

INTERFERENCE

Superposition of two light waves.

Conditions of Interference :-

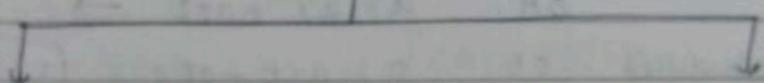
- Coherent Sources
- Monochromatic light
- Phase difference ($0^\circ/\text{constant}$)
- Constructive / Destructive,

↳ Condition of superposition

- Amplitudes of interfering waves should be nearly equal.

Types of Interference -

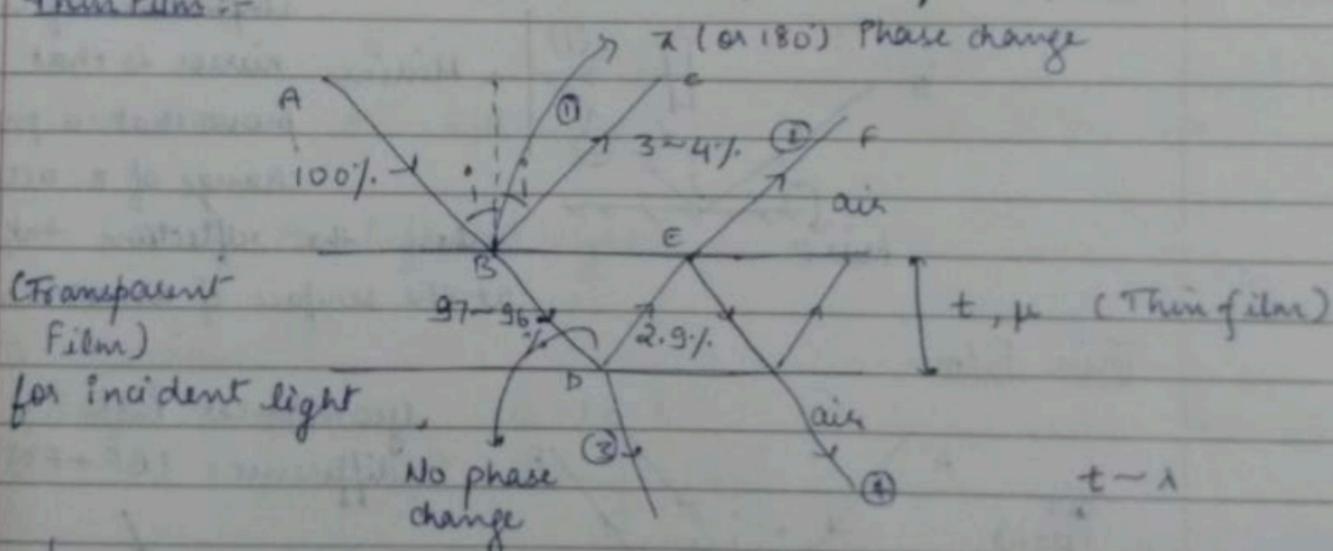
Interference



Division of Incident wf
Wavefront divides into
(YDSE) 2 parts by
reflⁿ, refl^m or diffⁿ

Division of Amplitude
(Thin Film, Newton's Ring
Interference, Michelson's Int.)
Amplitude is divided into 2 parts either by
parallel reflⁿ or refl^m

Thin Film :-

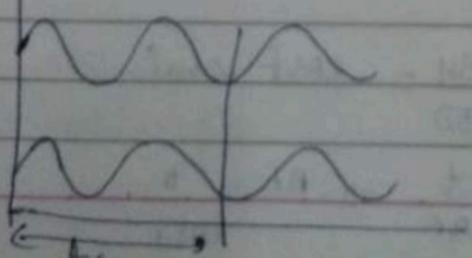


(Transparent
Film)

for incident light

No phase
change

$L_c \rightarrow$
Coherence length



$$\Delta \phi = \frac{2\pi}{\lambda} \times \Delta x$$

↓
Path difference
Phase diff.

Stoke's Law :-

When a light wave is reflected at the surface of an optically denser medium, it suffers a phase change of π i.e. p.d. of $\lambda/2$.

No such phase diff. is introduced if the reflection takes place from the surface of rarer medium

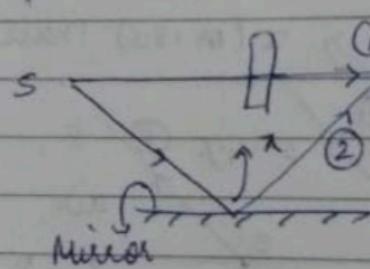
Incident	AOA	OB, ar	OC, at
Reflection	OB, ar	OA, ar. γ	OD, ar. γ
Transmission	OC, at	OD, ar. t	OA', att'

$$OA: a = ar^2 + att' \Rightarrow l = r^2 + tt'$$

$$OB: o = art + at\gamma' \Rightarrow l\gamma' = -\gamma$$

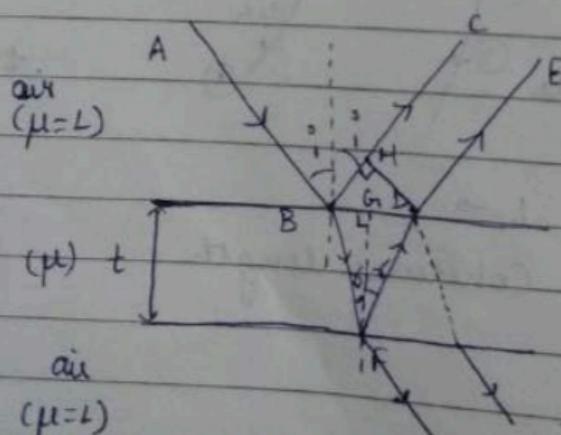
Represents
Out of phase

Lloyd's Mirror :-



Importance of Lloyd's mirror is that it proves that a phase change of π occurs when the reflection takes place at the surface of an OD medium.

Thin Film -



Geometrical Path difference = $(BF + FD) - BH$

$$\Delta BFG$$

$$BD = 2BG_1 = 2GD$$

$$\frac{BH}{BD} = \cos^2 \sin^2$$

$$\cos \gamma = \frac{t}{BF} \Rightarrow BF = \frac{t}{\cos \gamma}$$

$$\frac{BG}{BF} = \frac{\sin i}{\cos r}$$

$$BG = \frac{\sin i}{\cos r} t = t \cdot \tan i$$

$$BH = \frac{\sin i}{\cos r} 2t \tan r$$

$$\Rightarrow BH = 2t \sin i \cdot \tan r$$

$$\text{Geometrical Path difference} = \frac{2t}{\cos r} - 2t \sin i \cdot \tan r$$

$$= 2t - 2t \left[\frac{1 - \sin^2 i \cdot \sin r}{\cos r} \right]$$

$$\text{Optical Path difference} = \mu \left[(BF + FD) - BH \right]$$

$$= \mu (BF + FD) - 1 \cdot BH$$

$$= \mu \left[\frac{2t}{\cos r} \right] - 2t \sin i \cdot \tan r$$

$$= \frac{2t}{\cos r} \left[\frac{\sin i}{\sin r} - \sin i \cdot \sin r \right] = \frac{2t \sin i}{\cos r} \left[\frac{1 - \sin^2 r}{\sin r} \right]$$

$$= \frac{2t \mu \cos r}{\cos r} = 2\mu t \cos r$$

$$\text{Correction} = 2\mu t \cos r + \frac{\lambda}{2} = \Delta$$

(For Reflected Light)

(I) Maxima:

(Bright Fringe)

$$\Delta = \pm m \lambda$$

$$2\mu t \cos r + \frac{\lambda}{2} = \pm m \lambda$$

$$2\mu t \cos r = \pm (2m+1) \frac{\lambda}{2}$$

(II) Minima:

(Dark Fringe)

$$\Delta = \pm (2m+1) \frac{\lambda}{2}$$

$$2\mu t \cos r + \frac{\lambda}{2} = \pm (2m+1) \frac{\lambda}{2}$$

In Interference, we use extended source

Camlin Page
Date / /

$$2\mu t \cos\alpha = \pm m\lambda$$

For Transmitted Light-

$$\text{Optical Path Diff.} = 2\mu t \cos\alpha$$

(Dense to Rare)

(i) Maxima (Bright Fringe)-

$$\Delta = \pm m\lambda$$

$$2\mu t \cos\alpha = \pm m\lambda$$

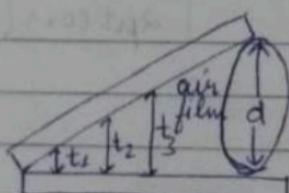
(ii) Minima (Dark Fringe)-

$$\Delta = \pm \frac{(2m+1)}{2} \lambda$$

$$2\mu t \cos\alpha = \pm \frac{(2m+1)}{2} \lambda$$

Fringes: Fringes are locus of equal thickness.

Wedge shaped:

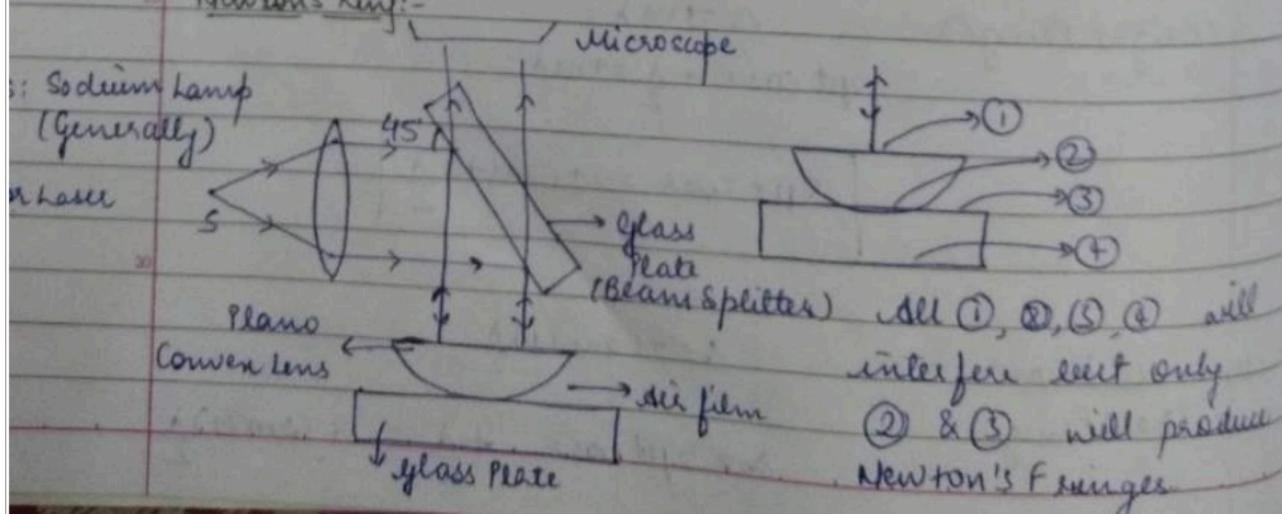


$$t_1 < t_2 < t_3 < \dots$$

Straight line pattern will be obtained.

(Cross secⁿ of air film is straight line)

Newton's Ring:-



All ①, ②, ③, ④ will interfere but only ② & ③ will produce Newton's Fringes.

[air film cross-section consists of circles and along this circle air film thickness is constant]

Camlin	Date	Page

Other interference pattern are not that much intense/visible.

① Condition for maxima/minima:-

(Bright) (Dark)

$$\Delta = \mu t \cos n + \frac{\lambda}{2} \quad \text{--- (1)}$$

Normal Incidence, $n=0$

Air film, $\mu=1$

$$2t + \frac{\lambda}{2} \quad \text{--- (2)}$$

(i) Maxima:-

$$2t + \frac{\lambda}{2} = +m\lambda$$

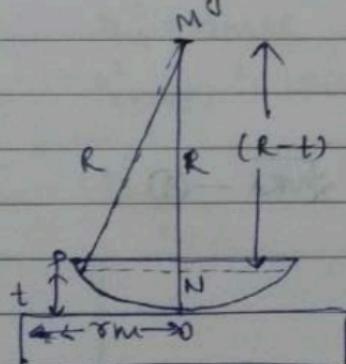
$$\boxed{2t = (2m-1)\frac{\lambda}{2}} \quad \text{--- (3)}$$

(ii) Dark:-

$$2t + \frac{\lambda}{2} = (2m+1)\frac{\lambda}{2}$$

$$\boxed{2t = m\lambda} \quad \text{--- (4)}$$

② Circular Fringes -



③ (Radii of Dark Fringes) -

Dark

Δ MNP :-

$$PM^2 = MN^2 + PN^2$$

$$R^2 = (R-t)^2 + r_m^2$$

$$r_m^2 = R^2 - R^2 - t^2 + 2Rt$$

$$r_m^2 = 2Rt - t^2 \quad \text{--- (5)}$$

∴ Air film thickness is very small

$$\therefore R \gg t^2$$

$$\Rightarrow \boxed{r_m^2 = 2Rt} \quad \text{--- (6)}$$

$$\Rightarrow r_m^2 = m\lambda R$$

$$\Rightarrow \boxed{r_m = \sqrt{m\lambda R}} \quad \text{--- (7)}$$

[air film cross-section consists of circles and along this circle air film thickness is constant]

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(Bright) (Dark)

$$\Delta = 2pt \cos n + \frac{\lambda}{2} \quad \text{--- (1)}$$

Normal Incidence, $n=0$

Air film, $\mu=1$

$$2t + \frac{\lambda}{2} \quad \text{--- (2)}$$

(ii) Maxima:-

$$2t + \frac{\lambda}{2} = \pm m\lambda$$

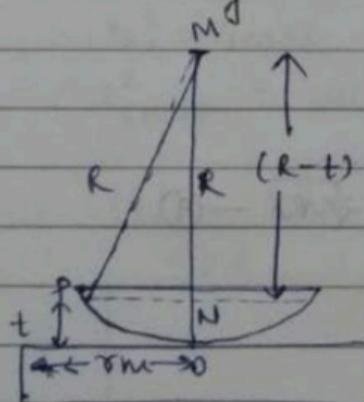
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(iii) Dark:-

$$2t + \frac{\lambda}{2} = (2m+1)\frac{\lambda}{2}$$

$$\boxed{2t = m\lambda} \quad \text{--- (4)}$$

(2) Circular Fringes -



(3) (Radii of Dark Fringes) -

Dark

$\triangle MNP$:-

$$PM^2 = MN^2 + PN^2$$

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$$\Rightarrow \boxed{r_m = \sqrt{m\lambda R}} \quad \text{--- (7)}$$

(4) Spacing:-

$$m = 1, 2, 3, \dots$$

$$\gamma_2 - \gamma_1 = \sqrt{2\lambda R} - \sqrt{\lambda R} = 0.414 \sqrt{\lambda R}$$

$$\gamma_3 - \gamma_2 = \sqrt{3\lambda R} - \sqrt{2\lambda R} = 0.318 \sqrt{\lambda R}$$

$$\gamma_4 - \gamma_3 = \sqrt{4\lambda R} - \sqrt{3\lambda R} = 0.268 \sqrt{\lambda R}$$

Area of m^{th} circle - Area of $(m-1)^{\text{th}}$ circle

[Spacing b/w fringes decreases but area remains constant.]

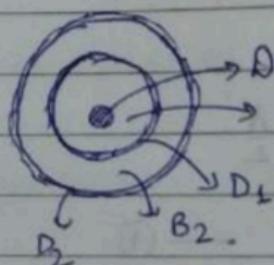
$$\pi \gamma_m^2 - \pi \gamma_{m-1}^2$$

$$\pi [m\lambda R - (m-1)\lambda R]$$

$$\pi \lambda R [m - m + 1]$$

$$\boxed{\pi \lambda R} \quad (8)$$

(5) central Dark ~~fringe~~ spot



Dark spot (Not fringe, made by reflected light)

(6) Fringes of equal Thickness-

(7) Diameter-

$$D_m = \sqrt{4m\lambda R} = 2\sqrt{m\lambda R} \quad (9)$$

Bright -

$$\gamma_m^2 = \frac{\lambda R (2m+1)}{4}$$

$$\gamma_m = \sqrt{\frac{(2m+1)\lambda R}{2}}$$

$$D = 2 \sqrt{\frac{(2m+1)\lambda R}{2}}$$

$$D = \sqrt{2(2m+1)\lambda R}$$

Dark fringes are clearly confined on bright fringe. That's why we are dark.

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Transmitted :-

$$\lambda = 2\mu t \cos\theta$$

$$\mu = 1, r = 0$$

$$\Delta = 2t$$

Bright: $2t = n\lambda$

Dark: $2t = (2m+1)\frac{\lambda}{2}$

⑧ Newton's Fringes are called Localised Fringes.

Because they are formed on top of convex lens.

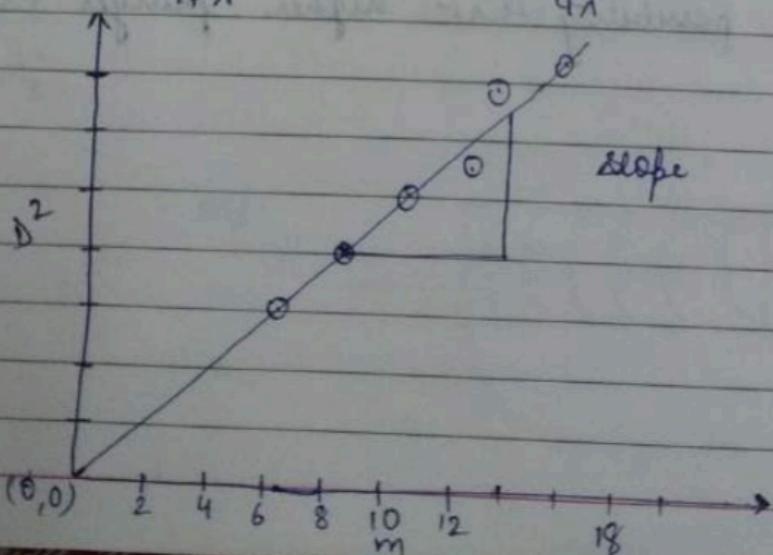
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$$A - B = D \approx 1$$

$$D_m^2 = 4m\lambda R$$

$$D_{(m+p)}^2 = 4(m+p)\lambda R$$

$$\frac{D_{(m+p)}^2 - D_m^2}{4p\lambda} = R = \frac{\text{slope}}{4\lambda}$$



Q- How Newton Rings (Fringes) are formed?
② & ③ interference

$$\rightarrow \mu \frac{[D_{M+P}^2 - D_m^2]_{\text{air}}}{4P\lambda} = R$$

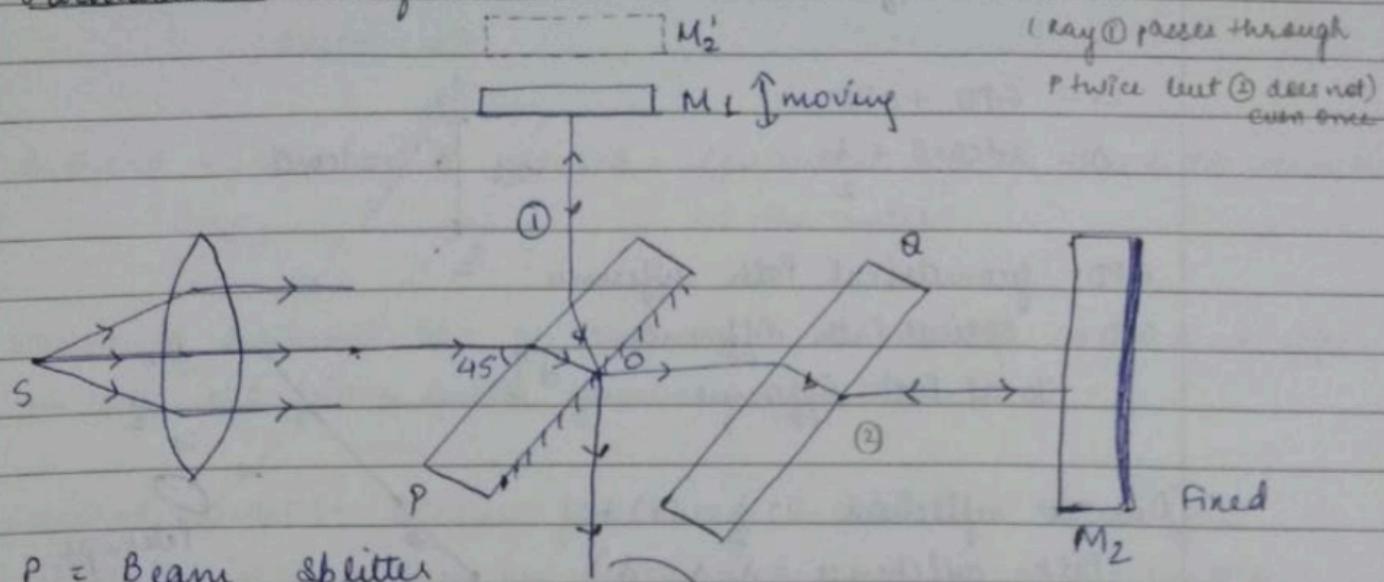
$$\frac{[D_{M+P}^2 - D_m^2]_{\text{air}}}{4P\lambda} = R$$

$$\Rightarrow \mu = \frac{[D_{M+P}^2 - D_m^2]_{\text{air}}}{[D_{M+P}^2 - D_m^2]_{\text{sig}}}$$

(We can find out the refractive index of liquid by performing the exp. two times \rightarrow for air & for liquid by placing liquid in place of air).

- Newton's ring exp is type of division of amplitude.
- We cannot use mirror instead of glass plate because due to mirror reflection brightness will be very large & dark fringes will get dull. Not appear clearly.
- If we use white light in place of monochromatic light (sodium lamp), then centre will be bright and then coloured fringes will be formed of those colours whose 'l' satisfy maxima cond'. There is a possibility that higher fringes may not appear.

Michelson's Interference :-



P = Beam splitter

50% silvered

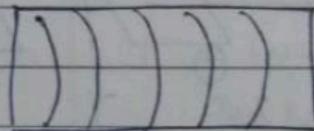
Q = Compensating glass plate

M_2' = Image of M_2

This ray appears to come from M_2' but not really comes from M_2' .

Types of Fringes:-

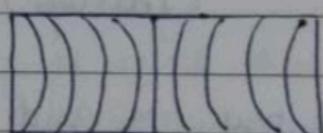
1) M_1 ——————→



Curved fringes with
Circular fringes
convexity towards
thin edge of the wedge

2)
—————→

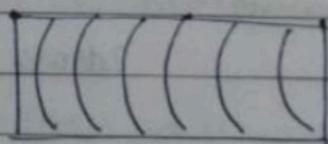
Fixed M_1 ——————→



Curvature
straight fringes

3)
—————→

M_2'



M_1

M_2' = Image of concave M_1 (just ter)

Michelson's Interferometer:-

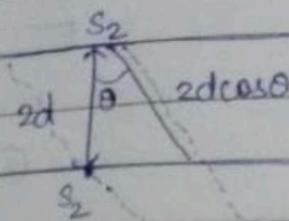
$$\Delta = \text{GPD} + \text{OPD}$$

$$\Delta = 2d \cos \theta + \frac{\lambda}{2}$$

GPD = geometrical Path difference

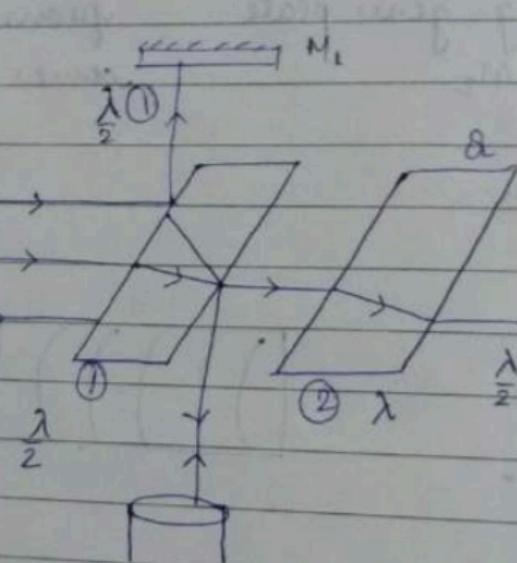
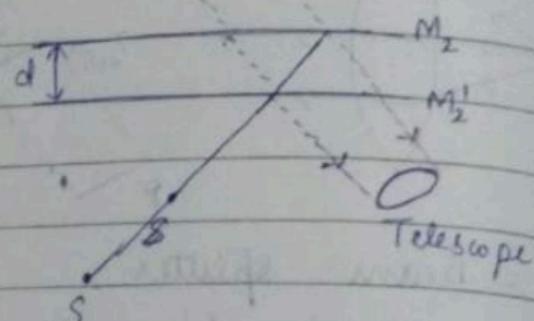
OPD = Optical Path difference

Δ = Total Path difference



(Due to reflection $(\frac{\lambda}{2})$ & $(\frac{\lambda}{2})$)

$$\text{Path difference} = \lambda - \frac{\Delta}{2} = \frac{\lambda}{2}$$



Reflection
of the wave
(Upper wave)

Fixed

(Telescope)

If the distance b/w M_1 and M_2 reduces, it appears that circles are vanishing in one.

(1) Bright (Maxima)-

$$2d \cos \theta + \frac{\lambda}{2} = m\lambda$$

$$2d \cos \theta = (2m-1) \frac{\lambda}{2}$$

use of compensating plate?

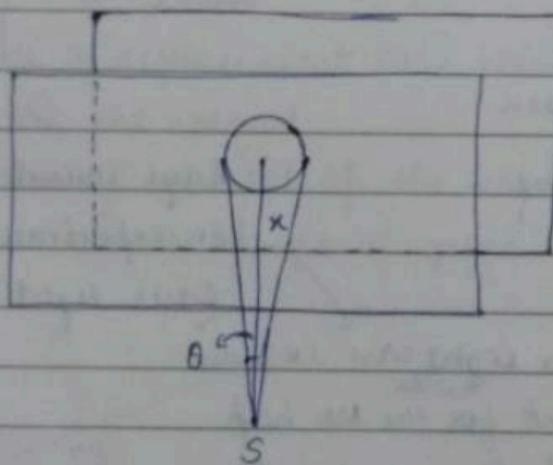
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(2) Minima -

$$2dc\cos\theta = n\lambda$$

- If M_1 and M_2 distance is reduced = concentric circles tends to vanish at the centre
- Whereas if distance b/w M_1 and M_2 is increased : circles tend to appear to come out from centre growing outwards.
- CIRCULAR FRINGES - Because for every inclination (θ) we get different fringe so they are called fringes of equal inclination.

Fringes of equal inclination - (Haidinger's Fringes)



No. of fringes vanished
in given by

$$N = \frac{x_1 - x_2}{\lambda} = N\lambda$$

($N =$ No. of fringes disappear in centre)
For particular angle ray
path difference is equal to $n\lambda$.
 \therefore Circular rings are obtained.

Fringes of equal thickness

Types

Fringes of equal inclination

- Here, the fringes are obtained on telescope.

- If both mirrors are at equal distance $d = 0$

\therefore Path difference $\Delta = \frac{\lambda}{2}$

\therefore Only dark light will be seen throughout the plane.

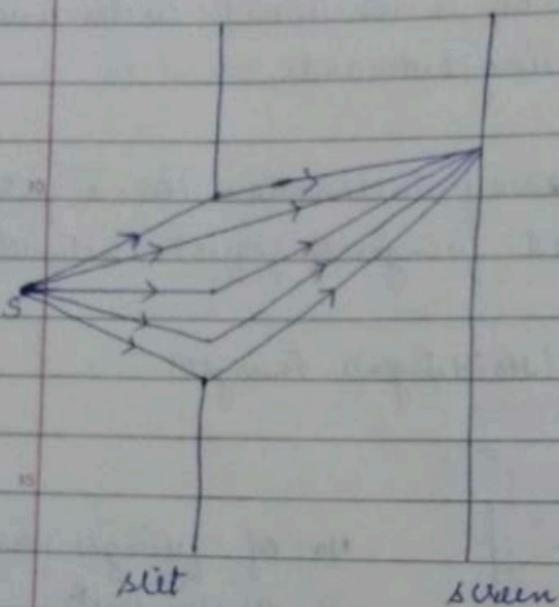
Diffraction:-

Bending of light

Diffraction

5

Fresnel's



Fraunhofer

source = ∞

Rays travel parallel
(In experiment we use
laser light)

No light can be used

but for the help
of lens combination

Rays travel making
angles

→ Fresnel's has drawback

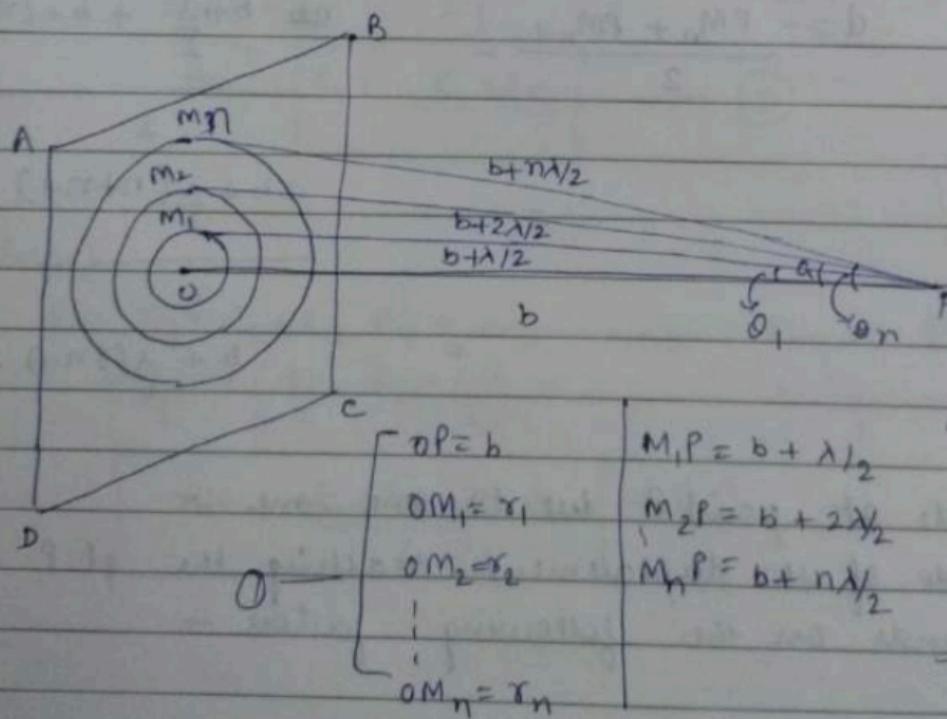
Fresnel's half period zone method:-
Theoretical concept

1 Assumption path difference b/w

2 Top and bottom rays $\Rightarrow \pm \frac{1}{2}$

Fresnel zone $\frac{1}{2}$ period zone method to find intensity of light at a point due to wavefront. This method is based on following assumptions -

- (1) Given wavefront is divided into small regions - each region is called a zone. These zones are such that there is a phase difference of π (path difference = $1/2$, time difference = $t/2$) b/w the light rays reaching the point P from the extreme of the zone. Hence, these are called as $\frac{1}{2}$ period zone. Each $\frac{1}{2}$ period zone behaves like a source of secondary wavelets.
- (2) Displacement of a point on the screen due to entire wavefront = algebraic sum of the displacements at that point due to secondary wavelets emitted from each zones.
- (3) Amplitude of displacement at a point due to a zone depends -
 - (i) angle b/w the normal
 - (ii) Line joining the pole of the wavefront to that point.
 - (iii) On the distance of point from the zone.



1) Area of half period zone -

$$OM_nP \rightarrow r_n^2 = n^2\lambda^2 + nb\lambda \quad \text{--- (3)}$$

$$\begin{aligned} \lambda^2 &\ll b \\ r_n^2 &= nb\lambda \end{aligned} \quad \text{--- (4)}$$

$$\begin{aligned} \text{Area of } n^{\text{th}} \text{ zone} &= \text{Area of } n^{\text{th}} \text{ circle} - \text{Area of } (n+1)^{\text{th}} \text{ circle} \\ &= \pi nb\lambda - \pi(n+1)b\lambda \\ &= \pi b\lambda [n - (n+1)] \\ \boxed{\text{Area of } n^{\text{th}} \text{ zone} = \pi b\lambda} & \quad \text{--- (5)} \end{aligned}$$

2) Separation between the zones -

$$\text{Width of zone} = r_n - r_{n-1} \quad \text{--- (6)}$$

$$r_2 - r_1 = \sqrt{2b\lambda} - \sqrt{b\lambda} = 0.414 \sqrt{b\lambda}$$

$$r_3 - r_2 = \sqrt{3b\lambda} - \sqrt{2b\lambda} = 0.318 \sqrt{b\lambda}$$

$$r_4 - r_3 = \sqrt{4b\lambda} - \sqrt{3b\lambda} = (2 - 1.732) \sqrt{b\lambda} = 0.268 \sqrt{b\lambda}$$

3) Average distance of n^{th} zone from point P :-

$$\begin{aligned} d &= \frac{PM_n + PM_{n-1}}{2} = \frac{\frac{n\pi b}{2} b + nb\lambda}{2} + \frac{b + (n+1)\lambda}{2} \\ &= \frac{2b + \frac{\lambda}{2}(n+n+1)}{2} \\ &= b + \frac{\lambda}{4}(2n+1) \end{aligned} \quad \text{--- (7)}$$

4) Amplitude at point P due to one zone :-

Amplitude of the displacement reaching the pt. P from the zone depends on the following factors -

1) Area of half period zone -

$$OM_nP \rightarrow r_n^2 = \frac{n^2 \lambda^2}{4} + nb\lambda \quad \text{--- (3)}$$

$$\lambda^2 \ll b \\ \boxed{r_n^2 = nb\lambda} \quad \text{--- (4)}$$

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4) Amplitude at point P due to one zone :-

Amplitude of the displacement reaching the pt. P from the zone depends on the following factors -

(i) Amplitude is directly proportional to the area of the zone.

$$R_n \propto \pi \left[b\lambda + (2n-1) \frac{\lambda^2}{4} \right]$$

(ii) Amplitude is directly proportional to the cosθ.

θ = angle of inclination of zone.

$$R_n \propto (1 + \cos \theta_n)$$

(iii) Amplitude is inversely proportional to the avg. distance of point P from zone.

$$R_n \propto \frac{1}{b + (2n-1)\frac{\lambda}{4}}$$

$$R_n \approx \pi \lambda [1 + \cos \theta_n] \quad \text{--- (8)}$$

(iii) Resultant amplitude at the point of observation due to entire wavefront ABCD:-

$$R_{\text{res}} = R_1 - R_2 + R_3 - R_4 + \dots + R_n \quad \text{--- (9)}$$

(Odd)

$$= R_1 + \left[\frac{R_1 - R_2 + R_3}{2} \right] + \left[\frac{R_3 - R_4 + R_5}{2} \right] - \dots + \frac{R_n}{2}$$

$$\therefore R = \frac{R_1 + R_n}{2} \quad \text{--- (10)}$$

$$R_2 = \frac{R_1 + R_3}{2}$$

↓
Assumption

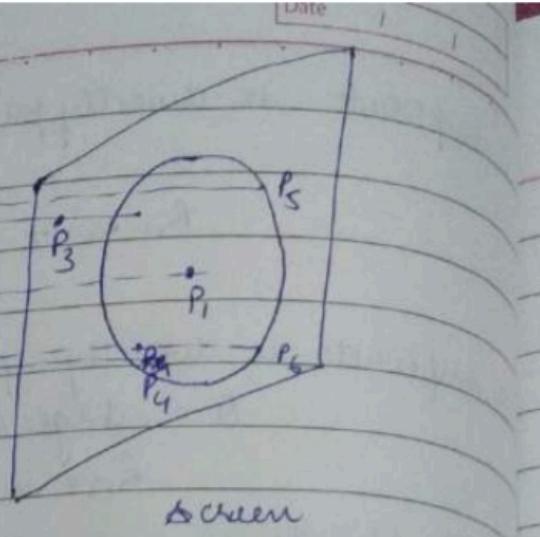
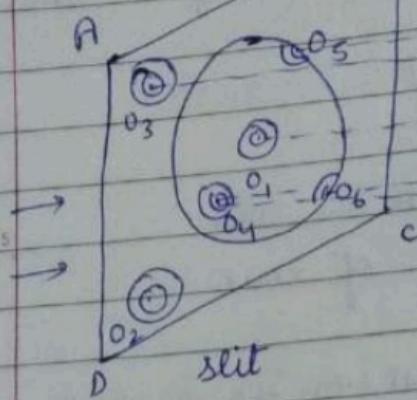
(Even)

$$R = R_1 - R_2 + R_3 - R_4 + \dots - R_n \quad \text{--- (11)}$$

$$= \frac{R_1}{2} + \left(\frac{R_1 - R_2 + R_3}{2} \right) + \dots + \frac{R_{n-1}}{2} - R_n \quad \text{--- (12)}$$

$$R = \frac{R_1 + R_{n-1}}{2} - R_n \quad \text{--- (13)}$$

Rectilinear Propagation of light :-



The intensity through the slits at corner is much different from theoretical data.

Zone Plate:-

- When we have to deal with X-ray, zone plate is used in Fresnel's Diffraction.
- Dark \rightarrow opaque
- Blank \rightarrow Transparent

Central Zone

Da Transparent $\rightarrow \Theta_{\text{one}}$
Opaque $\rightarrow \Theta_{\text{two}}$

$$r \propto \sqrt{n}$$

$$SO + OP = a + b - \textcircled{1}$$

$$SM_1 + M_1 P = SO + OP + \frac{1}{2} = a + b + \frac{1}{2}$$

(2)

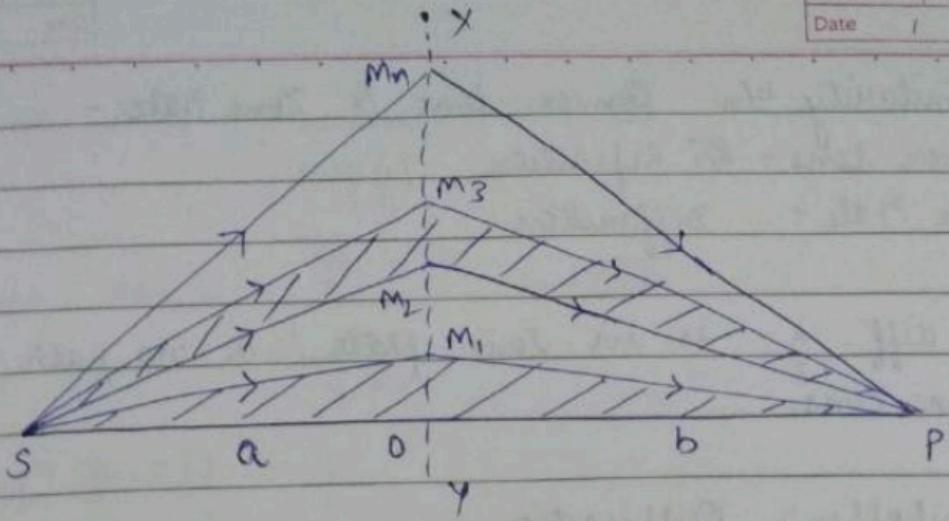
$$SM_n + M_n P = a + b + \frac{n\lambda}{2}$$

$$\Delta SM_n O \rightarrow SM_n^2 = a^2 + r_n^2 \quad \textcircled{3}$$

$$SM_n = (a^2 + r_n^2)^{1/2}$$

$$= a \left[1 + \frac{r_n^2}{a^2} \right]^{1/2} = a \left[1 + \frac{\lambda^2}{2a^2} \right]$$

$$SM_n = a + \frac{\lambda^2}{2a} \quad \textcircled{4}$$



$$\triangle PM_nD \rightarrow PM_n^2 = b^2 + r_n^2$$

$$PM_n = b \left[b + \frac{r_n^2}{2b} \right] - \textcircled{5}$$

$$\frac{1}{a} + \frac{1}{b} = \frac{n\lambda}{r_n^2} - \textcircled{6}$$

$$SM_n + & M_n P = a + b + \frac{n\lambda}{2}$$

$$a + b + \frac{n\lambda}{2} = a + b + \frac{r_n^2}{2a} + \frac{r_n^2}{2b}$$

$$\frac{1}{a} + \frac{1}{b} = \frac{n\lambda}{r_n^2}$$

$$\left[\frac{1}{a} + \frac{1}{b} = \frac{1}{f_n} \right] - \textcircled{7}$$

$$f_n = \frac{r_n^2}{n\lambda} - \textcircled{8}$$

$$\frac{1}{V} - \frac{1}{U} = \frac{1}{f} - \textcircled{9}$$

- Like a converging lens, it zone plate focusses light at pt. with same intensity.

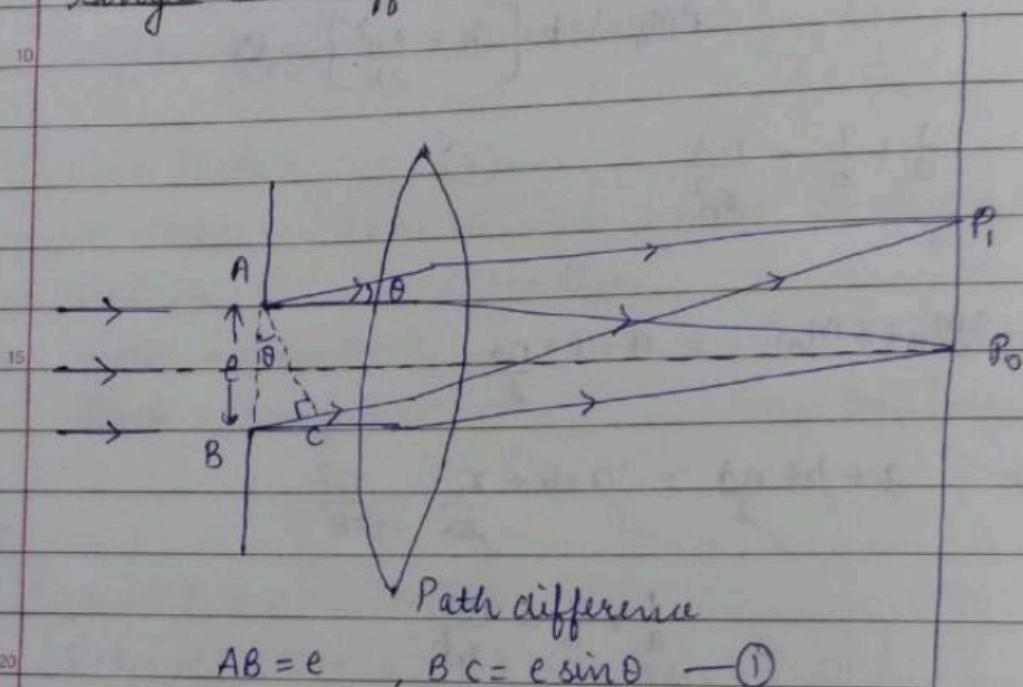
- It also possess chromatic aberration & focus light of different wavelength at different pts.

- Dissimilarity b/w Convex lens & Zone Plate:-
 Convex lens - Di Refraction
 Zone Plate - Diffraction

- Path diff. $\frac{\lambda}{2}$ is in zone plate & no path diff. in convex lens.

Eraunhofer's Diffraction:-

Single slit Diffraction:-



$$AB = e, BC = e \sin \theta \quad \text{--- (1)}$$

$$\text{Phase difference} = \frac{2\pi e \sin \theta}{\lambda} \quad \text{--- (2)}$$

n-part

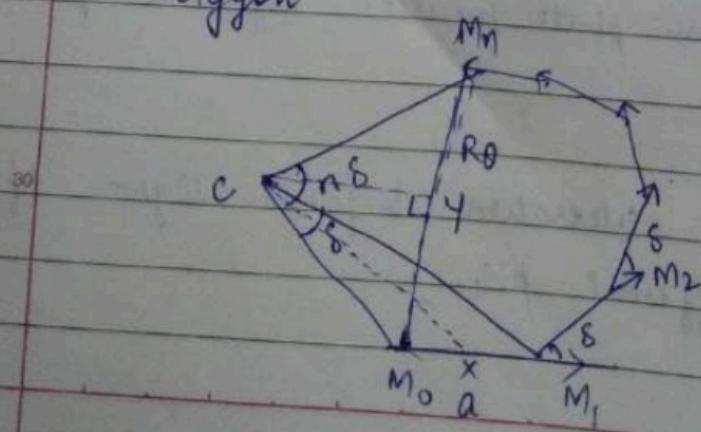
$$\delta = \frac{1}{n} \cdot \frac{2\pi}{\lambda} e \sin \theta \quad \text{--- (3)}$$

Polygon

$$M_0 X = \frac{a}{2}$$

$$M_0 Y = \frac{R_0}{2}$$

$$\angle M_0 CX = \frac{s}{2}$$



$$\Delta CM_0 X \rightarrow CM_0 = \frac{\frac{a}{2}}{\sin\left(\frac{\delta}{2}\right)} \quad \text{--- (4)}$$

$$\Delta CM_0 Y \rightarrow CM_0 = \frac{\frac{R_0}{2}}{\sin\left(\frac{n\delta}{2}\right)} \quad \text{--- (5)}$$

eqn (5) ÷ (4)

$$\frac{\frac{R_0}{2}}{\sin\left(\frac{n\delta}{2}\right)} = \frac{\frac{a}{2}}{\sin\left(\frac{\delta}{2}\right)}$$

$$R_0 = \frac{a \sin\left(\frac{n\delta}{2}\right)}{\sin\left(\frac{\delta}{2}\right)} \quad \text{--- (6)}$$

$$R_0 = \frac{a \sin\left[\frac{\pi \sin\theta}{\lambda}\right]}{\sin\left[\frac{\pi \sin\theta}{n\lambda}\right]} \quad \text{--- (7)}$$

$$R_0 = \frac{a \sin p}{\sin(p/h)} \quad \text{--- (8)}$$

$$R_0 = a n \left[\frac{\sin p}{p} \right] \quad \text{--- (9)}$$

$$p = \frac{\pi \sin\theta}{\lambda}$$

$$n \ggg, \sin \approx \frac{p}{\pi}$$

$$\text{If } \theta = 0, p = 0, \delta = 0$$

$$R_0 = a n$$

$$R_0 = R_0 \left[\frac{\sin p}{p} \right] \quad \text{--- (10)}$$

P₁

$$I \propto R_0^2 \Rightarrow I = k R_0^2 \left[\frac{\sin p}{p} \right]^2 \quad \text{--- (11)}$$

P₀

$$I_0 = k R_0^2 = k a^2 n^2$$

$$I = I_0 \left[\frac{\sin p}{p} \right]^2$$

(12)

I) Principal Maxima :-

$$p = 0$$

$$I = I_0$$

$$\frac{y \sin \theta}{\lambda} = 0$$

$$y \sin \theta = 0$$

$$\boxed{\theta = n\pi}$$

Principal Maxima : $\theta = 0$

II) Minima :-

$$\sin p = 0, p \neq 0$$

$$p = \pm m\pi$$

$$\frac{y \sin \theta}{\lambda} = \pm m\pi$$

$$\boxed{y \sin \theta = \pm m\lambda}$$

$y = \text{Slit width}$

Eqⁿ of Minima.

(13)

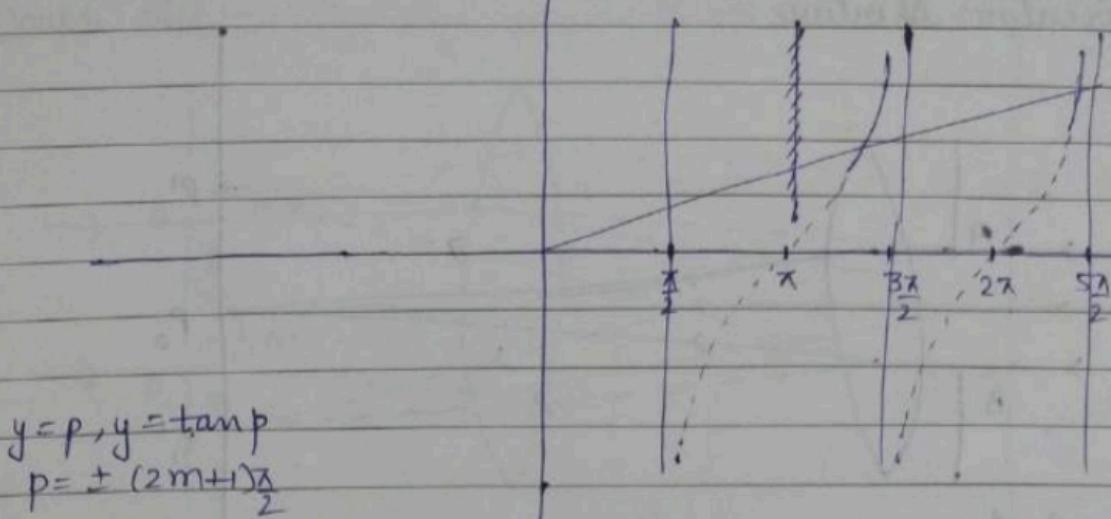
III) Secondary Maxima :-

$$\frac{dI}{dp} = 0$$

$$\sin p = 0$$

or $p = \tan^{-1} p \rightarrow$ condition for
Secondary Maxima

✓



$$y = p, y = \tan p$$

$$p = \pm \frac{(2m+1)\pi}{2}$$

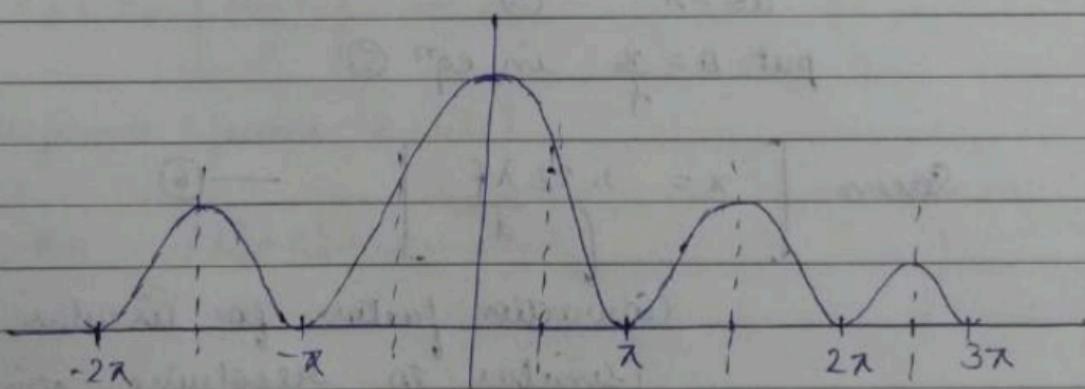
$$p = 0, \pm \frac{3\pi}{2}, \pm \frac{5\pi}{2}, \dots$$

1st Order Secondary Maxima $\leftarrow \frac{3\pi}{2} \Rightarrow I_1 = \frac{I_0}{22}$

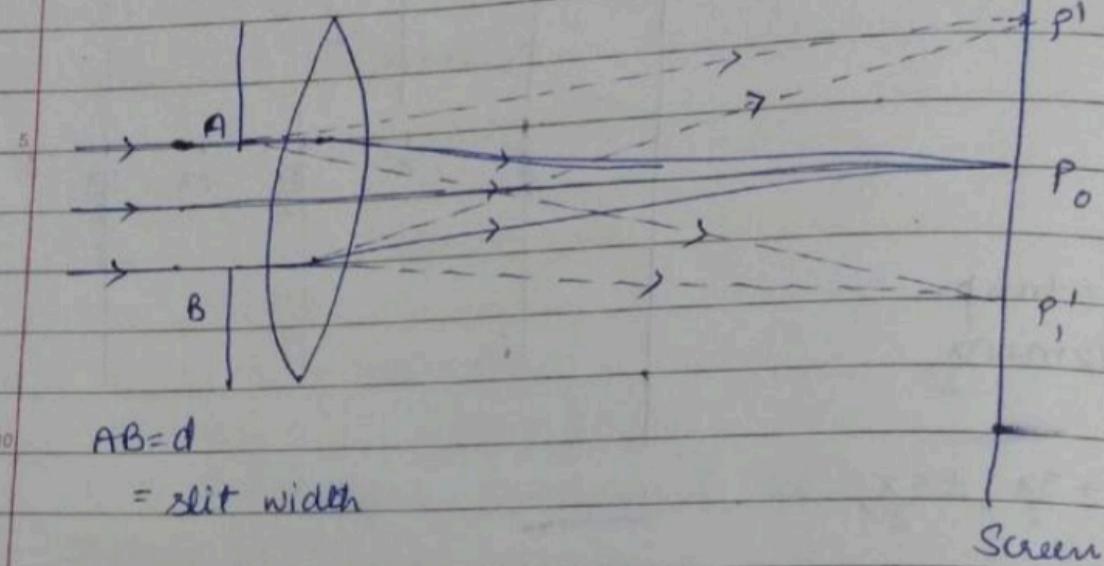
2nd Order Secondary Maxima $\leftarrow \frac{5\pi}{2} \Rightarrow I_2 = \frac{I_0}{61}$

3rd Order Secondary Maxima $\leftarrow \frac{7\pi}{2} \Rightarrow I_3 = \frac{I_0}{121}$

} Intensity
goes on
decreasing



Circular Aperture :-



$$\text{Dark: } d \sin \theta = m\lambda \quad \text{--- (1)}$$

$$\text{Bright: } d \sin \theta = (2m-1) \frac{\lambda}{2} \quad \text{--- (2)}$$

$m=1$

$$d \sin \theta = \lambda \quad \text{--- (3)}$$

$$\sin \theta \approx \theta \approx \frac{x}{f} \quad \text{--- (4)}$$

$$d\theta = \lambda \quad \text{--- (5)}$$

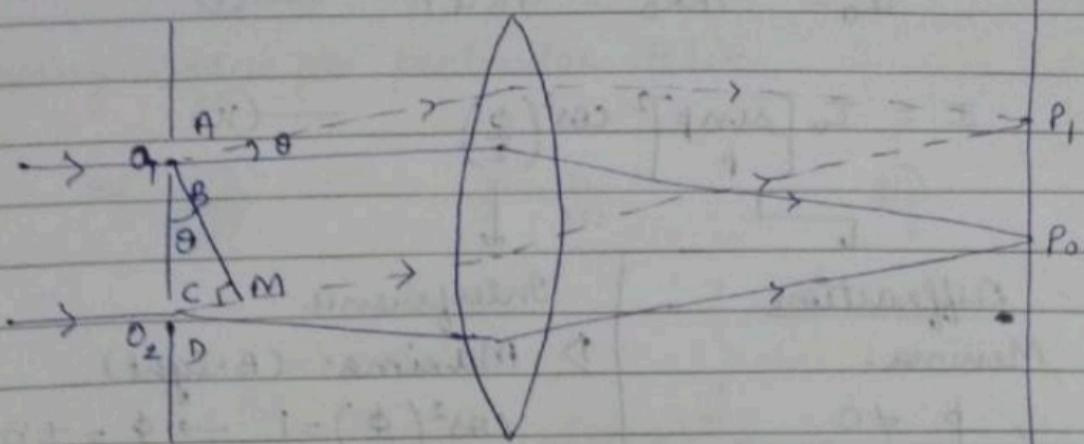
$$\text{put } \theta = \frac{x}{f} \text{ in eqn (5)}$$

Screen

$$x = 1.22 \frac{\lambda f}{d} \quad \text{--- (6)}$$

(Correction factor for circular aperture
[similar to resolving power of telescope])

Double Slit :-

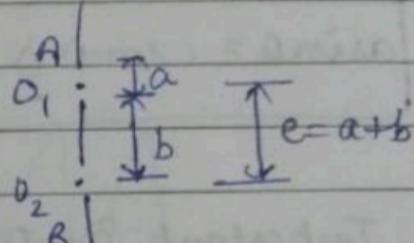


$$\text{Path difference, } DM = c \sin \theta \quad \text{--- (1)}$$

c = distance between centre of two slits

$$\text{Phase difference, } \phi = \frac{2\pi}{\lambda} c \sin \theta \quad \text{--- (2)}$$

$$p = \frac{\pi a \sin \theta}{\lambda} \quad \text{--- (4)}$$



Single Slit:

$$R_0 = R_0 \left[\frac{\sin p}{p} \right]^* \quad \text{--- (3)}$$

Interference (from 2 slits)

$$R = \sqrt{R_0^2 + R_0^2 + 2R_0 R_0 \cos \phi} \quad \text{--- (5)}$$

$$[\because A = \sqrt{a_1^2 + a_2^2 + 2a_1 a_2 \cos \phi}]$$

$$R = 2R_0 \cos \left(\frac{\phi}{2} \right) \quad \text{--- (6)}$$

$$I \propto R^2$$

$$I = KR^2 = 4KR_0^2 \cos^2 \left(\frac{\phi}{2} \right) \quad \text{--- (7)}$$

$$I = 4KR_0^2 \left[\frac{\sin p}{p} \right]^2 \cos^2 \left(\frac{\phi}{2} \right) \quad \text{--- (8)}$$

$$\text{If } \theta_0 = 0, p = 0, \phi = 0 \\ I_0 = 4KR_0^2 = 4KA^2n^2 \quad \text{--- (9)}$$

$$I = I_0 \left[\frac{\sin p}{p} \right]^2 \cos^2\left(\frac{\phi}{2}\right) \quad \text{--- (10)}$$

Diffraction

1) Maxima: Minima:

$$\sin p = 0, p \neq 0$$

$$\text{Path diff. } a \sin \theta = \pm m\lambda \quad \text{--- (11)}$$

2) Second. Maxima:

$$p = \pm \frac{3\pi}{2}, \frac{5\pi}{2}, \dots$$

$$a \sin \theta = (2m+1) \cdot \frac{\lambda}{2} \quad \text{--- (12)}$$

Interference

D) Maxima: (Bright)

$$\cos^2\left(\frac{\phi}{2}\right) = 1 \rightarrow \frac{\phi}{2} = n\pi$$

$$\text{Path diff. } a \sin \theta = n\lambda \quad \text{--- (13)}$$

$$n = 0, 1, 2, 3, \dots$$

2) Minima (Dark):

$$\cos^2\left(\frac{\phi}{2}\right) = 0 \rightarrow \frac{\phi}{2} = (2n+1)\frac{\pi}{2}$$

$$a \sin \theta = (2n+1) \frac{\lambda}{2} \rightarrow n = 0, 1, 2, \dots \quad \text{--- (14)}$$

Important Points:-

D) Envelope of fringe pattern depends on the width 'a' of each slit and wavelength of incident light 'λ'.

2) On the other hand, the fringe width and no. of interference maxima within the central maxima depends on the opaque separation 'b', b/w the slit.

3) If increase the width of each slit, central peak becomes sharp.

4) If increase the 'λ', envelope becomes wide and fringes spread.

5) If we increase the 'b' within the central maxima the no. of interference maxima increases but separation

b/w interference maxima decreases.

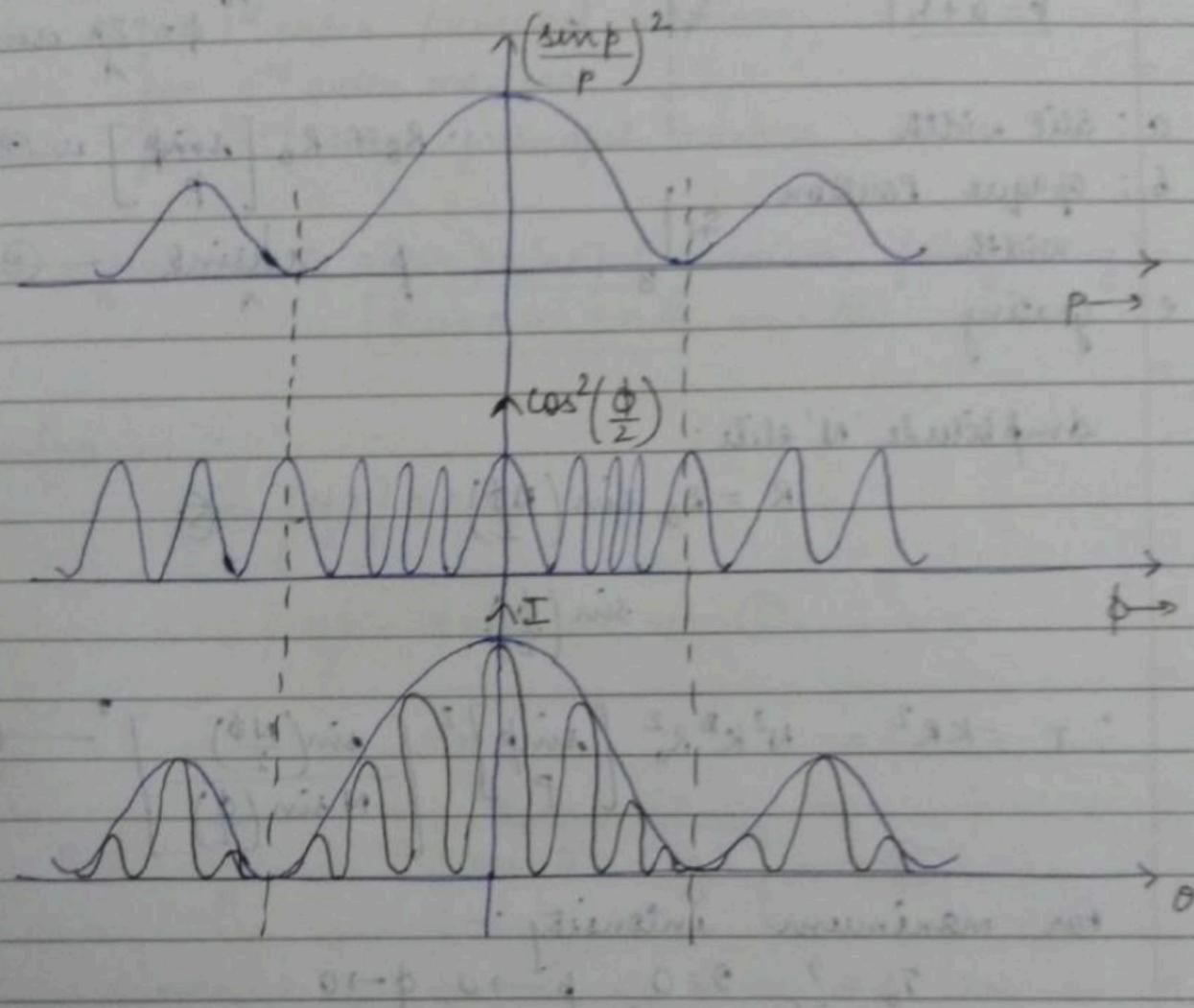
→ Missing order for particular $[\theta]$:-

$$\text{eq}^n \frac{(13)}{(11)} \Rightarrow \frac{e}{a} = \frac{n}{m} \quad \dots \quad (5)$$

$$b = 3a$$

$$n = 4m$$

$$e = a + b$$



Q

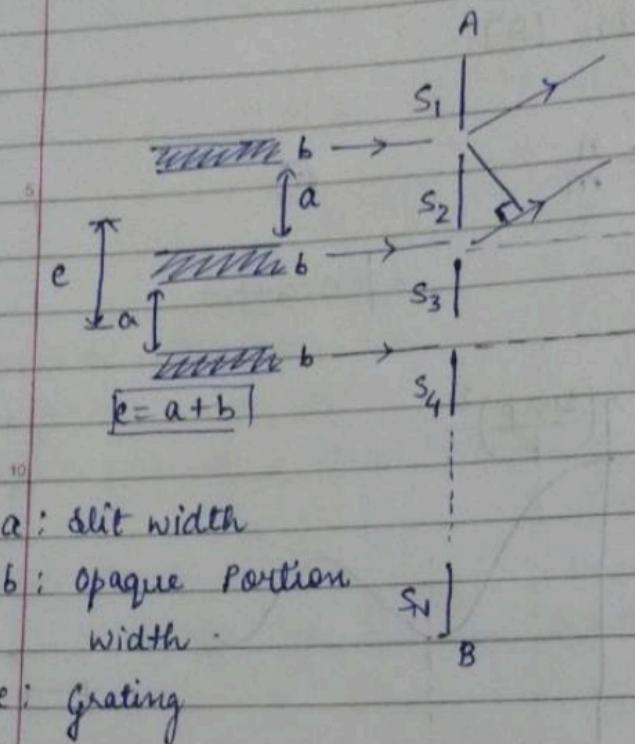
Ans

Ans

30

Plane Transmission Diffraction Grating -

N - No. of slits



a : slit width

b : opaque portion width

e : grating

Path difference,

$$\Delta = e \sin \theta \quad \text{--- (1)}$$

Phase difference,

$$\phi = \frac{2\pi}{\lambda} e \sin \theta \quad \text{--- (2)}$$

$$R_D = R_0 \left[\frac{\sin p}{p} \right] \quad \text{--- (3)}$$

$$p = \frac{\pi e \sin \theta}{\lambda} \quad \text{--- (4)}$$

Amplitude 'N' slits:

$$R = R_0 \frac{\sin \left(\frac{N\phi}{2} \right)}{\sin \left(\frac{\phi}{2} \right)} \quad \text{--- (5)}$$

$$\therefore I = K R^2 = N^2 K R_0^2 \left[\frac{\sin p}{p} \right]^2 \left[\frac{\sin \left(\frac{N\phi}{2} \right)}{N \sin \left(\frac{\phi}{2} \right)} \right]^2 \quad \text{--- (6)}$$

for maximum intensity :-

$$I_0 = ?, \theta = 0, p \rightarrow 0, \phi \rightarrow 0$$

$$\therefore \boxed{I_0 = K N^2 R_0^2}$$

$$\therefore I = I_0 \left[\frac{\sin p}{p} \right]^2 \cdot \left[\frac{\sin \left(\frac{N\phi}{2} \right)}{N \sin \left(\frac{\phi}{2} \right)} \right]^2 \quad \text{--- (7)}$$

(I) Principal Maxima-

$$\sin\left(\frac{\phi}{2}\right) = 0$$

$$I = I_0 \left[\frac{\sin p}{p} \right]^2 \quad \text{--- (8)}$$

$$\frac{\phi}{2} = \pm n\pi \quad \text{--- (9)}$$

$n = 1, 2, 3, \dots$ [$n \neq 0$ because $n=0$ is for central maxima]

$n=1$, for 1st order principal maxima

$n=2$, for 2nd order maxima

$n=3$, for 3rd order principal maxima

Path difference is (for principal maxima for grating)-

$$es \sin \theta = \pm n\lambda \quad \text{--- (10)}$$

(II) Minima:-

$$\sin\left(\frac{N\phi}{2}\right) = 0$$

$$\frac{N\phi}{2} = \pm m\pi \quad \text{--- (11)}$$

$$\frac{\phi}{2} = \frac{\pm m\pi}{N}$$

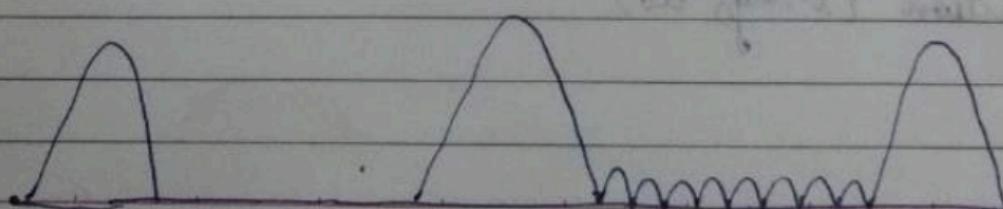
Path difference : $es \sin \theta = \pm \frac{m\lambda}{N} \quad \text{--- (12)}$

$m = 1, 2, 3, \dots, m \neq 0, N, 2N, 3N, \dots$

$N \rightarrow (N-1)$ No. of minima

($N-2$) No. of secondary maxima

$N=10$



1st order
principal max.

(III) Secondary Maxima:-

$$\frac{dI}{d\phi} = 0$$

$$\tan \left[\frac{N\phi}{2} \right] = N \tan \left[\frac{\phi}{2} \right]. \quad \text{--- (13)}$$

$$\sin \left[\frac{N\phi}{2} \right] = N \tan \left[\frac{\phi}{2} \right] \sec \left[\frac{N\phi}{2} \right]$$

$$\frac{\sin^2 \left[\frac{N\phi}{2} \right]}{\sin^2 \left[\frac{\phi}{2} \right]} = \frac{N^2}{1 + (N^2 - 1) \sin^2 \frac{\phi}{2}} \quad \text{--- (14)}$$

$$\begin{aligned} I_{\text{at secondary max.}} &= \frac{1}{1 + (N^2 - 1) \sin^2 \left(\frac{\phi}{2} \right)} \\ I_{\text{at principal max.}} &= 1 \end{aligned} \quad \text{--- (15)}$$

Conclusion -

- 1) As $N \uparrow$, intensity of secondary minima decreases.
- 2) There are large no. of slits in a grating that's why secondary maxima are not visible and there is darkness b/w consecutive principal maxima.
- We can find out crystal structure of a material by using diffraction (x-rays etc.)