,3,4 (no of elements) (globalizeStiffMat.m) (see Appendix D) and add them to get the global stiffness matrix [K]

$$[K_i]_{8\times 8} \xrightarrow{\text{globalize}} [\mathbf{K}_i]_{18\times 18}$$

$$[\mathbf{K}_{\mathrm{struc}}]_{18 \times 18} = \sum_{i=1}^{4} [\mathbf{K}_i]_{18 \times 18}$$

5. Apply boundary conditions (3 BCs, hence 3 rows and columns are dropped)

$$[\mathbf{K}_{\mathrm{struc}}]_{18 \times 18} \xrightarrow{\mathrm{apply \ BC}} [\mathbf{K}_{\mathrm{struc}}]_{15 \times 15}$$

6. Solve for nodal displacements using:

$$[\mathbf{K}_{\text{struc}}]_{15\times15}\{d\}_{15\times1} = \{F\}_{15\times1} \qquad \{d\}_{15\times1} = [\mathbf{K}_{\text{struc}}]_{15\times15}^{-1}\{F\}_{15\times1}$$

$$\left\{d\right\}_{15\times1} = \left\{ \begin{array}{l} u_2 \\ v_2 \\ u_3 \\ u_4 \\ v_4 \\ v_5 \\ v_5 \\ v_6 \\ v_6 \\ v_7 \\ v_7 \\ u_8 \\ v_8 \\ u_9 \\ v_9 \end{array} \right\} = \left\{ \begin{array}{l} 0.0005 \\ -0.001 \\ 0.0008 \\ 0.0006 \\ -0.0011 \\ 0.0007 \\ -0.0015 \\ 0.0003 \\ -0.0015 \\ 0.0002 \\ -0.0016 \\ 0.0003 \\ -0.0014 \\ 0.0004 \\ -0.0013 \end{array} \right\}$$

It is evident from the two problems described above that using more elements will change the results a bit but they should be close to each other (as can be seen here as well)

Que	Max. Horizontal Displacement, u_{max}	Max. Vertical Displacement, v_{max}
1	+0.0005 (nodes 2, 3)	-0.0010 (nodes 3, 4)
2	+0.0008 (node 3 = node 2 in que 1)	-0.0016 (node 7 = node 3 in que 1)

Listing 2: Nodal displacements of a Q4 element with 4 element meshes

```
rng('shuffle')
18
     19
20
     E_-0 = 1e6;
     nu = 0.5;
     t = 0.001;
     25
26
     syms n e x y u2 v2 u3 v3 u4 v4 u5 v5 u6 v6 u7 v7 u8 v8 u9 v9 X Y
27
     28
30
     elements = 4;
     order = 2;
     totNodes = 9;
      \begin{array}{l} {\rm xyMat} = \left[ \begin{smallmatrix} 0 & 0.75 ; & 0.25 & 0.75 ; & 0.25 & 1; & 0 & 1 \end{smallmatrix} \right]; \\ {\rm xyMat2} = \left[ \begin{smallmatrix} 0 & 0; & 0.5 & 0; & 0.25 & 0.75 ; & 0 & 0.75 \end{smallmatrix} \right]; \\ {\rm xyMat3} = \left[ \begin{smallmatrix} 0.5 & 0; & 1 & 0; & 1 & 0.6; & 0.25 & 0.75 \end{smallmatrix} \right]; \\ {\rm xyMat4} = \left[ \begin{smallmatrix} 0.25 & 0.75 ; & 1 & 0.6; & 1 & 1; & 0.25 & 1 \end{smallmatrix} \right]; \\ \end{array} 
34
36
38
     40
41
     xy = cell(1,4);
     xy {1,1} = xyMat;
xy {1,2} = xyMat2;
xy {1,3} = xyMat3;
42
43
44
45
     xy\{1,4\} = xyMat4;
46
     47
     kmat_all = cell(1,elements);
intgrd_all = cell(1,elements);
     %% %%%%% function callback: to get elemental stiff mat. %%%%%%%
     %auxiliary function files
     for p=1:elements
             \begin{bmatrix} [integrand \ ,B,B_-t] = IntegrandStiffMatQ4(xy\{1,p\},t,E_-0,nu,0,1); \\ [intgrd_all \{1,p\} = integrand; \\ [stiffMat] = GaussQuadQ4(order,intgrd_all \{1,p\}); \\ \end{bmatrix} 
56
57
58
           kmat_all\{1,p\} = stiffMat;
     end
     62
63
64
     %
%
     %
               #1
                             #4
    %
%
70
     %
%
%
71
72
73
74
75
76
77
78
               #2
                               #3
     %
                                     _ 3
     %
     %
                                     00__
     \% order of nodes in an element matter
     ele1 = [8, 9, 6, 7];
ele2 = [1, 2, 9, 8];
80
81
     ele3 = [2,3,4,9];
ele4 = [9,4,5,6];
82
83
85
     {\tt nod\_ele} \ = \ [\ {\tt ele1}\ ; \ \ {\tt ele2}\ ; \ \ {\tt ele3}\ ; \ \ {\tt ele4}\ ]\ ;
86
87
     % function callback for globalization
     for u=1:elements
89
           [\,mat\_cp\,] \ = \ globalizeStiffMat\,(\,kmat\_all\,\{1\,,u\}\,,nod\_ele\,(\,u\,,:\,)\ ,4\,,9\,,2\,)\,;
```

```
\mathtt{stiffMatSet}\left\{\mathtt{u}\,,\mathtt{1}\right\} \;=\; \mathtt{mat\_cp}\,;
90
    end
93
    globalMat = zeros(size(mat_cp));
94
    for v=1:elements
95
        globalMat \ = \ globalMat \ + \ stiffMatSet\{v\,,1\}\,;
96
97
    end
98
99
    100
    \% \text{ disp } = [0;0;u2;v2;u3;0;u4;v4;u5;v5;u6;v6;u7;v7;u8;v8;u9;v9];
    % force =
        [0;0.25;0;0.5;0;0.25;0;-0.125;0;-0.75/2;0;-0.5;0;-0.25/2;0;0.1250;0;+0.5];
    disp = [0;0;u2;v2;u3;0;u4;v4;u5;v5;u6;v6;u7;v7;u8;v8;u9;v9];
    force = [0;0.5;0;0;0;0.5;0;0;0;-0.75/2;0;-0.5;0;-0.25/2;0;0;0];
106
    % solved by hand
109
    % solved by hand disp_BC = [u2;v2;u3;u4;v4;u5;v5;u6;v6;u7;v7;u8;v8;u9;v9]; force_BC = [0;0;0;0;0;0;0;-0.75/2;0;-0.5;0;-0.25/2;0;0;0;0];
    new\_integral = globalMat;
    116
    % dynamic deletion (matrix index changes with each progressive line)
    118
        mod. matrix
    new\_integral(:,4) = []; \% delete 4th column (6th col. of original) of
        mod. matrix
    new_integral(1,:) = []; % same as above but for rows
    new_integral(1,:) =
    new_integral(4,:) = [];
    126
    nod_disp = new_integral\force_BC;
128
    129
130
    allDisp = [0 \ 0; \ nod\_disp(1) \ nod\_disp(2); \ nod\_disp(3) \ 0; \ nod\_disp(4)
        nod_disp(5); .
        nod_disp(6) nod_disp(7); nod_disp(8) nod_disp(9); nod_disp(10)
        nod_disp(11); nod_disp(12) nod_disp(13); nod_disp(14) nod_disp(15)];
    % side lengths of quadrilateral
    xlo = 0; ylo = 0; 
 xhi = 1; yhi = 1;
136
139
    % no of nodes from the size of coordinate matrix (for plotting purposes)
140
    reShapingSize = sqrt(totNodes); % totNodes = 9;
    \% reshape u and v matrices for contouring
    what = reshape(allDisp(:,1),reShapingSize,reShapingSize)';
vMat = reshape(allDisp(:,2),reShapingSize,reShapingSize)';
143
    146
147
    hold on
150
    box on
    %% u-disp contour plot
    % subplot (2,1,1);
    contourf(xcoords, ycoords, uMat, 20, 'LineWidth',2);
set(gca, 'FontName', 'Garamond', 'FontSize',18, 'FontWeight', 'bold',...
    'LineWidth',2, 'XMinorTick', 'off',...
    'YMinorTick', 'off', 'GridAlpha',0.07,...
    'GridLineStyle', '—', 'LineWidth',2);
    title ('Contour Plot: u');
```

```
xlabel('X');
ylabel('Y');
        colorbar;
162
        showQ4 = 1;
         if showQ4 == 1
               hold on
               nold on [ine ([0,0.25],[0.75,0.75], 'LineWidth',2,'Color','r'); line ([0.25,0.25],[0.75,1], 'LineWidth',2,'Color','r'); line ([0.25,1],[0.75,0.6], 'LineWidth',2,'Color','r'); line ([0.25,0.5],[0.75,0],'LineWidth',2,'Color','r');
                hold off
         end
         [gcf] = plotNodes(gcf,totNodes);
        %% v-disp contour plot
        figure;
176
        % subplot (2,1,2);
         contourf(xcoords, ycoords, vMat, 20, 'LineWidth',2);
         hold on
        \% plots the original system
         if showQ4 == 1
180
               181
182
184
        end
186
        set(gca, 'FontName', 'Garamond', 'FontSize',18, 'FontWeight', 'bold',...
    'LineWidth',2, 'XMinorTick', 'off',...
    'YMinorTick', 'off', 'GridAlpha',0.07,...
    'GridLineStyle', '—', 'LineWidth',2);
187
188
         title ('Contour Plot: v');
        xlabel('X');
ylabel('Y');
         colorbar;
         [gcf] = plotNodes(gcf,totNodes);
195
196
        199
        {\tt plotDeform}\!=\!0;
         if plotDeform
200
                hold off
                figure;
               % plots the original system

11 = line([0,0.25],[0.75,0.75], 'LineWidth',3,'Color','k');
line([0.25,0.25],[0.75,1], 'LineWidth',3,'Color','k');
line([0.25,1],[0.75,0.6], 'LineWidth',3,'Color','k');
line([0.25,0.5],[0.75,0],'LineWidth',3,'Color','k');
206
                hold on
                \begin{array}{l} \text{Boto Sin} \\ x = [0; \ 0.5; \ 1; \ 1; \ 1; \ 0.5; \ 0; \ 0; \ 0]; \\ y = [0; \ 0; \ 0.6; \ 1; \ 1; \ 1; \ 0.75; \ 0]; \\ \text{disp_u} = [\text{allDisp}(1,1); \ \text{allDisp}(2,1); \ \text{allDisp}(3,1); \ \text{allDisp}(4,1); \end{array} 
                        allDisp\left(5\,,1\right);\ allDisp\left(6\,,1\right);\ allDisp\left(7\,,1\right);\ allDisp\left(8\,,1\right);\ allDisp\left(8\,,1\right);
                disp_v = [allDisp(1,2); allDisp(2,2); allDisp(3,2); allDisp(4,2);
                        allDisp(5,2); allDisp(6,2); allDisp(7,2); allDisp(8,2); allDisp
                               (9,2);
                defX = x + disp_u;
                defY = y + disp_v;
                hold on
220
                box on
               % plots
                              the deformed system
               % plots the deformed system
p1 = plot(defX, defY, 'c-', 'LineWidth', 1.5);
set(gca, 'FontName', 'Garamond', 'FontSize', 18, 'FontWeight', 'bold', ...
    'LineWidth', 2, 'XMinorTick', 'off', ...
    'YMinorTick', 'off', 'GridAlpha', 0.07, ...
    'GridLineStyle', '--', 'LineWidth', 2);
title('Deformation Plot in Real Space (global coordinate system)');
                xlabel('X');
```

```
\label{localization} $$ ylabel('Y'); legend([l1\ p1],{'Original\ System',\ 'Deformed\ System'},'Location',' $$ $$
             southeast',...
'Color',[0.941176470588235 0.941176470588235 0.941176470588235])
         set(gcf, 'units', 'points', 'position', [100,100,1024,700])
    end
    sprintf('Max Vertical displacement occurs at node %d: %0.4f units', id_v
    , allDisp(id_v,2))
sprintf('Max Horizontal displacement occurs at node %d: %0.4f units', id_u, allDisp(id_u,1))
    %
%
%
243
    %
            #1
                       #4
    %
246
    %%%%%
248
            #2
                        #3
                            -00--
254
    258
     str = string(1:totNodes);
259
    plotNodes=1;
260
     if plotNodes
         for b=1:totNodes
             \begin{array}{c} text\left(pos\left(b,1\right),pos\left(b,2\right),str\left(b\right),"Color","red","FontSize",18,"FontName","Garamond","FontWeight","bold") \end{array}
         end
264
     end
```

Output of the code:

Max Vertical displacement occurs at node 7: -0.0016 units. Max Horizontal displacement occurs at node 3: 0.0008 units

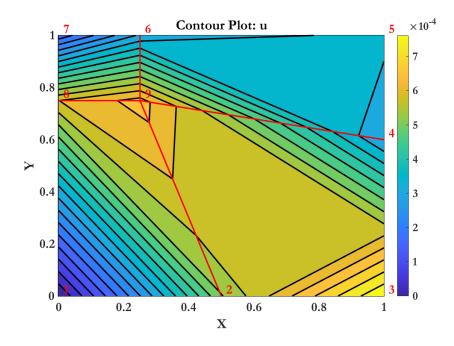


Figure 4: Contour Plot of u-displacement

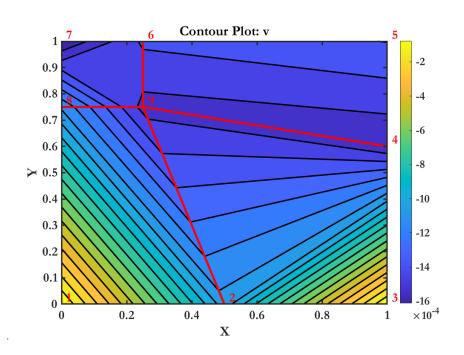


Figure 5: Contour Plot of v-displacement

Problem 3

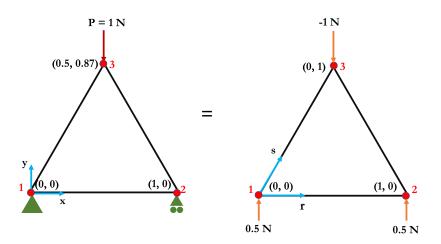


Figure 6: CST

Algorithm for solving for displacements when 1 CST element is considered:

1. Get shape functions, N, for CST:

$$N_1 = 1 - r - s$$
, $N_2 = r$, and $N_3 = s$

2. Get x(r, s) and y(r, s) from

$$x(r,s) = x_1 N_1 + x_2 N_2 + x_3 N_3 = r x_2 - x_1 (r+s-1) + s x_3$$
$$y(r,s) = y_1 N_1 + y_2 N_2 + y_3 N_3 = r y_2 - y_1 (r+s-1) + s y_3$$

3. Get Jacobian matrix, [J], from derivatives of x and y w.r.t. r and s

$$[J]_{2\times 2} = \begin{bmatrix} \frac{\partial x}{\partial r} & \frac{\partial y}{\partial r} \\ \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \end{bmatrix} = \begin{bmatrix} x_2 - x_1 & y_2 - y_1 \\ x_3 - x_1 & y_3 - y_1 \end{bmatrix}$$

4. Get u(r, s) and v(r, s):

$$u(r,s) = u_1 N_1 + u_2 N_2 + u_3 N_3 = r u_2 - u_1 (r+s-1) + s u_3$$
$$v(r,s) = v_1 N_1 + v_2 N_2 + v_3 N_3 = r v_2 - v_1 (r+s-1) + s v_3$$

5. Get $\{u_{,real}\}$ and $\{v_{,real}\}$:

$$\{u_{,real}\}_{2\times 1} = \left\{\frac{\frac{\partial u}{\partial x}}{\frac{\partial u}{\partial y}}\right\}_{2\times 1} = [J]_{2\times 2}^{-1} \left\{\frac{\frac{\partial u}{\partial r}}{\frac{\partial u}{\partial s}}\right\}_{2\times 1}$$

$$\{v_{,real}\}_{2\times 1} = \begin{bmatrix} \frac{\partial v}{\partial x} \\ \frac{\partial v}{\partial y} \end{bmatrix}_{2\times 1} = [J]_{2\times 2}^{-1} \begin{bmatrix} \frac{\partial v}{\partial r} \\ \frac{\partial v}{\partial s} \end{bmatrix}_{2\times 1}$$

6. Get $\epsilon_x, \epsilon_y, \epsilon_{xy}$ from $\{u_{,real}\}$ and $\{v_{,real}\}$

$$\{\epsilon\}_{3\times 1} = \begin{bmatrix} \frac{\partial u}{\partial x} \\ \frac{\partial v}{\partial y} \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \end{bmatrix}_{3\times 1}$$

7. Matricize these 3 equations: ϵ_x , ϵ_y , ϵ_{xy} and compare $\{\epsilon\}$ with the following equation:

$$\{\epsilon\}_{3\times 1} = [B]_{3\times 6}\{d\}_{6\times 1}$$

8. Strain-displacement matrix is:

$$[B]_{3\times 6} = \frac{1}{2A} \begin{bmatrix} y_2 - y_3 & 0 & y_3 - y_1 & 0 & y_1 - y_2 & 0 \\ 0 & x_3 - x_2 & 0 & x_1 - x_3 & 0 & x_2 - x_1 \\ 2x_1 - x_2 - x_3 & 2y_1 - y_2 - y_3 & x_1 - x_3 & y_3 - y_1 & x_2 - x_1 & y_1 - y_2 \end{bmatrix}_{3\times 6}$$

9. Use Gauss Quadrature to get the integral or stiffness matrix:

$$[\mathbf{K}]_{6\times 6} = \int_{-1}^{1} [B]_{6\times 3}^{T} [E]_{3\times 3} [B]_{3\times 6} t |J| dr ds = \int_{-1}^{1} [\text{integrand}]_{6\times 6} dr ds =$$

$$[\mathbf{K}]_{6\times 6} = [\text{integrand}]_{6\times 6} \int_{-1}^{1} dr ds$$

here, integrand $\neq f(r,s) = \text{constant}$

10. Apply boundary conditions (3 BCs, hence 3 rows and columns are dropped)

$$[\mathbf{K}]_{6\times 6} \xrightarrow{\mathrm{apply \ BC}} [\mathbf{K}]_{3\times 3}$$

11. Solve for nodal displacements using:

$$[\mathbf{K}]_{3\times3}\{d\}_{3\times1} = \{F\}_{3\times1} \qquad \{d\}_{3\times1} = [\mathbf{K}]_{3\times3}^{-1}\{F\}_{3\times1}$$

$$\left\{ \begin{array}{l} u_2 \\ u_3 \\ v_3 \end{array} \right\} = \left\{ \begin{array}{l} 0.0005 \\ 0.00025 \\ -0.000866 \end{array} \right\}$$

It can be seen that CST with single mesh has similar and comparable horizontal and vertical displacements than those in the case of Q4 with single element. However, displacements for 4 Q4 elements differ slightly from those obtained in CST and single Q4 element. Also, the field variables, u(x,y) and v(x,y) have been expressed in terms of x and y (PART B, line 164 in the attached code below).

Que	Max. Horizontal Displacement, u_{max}	Max. Vertical Displacement, v_{max}
1	+0.0005 (nodes 2, 3)	-0.0010 (nodes 3, 4)
2	+0.0008 (node 3 = node 2 in que 1)	-0.0016 (node 7 = node 3 in que 1)
3	+0.0005 (node 2)	-0.000866 (node 3)

Listing 3: Nodal displacements of a CST element with one mesh

```
%% FEM, HW 3, Problem 3
     %% Afnan Mostafa
%% 11/28/2023
     6
     clc
     clear
     close all rng('shuffle')
     syms r s r1 s1 r2 s2 r3 s3 u1 u2 u3 v1 v2 v3 E_0 nu t l x1 y1 x2 y2 x3
           y3 x_xy y_xy
     16
     E_0 = 1e6;
18
19
     nu = 0.5;
     t = 0.001;

t = 1;
20
     totNodes = 3;
     triangle
     x1 = xyMat(1,1); y1 = xyMat(1,2);
x2 = xyMat(2,1); y2 = xyMat(2,2);
x3 = xyMat(3,1); y3 = xyMat(3,2);
26
     30
     \begin{array}{l} {\rm xyMat} \, = \, \left[ \, {\rm x1} \  \  \, {\rm y1} \, ; \  \  \, {\rm x2} \  \  \, {\rm y2} \, ; \  \  \, {\rm x3} \  \  \, {\rm y3} \, \right]; \\ {\rm N1} \, = \, 1 - {\rm r} - {\rm s} \, ; \  \  \, {\rm N2} \, = \, {\rm r} \, ; \  \  \, {\rm N3} \, = \, {\rm s} \, ; \end{array}
33
     x = N1*x1+N2*x2+N3*x3;
     y = N1*y1+N2*y2+N3*y3;
36
     J11 = diff(x,r);
     J21 = diff(x, s);
     J12 = diff(y,r);
40
     J22 = diff(y,s);
41
     J = \begin{bmatrix} J11 & J12; \\ J21 & J22 \end{bmatrix};
42
44
45
     invJ = inv(J);
47
     Zer = zeros(size(invJ));
50
     u = N1*u1+N2*u2+N3*u3;
     v = N1*v1+N2*v2+N3*v3;
     \begin{array}{ll} du\_dr \; = \; d\,i\,f\,f\,(\,u\,,\,r\,)\,\,; \\ du\_ds \; = \; d\,i\,f\,f\,(\,u\,,\,s\,)\,\,; \\ dv\_dr \; = \; d\,i\,f\,f\,(\,v\,,\,r\,)\,\,; \end{array}
56
     dv_{-}ds = diff(v,s);
     \begin{array}{lll} d\,U\,\text{\_iso} &=& \left[\,d\,u\,\text{\_dr}\,; & d\,u\,\text{\_ds}\,\right]\,; \\ d\,V\,\text{\_iso} &=& \left[\,d\,v\,\text{\_dr}\,; & d\,v\,\text{\_ds}\,\right]\,; \end{array}
58
    dU_{real} = invJ*dU_{iso};
```

```
dV_{real} = invJ*dV_{iso}:
    du_dx = dU_real(1);
                          %% epsilon_xx
65
    du_dy = dU_real(2);
                          %% epsilon_xy
66
    dv_dx = dV_real(1);
                          %% epsilon_yx
    dv_dy = dV_real(2);
                          %% epsilon_yy
    gamma_xy = du_dy + dv_dx;
    % solving by hand (transforming equations into matrix)
73
74
        [
(y1-y3)-(y1-y2)
0;
                                    0
                                                 -(y1-y3)
                                                                 0
                                                                         (y1-
            y2)
                    (\,(\,{\bf x}1{-}{\bf x}2\,)\,{-}({\bf x}1{-}{\bf x}3\,)\,)
                                                                     0
                                                     (x1-x3)
             (x2-x1);
                           ((y1-y3)-(y2-y1))
                                                                          (x2
        ((x1-x2)-(x3-x1))
                                                              (y3-y1)
            -x1)
                     (y1-y2)]*1/(0.866);
    B_{-t} = transpose(B);
78
    %% %%%%%%%%%% Constitutive Matrix: plane stress %%%%%%%%
80
    E = (E_0/(1-(nu)^2))*[1 nu 0; nu 1 0; 0 0 (1-nu)/2];
81
82
    83
84
    integrand = eval(B_t*E*B*t*det(J));
85
86
    %% %%%%%%%%%%% Gauss Quadrature (3rd order) %%%%%%%%%%
87
88
89
    % [stiffMat] = GaussQuadCST(order, integrand);
90
    switch (order)
93
        case 1
94
            gaussPt = [1/3 \ 1/3];
95
            \mathrm{wt}\ =\ 1\,;
96
        case 3
            gaussPt =
98
                2/3 1/6;
                1/6 2/3;
1/6 1/6];
99
100
            wt = [1/3; 1/3; 1/3];
        case 4
            gaussPt = [
                1/3 \ 1/3;
                3/5 1/5;
                1/5 1/5;
106
                1/5 3/5];
            wt = [-27/48; 25/48; 25/48; 25/48];
            % case 5
        otherwise
            error ("Can't do more than 4th order GQ")
    end
114
    isIntegrandConst = 1; % for CSTs
     if \ isIntegrandConst == 0 
118
        gq = [];
integral = [];
119
        for i=1:length(integrand)
            for j=1:length(integrand)
                func = integrand(i,j);
                \begin{array}{ll} \text{for } k = 1 : length (gaussPt) \\ r = gaussPt (k,1); \end{array}
                    s = gaussPt(k,2);
                    gq(k) = eval(subs(func))*wt(k,1);
                end
                integral(i,j) = sum([gq]);
            end
        end
    stiffMat = integrand*(1*1*1);
```

```
136
      dsplmnt = [u1; v1; u2; v2; u3; v3];
     force = [0;0.5; 0;0.5; 0;-1]
     141
     % solved by handw
     disp_BC = [u2; u3; v3];

force_BC = [0; 0; -1];
143
144
      new_integral = stiffMat;
147
148
     150
     % dynamic deletion (matrix index changes with each progressive line)
     mod. matrix
      new\_integral(:,2) = []; \% delete 2st column (4th col. of original) of
          mod. matrix
     new\_integral(2,:) = [];
158
     159
     nod\_disp = new\_integral \setminus force\_BC; \% (inverse)
     %% PART B
164
     %% u(x,y), v(x,y)

N_x y = \begin{bmatrix} 1 & x_x y & y_x y \end{bmatrix} * inv(\begin{bmatrix} 1 & x1 & y1; & 1 & x2 & y2; & 1 & x3 & y3 \end{bmatrix});
166
     u1 = 0;
               v1 = 0; u2 = nod_disp(1); v2 = 0; u3 = nod_disp(2); v3 =
          nod_disp(3);
     \begin{array}{l} u_{-}xy = u1*N_{-}xy(1,1) + u2*N_{-}xy(1,2) + u3*N_{-}xy(1,3); \\ v_{-}xy = v1*N_{-}xy(1,1) + v2*N_{-}xy(1,2) + v3*N_{-}xy(1,3); \end{array}
     %% if I plug in x, y values into u and v fields, I get righ double(subs(u_xy, [x_xy,y_xy], [1,0])) == nod_disp(1) double(subs(u_xy, [x_xy,y_xy], [0.5,0.866])) == nod_disp(2)
                                                                   I get right answers
172
     abs(double(subs(v\_xy\,,\ [x\_xy\,,y\_xy\,]\,,\ [0.5\,,0.866])) - nod\_disp(3)) \ \%\% \ very + (0.5\,,0.866)
           low number
176
     \% plots the original system showCST = 1;
178
     if showCST == 1
181
          hold on
          line ([0,1],[0,0], 'LineWidth',3,'Color','b');
line ([0,0.5],[0,sqrt(3)/2],'LineWidth',3,'Color','b');
line ([0.5,1],[sqrt(3)/2,0],'LineWidth',3,'Color','b');
182
183
184
185
     end
187
     % plots the deformed system
     plotDeform=1;
188
      if plotDeform
189
           \begin{array}{l} x = [0; 1; 0.5; 0]; \\ y = [0; 0; sqrt(3)/2; 0]; \end{array} 
190
          y = [0; 0; sqrt(3)/2; 0];
disp_u = [0; subs(nod_disp(1)); subs(nod_disp(2)); 0];
disp_v = [0; 0; subs(nod_disp(3)); 0];
pt1 = [0 1]; pt2 = [1 0]; pt3 = [0.5 sqrt(3)/2];
defX = x + disp_u;
194
195
196
           defY = y + disp_v;
          hold on
          box on
          plot(defX, defY, 'r-', 'LineWidth', 1.5);
set(gca,'FontName','Garamond','FontSize',18,'FontWeight','bold',...
'LineWidth',2,'XMinorTick','off',...
'YMinorTick','off','GridAlpha',0.07,...
```

```
'GridLineStyle','—','LineWidth',2);
           206
      end
      subs(nod_disp);
      all Disp = \begin{bmatrix} 0 & 0 \\ \vdots & subs(nod\_disp(1)) & 0 \\ \vdots & subs(nod\_disp(2)) & subs(nod\_disp(3)) \\ \end{bmatrix}
      213
      % plots contour
214
      is Contour = 0;\\
      if isContour
218
           % side lengths of quadrilateral
219
           xlo = 0; ylo = 0;
           xhi = 1; yhi = 1;
           % no of nodes from the size of coordinate matrix (for plotting
                purposes)
           reShapingSize = 3;
           % reshape u and v matrices for contouring
           wMat = reshape(allDisp(:,1),reShapingSize,reShapingSize)';
vMat = reshape(allDisp(:,2),reShapingSize,reShapingSize)';
228
           % mesh a grid between [xlo, xhi] and [ylo, yhi] [coordsX, coordsY] = meshgrid(linspace(xlo, xhi, reShapingSize), linspace(ylo, yhi, reShapingSize));
230
           hold on
           box on
234
           % subplot(2,1,1);
           contour(coordsX, coordsY, uMat, 20, 'LineWidth', 2);
set(gca, 'FontName', 'Garamond', 'FontSize', 18, 'FontWeight', 'bold', ...
    'LineWidth', 2, 'XMinorTick', 'off', ...
    'YMinorTick', 'off', 'GridAlpha', 0.07, ...
    'GridLineStyle', '—', 'LineWidth', 2);
236
240
           title ('Contour Plot: u');
           xlabel('X');
ylabel('Y');
           colorbar;
247
           figure;
248
           % subplot (2,1,2);
           {\tt contour}({\tt coordsX}\;,\;\;{\tt coordsY}\;,\;\;{\tt vMat}\;,\;\;20\,,\,\,{\tt 'LineWidth'}\;,2)\;;
           box on
           title('Contour Plot: v');
xlabel('X');
ylabel('Y');
           colorbar;
           set (gca, 'FontName', 'Garamond', 'FontSize', 16, 'FontWeight', 'bold',...
    'LineWidth', 2, 'XMinorTick', 'off',...
    'YMinorTick', 'off', 'GridAlpha', 0.07,...
'GridLineStyle', '—', 'LineWidth', 2);
258
      end
     262
      disp('Displacement Matrix: ')
      eval(subs(allDisp))
265
266
      267
268
      sprintf('Max Vertical displacement occurs at node %d: %0.6f units', id_v
           , allDisp(id_v,2))
ntf('Max Horizontal displacement occurs at node %d: %0.6f units',
      sprintf('Max
           id_u, allDisp(id_u,1))
```

Output of the code:

Max Vertical displacement occurs at node 3: -0.000866 units. Max Horizontal displacement occurs at node 2: 0.0005 units

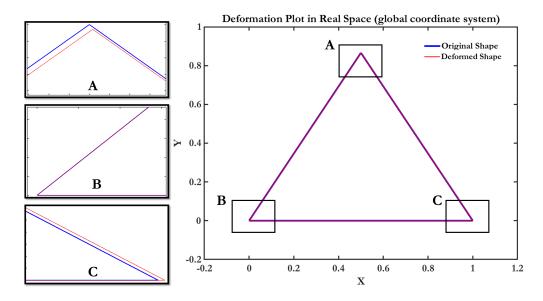


Figure 7: Deformation Plot of a CST element with zoomed-in views of the nodal displacements

Problem 4

Steps:

1. Get shape functions, [N], for Q4:

$$[N] = [x][A]^{-1}$$

$$\begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}_{1\times 4} = \begin{bmatrix} 1 & x & y & xy \end{bmatrix}_{1\times 4} \begin{bmatrix} 1 & x_1 & y_1 & x_1y_1 \\ 1 & x_2 & y_2 & x_2y_2 \\ 1 & x_3 & y_3 & x_3y_3 \\ 1 & x_4 & y_4 & x_4y_4 \end{bmatrix}_{4\times 4}^{-1}$$

$$\begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix}_{1\times 4} = \begin{bmatrix} 1 & x & y & xy \end{bmatrix}_{1\times 4} \begin{bmatrix} 1 & -0.5 & -0.5 & (-0.5)(-0.5) \\ 1 & 0.5 & -0.25 & 0.5(-0.25) \\ 1 & 0.5 & 0.25 & 0.5(0.25) \\ 1 & -0.5 & 0.5 & (-0.5)0.5 \end{bmatrix}_{4\times 4}^{-1}$$

$$= \begin{bmatrix} (xy - \frac{y}{2} - \frac{x}{2} + \frac{1}{4}) & (\frac{x}{2} - y - 2xy + \frac{1}{4}) & (\frac{x}{2} + y + 2xy + \frac{1}{4}) & (\frac{y}{2} - \frac{x}{2} - xy + \frac{1}{4}) \end{bmatrix}$$

- 2. Get $[N_{,x}]_{1\times 4}$ and $[N_{,y}]_{1\times 4}$ through derivative of shape functions w.r.t. x and y.
- 3. Integrate the integrand over $[y_1, y_2] = [\frac{-3}{8} + \frac{x}{4}, \frac{3}{8} \frac{x}{4}]$ and $[x_1, x_2] = [-0.5, 0.5]$ domains to get stiffness matrix, $[\mathbf{K}]_{4\times4}$

$$[\mathbf{K}]_{4\times4} = \int_{\Omega} (N_{,x}^T N_{,x} + N_{,y}^T N_{,y}) d\Omega$$

$$[\mathbf{K}]_{4\times4} = \begin{bmatrix} 0.5182 & -0.0156 & -0.3594 & -0.1432 \\ -0.0156 & 1.1771 & -0.8021 & -0.3594 \\ -0.3594 & -0.8021 & 1.1771 & -0.0156 \\ -0.1432 & -0.3594 & -0.0156 & 0.5182 \end{bmatrix}$$

4. Apply BC (removing 2nd and 3rd rows and columns) to get $[\mathbf{K}]_{2\times 2}$ and then use:

$$\begin{bmatrix} \mathbf{K} \end{bmatrix}_{2 \times 2} = \begin{bmatrix} 0.5182 & -0.1432 \\ -0.1432 & 0.5182 \end{bmatrix}$$

5. Solve for $\{\phi\}_{2\times 1}$:

$$\{\phi\}_{2\times 1} = [\mathbf{K}]_{2\times 2}^{-1} \{f\}_{2\times 1}$$

6. We get ϕ_1 and ϕ_4 from solving the above equation and use them to find r_2 and r_3 :

$$\{f\}_{4\times 1} = [\mathbf{K}]_{4\times 4} \{\phi\}_{4\times 1}$$

where,

$$\{f\}_{4\times 1} = \begin{Bmatrix} u_0/2 \\ r_2 \\ r_3 \\ u_0/2 \end{Bmatrix}, \{\phi\}_{4\times 1} = \begin{Bmatrix} 4u_0/3 \\ 0 \\ 0 \\ 4u_0/3 \end{Bmatrix}$$

7. Then using r_2 , we find velocity $\phi_{,x}$ at right vertical boundary (here, l=1, m=0, $\phi_{,x} \neq 0$ for right vertical boundary and l=0, m =-1, but $\phi_{,y} = 0$ for bottom boundary):

$$r_2 = \int_{-1}^{1} N_2(\phi_{,x}l + \phi_{,y}m)ds$$

$$\phi_{,x} = r_2/\text{Area}$$

$$\phi_{,x} = (-0.5u_0)/0.25 = -2u_0$$

$$|\phi_{,x}| = 2u_0$$

Similarly,

$$r_3 = \int_1^{-1} N_3(\phi_{,x}l + \phi_{,y}m)ds$$

 $\phi_{,x} = r_3/\text{Area}$
 $\phi_{,x} = (-0.5u_0)/0.25 = -2u_0$
 $|\phi_{,x}| = 2u_0$

```
%% ME 441: FEM, HW 3, Problem 4
  %% Afnan Mostafa
  clear
  close all
  rng('shuffle')
  16
17
  nu = 0.5;
  t = 0.001;

u_0 = 1;
18
  syms x y x1 y1 x2 y2 x3 y3 x4 y4 u_0 r2 r3 phi_x phi_y
  27
  x1 = -0.5; y1 = -0.5;
  x2 = 0.5; y2 = -1/4;

x3 = 0.5; y3 = 1/4;

x4 = -0.5; y4 = 0.5;
29
30
  32
33
  X = [1 \ x \ y \ x*y];
35
36
    1 x2 y2 x2*y2;
1 x3 y3 x3*y3;
1 x4 y4 x4*y4];
39
40
41
  N = X*(inv(A));
42
  43
44
  N_dx = diff(N,x);
```

```
| N_dx_T = transpose(N_dx);
47
48
    N_{-}dy = diff(N,y);
    N_dy_T = transpose(N_dy);
50
    integrand = (N_dx_T*N_dx) + (N_dy_T*N_dy);
    integral_1 = int(integrand,y,[(-3/8)+(x/4), (3/8)-(x/4)]);   
K = double(int(integral_1,x,[-0.5 0.5]));
56
    K_BC = K;
    %% %%%%%%%% Apply Boundary Conditions %%%%%%%%%%
61
    K_{.}BC(:,2) = [];

K_{.}BC(:,2) = [];

K_{.}BC(2,:) = [];
62
63
64
    K_BC(2,:) =
    %% %%%%%%%%% Phi matrix from phi = K*f %%%%%%%%%%%%
67
68
    phiMat_BC = K_BC \setminus [u_0/2; u_0/2];
69
70
71
72
73
     phi_all = [phiMat_BC(1); 0; 0; phiMat_BC(2)];
    %% %%%%%%%% Force matrix %%%%%%%%%
74
    \begin{array}{lll} force \, = \, \left[\, u\_0 \, / \, 2 \, ; \, r2 \, ; \, r3 \, ; \, u\_0 \, / \, 2 \, \right]; \\ force\_mat \, = \, K* \, p \, hi\_all \, ; \end{array}
76
77
78
79
    % integration of N w.r.t. dy gives area of the N-y plot Area = (1*1/2)/2;
80
81
    \%\% l = 1, m = 0 at right vertical boundary
82
    83
84
85
86
```

Output:

Velocity at right vertical boundary is: $-2u_0$ Velocity at right vertical boundary is: -2 units (if $u_0 = 1$ unit)

Appendix A

Listing 4: MATLAB auxiliary function to get Jacobian matrix of a Q4 element

```
function [J,invJ,betaMat] = JacobianMatQ4(xyMat)
     \%\% written by Afnan Mostafa as part of ME 441 at on %JacobianMat evaluates the Jacobian matrix for Q4 in isoparametric space
            takes the [x y] matrix (4x2) and multiplies it with a prefactor and another matrix (2x4) that consists of the derivatives of shape functions w.r.t. eta and n. Also, it calculates the inverse of
 6
            and then assembles the Beta matrix needed for stiffness matrix of Q4
            elements in isoparametric space.
     % input: [x y] matrix
% outputs: Jacobian matrix, inverse Jacobian matrix, and Beta Matrix
14
     %% sanity check for symbolic e,n % if sum([strcmp(class(n), 'sym'), strcmp(class(e), 'sym')]) == 2
     \% elseif sum([strcmp(class(n),'sym'), strcmp(class(e),'sym')]) < 2
           syms n e
19
     % end
     \begin{array}{l} \text{\%\% main body function} \\ \mathrm{J} = (1/4)*[-(1-n)\ (1-n)\ (1+n)\ -(1+n)\,;} \\ -(1-e)\ -(1+e)\ (1+e)\ (1-e)\,]*xy\mathrm{Mat}; \end{array}
      invJ = inv(J);
26
      Zer = zeros(size(invJ));
      betaMat = [invJ Zer; Zer invJ];
```

Appendix B

Listing 5: MATLAB auxiliary function to get integrand (matrix function inside the integral of the stiffness matrix of a Q4 element

```
function [integrand, B, B_t] = IntegrandStiffMatQ4(xyMat, t, E_0, nu,
          isPlaneStrain, isPlaneStress)
    \%\% written by Afnan Mostafa as part of ME 441 at UR \%IntegrandStiffMatQ4 evaluates the "integrand" inside the integral of
        stiffness matrix of Q4 elements in isoparametric space
        takes the coords matrix, thickness, Poisson's ratio, Young's Mod, and either plane strain or stress condition and then calls Jacobian MatQ4 matrix to compute strain—displacement matrix (B) and integrand
                                                                                Young's Mod, and
         Jacobian\mathrm{MatQ4} takes the beta matrix (4\mathrm{x4}) and Jacobian (2\mathrm{x2}) and then
        does: transpose(B)*E*B*thickness*determinant(J)
Please Note: B ~= betaMat
        B = \, strain - displacement \, \, matrix \, , \, \, betaMat \, = \, matrix \, \, of \, \, derivatives \, \, of \, \, N
    %
         inputs: [x y] matrix, thickness (t), Poisson's ratio (nu), Young's
    %
                  (E_0), either plane strain or stress condition (just use 1 or
          0)
                  ex1: IntegrandStiffMatQ4(xyMat,0.001,1e6,0.5,0,1)
                  ex2: IntegrandStiffMatQ4(xyMat, 0.001, 1e6, 0.5, 1, 0)
    %
                  ex3: IntegrandStiffMatQ4(xyMat,0.001,1e6,0.5,0,0) (plane
    %
20
                  ex4: IntegrandStiffMatQ4(xyMat,0.001,1e6,0.5,1,1) (ERROR)
    %
         outputs: integrand, B, transpose of B,
```

```
%% hard-coding plane conditions (commented-out)
26
    \%isPlaneStrain = 0;
28
    %isPlaneStress = 1;
    \begin{array}{l} \mbox{if sum} \left( \left[ \mbox{isPlaneStrain} \; , \; \mbox{isPlaneStress} \right] \right) \; = \; 2 \\ \mbox{error} \left( \mbox{"Can't use both plane strain and plane stress} \; , \; \mbox{use any one"} \right) \\ \mbox{elseif sum} \left( \left[ \mbox{isPlaneStrain} \; , \; \mbox{isPlaneStress} \right] \right) \; = \; 1 \end{array}
        % do nothing
    else
       warning ('Choosing plane stress condition by default')
38
    end
40
    787878787878787878787878787
42
    \% if sum([strcmp(class(n), 'sym'), strcmp(class(e), 'sym')]) == 2
          % do nothing
    \% \ \ elseif \ \ sum\left(\left[\ strcmp\left(\ class\left(n\right), 'sym'\right), \ \ strcmp\left(\ class\left(e\right), 'sym'\right)\right]\right) \ < \ 2
45
         syms n e
    % end
46
47
    75757777777777777777777777
    [J, \tilde{\ }, betaMat] = JacobianMatQ4(xyMat);
    %% %%%%%%%%%%%%%%%% Alpha Matrix
         alphaMat = [1 \ 0 \ 0 \ 0; \ 0 \ 0 \ 1; \ 0 \ 1 \ 1 \ 0];
    %% %%%%%%%%%%%%%%%% Beta Matrix
56
         \%betaMat = [[invJ] [Zer]; [Zer] [invJ]]; \%\% no need to redefine
    %% %%%%%%%%%%%%%%% Gamma Matrix
         65
         0 - 1 + e \ 0 - 1 - e \ 0 \ 1 + e \ 0 \ 1 - e ];
    %% %%%%%%%%%%%%%%% Strain-Displacement Matrix
         B = alphaMat*betaMat*gammaMat;
    B_{-t} = transpose(B);
    73
74
    if isPlaneStress == 1 && isPlaneStrain == 0
     E = (E_{-}0/(1-(nu)^{2}))*[1 \text{ nu } 0; \text{ nu } 1 \text{ 0; } 0 \text{ 0 } (1-nu)/2]; \\ else if is Plane Strain == 1 && is Plane Stress == 0 
        E = (E_0/((1+nu)*(1-2*nu)))*[1-nu \ nu \ 0; \ nu \ 1-nu \ 0; \ 0 \ 0.5-nu];
        \begin{array}{l} disp\,(\,\,{}^{'}\,Choosing\ plane\ stress\ condition\ by\ default\,\,{}^{'}\,)\\ E\,=\,(\,E_{-}0/(1-(nu)\,\,{}^{^{'}}2)\,)*[1\ nu\ 0;\ nu\ 1\ 0;\ 0\ 0\ (1-nu)\,/\,2]; \end{array}
80
81
    end
82
83
    %% %%%%%%%%%%%%%%%%%% Stiffness Matrix
         integrand = eval(B_t*E*B*t*det(J));
85
86
    \quad \text{end} \quad
```

Appendix C

Listing 6: MATLAB auxiliary function to get the Gauss Quadrature integration of a Q4 element

```
function [stiffMat] = GaussQuadQ4(order,integrand)
    %% written by Afnan Mostafa as part of ME 441 at UR
    %GaussQuadQ4 evaluates the gauss integral for Q4 in isoparametric space
    %obtain the stiffness matrix of a Q4 element.
   %
        takes the GQ order (either 1 or 2 or 3) and integrand obtained from
 6
        IntegrandStiffMatQ4.m\ file\ (function\ file)\ and\ then\ performs\ the\ GQ
        integration to obtain stiffness matrix (integral)
 8
   % input: GQ order and integrand matrix in terms of e,n % outputs: Stiffness Matrix
   757575757575757575757575757
    \% if sum([strcmp(class(n), 'sym'), strcmp(class(e), 'sym')]) == 2
   \% elseif sum([strcmp(class(n),'sym'), strcmp(class(e),'sym')]) < 2
18
        syms n e
    % end
21
   \%\% %%%%%%%%% gauss points and weights for 2d integration
        77777777777777777
    switch (order)
        case 1
           gaussPt = 0; wt = 4;
        case 2
27
            gaussPt = [
28
                 -1/sqrt(3) -1/sqrt(3);
                 1/sqrt(3) -1/sqrt(3);
1/sqrt(3) 1/sqrt(3);
                 -1/sqrt(3) 1/sqrt(3)];
             wt = [
                 1 1:
                 1 1;
35
36
        case 3
            gaussPt = [
39
                 0 0;
40
                 0 - sqrt(3/5);
41
                 0 sqrt (3/5)
42
                 \operatorname{sqrt}(3/5) 0;
                 -\operatorname{sqrt}(3/5) 0;
43
                 sqrt (3/5) sqrt (3/5);
sqrt (3/5) -sqrt (3/5);
-sqrt (3/5) sqrt (3/5);
44
45
46
47
                 -\operatorname{sqrt}(3/5) - \operatorname{sqrt}(3/5)];
             wt = [ \\ 8/9 \ 8/9; \\
48
49
                 8/9 5/9;
                 8/9 5/9;
5/9 8/9;
                 5/9 8/9;
54
                 5/9 5/9;
                 5/9 5/9;
56
57
                 5/9 5/9:
                 5/9 5/9];
58
            % case 4
        otherwise
60
             error ("Can't do more than 3rd order GQ")
61
```

```
gq = [];
integral = [];
for i=1:length(integrand)
66
67
             for j=1:length(integrand)
69
70
71
72
73
74
                    func = integrand(i,j)
                    for k=1:length(gaussPt)
    e = gaussPt(k,1);
    n = gaussPt(k,2);
    gq(k) = eval(subs(func))*wt(k,1)*wt(k,2);
                    end
75
76
77
78
79
                    integral(i,j) = sum([gq]);
      end
       stiffMat = integral;
       end
```

Appendix D

Listing 7: MATLAB auxiliary function to globalize any local stiffness matrix

```
function [mat3] = globalizeStiffMat(mat,posNodes,eleNodes,totNodes,DoF)
%globalizeStiffMat = globalizeS element matrix if given nodes (CCW)
% mat = matrix for globalization, posNodes = nodal positions (CCW) from
% bottom left, eleNodes = how many nodes in an element, totNodes = total
% nodes in the entire system, DoF = 2 for u, v (per node)
%
%
 6
     %%
     mat_cp = mat:
      diffDOF = totNodes*DoF - length(mat);
     mat_cp(end+diffDOF;) = 0;
mat_cp(:,end+diffDOF) = 0;
13
14
     mat2=zeros(size(mat_cp));
     posDisp = [(posNodes.*2) - 1; posNodes.*2];
18
      for m=1:eleNodes
19
20
            for n=1:DoF
                 mat2\,(\,:\,,\,posDisp\,(\,n\,,\!m)\,)\,\,=\,\,mat\_cp\,(\,:\,,n+(2*p)\,)\,\,;
           end
           p=p+1;
24
     26
27
     mat3=zeros(size(mat2));
     p=0;
for m=1:eleNodes
29
           for n=1:DoF
30
                 mat3(posDisp(n,m),:) = mat2(n+(2*p),:);
           end
31
           \mathbf{p} \!\!=\!\! \mathbf{p} \!+\! 1;
     end
     end
```