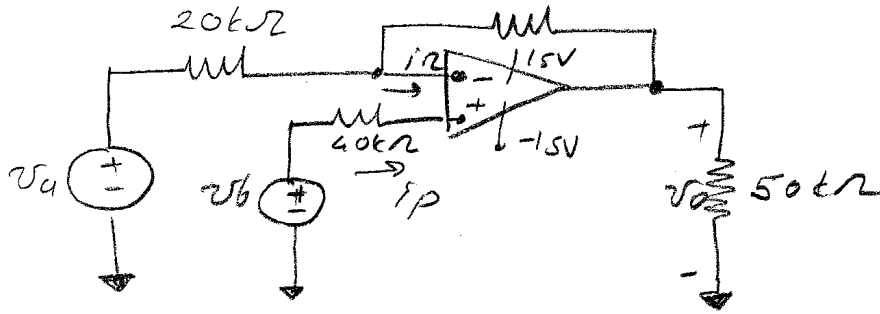


5.2



a) For an ideal opamp $i_p = i_n = 0$, which implies that $v_b = v_p$, also for an ideal opamp $v_p = v_n$, thus

$$v_b = v_n, \text{ thus}$$

$$\frac{v_b - v_a}{20} + \frac{v_b - v_o}{100} = 0 \Rightarrow 5(v_b - v_a) + v_b - v_o = 0$$

$$v_o = 6v_b - 5v_a$$

(a) $v_a = 4V, v_b = 0V, v_o = -15V$ (sat)

(b) $v_a = 2V, v_b = 0V, v_o = -10V$

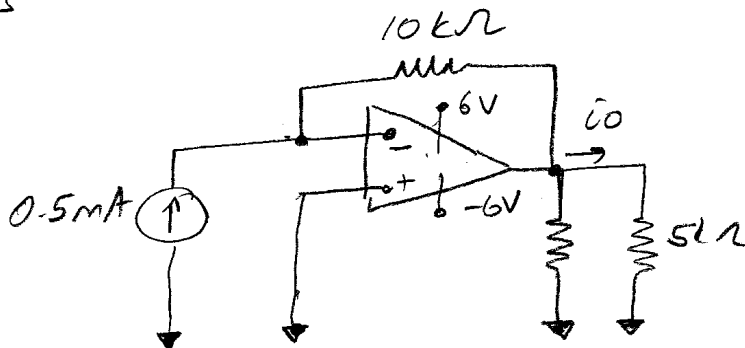
(c) $v_a = 2V, v_b = 1V, v_o = -4V$

(d) $v_a = 1V, v_b = 2V, v_o = 7V$

(e) If $v_b = 1.6V, v_o = 8 - 6 - 5v_a = \pm 15$

$$\therefore -1.08 \leq v_a \leq 4.92V$$

5.3



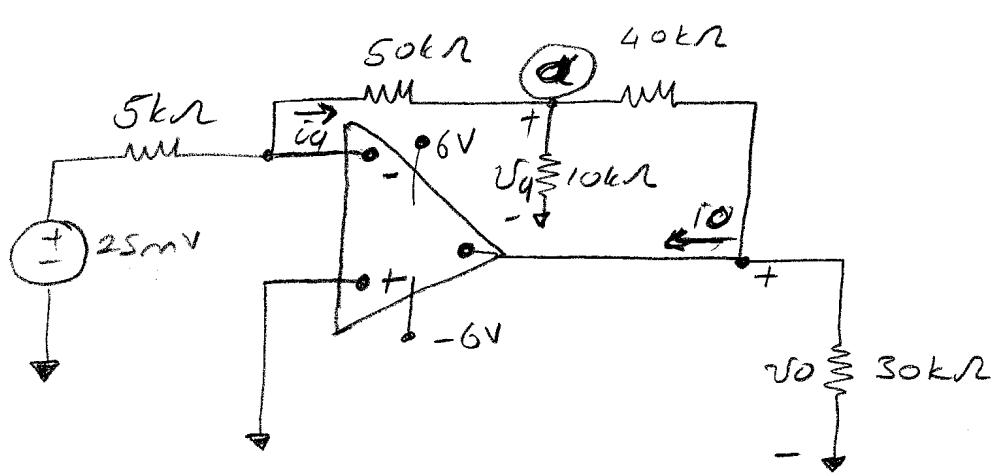
node equation at the inverting input $-0.5 + \frac{v_n - v_o}{10} = 0$ (I)

But $v_p = 0$ and for an ideal opamp $v_p = v_n$, thus

v_n is also zero Equation (I) becomes $-0.5 = \frac{v_o}{10} \Rightarrow v_o = -5V$

$$i_o = \frac{-5V}{5k\Omega} = -1mA$$

5.5



a) as $i_p = i_n =$ the current in the $5k\Omega$ resistor equals to the current in the $50k\Omega$ resistor, thus

$$i_a = \frac{25mV}{5k\Omega} = 5\mu A$$

The inverting input is at zero volts thus the voltage from the inverting input to node @ equals to v_a

$$v_a = -50 \times 10^3 i_a = -250mV$$

(b) We write the node equation at node @.

$$\frac{v_a}{50} + \frac{v_a}{10} + \frac{v_a - v_o}{40} = 0$$

$$4v_a + 20v_a + 5(v_a - v_o) = 0$$

$$29v_a = 5v_o \quad v_o = 5.8v_a = \underline{\underline{-1.45V}}$$

(c) $i_a = 5\mu A$

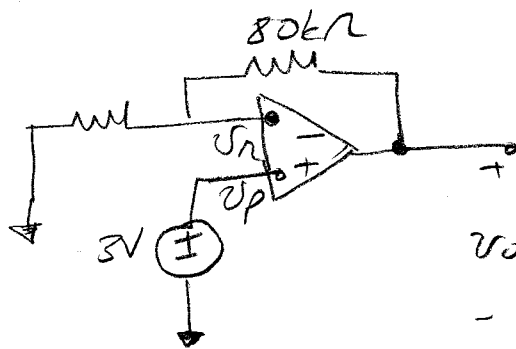
(d) We write the node equation at the output terminal.

$$\frac{v_o - v_a}{40} + \frac{v_o}{30} + i_o = 0$$

$$i_o = -\frac{v_o}{30} - \frac{v_o}{40} + \frac{v_a}{40}$$

$$i_o = \frac{+1.45}{30} + \frac{1.45}{40} - \frac{0.25}{40} = 0.0783mA = 78.33\mu A$$

5-7



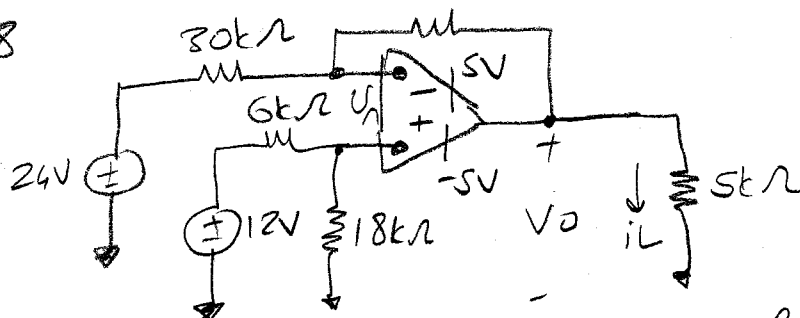
$$v_p = v_n = 3V$$

$$\frac{3-0}{40} + \frac{3-v_o}{80} = 0$$

$$6+3-v_o=0$$

$$v_o = 9V$$

5-8



If we can find v_o , we can find i_L

$$I \quad \frac{v_n-24}{30} + \frac{v_n-v_o}{20} = 0 \quad II \quad \frac{v_p-12}{6} + \frac{v_p}{18} = 0$$

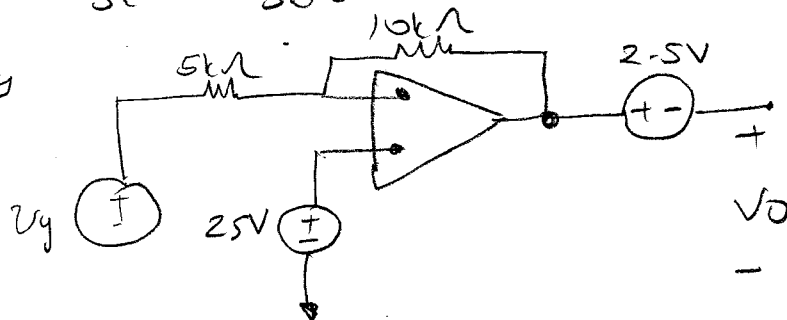
$$3v_p - 36 + v_p = 0 \quad 4v_p = 36 \quad v_p = 9V \quad v_n = v_p = 9V$$

$$\frac{9-24}{30} + \frac{9-v_o}{20} = 0 \Rightarrow 2(9-24) + 3(9-v_o) = 0$$

$$18-48+27-3v_o=0 \quad -3v_o=3V \quad v_o = -1V$$

$$i_L = \frac{v_o}{5k\Omega} = \frac{-1V}{5k\Omega} = -0.200mA$$

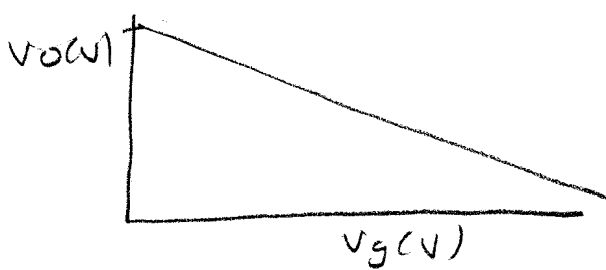
5-9



Let v_{o1} equal the voltage of the op-amp, then

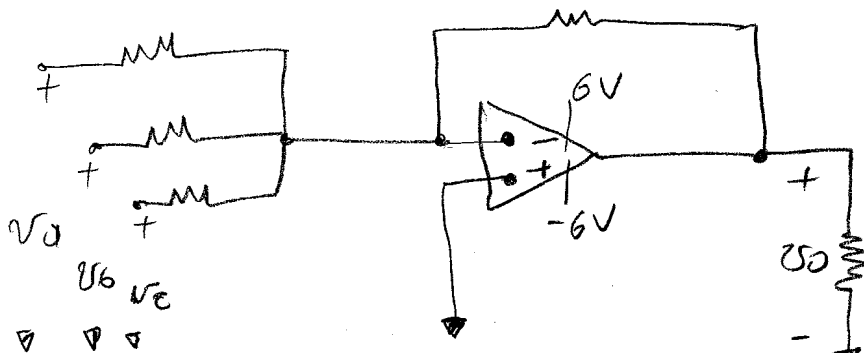
$$\frac{2.5-v_y}{5000} + \frac{2.5-v_{o1}}{10000} = 0 \quad \therefore v_{o1} = 7.5-2v_y$$

$$\text{Also note that } v_{o1}-2.5 = v_o \quad \therefore v_o = 5-2v_y.$$



(b) Yes, the circuit designer is correct!

5-16.



a) The circuit is an example of an inverting summing amplifier.

b) $v_p = v_n = 0 \Rightarrow \frac{-v_a}{33} - \frac{v_b}{22} - \frac{v_c}{80} - \frac{v_o}{220} = 0$

$$v_o = 220 \times \left[\frac{-v_a}{33} - \frac{v_b}{22} - \frac{v_c}{80} \right] = \frac{-220v_a}{33} - \frac{220v_b}{22} - \frac{220v_c}{80}$$

$$-8 + 15 - 11 = -4V$$

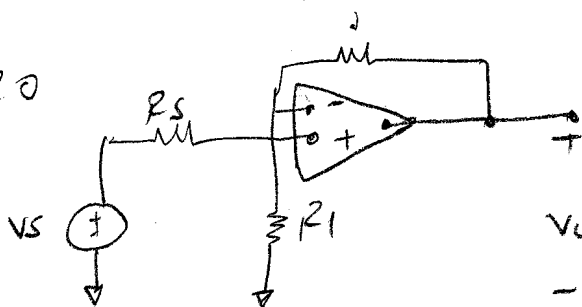
(c) $v_o = \frac{-220}{33} \times (1-2) - \frac{220}{80} (6) - \frac{220}{22} v_b = -19 - 10v_b = \pm 6$

$\therefore v_b = -1.3V$ when $v_o = -6V$

$v_b = -2.5V$ when $v_o = 6V$

$-2.5V \leq v_b \leq -1.3V$

5-20



Node Equation at the inverting terminal:

$$\frac{v_n}{R_1} + \frac{v_n - v_o}{R_2} = 0$$

v_o Node Equation at the non-inverting terminal II

$\frac{v_s - v_p}{R_s} = 0 \Rightarrow v_s = v_p$

As the op amp is ideal $v_p = v_n \therefore v_s = v_o$

-5

substituting $v_s = v_n$ into the first node equation:

$$\frac{v_s}{R_1} + \frac{v_s - v_o}{R_2} = 0$$

$$v_s \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = \frac{v_o}{R_2}$$

$$v_s \left(\frac{R_2 + R_1}{R_1 R_2} \right) = \frac{v_o}{R_2} \Rightarrow v_o = \frac{v_s (R_1 + R_2)}{R_1}$$

$$\text{or } v_o = v_s \left[1 + \frac{R_2}{R_1} \right]$$

$$(6) \quad v_o = v_s$$

(c) Because $v_o = v_s$, the output voltage follows the signal voltage.

$$S-32 \quad v_p = \frac{v_b R_b}{R_a + R_b} = v_n$$

$$\frac{v_n - v_y}{4700} + \frac{v_n - v_o}{R_f} = 0$$

$$v_n \left(\frac{R_f}{4700} + 1 \right) - \frac{v_o R_f}{4700} = v_o$$

$$\therefore \left(\frac{R_f}{4700} + 1 \right) \frac{R_b}{R_a + R_b} v_b - \frac{R_f}{4700} v_o = v_o$$

$$\therefore \frac{R_f}{4700} = 10, \quad R_f = 47k\Omega$$

$$\therefore \frac{R_f}{4700} + 1 = 11 \quad \therefore 11 \left(\frac{R_b}{R_a + R_b} \right) = 10$$

$$11R_b = 10R_b + 10R_a \quad R_b = 10R_a$$

$$R_a + R_b = 220k\Omega \Rightarrow 11R_a = 220k\Omega$$

$$R_a = 20k\Omega \quad R_b = 220 - 20 = 200k\Omega$$

5.33 $v_p = v_n = R_b i_b$

The node-equation at the inverting terminal.

$$\frac{R_b i_b - 3000 i_b}{3000} + \frac{R_b i_b - v_o}{R_f} = 0$$

$$\left(\frac{R_b}{3000} + \frac{R_b}{R_f} \right) i_b - \frac{v_o}{R_f} = 0$$

$$v_o = \left[\frac{R_b R_f}{3000} + R_b \right] i_b - R_f i_b = R_f = 2000 \Omega$$

$$\left(\frac{2}{3} \right) R_b + R_b = 2000 \Rightarrow R_b = 1200 \Omega$$