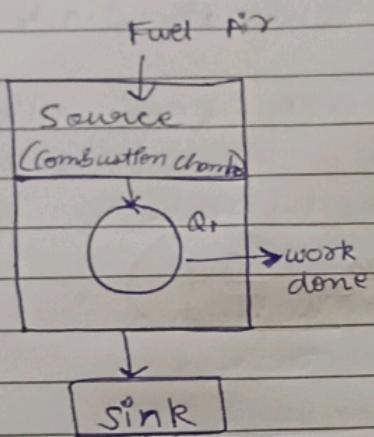


## Unit - 3

### Air standard cycles

#### Basic Principle of internal combustion -



Assumptions -

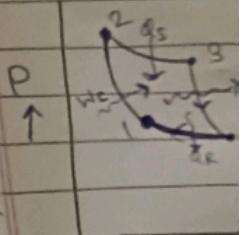
Ideal / Air standard cycle assumption.

Air cycle Analyse

working medium perfect gas throughout.

Heat is reversible,  
Heat is instantaneous  
Compression reversible  
Entropy, Kinetic and  
operation

Carnot



#### Theoretical Assumptions -

- (1) Working medium is a perfect gas throughout. It follows ideal gas equation  $PV = nRT$ .
- (2) Working medium is a fixed mass of air either contained in closed system or flowing with constant rate in a closed circuit.
- (3) Physical constants of working medium are same as that of air.
- (4) Working medium has constant specific heat.
- (5) The working medium does not undergo any chemical changes throughout the cycle.

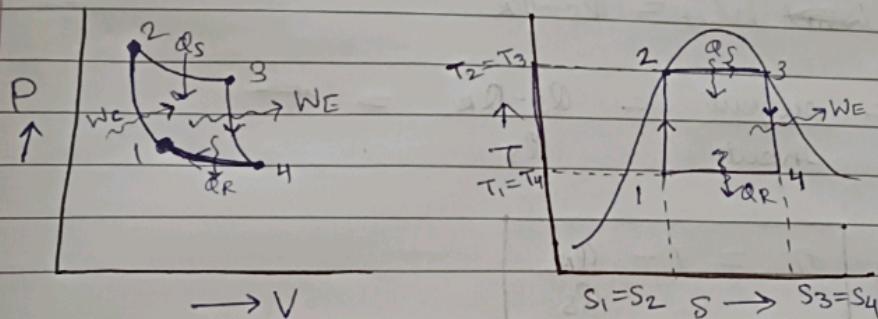
1-2  
2-3

3-1

Change  
refe

- ⑥ Heat is supplied and rejected in a reversible manner  
 ⑦ Heat is supplied and rejected instantaneously  
 ⑧ Compression and expansion processes are reversible adiabatic. (No loss or gain of entropy, zero friction)  
 ⑨ Kinetic and potential energies are neglected.  
 ⑩ Operation of the engine is frictionless.

### Carnot Cycle -



1-2 : Reversible adiabatic compression

2-3 : Reversible isothermal Heat Addition to working fluid from external source.

3-4 : Reversible Adiabatic expansion of working fluid.

4-1 : Reversible isothermal Heat rejection in the same sink.

Change in entropy during heat supply and heat rejection is same.

$$dS = \frac{dq}{T} \Rightarrow dq = TdS$$

$$dq_s = (S_3 - S_2)T \quad \text{and} \quad dq_R = (S_4 - S_1)T$$

$$\text{Q}_S = m \times T_H (S_3 - S_2)$$

$$\text{Q}_R = m \times T_L (S_4 - S_1)$$

$T_H$  = Highest temp. of working fluid in cycle  
 $T_L$  = Lowest temp.

Accn to first law:

Net work done = Net Heat transfer

$$\text{Net Work} = Q_S - Q_R$$

$$\eta = \frac{\text{output}}{\text{Input}} = \frac{Q_S - Q_R}{Q_S} = +$$

$$\eta = 1 - \frac{Q_R}{Q_S}$$

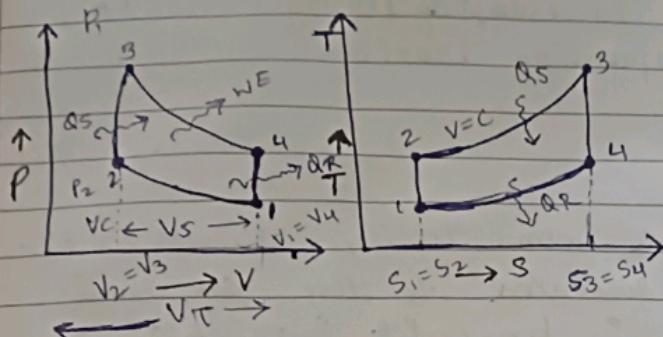
$$\eta = \frac{m T_H (S_3 - S_2) - m T_L (S_4 - S_1)}{m T_H (S_3 - S_2)}$$

$$\therefore S_1 = S_2 \text{ and } S_4 = S_3$$

$$\eta = \frac{T_H (S_3 - S_2) - T_L (S_3 - S_2)}{T_H (S_3 - S_2)}$$

$$\eta = 1 - \frac{T_L}{T_H}$$

Air standard Otto cycle :-



$V_s$  = Stroke Volume

$V_t$  = Total volume

$V_c$  = Clearance Volume

-  $V_{1-2}$ : Air is compressed adiabatically through a compression ratio:

$$\alpha = \frac{V_1}{V_2} = \frac{V_t}{V_c}$$

$$\alpha = \frac{V_s + V_c}{V_c} = 1 + \frac{V_s}{V_c}$$

$V_{2-3}$ : Piston is momentarily at rest at TDC and heat is added to the working fluid at a constant volume with an external source which has The pressure rises through an explosion ratio:

$$\alpha = \frac{P_3}{P_2}$$

$V_{3-4}$ : This increased high pressure exerts a greater amt of force on the piston and pushes the piston towards the

BDC and expansion of working fluid takes place isentropically. This gives work.

~~TED~~ • The expansion ratio

$$\frac{T_2}{T_1}$$

V<sub>4-1</sub>:

The piston is momentarily at rest at BDC and heat is rejected to the external sink, which is brought into contact with the The process comes to V<sub>1</sub> and the cycle is completed.

Thermal efficiency:-

Let m is fixed mass of air flowing through the cycle.

Heat supplied during process 2 → 3:

$$Q_S = mC_V(T_3 - T_2)$$

Heat rejected during (4 → 1):

$$Q_R = mC_V(T_4 - T_1)$$

Thermal efficiency -

$$\eta = \frac{\text{output}}{\text{input}} = \frac{Q_S - Q_R}{Q_S} = \frac{mC_V(T_3 - T_2)}{mC_V(T_3 - T_2)}$$

$$\eta = 1 - \frac{(T_4 - T_1)}{T_3 - T_2}$$

At point 2 -

$$\frac{V_1}{V_2} = \gamma \Rightarrow V_2 = \frac{V_1}{\gamma}$$

At 1 → 2 :-

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$

$$P_2 = P_1 \left(\frac{V_1}{V_2}\right)^\gamma \Rightarrow P_2 = P_1 (\gamma)^{\gamma}$$

$$\frac{T_2}{T_1} = \left(\frac{V_1}{V_2}\right)^{\gamma-1}$$

$$T_2 = T_1 (\alpha)^{\gamma-1}$$

At point 3 -

$$V_3 = V_2$$

$$V_3 = \frac{V_1}{\alpha}$$

$$\alpha = \frac{P_3}{P_2} \Rightarrow P_3 = P_2 \alpha$$

$$P_3 = P_1 \alpha (\alpha)^{\gamma}$$

Between  $2 \rightarrow 3$  -

$$\frac{P_2 V_2}{T_2} = \frac{P_3 V_3}{T_3}$$

$$T_3 = T_2 \cdot \frac{P_3}{P_2} = T_1 (\alpha)^{\gamma-1} \alpha$$

At point 4 -

$$V_4 = V_1$$

$$P_3 V_3^{\gamma} = P_4 V_4^{\gamma}$$

$$P_4 = P_3 \left(\frac{V_3}{V_4}\right)^{\gamma} = P_3 \left(\frac{V_2}{V_1}\right)^{\gamma}$$

$$P_4 = P_1 \alpha \cdot \frac{\alpha^{\gamma}}{\alpha^{\gamma}} = P_1 \alpha$$

$$P_4 = P_1 \alpha \cdot \alpha^{\gamma} = \alpha^{\gamma+1}$$

Adiabatic expansion (3 → 4) -

$$\frac{T_4}{T_3} = \left(\frac{V_3}{V_4}\right)^{\gamma-1}$$

$$T_4 = T_3 \left(\frac{V_2}{V_1}\right)^{\gamma-1}$$

$$T_4 = T_1 \alpha g_1^{r-1} \times \frac{1}{g_1^{r-1}}$$

$$T_4 = T_1 \alpha \cdot$$

NOW, Substituting values in  $\eta$  -

$$\eta = 1 - \left( \frac{T_4 - T_1}{T_3 - T_2} \right)$$

$$= 1 - \frac{T_1 \alpha - T_1}{T_1 \alpha g_1^{r-1} - T_1 g_1^{r-1}}$$

$$= 1 - \frac{T_1(\alpha - 1)}{T_1 g_1^{r-1}(\alpha - 1)} = 1 - \frac{1}{g_1^{r-1}}$$

$$\boxed{\therefore \eta = 1 - \frac{1}{g_1^{r-1}}}$$

Q. Calculate air standard efficiency of otto cycle having compression ratio 7.

$$\Rightarrow \frac{T_2}{T_1} = \left( \frac{V_1}{V_2} \right)^{r-1}$$

$$\frac{T_3}{T_4} = \left( \frac{V_4}{V_3} \right)^{r-1} = \left( \frac{V_1}{V_2} \right)^{r-1}$$

$$\frac{T_2}{T_1} = \frac{T_3}{T_4} \Rightarrow \frac{T_3}{T_2} = \frac{T_4}{T_1}$$

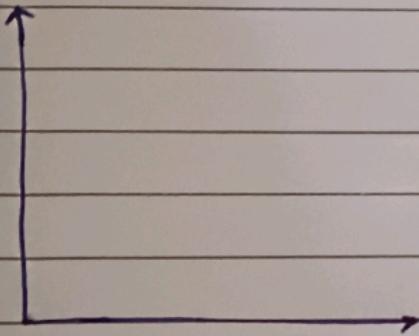
$$\frac{T_3}{T_2} - 1 = \frac{T_4 - 1}{T_1}$$

$$\frac{T_3 - T_2}{T_2} = \frac{T_4 - T_1}{T_1}$$

$$\frac{T_4 - T_1}{T_3 - T_2} = \frac{T_1}{T_2} = \left(\frac{V_2}{V_1}\right)^{\gamma-1}.$$

Mean effective pressure :-

Actual engine.



$$\frac{T_3}{T_2} - 1 = \frac{T_4}{T_1} - 1$$

$$\frac{T_3 - T_2}{T_2} = \frac{T_4 - T_1}{T_1} \rightarrow \frac{T_4 - T_1}{T_3 - T_2} = \frac{T_1}{T_2} \Rightarrow \left(\frac{V_2}{V_1}\right)^{4-1}$$

$$\eta_{ih} = 1 - \frac{T_4 - T_1}{T_3 - T_2}$$

$$1 - \frac{T_1}{T_2} = 1 - \left(\frac{V_2}{V_1}\right)^{4-1}$$

$$\eta_{ih,0ff} = 1 - \frac{1}{\lambda^{4-1}}$$

Inlet valve  
Exhaust valve

process 0-1 suction

1-2 Adiabatic compression

2-3 Constant volume

3-4 Adiabatic expansion

4-1 Blowdown of gasses

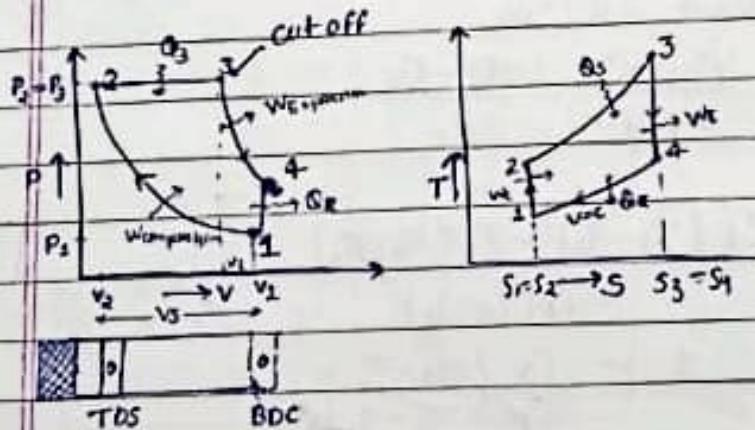
1-0 exhaust

Mean effective pressure

Rudolf Diesel name of scientist

Air Standard Diesel cycle (Corresponds to CI Engine)

compression ignition



Otto cycle  
(SI engine)  
Spark ignited

process 1 to 2

Piston move from TDS to BDC  
through a compression

Compression ratio  $\lambda = \frac{V_1}{V_2}$

ratio  $\lambda = \frac{V_1}{V_2}$

process 2 to 3, Heat is added  
to compressed air at constant pressure  
from an external source which brings  
in contact with cyl. head.

process 3 to 4, This increases high

pressure exert a amount of force

on piston & pushes piston toward

BDC expansion of working fluid air

take place adiabatically Work is done by system

point 3, heat stops This point

is known as point off Cut off

This expansion take place through expansion ratio

$$\eta_e = \frac{V_4}{V_3}$$

process 4 to 1, piston is momentarily addressed at BDC & heat is rejected to the external side the process is irreversible so control heat ultimately the initial state 1 and cycle is completed

Consider 1 kg of working fluid Air flowing through the cycle.

Heat supplied in process 2-3

$$Q_s = 1 \times c_p (T_3 - T_2)$$

Heat rejected during process 4-1

$$Q_r = 1 \times c_v (T_4 - T_1)$$

1st law

$$W_{net} = Q_{net} = Q_s - Q_r$$

$$\eta_{diesel} = \frac{\text{Output}}{\text{Input}} = \frac{Q_s - Q_r}{Q_s}$$

$$\gamma = \frac{c_p}{c_v}$$

$$\frac{c_v}{c_p} = \frac{1}{\gamma}$$

$$\frac{c_p(T_3 - T_2) - c_v(T_4 - T_1)}{c_p(T_3 - T_2)}$$

$$1 - \frac{c_v}{c_p} \left( \frac{T_4 - T_1}{T_3 - T_2} \right)$$

$$\eta_{diesel} = 1 - \frac{1}{\gamma} \left( \frac{T_4 - T_1}{T_3 - T_2} \right)$$

$$\text{Compression ratio } \eta_k = \frac{V_1}{V_2}$$

$$\text{Expansion ratio } \eta_e = \frac{V_4}{V_3}$$

$$\text{Cutoff ratio } \eta_c = \frac{V_3}{V_2}$$

$$\eta_k = \eta_e \times \eta_c$$

$$\frac{V_1}{V_2} = \frac{V_4}{V_3} \times \frac{V_3}{V_2}$$

$$\frac{V_1}{V_2} = \frac{V_4}{V_3}$$

Process 3 to 4 Adiabatic Expansion.

$$\frac{T_4}{T_3} = \left( \frac{V_3}{V_4} \right)^{\gamma-1} = \left( \frac{1}{\eta_{le}} \right)^{\gamma-1}$$

$$\frac{1}{\eta_{le}} = \frac{\eta_{le}}{\eta_K}$$

$$\frac{T_4}{T_3} = \left( \frac{\eta_{le}}{\eta_K} \right)^{\gamma-1}$$

$$\boxed{T_4 = T_3 \left( \frac{\eta_{le}}{\eta_K} \right)^{\gamma-1}}$$

Process 1 - 2

Process 2 - 3,

$$\frac{P_2' V_2}{T_2} = \frac{P_3' V_3}{T_3}$$

$$\frac{T_2}{T_3} = \frac{V_2}{V_3} \cdot \frac{T_3}{T_2}$$

$$\frac{T_1}{T_2} = \left( \frac{V_2}{V_1} \right)^{\gamma-1} = \left( \frac{1}{\eta_K} \right)^{\gamma-1}$$

$$T = T_2 \cdot \frac{1}{\eta_K^{\gamma-1}} = \frac{T_3}{\eta_{le}} \cdot \frac{1}{\eta_K^{\gamma-1}}$$

$$\boxed{T_2 = T_3 \cdot \frac{1}{\eta_{le}}}$$

$$\eta_{D(\text{ASE})} = 1 - \frac{1}{\gamma} \left( \frac{T_4 - T_1}{T_3 - T_2} \right)$$

$$= 1 - \frac{1}{\gamma} \left( \frac{\frac{T_3 \cdot \eta_C^{\gamma-1}}{\eta_K^{\gamma-1}} - \frac{T_3 \cdot 1}{\eta_{le} \eta_K^{\gamma-1}}}{T_3 - T_3 \cdot \frac{1}{\eta_{le}}} \right)$$

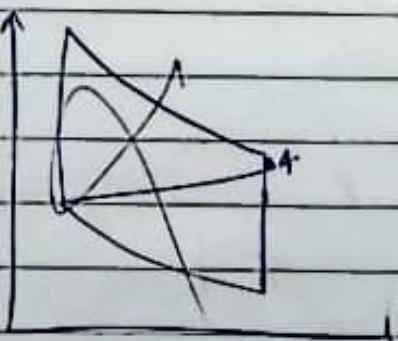
$$\eta_C = \frac{V_3}{V_2} > 1$$

$$= 1 - \frac{1}{\gamma \eta_K^{\gamma-1}} \left( \eta_C^{\gamma-1} - \frac{1}{\eta_{le}} \right)$$

$$\frac{1}{\gamma} \left( \frac{\eta_C^{\gamma-1}}{\eta_C - 1} \right) > 1$$

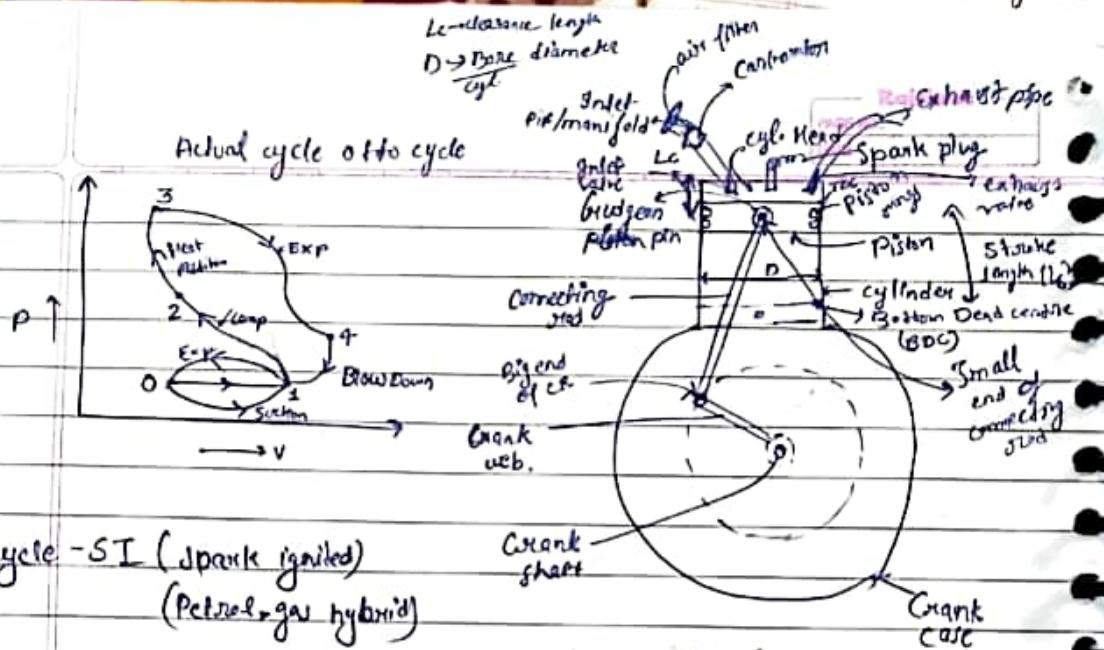
$$\boxed{\eta_D = 1 - \frac{1}{\gamma \eta_K^{\gamma-1}} \left( \eta_C^{\gamma-1} - \frac{1}{\eta_{le}} \right)}$$

for same C.R (x) ASE of Diesel cycle will always less than the ASE of Otto cycle for same CR = 15



Output:

{ 'name': 'Sakshi', 'age': 20 }



otto cycle - SI (spark ignited)  
(Petrol + gas hybrid)

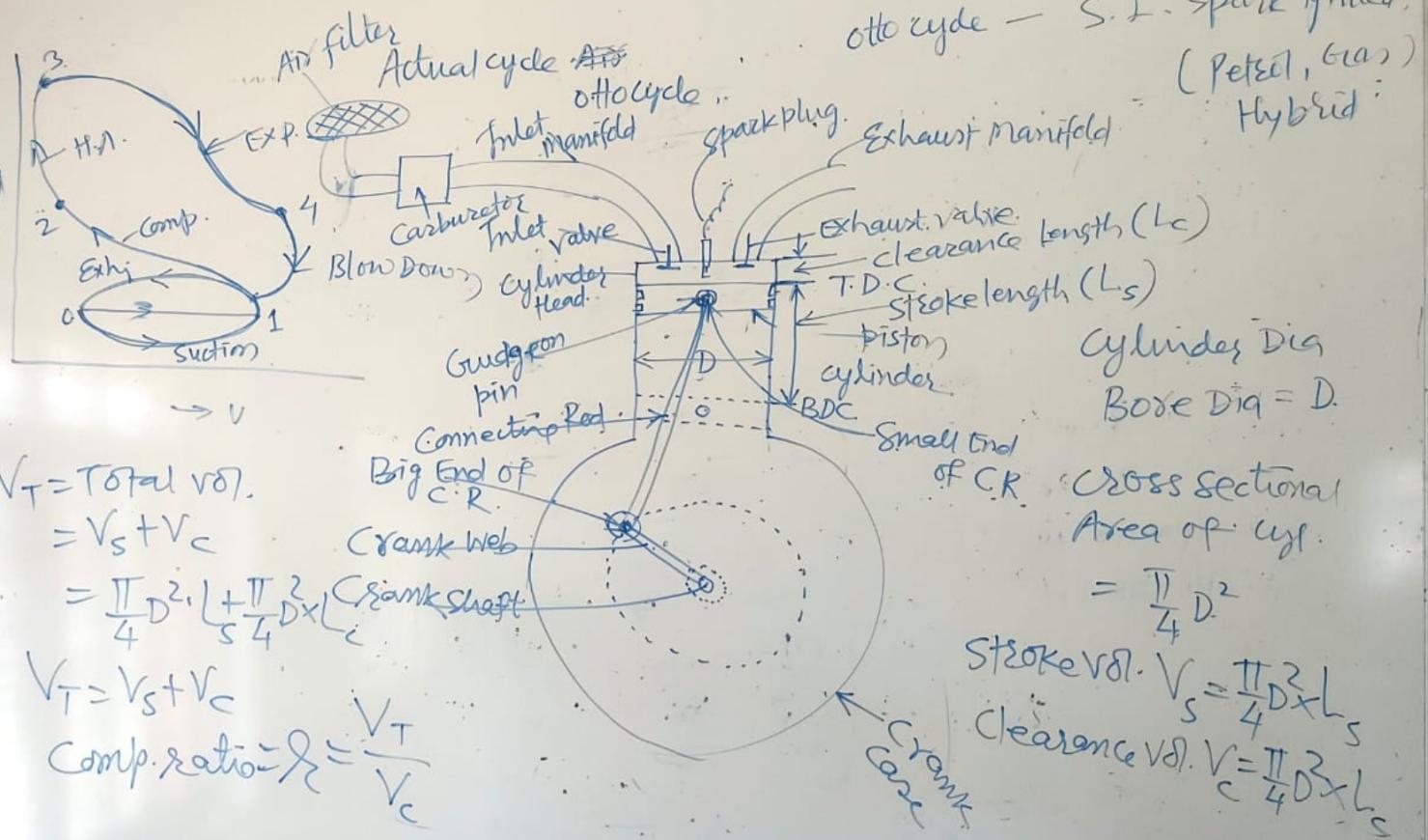
$$\text{Cross sectional area of cyl.} = \frac{\pi}{4} D^2$$

$$\text{Stroke Vol. } V_s = \frac{\pi}{4} D^2 \times L_s$$

$$\text{Clearance Vol. } V_c = \frac{\pi}{4} D^2 \times L_c$$

$$V_T = \text{Total volume} = \frac{\pi}{4} D^2 (L_c + L_s)$$

$$\text{Compression Ratio} = \frac{V_T}{V_c}$$



$$V_T = \text{Total vol.}$$

$$= V_s + V_c$$

$$= \frac{\pi D^2}{4} L_s + \frac{\pi D^2}{4} L_c$$

$$V_T = V_s + V_c$$

$$\text{Comp. ratio} - \lambda = \frac{V_T}{V_c}$$

