

Spring 2022 EE214 Project Work

Preliminary Work

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1 Introduction

In this document, the Preliminary report of the term project of the EE214 course will be presented. The transmitter unit, receiver unit and the speaker unit studies for the preliminary design phase will be explained respectively.

1.1 Transmitter Unit

In this section, a transmitter unit should be designed which produces sine waves with 12 different frequency tones and collect them into one wave. For project requirements to be satisfied sinusoidal waves with 1 kHz, 2 kHz, 3 kHz, 5kHz, 6 kHz, 7 kHz, 9 kHz, 10 kHz, 11 kHz, 13 kHz, 14 kHz and 15 kHz frequencies will be produced and collected into one signal which will be transmitted to receiver unit through the wire. Frequencies that 4 kHz and its multiples are not going to be produced and magnitudes of produced signals must be large enough to receiver unit be able to distinguish it from the noise.

Therefore, a sine wave generator circuit must be designed which can be produce all the signals above. For this purpose, Wien Bridge Oscillator circuit is a suitable choice. Wien Bridge Oscillator is a type of electronic oscillator that generates sine waves that can have a large range of frequencies. Wien Bridge Oscillator circuit schematic is given in Figure

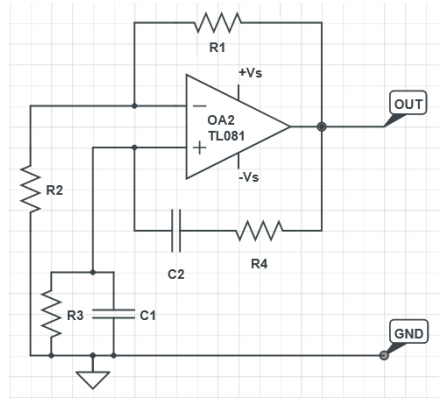


Figure 1: Wien Bridge Oscillator

X. When C_1 equal C_2 , and R_3 equals R_4 , frequency of the signal that is produced by this circuit is calculated using the following formula:

$$f = \frac{1}{2\pi\sqrt{C_1 R_3 C_2 R_4}}$$

Let C_1, C_2 be C , and R_3, R_4 be R then frequency is:

$$f = \frac{1}{2\pi RC}$$

Hence, if C is set to be $1\mu F$, R should be calculated to obtain the correct frequency.

Gain of this circuit is $\frac{R_1}{R_2}$. If the gain is inadequate oscillation would be weak, but if the gain is too much, circuit might go into saturation. In order oscillation to be well, gain should be approximately 2-3. Therefore, $R_1 = 68k\Omega$ and $R_2 = 33k\Omega$ would be proper choice.

From above calculations, it can be calculated that when $16kHz$ frequency is wanted to be obtain, $1k\Omega$ resistors should be used for R value. By doing same calculations following table can be obtained.

Table 1: Required Resistances Corresponding Frequencies 1

Frequencies	$1kHz$	$2kHz$	$3kHz$	$5kHz$	$6kHz$	$7kHz$
Resistances	$15915k\Omega$	$7957k\Omega$	$5305k\Omega$	$3183k\Omega$	$2652k\Omega$	$2273k\Omega$

Table 2: Required Resistances Corresponding Frequencies 2

Frequencies	$9kHz$	$10kHz$	$11kHz$	$13kHz$	$14kHz$	$15kHz$
Resistances	$1768k\Omega$	$1591k\Omega$	$1446k\Omega$	$1224k\Omega$	$1136k\Omega$	$1061k\Omega$

After generating necessary signals, one should sum this signals into one by using summing amplifier circuit given in Figure X.

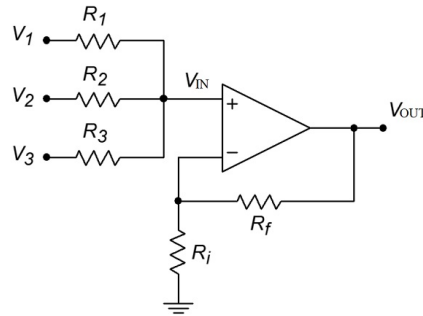


Figure 2: Non-inverting summing amplifier

1.2 Receiver Unit

In this part a receiver needed to be designed. So, let us first define the design requirements.

- The receiver should be able extract the desired signal amongst the signals with 12 different frequencies.
- The receiver should be able make a difference between the needed signal and others at least 10dB. (Closely related to the Q factor.)
- The receiver should provide option of channel adjustment with (at most) 2 potentiometer. Adjustment with 1 pot is the target.

In order to design a receiver unit that satisfies the fundamental requirements specified above, a circuit that only allows the signal with desired frequency to pass needed to be constructed. So , a filter design is expected which act like as a fourier transformer. There are passive and active filter designs which allows to pass below (low pass) or above (high pass) threshold frequencies. By combining those two filters one can build a filter which allows only certain band of signals. This is called band pass filter. In this section the design guides prepared by the Analog Devices Company. ([Main Source](#))

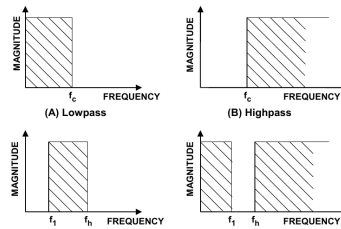


Figure 3: Filter Responses (ideal)

Passive filters are not considered here since they would not be feasible in an adjustable setup. The transfer function of a basic band-pass filter can be presented as following.

$$H(s) = \frac{H_0(\omega_0)^2}{s^2 + \frac{\omega_0}{Q}s + (\omega_0)^2}$$

Now let us examine briefly transfer responses in the literature to choose an optimum design path.

1.2.1 Butterworth

Butterworth transfer response offers clean pass and not-pass regions in other words no ripple. However, the band that allows the signals is not narrow.

1.2.2 Chebyshev

Chebyshev transfer response offers narrower band however it has ripples in the pass band.

1.2.3 Bessel

Bessel filter is optimized to obtain better transient response due to a linear phase (i.e. constant delay) in the passband.

For our case as long as it is tuned carefully all three transfer responses can be used. However in order to have better frequency discrimination Chebyshev function is selected to be used in this phase of the project. The values for the Chebyshev function will be fetched from the design tables available in internet. (The table is not included here in order not to excess page limit.)

Now let us examine briefly the available design topologies to choose which design path to go for. There are three main topologies for the band-pass filter design.

1.2.4 Multiple Feedback Band Pass

Multiple feedback band-pass filter designs are widely used (over sallén-key filter) however does not offer much tunability. ([Source](#))

1.2.5 State Variable Filter

This configuration offers the most precise implementation of the filter function, at the expense of many more circuit elements. All three major parameters (gain, Q, and ω_0) can be adjusted independently, and low-pass, high-pass, and band-pass outputs are available simultaneously. Note that the low-pass and high-pass outputs are inverted in phase while the band-pass output maintains the phase. ([Source](#))

1.2.6 Dual Amplifier Band Pass

The dual amplifier band-pass filter structure is useful in designs requiring high Qs and high frequencies. Its component sensitivity is small, and the element spread is low. A useful feature of this circuit is that the Q and resonant frequency can be adjusted more or less independently. ([Source](#))

So, it can be said that both state variable filter and dual amplifier band pass filter is quite suitable for our purposes. In this stage of the project dual amplifier band pass filter topology is selected in order to have less components. Now let us examine general outlook of the topology. In Figure X the in and out characteristics also provided. In order to be able

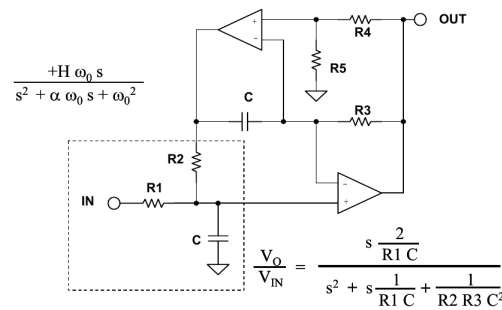


Figure 4: Dual Band-Pass Topology

to adjust all the range of the needed frequencies, the target frequency for the base design is

selected as 7kHz. With the adjustment of safety factor of 1.5 separation is targeted as 15dB. The resulting (targeted) curve is obtained as given in Figure X. To conclude the receiver

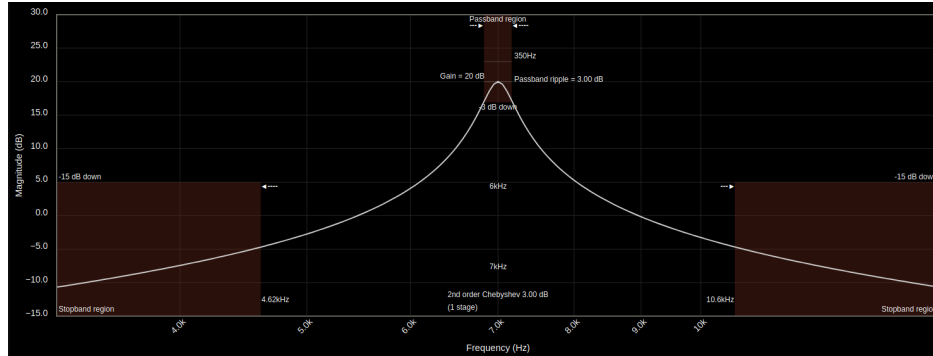


Figure 5: Targeted base frequency response

unit, the trade-offs for first design steps are created according to the requirements specified. As explained the accuracy of the receiver part dependent on the multiple factors such as the opamp used the Q factor aimed and so on. To avoid misleading false-positive results and preserve the length of the preliminary report no simulation results are given even though they are done. The milestones that will be done in the next phase of the project for the receiver side can be summerized as;

- Filter parameters will be iteratively tuned.
- Opamp's for the application will selected and purchased.
- Input buffer will be determined in order to satisfy low input impedance assumption of the filter design.
- Real life tests will be conducted and the circuit parameters will be tuned further.

1.3 Speaker Unit

2 Conclusion

In this document, the Preliminary report of the term project of the EE214 course is presented. The transmitter unit, receiver unit and the speaker unit studies for the preliminary design phase are explained respectively in the constrains of the preliminary report.