



# Digital Signal Processing

Design of IIR filter (part2 )

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# Step1: performance specifications

The frequency response specifications are often in the form of the tolerance scheme.

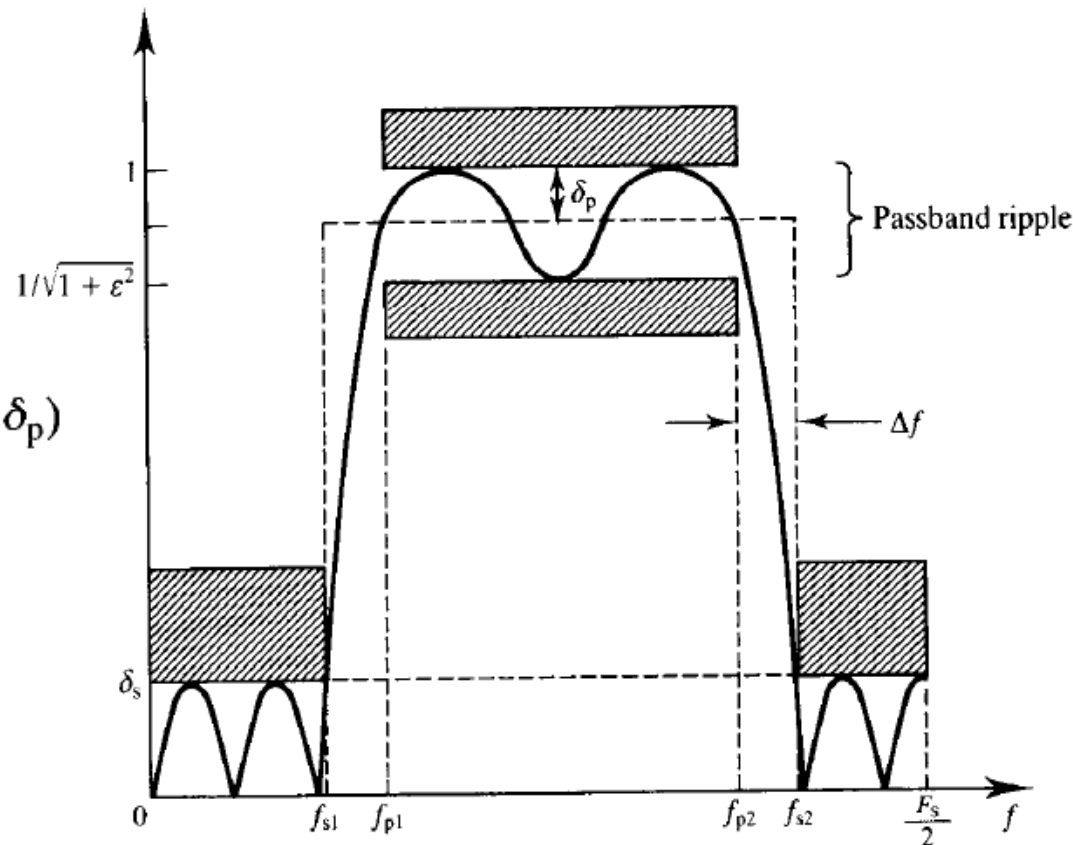
$\epsilon^2$	passband ripple parameter
$\delta_p$	passband deviation
$\delta_s$	stopband deviation
$f_{p1}$ and $f_{p2}$	passband edge frequencies
$f_{s1}$ and $f_{s2}$	stopband edge frequencies

The passband attenuation in decibels is:

$$A_p = 10 \log_{10}(1 + \epsilon^2) = -20 \log_{10}(1 - \delta_p)$$

And The Stopband attenuation in decibels is:

$$A_s = -20 \log_{10}(\delta_s)$$



**Figure 7.2** Tolerance scheme for an IIR bandpass filter.

## Step2: Calculating the filter coefficient filter Using the BZT method

### Summary of the procedure for calculating digital filter coefficients by the BZT method

- (1) Use the digital filter specifications to determine a suitable normalized transfer function,  $H(s)$ .
- (2) Determine the cutoff frequency (or passband edge frequency) of the digital filter and call this  $\omega_p$ .
- (3) Obtain an equivalent analogue filter cutoff frequency ( $\omega'_p$ ) using the relation (prewarped)

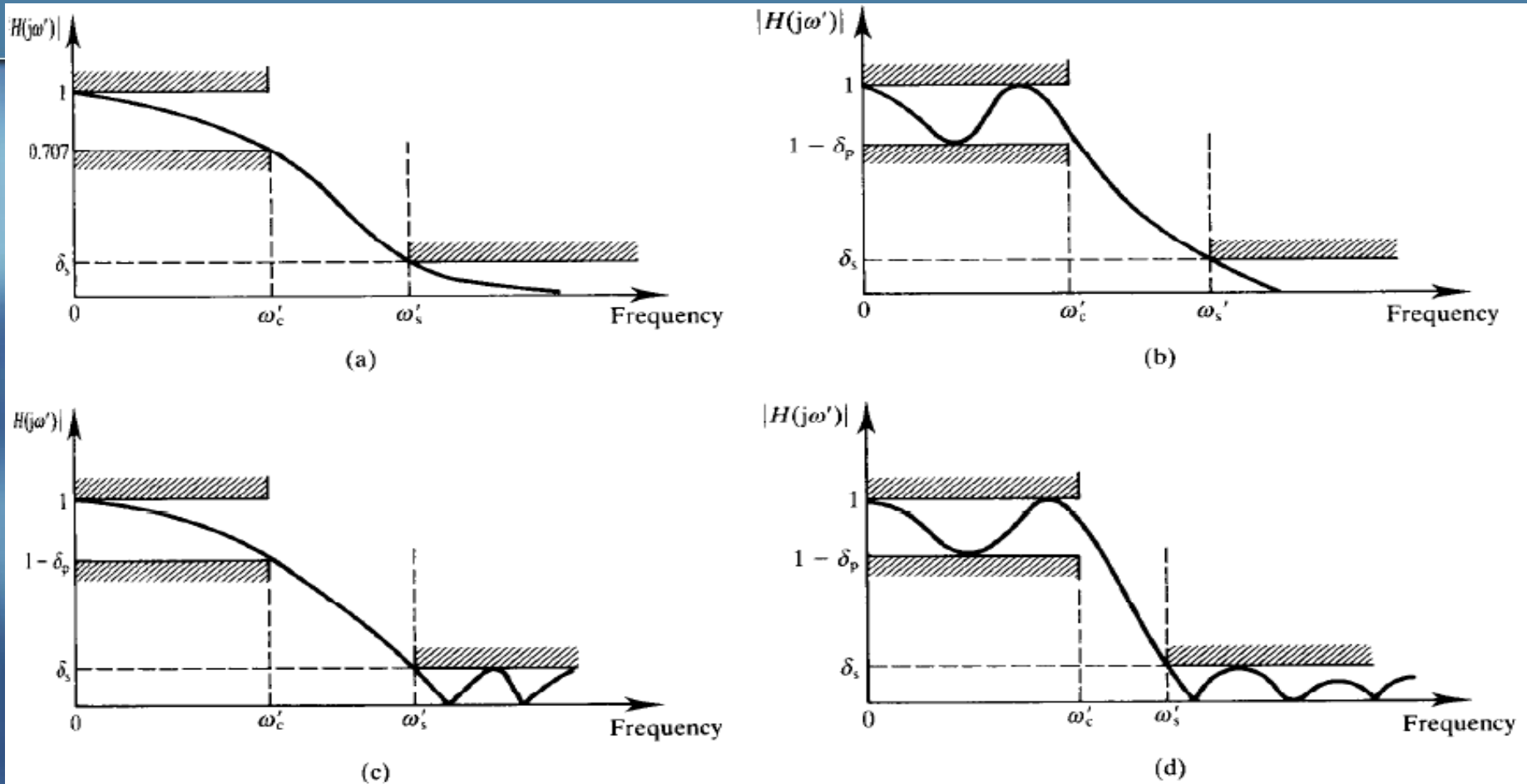
$$\omega'_p = k \tan\left(\frac{\omega_p T}{2}\right), \quad k = 1 \text{ or } \frac{T}{2}$$

- (4) Denormalize the analogue filter by frequency scaling  $H(s)$ . This is achieved by replacing  $s$  with  $s/\omega'_p$ .
- (5) Apply the bilinear transformation to obtain the desired digital filter transfer function  $H(z)$  by replacing  $s$  by  $(z - 1)/(z + 1)$ .

For computational efficiency we can combine step 4&5 as follows:

$$S = \frac{K(z-1)/(Z+1)}{K \tan(\frac{WpT}{2})} \longrightarrow s = \cot\left(\frac{\omega_p T}{2}\right) \frac{z - 1}{z + 1}$$

# Classical Analogue filters



**Figure 7.12** Sketches of frequency responses of some classical analogue filters: (a) Butterworth response; (b) Chebyshev type I; (c) Chebyshev type II; (d) elliptic.

Tables of the polynomials of  $H(s)$  for the Butterworth, Chebyshev and elliptic characteristics are available in most analogue design books in normalized form

# Butterworth filter

Low pass butterworth filter is characterized by:

$$|H(\omega')|^2 = \frac{1}{1 + (\omega'/\omega'_p)^{2N}}$$

where  $N$  is the order of the filter and  $\omega'_p$  is the 3 dB cutoff frequency.

the filter order is

$$N \geq \frac{\log_{10} [(1/\delta_s) - 1]}{2 \log_{10} (\omega'_s/\omega'_p)}$$

# Butterworth filter transfer fn $H(s)$

n	Factors of Polynomial $B_n(s)$
1	$(s + 1)$
2	$(s^2 + 1.4142s + 1)$
3	$(s + 1)(s^2 + s + 1)$
4	$(s^2 + 0.7654s + 1)(s^2 + 1.8478s + 1)$
5	$(s + 1)(s^2 + 0.6180s + 1)(s^2 + 1.6180s + 1)$
6	$(s^2 + 0.5176s + 1)(s^2 + 1.4142s + 1)(s^2 + 1.9319s + 1)$
7	$(s + 1)(s^2 + 0.4450s + 1)(s^2 + 1.2470s + 1)(s^2 + 1.8019s + 1)$
8	$(s^2 + 0.3902s + 1)(s^2 + 1.1111s + 1)(s^2 + 1.6629s + 1)(s^2 + 1.9616s + 1)$
9	$(s + 1)(s^2 + 0.3473s + 1)(s^2 + s + 1)(s^2 + 1.5321s + 1)(s^2 + 1.879s + 1)$
10	$(s^2 + 0.3129s + 1)(s^2 + 0.9080s + 1)(s^2 + 1.4142s + 1)(s^2 + 1.7820s + 1)(s^2 + 1.9754s + 1)$

The normalized Butterworth polynomials can be used to determine the transfer function for any low-pass filter cut-off frequency  $\omega_c$ , as follows

$$H(s) = \frac{G_0}{B_n(a)}, \text{ where } a = \frac{s}{\omega_c}.$$

$G_0$  is the DC gain (gain at zero frequency)



# Butterworth example 2

Obtain the transfer function of a lowpass digital filter meeting the following specifications:

passband	0–60 Hz
stopband	> 85 Hz
stopband attenuation	> 15 dB

Assume a sampling frequency of 256 Hz and a Butterworth characteristic.

## Solution

- (1) The critical frequencies for the digital filter are

$$W_p T = \frac{2\pi f_1}{F_s} = \frac{2\pi 60}{256} = 2\pi \times 0.2344$$

$$W_s T = \frac{2\pi f_2}{F_s} = \frac{2\pi 85}{256} = 2\pi \times 0.3320$$

- (2) The prewarped equivalent analogue frequencies are:

$$W'_p = \tan\left(\frac{W_p T}{2}\right) = 0.906347 \quad W'_s = \tan\left(\frac{W_s T}{2}\right) = 1.71580$$

# Butterworth example 2

- (3) Next we need to obtain  $H(s)$  with Butterworth characteristics, a 3 dB cutoff frequency of 0.906 347, and a response at 85 Hz that is down by 15 dB. For an attenuation of 15 dB,  $\delta_s = 0.1778$  and so from Equation 7.16b  $N = 2.468$ . We use  $N = 3$ , since it must be an integer. A normalized third-order filter is given by

$$A_s = -20 \log_{10}(\delta_s) = 15 \longrightarrow \delta_s = 0.1778$$

$$N \geq \frac{\log_{10}[(1/\delta_s) - 1]}{2 \log_{10}(\omega'_s/\omega'_p)} \longrightarrow N = 2.468. \text{ We use } N = 3$$

$$\begin{aligned} H(s) &= \frac{1}{(s+1)(s^2+s+1)} = \frac{1}{s+1} \frac{1}{s^2+s+1} \\ &= H_1(s) H_2(s) \end{aligned}$$

Then continue using bilinear z transform: we can combine step 4&5 in one equation using

$$s = \cot\left(\frac{\omega_p T}{2}\right) \frac{z-1}{z+1}$$



# Butterworth example 2

$$\cot\left(\frac{\omega_p T}{2}\right) = \cot\left(\frac{2\pi \times 0.2344}{2}\right) = 1.103155$$

Performing the transform in two stages, one for each of the factors of  $H(s)$  above, we obtain

$$\begin{aligned} H_2(z) &= H_2(s)|_s = \frac{1}{1 + 2z^{-1} + z^{-2}} \cdot \frac{1 + \cot(\omega_p T/2)[(z-1)/(z+1)]}{1 - 0.1307z^{-1} + 0.3355z^{-2}} \\ &= 0.3012 \frac{1 + 2z^{-1} + z^{-2}}{1 - 0.1307z^{-1} + 0.3355z^{-2}} \end{aligned}$$

which we have arrived at after considerable manipulation. Similarly, we obtain  $H_1(z)$  as

$$H_1(z) = 0.4754 \frac{1 + z^{-1}}{1 - 0.0490z^{-1}}$$

$H_1(z)$  and  $H_2(z)$  may then be combined to give the desired transfer function,  $H(z)$ :

$$H(z) = H_1(z)H_2(z) = 0.1432 \frac{1 + 3z^{-1} + 3z^{-2} + z^{-3}}{1 - 0.1801z^{-1} + 0.3419z^{-2} - 0.0165z^{-3}}$$

# Designing highpass, Bandpass and bandStop filters

The steps involved in the first method are outlined below.

- (1) Use the digital filter specifications to determine a suitable normalized lowpass filter,  $H(s)$ .
- (2) Determine and prewarp the critical frequencies of the digital filter. For lowpass or highpass filters there is just one critical frequency – the band edge or cutoff frequency,  $\omega'_p$ ; for bandpass or bandstop filters, we have the lower and upper band edge frequencies,  $\omega'_1$  and  $\omega'_2$ .
- (3) Replace  $s$  in the transfer function,  $H(s)$ , using one of the following transformations, depending on the type of filter required:

$$s = \frac{s}{\omega'_p} \quad \text{lowpass to lowpass} \quad (7.22a)$$

$$s = \frac{\omega'_p}{s} \quad \text{lowpass to highpass} \quad (7.22b)$$

$$s = \frac{s^2 + \omega_0^2}{Ws} \quad \text{lowpass to bandpass} \quad (7.22c)$$

$$s = \frac{Ws}{s^2 + \omega_0^2} \quad \text{lowpass to bandstop} \quad (7.22d)$$

where  $\omega_0^2 = \omega'_1 \omega'_2$ ,  $W = \omega'_2 - \omega'_1$ .

- (4) Apply the BZT to the new  $H(s)$ :

$$s = \frac{z - 1}{z + 1}$$

# Designing highpass Example 3:

**Highpass filter design** Convert the simple lowpass filter in Example 1 into an equivalent highpass discrete filter. The  $s$ -plane transfer function is given by

$$H(s) = \frac{1}{s + 1}$$

**Solution** The critical frequency for the digital filter is  $\omega_p = 2\pi \times 30$  rad.

$$\omega'_p = \tan(\omega_p T/2) = 0.7265$$

Using the LPF-to-HPF transformation of Equation 7.22b, the denormalized analogue transfer function is obtained as

$$H'(s) = H(s)|_{s = \omega'_p/s} = \frac{1}{\omega'_p/s + 1} = \frac{s}{s + 0.7265}$$

The  $z$ -plane transfer function is obtained by applying the BZT:

$$H(z) = H'(s)|_{s = (z-1)/(z+1)} = \frac{(z-1)/(z+1)}{(z-1)/(z+1) + 0.7265}$$

# Designing highpass example

Simplifying, we have

$$H(z) = 0.5792 \frac{1 - z^{-1}}{1 + 0.1584z^{-1}}$$

The coefficients of the digital filter are

$$a_0 = 0.5792 \quad b_1 = 0.1584$$

$$a_1 = -0.5792$$

# Bandpass filter design Example 4

**Bandpass filter design** A discrete bandpass filter with Butterworth characteristics meeting the following specifications is required. Obtain the coefficients of its transfer function,  $H(z)$ .

passband	200–300 Hz
sampling frequency	2000 Hz
filter order	2

## Solution

The prewarped passband edge frequencies are given by

$$\omega'_1 = \tan\left(\frac{\omega_1 T}{2}\right) = \tan(200\pi/2000) = 0.3249$$

$$\omega'_2 = \tan\left(\frac{\omega_2 T}{2}\right) = \tan(300\pi/2000) = 0.5095$$

Thus  $\omega_0^2 = 0.1655$  and  $W = \omega'_2 - \omega'_1 = 0.1846$ . A first-order normalized analogue lowpass filter is required (half the order of the bandpass filter). Thus we have

$$H(s) = \frac{1}{s + 1}$$

Using the lowpass-to-bandpass transformation (Equation 7.22c) we have

$$\begin{aligned} H'(s) &= H(s)|_{s=(s^2+\omega_0^2)/Ws} = \frac{1}{(s^2 + \omega_0^2)/Ws + 1} \\ &= \frac{Ws}{s^2 + Ws + \omega_0^2} \end{aligned}$$

# Bandpass filter design Example 4

Applying the BZT to the analogue bandpass filter we have

$$\begin{aligned} H(z) &= H'(s)|_{s=(z-1)/(z+1)} = \frac{W(z-1)/(z+1)}{[(z-1)/(z+1)]^2 + W(z-1)/(z+1) + \omega_0^2} \\ &= \frac{W(z^2 - 1)/(1 + W + \omega_0^2)}{z^2 + [2(\omega_0^2 - 1)/(1 + W + \omega_0^2)]z + (1 - W + \omega_0^2)/(1 + W + \omega_0^2)} \end{aligned}$$

Substituting the values of  $\omega_0^2$  and  $W$  and simplifying we have

$$H(z) = 0.1367 \frac{1 - z^2}{1 - 1.2362z^{-1} + 0.7265z^{-2}}$$



Thanks for good listening

*Best wishes*

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