

# Linear Quadratic Regulator (LQR)

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## 목 차

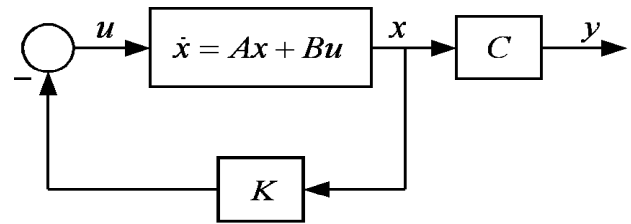
LQR Problem  
Fast Response vs. Low Control Effort  
Optimal Root Locus  
Robustness of LQR  
LQR + Integral Control  
Simulation Using Simulink

# State Feedback Control Law

## Control-law design

$$u = -Kx = -[k_1 \ k_2 \ \cdots \ k_n] \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$
$$\dot{x} = Ax + Bu$$
$$\Rightarrow \dot{x} = (A - BK)x$$

How to design  $K$  ?



Picking the gains  $K$  so  
that  $\lambda(A - BK)$  are in  
desirable locations

Reference input is set to  
zero at this time

$$G_o = C(sI - A)^{-1}B$$

$$G_q = K(sI - A)^{-1}B$$

$$G_{cl} = \frac{G(s)}{1 + G(s)}$$

## Selection of Pole Locations

Dominant Second-Order Poles Method

Linear Quadratic Regulator (LQR) Design

**System speed** vs. **Control effort**

For the faster system response, the bigger control effort is necessary

How to balance between the fast response and low control effort ?

The simplified version of LQR problem

Performance index (**cost function**)

$$J = \int_0^\infty [z^2(t) + \rho u^2(t)] dt$$

$\rho$  : weighting factor

What is the control law that minimize  $J$  for

$$\dot{x} = Ax + Bu \quad z = C_1 x$$

$z$  : output or tracking error to be minimized

# Simplified version of LQR

## Linear Quadratic Regulator (LQR) Design

Choosing different values of  $\rho$  can provide us with pole locations that achieve varying balances between a **fast response** and a **low control** effort.

$$J = \int_0^\infty [z^2(t) + \rho u^2(t)] dt$$

### Small $\rho$

- Low penalty on the control usage
- Small values of  $\int_0^\infty z^2(t) dt$
- **Faster** response

### Large $\rho$

- High penalty on the control usage
- Small values of  $\int_0^\infty u^2(t) dt$
- **Low control** effort

Optimal control law is given by linear state feedback  $u = -Kx$

$K$  : determined from **Riccati** equation

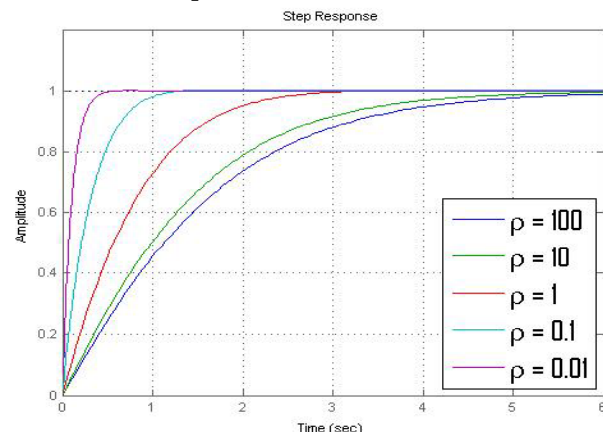
# Simplified version of LQR



Simple Inverted Pendulum  $A = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$ ,  $B = \begin{bmatrix} 0 \\ -1 \end{bmatrix}$ ,  $C = [2 \ 1]$ ,  $D = 0$

$z = y$  and “ $\rho = 1$ ” Case →  $K = [-3.24 \ -2.73]$

$\rho$	$K$	$\lambda$
100	-2.0198 -2.0124	-1.0062 + 0.0860i -1.0062 - 0.0860i
10	-2.1832 -2.1134	-1.0567 + 0.2581i -1.0567 - 0.2581i
1	-3.2361 -2.7335	-1.3668 + 0.6067i -1.3668 - 0.6067i
0.1	-7.4031 -4.9806	-2.4903 + 0.4490i -2.4903 - 0.4490i
0.01	-21.0250 -11.9185	-2.0238 -9.8947



## Comparison between LQR and pole placement

LQR provides guaranteed stability margins, while the stability margins of state feedback pole placement technique are not known

# Preliminaries

The sol. Of  $\dot{x} = Fx$  :  $x = e^{Ft}x_0$

A matrix is symmetric if  $A^T = A$

A symmetric matrix  $Q$  is *positive (semi)definite* if

$$x^T Q x > 0 \ (x^T Q x \geq 0), \ \forall x \in R^n$$

If  $(A, B)$  is **controllable** (*stabilizable*),  $\exists K$  s.t. all the eigenvalues of  $(A - BK)$  can be placed at any position (*LHP*) of the complex plane.

If  $(C, A)$  is **observable** (*detectable*),  $\exists L$  s.t. all the eigenvalues of  $(A - LC)$  can be placed at any position (*LHP*) of the complex plane.

## LQR Design

Linear Quadratic Regulator (LQR) problem

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx \end{aligned} \quad J = \int_0^\infty (x^T Q x + u^T R u) dt$$

- $Q, R$  : **weighting matrix** ( $Q$  : p.s.d.  $R$  : p.d.  $\rightarrow J \geq 0$ )
- For  $J$  to achieve its min. value, both terms must go to zero.

$$\begin{aligned} J &= \int_0^\infty x^T \overbrace{(Q + K^T R K)}^S x dt & u &= -Kx \\ &= x_0^T \left( \int_0^\infty e^{F^T t} S e^{Ft} dt \right) x_0 & F &= A - BK \\ &=: x_0^T P x_0, \ P \geq 0. & x &= e^{Ft} x_0 \end{aligned}$$

# ARE for LQR Design

Controller Design : algebraic Riccati equation (ARE)

$$A^T P + PA + Q - PBR^{-1}B^T P = 0$$
$$u = -Kx, \quad K = R^{-1}B^T P$$

Matlab :  $K = \text{lqr}(A, B, Q, R)$

When  $Q = D^T D$ , the closed-loop matrix  $F$  is stable if  $(D, A)$  is detectable.

When  $Q = D^T D$ , the matrix  $P$  is positive definite if  $(D, A)$  is observable.

## Selection of Q and R

Bryson's rule

$$J = \int_0^\infty (x^T Q x + u^T R u) dt$$

Initial choice of Diagonal matrices Q & R

$$Q_{ii} = 1/\text{max. acceptable value of } [x_i^2]$$

$$R_{ii} = 1/\text{max. acceptable value of } [u_i^2]$$

Symmetric Root Locus

$$J = \int_0^\infty (\underbrace{x^T C^T C x}_{y^T y} + u^T R u) dt$$

$$A^T P + PA + C^T C - PBR^{-1}B^T P = 0$$

$$K = R^{-1}B^T P$$

# Symmetric Root Locus

$$G_o = C(sI - A)^{-1}B$$

$$G_q = K(sI - A)^{-1}B$$

$$A^T P + PA + C^T C - PBR^{-1}B^T P = 0$$

$$C^T C = (-sI - A^T)P + P(sI - A) + PBR^{-1}B^T P$$

$$B^T(-sI - A^T)^{-1}C^T C(sI - A)^{-1}B$$

$$= B^T P(sI - A)^{-1}B + B^T(-sI - A^T)^{-1}PB$$

$$+ B^T(-sI - A^T)^{-1}PBR^{-1}B^T P(sI - A)^{-1}B$$

$$K = R^{-1}B^T P$$

$$RK = B^T P,$$

$$K^T R = PB$$

$$G_o^T(-s)G_o(s) = RG_q(s) + G_q^T(-s)R + G_q^T(-s)RG_q(s)$$

$$R + G_o^T(-s)G_o(s) = R + RG_q(s) + G_q^T(-s)R + G_q^T(-s)RG_q(s)$$

$$R + G_o^T(-s)G_o(s) = [I + G_q^T(-s)] R [I + G_q(s)]$$

$$1 + \rho^{-1}G_o(-s)G_o(s) = [1 + G_q(-s)][1 + G_q(s)]$$

$$1 + \frac{1}{\rho}(-1)^{m-n} \frac{\prod_{i=1}^m (s-z_i) \prod_{i=1}^m (s+z_i)}{\prod_{i=1}^n (s-p_i) \prod_{i=1}^n (s+p_i)} = 0$$

## Symmetric Root Locus Ex.



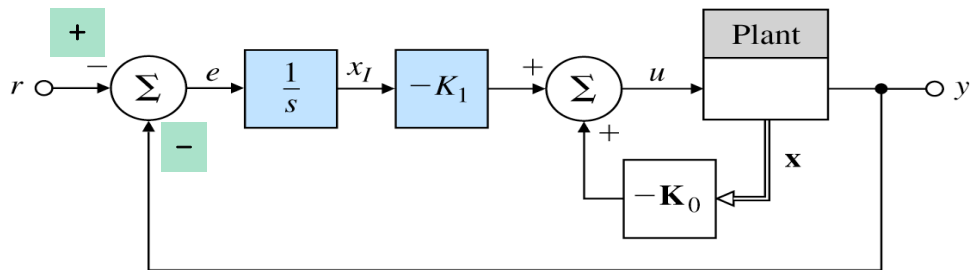
$$A = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, B = \begin{bmatrix} 0 \\ -1 \end{bmatrix}, C = \begin{bmatrix} 2 & 1 \end{bmatrix}, D = 0$$

```

3 % Optimal Root Locus
4 clear, clc
5
6 % Simple LQR
7 A = [0 1; 1 0]; B = [0; -1]; C = [2 1]; D=0;
8
9 sys0 = ss(A,B,C,D);
10 sysos = ss(-A,B,(-1)*C, D);
11 sys02 = series(sys0, sysos);
12
13 figure(1)
14 rlocus(sys02)
15 axis([-10 10 -1 1])

```

# LQR + Integral Control



$$x_I \triangleq \int e \, dt = \int (r - y) dt = \int (r - Cx) dt \Rightarrow \dot{x}_I = r - Cx$$

$$\begin{bmatrix} \dot{x} \\ \dot{x}_I \end{bmatrix} = \begin{bmatrix} A & 0 \\ -C & 0 \end{bmatrix} \begin{bmatrix} x \\ x_I \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} u + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r \quad u = -K_0 x - K_I x_I = -[K_0 \quad K_I] \begin{bmatrix} x \\ x_I \end{bmatrix}$$

$$\begin{bmatrix} \dot{x} \\ \dot{x}_I \end{bmatrix} = \begin{bmatrix} A - BK_0 & -BK_I \\ -C & 0 \end{bmatrix} \begin{bmatrix} x \\ x_I \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r$$

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## Matlab Simulation (LQR+Integral)

$$A = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, B = \begin{bmatrix} 0 \\ -1 \end{bmatrix}, C = \begin{bmatrix} 2 & 1 \end{bmatrix}, D = 0 \quad (\text{Simple Inverted Pendulum})$$

% Sec.2-3 / p.19 / LQR + Integral

clear, clc

A= [0 1; 1 0]; B= [0 ; -1]; C= [2 1]; D=0;

Aa = [A zeros(2,1); -C 0]; Ba = [B; 0]; Ca = [C 0; zeros(1,2) 1]; Da = [0 0]';

rho = 1;

Q = Ca'\*Ca; R = rho;

K = lqr(Aa, Ba, Q, R)

lambda = eig(Aa - Ba\*K);

syscl = ss(Aa-Ba\*K, [0 0 1]', Ca, Da);

figure(1)

step(syscl), grid on,

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