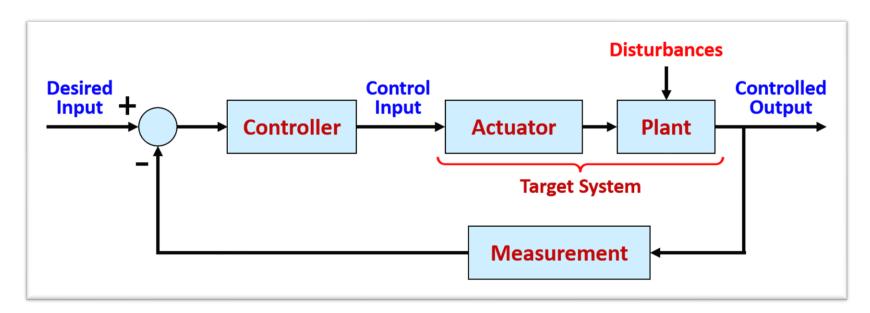
# **Dynamic Response 1**

#### Lecture 4:

- Important Aspects of Dynamic Response
- Step Response Analysis



#### **Prof. Seunghoon Woo**

Department of Automotive Engineering | College of Automotive Engineering | KOOKMIN UNIVERSITY

## **Application of Control Engineering in Our Life (1)**

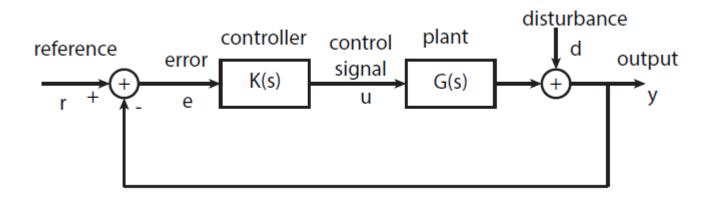
#### **❖ NAVER LABS Intelligence in Mobility**





https://www.youtube.com/watch?v=B-RXhvcV0Pc

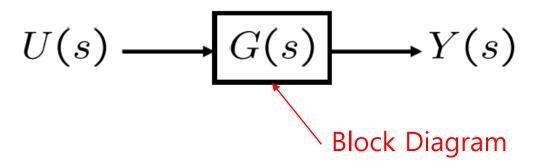
- (1) Block diagram: Controller + Plant Model
- (2) Poles and zeros
- (3) Effect of pole locations
- (4) Effect of zero locations
- (5) Control Performance Measurement Index



## (1) Block Diagram with Single Transfer Function (Revisited)

A transfer function is defined by,

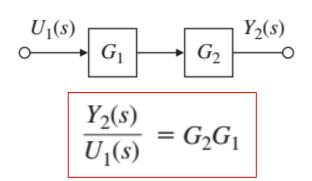
$$G(s) := \frac{Y(s)}{U(s)}$$
 Laplace transform of system output Laplace transform of system input



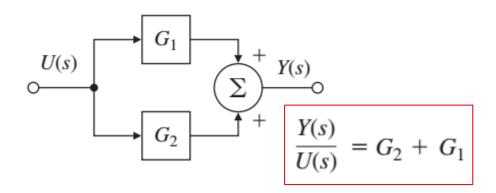
But, a system is assumed to be at rest. (zero initial condition)

## (1) Block Diagram with Multi-Transfer Functions (cont'd)

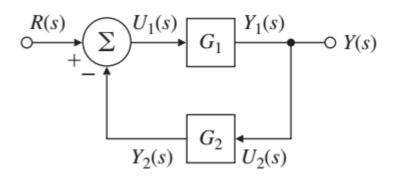
Serial Connection



Parallel Connection



Feedback Connection (Type I)



**Proof:** 

$$U_{1}(s) = R(s) - Y_{2}(s), U_{1} = R - G_{2}G_{1}U_{1} (1 + G_{1}G_{2})U_{1} = R$$

$$Y_{2}(s) = U_{1}(s), U_{1} = \frac{R}{1 + G_{1}G_{2}}$$

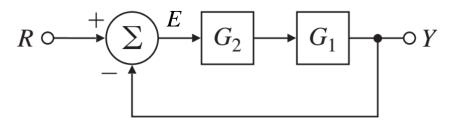
$$Y_{1}(s) = G_{1}(s)U_{1}(s), U_{1} = \frac{R}{1 + G_{1}G_{2}}$$

$$where, Y_{1}(s) = Y(s)$$

$$\frac{Y(s)}{R(s)} = \frac{G_{1}}{1 + G_{2}G_{1}}$$

#### (1) Block Diagram with Multi-Transfer Functions (cont'd)

Feedback Connection (Type II)



#### **Proof:**

$$E = Y = E$$

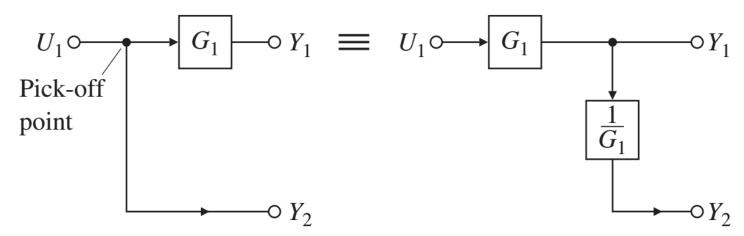
$$Y =$$
  $(1 + G_1G_2)Y = (G_1G_2)R$ 



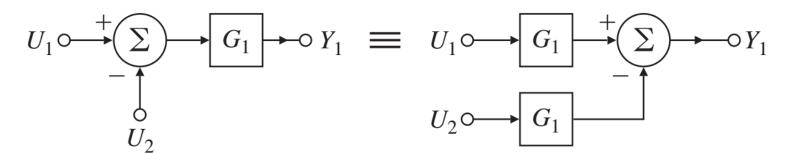
$$\frac{Y(s)}{R(s)} = \frac{G_1 G_2}{1 + G_1 G_2}$$

#### (1) Block Diagram with Multi-Transfer Functions (cont'd)

Block Diagram Algebra (1): Moving a pickoff point

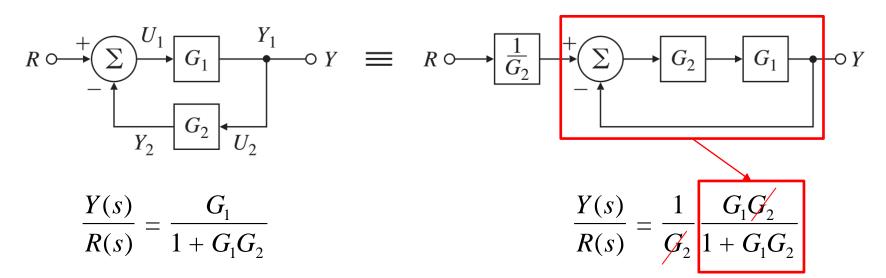


Block Diagram Algebra (2): Moving a summer



#### (1) Block Diagram with Multi-Transfer Functions (cont'd)

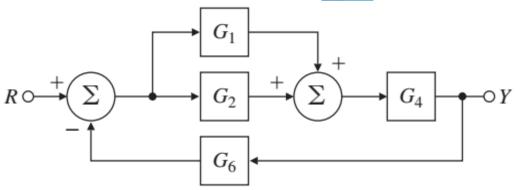
Block Diagram Algebra (3): Conversion to unity feedback



#### (1) Block Diagram with Multi-Transfer Functions (cont'd)

Example using Matlab

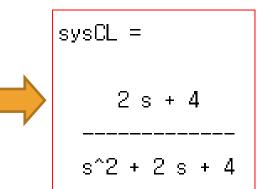




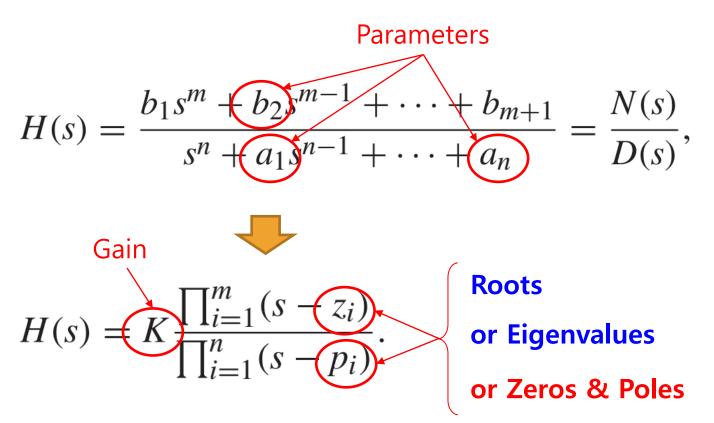
where,

$$G_1 = 2, G_2 = \frac{4}{s}, G_4 = \frac{1}{s}, G_6 = 1$$

```
s=tf('s'); % specify a TF in the Laplace variable s
sysG1=2; % define subsystem G1
sysG2=4/s; % define subsystem G2
sysG3=parallel(sysG1,sysG2); % parallel combination of G1 and G2
sysG4=1/s; % define subsystem G4
sysG5=series(sysG3,sysG4); % series combination of G3 and G4
sysG6=1;
sysCL=feedback(sysG5,sysG6,-1) % feedback combination of G5 and G6
```



#### (2) Poles and Zeros of Transfer Function



• Question: So, why we call these Zeros & Poles??

#### (2) Poles and Zeros of Transfer Function (cont'd)

$$H(s) = K \frac{\prod_{i=1}^{m} (s - z_i)}{\prod_{i=1}^{n} (s - p_i)}.$$

If 
$$s = z_i$$
, then



If 
$$s = z_i$$
, then  $H(s)|_{s=z_i} = 0$ .

Zeros

If 
$$s = p_i$$
, then

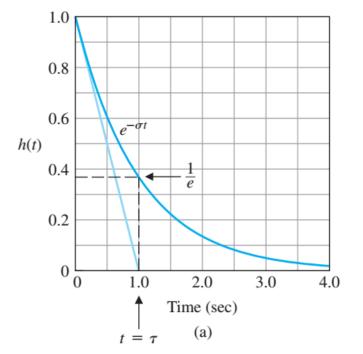


If 
$$s = p_i$$
, then  $|H(s)|_{s=p_i} = \infty$ . Poles

#### (3) Effect of Pole Locations

Ex) For a first-order pole with the impulse response,

$$H(s) = \frac{1}{s+\sigma} \cdot \stackrel{\mathcal{L}^{-1}}{\longmapsto} h(t) = e^{-\sigma t} 1(t).$$



$$\sigma > 0 \Rightarrow$$
 pole location s  $< 0 \Rightarrow$  stable  $\sigma < 0 \Rightarrow$  pole location s  $> 0 \Rightarrow$  unstable

Thus, system stability depends on pole location!!

#### (3) Effect of Pole Locations (cont'd)

Example 1: Real Poles

$$H(s) = \frac{2s+1}{s^2+3s+2}.$$

Partial-fraction expansion gives,

$$H(s) = -\frac{1}{s+1} + \frac{3}{s+2}.$$

$$\mathcal{L}^{-1}$$

$$h(t) = \begin{cases} -e^{-t} + 3e^{-2t} & t \ge 0, \\ 0 & t < 0. \end{cases}$$

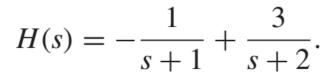
#### (3) Effect of Pole Locations (cont'd)

Example 1: Real Poles (cont'd)

$$H(s) = \frac{2s+1}{s^2+3s+2}.$$
 num = [2 1];  
den = [1 3 2];  
pzmap(num,den)

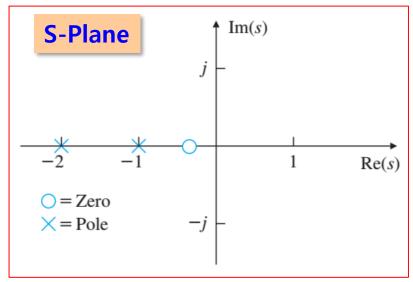




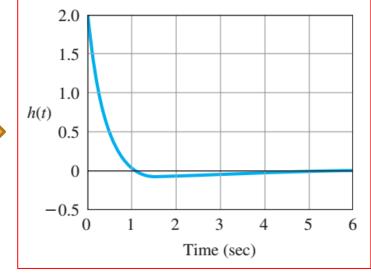


$$h(t) = \begin{cases} -e^{-t} + 3e^{-2t} & t \ge 0, \\ 0 & t < 0. \end{cases}$$









#### (3) Effect of Pole Locations (cont'd)

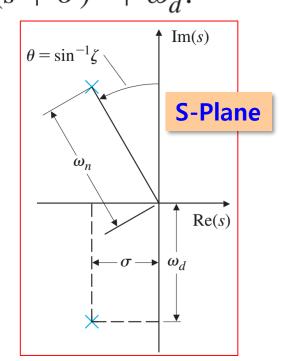
**Example 2: Complex (conjugate) Poles** 

$$H(s) = \frac{b(s)}{a(s)} \qquad s = -\sigma \pm j\omega_d.$$

$$a(s) = (s + \sigma - j\omega_d)(s + \sigma + j\omega_d) = (s + \sigma)^2 + \omega_d^2.$$

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}.$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2},$$
Natural frequency



#### (3) Effect of Pole Locations (cont'd)



**Example 2: Complex (conjugate) Poles** 

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}.$$



Re-written

$$H(s) = \frac{\omega_n^2}{(s + \zeta \omega_n)^2 + \omega_n^2 (1 - \zeta^2)}.$$

$$\frac{b}{(s + a)^2 + b^2} \mathcal{L}^{-1}$$

$$e^{-at} \sin bt$$

$$\mathcal{L}^{-}$$

$$\frac{b}{(s+a)^2+b^2}$$

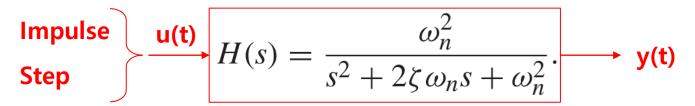
$$h(t) = \frac{\omega_n}{\sqrt{1 - \zeta^2}} e^{-\sigma t} (\sin \omega_d t) 1(t).$$

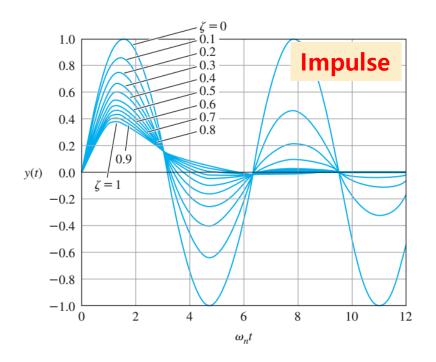
where, 
$$a \Rightarrow \zeta \omega_n$$

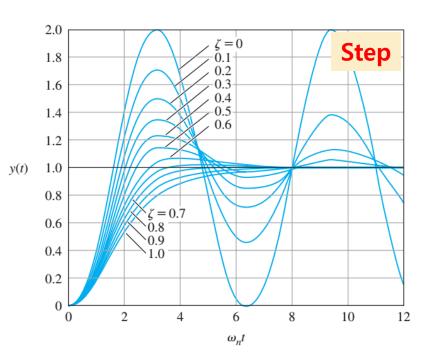
$$b \Rightarrow \omega_d = \omega_n \sqrt{1 - \zeta^2}$$

#### (3) Effect of Pole Locations (cont'd)

Example 2: Complex (conjugate) Poles (cont'd)

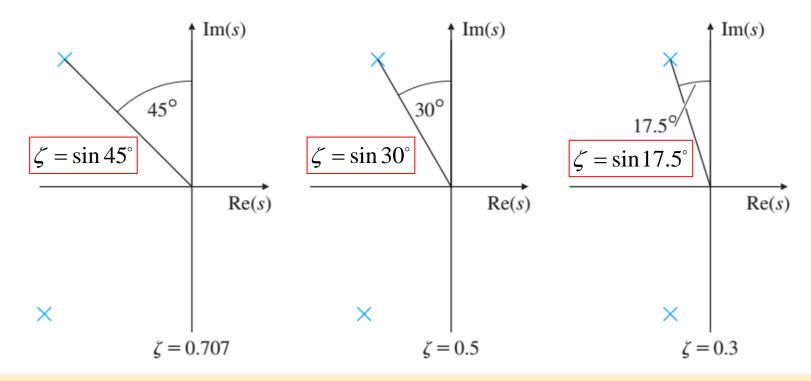






#### (3) Effect of Pole Locations (cont'd)

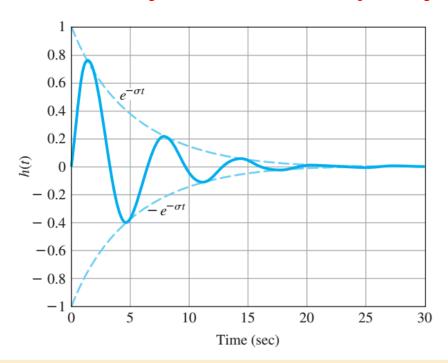
Summary 1: Damping Ratio vs. System Response (Oscillation)



• Question: How can we understand the relationship btw Damping Ratio (i.e., energy dissipation) vs. System Oscillation?

#### (3) Effect of Pole Locations (cont'd)

Summary 2: Natural Frequency vs. System Response (Oscillation)



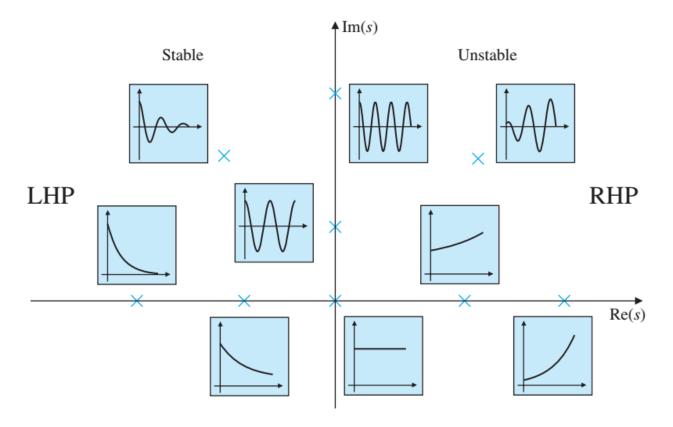
$$\sigma = \zeta \omega_n$$

@ constant damping

• Question: How can we understand the relationship btw Natural Frequency vs. System Oscillation?

#### (3) Effect of Pole Locations (cont'd)

Summary 3: Natural Frequency & Damping vs. System Response



#### (4) Effect of Zero Locations

Case 1: No Zero TF

$$H_1(s) = \frac{2}{(s+1)(s+2)}$$
$$= \frac{2}{s+1} - \frac{2}{s+2},$$

Case 2: One Zero near Pole in TF

$$H_2(s) = \frac{2(s+1.1)}{1.1(s+1)(s+2)}$$
Almost cancellation
$$= \frac{2}{1.1} \left( \frac{0.1}{s+1} + \frac{0.9}{s+2} \right)$$

$$= \frac{0.18}{s+1} + \frac{1.64}{s+2}.$$

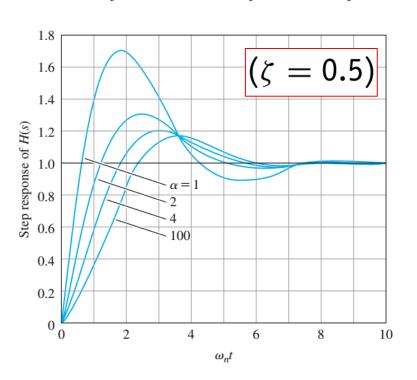
#### (4) Effect of Zero Locations (cont'd)

Normalized time and zero locations:

$$H(s) = \frac{s/\alpha\zeta + 1}{s^2 + 2\zeta s + 1}. \quad \Rightarrow H(s) = \frac{1}{s^2 + 2\zeta s + 1} + \frac{1}{\alpha\zeta} \frac{s}{s^2 + 2\zeta s + 1}.$$

- Important Questions about effects on zero locations:
- (1) Transient Response??
- (2) Overshoot??
- (3) Stability??

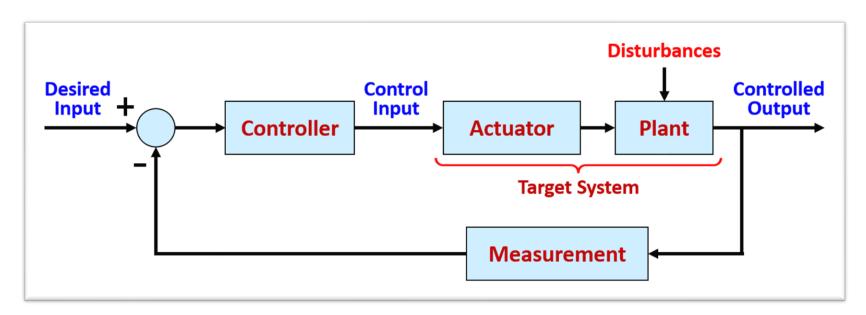
$$s_{zero} = -\alpha \zeta$$



## **Dynamic Response 1**

#### Lecture 4:

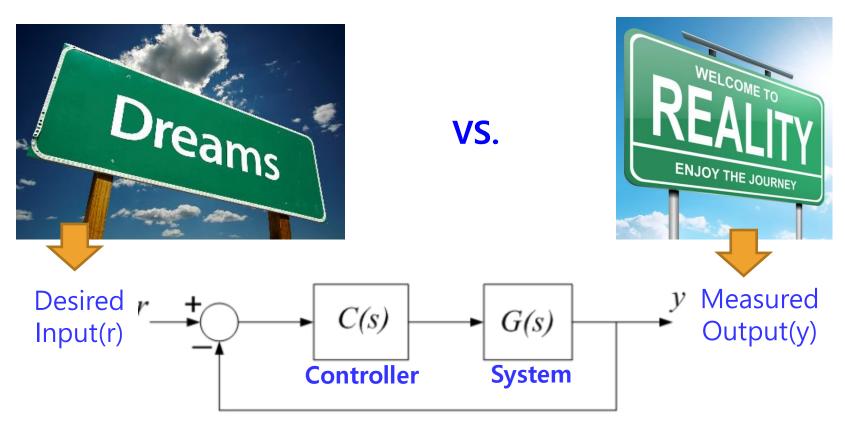
- Important Aspects of Dynamic Response
- Step Response Analysis



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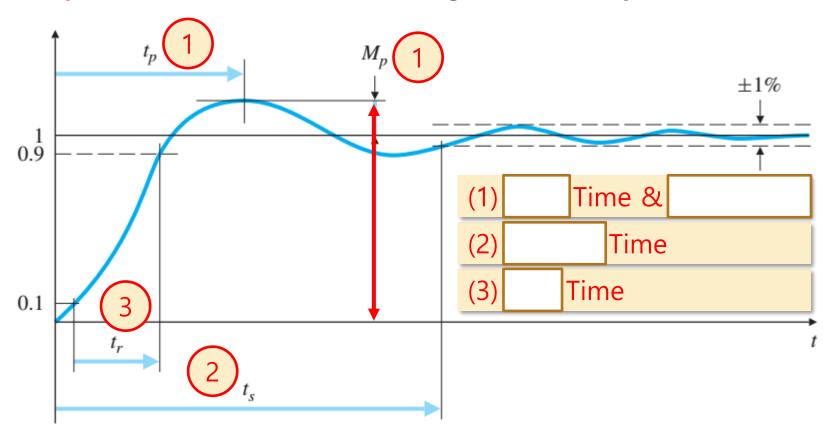
## What is the Control Concept? (Revisited)



- Controller is to minimize error between the desired input (dream) between the measured output (reality) !!
- Then, how to measure the gap btw desire vs. reality ??

## (5) Control Performance Index: Step Response

Key Three Attributes for checking the control performance

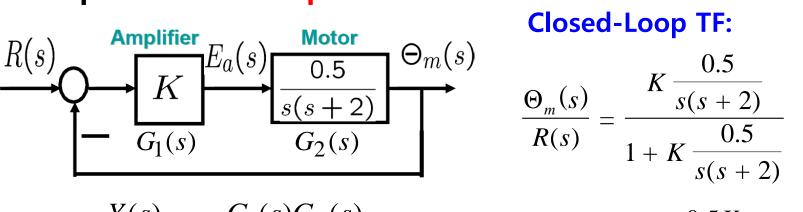


## (5) Control Performance Index: Step Response

A standard form of the second-order system

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad \begin{cases} \zeta : & \text{damping ratio} \\ \omega_n : & \text{undamped natural frequency} \end{cases}$$

Example: DC motor position control

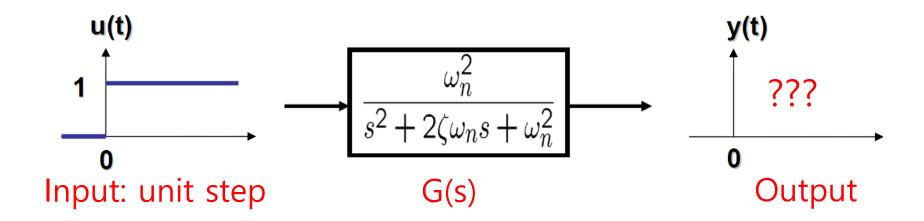


$$\frac{Y(s)}{R(s)} = \frac{G_1(s)G_2(s)}{1 + G_1(s)G_2(s)}$$

$$\frac{\Theta_m(s)}{R(s)} = \frac{K \frac{0.5}{s(s+2)}}{1 + K \frac{0.5}{s(s+2)}}$$
$$= \frac{0.5K}{s^2 + 2s + 0.5K}$$

## (5) Control Performance Index: Step Response

• Input a unit step function to a 2<sup>nd</sup>-order system. What is the output?



We are interested in the error (i.e., input – output) !!

## (5) Control Performance Index: Step Response

Undamped

$$\zeta = 0$$

Underdamped

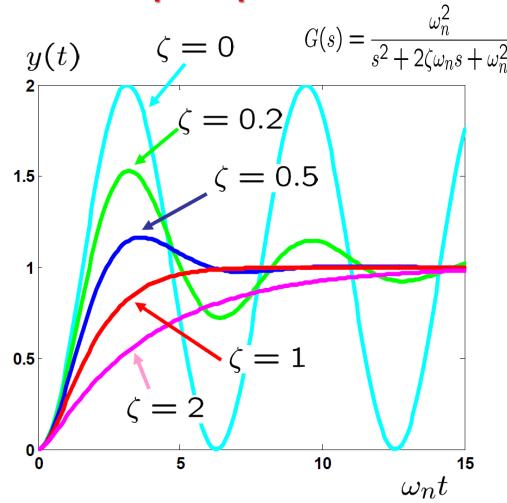
$$0 < \zeta < 1$$

Critically damped

$$\zeta = 1$$

Overdamped

$$\zeta > 1$$



## (5) Control Performance Index: Step Response



 Math expression of y(t) {or Y(s)} for underdamped case with the step input  $\{R(s) = 1/s\}$  $0 < \zeta < 1$ 

$$Y(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \cdot \frac{1}{s}$$

- (1) Peak Time & Overshoot ??
- (2) Settling Time ??
- (3) Rise Time ??

$$\mathcal{L}^{-1}$$

$$y(t) = 1 - \frac{e^{-\zeta \omega_n t}}{\sqrt{1 - \zeta^2}} \sin(\omega_d t + \varphi)$$





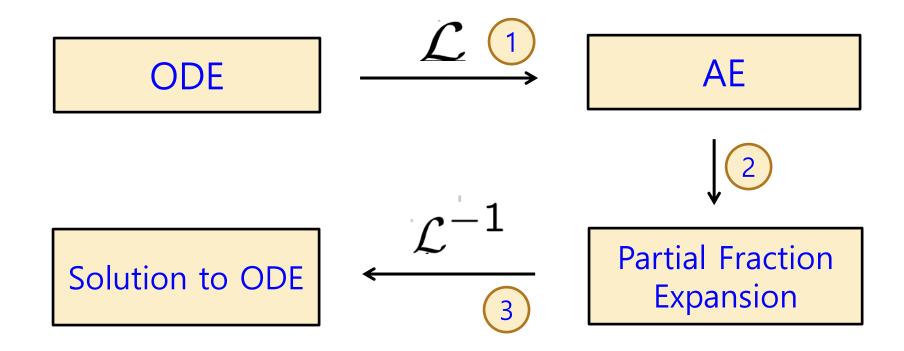
where,

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$
: Damped Natural Frequency [rad/sec]

$$\varphi = \cos^{-1}(\zeta)$$
: time delay [rad]



Transform an ordinary differential equation (ODE) into an algebraic equation (AE).



Example 1: ODE with initial conditions (cont'd)

$$\frac{d^2y(t)}{dt^2} + 3\frac{dy(t)}{dt} + 2y(t) = 5u_s(t), \ y(0) = -1, \ y'(0) = 2$$
Step input

## Laplace transform

$$S^{2}Y(s)-sy(0)-y'(0)+3\{sY(s)-y(0)\}+2Y(s) = \frac{5}{s}$$

$$\mathcal{L}\left\{y''(t)\right\}$$

$$\mathcal{L}\left\{y'(t)\right\}$$

$$\Rightarrow Y(s) = \frac{-s^{2}-s+5}{s(s+1)(s+2)}$$

#### Example 1: ODE with initial conditions (cont'd)

## 2. Partial fraction expansion

$$Y(s) = \frac{-s^2 - s + 5}{s(s+1)(s+2)} = \frac{A}{s} + \frac{B}{s+1} + \frac{C}{s+2}$$

Multiply both sides by s & let s go to zero:

$$sY(s)|_{s\to 0} = A + s \frac{B}{s+1}\Big|_{s\to 0} + s \frac{C}{s+2}\Big|_{s\to 0} \implies A = sY(s)|_{s\to 0} = \frac{5}{2}$$

Similarly,

$$B = (s+1)Y(s)|_{s\to -1} = \dots = -5$$
  
 $C = (s+2)Y(s)|_{s\to -2} = \dots = \frac{3}{2}$ 

## Example 1: ODE with initial conditions (cont'd)



Inverse Laplace transform

$$\mathcal{L}^{-1}\left\{Y(s) = \frac{A}{s} + \frac{B}{s+1} + \frac{C}{s+2}\right\}$$

$$\Longrightarrow y(t) = \left(\underbrace{\frac{5}{2}}_{A} + \underbrace{(-5)}_{B} e^{-t} + \underbrace{\frac{3}{2}}_{C} e^{-2t}\right) u_{s}(t)$$

If we are interested in only the final value of y(t), apply Final Value Theorem:

$$\lim_{t \to \infty} y(t) = \lim_{s \to 0} sY(s) = \lim_{s \to 0} \frac{-s^2 - s + 5}{(s+1)(s+2)} = \frac{5}{2}$$

## (5) Control Performance Index: Step Response (cont'd)

#### (1) Peak Time & Value

$$y(t) = 1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin(\omega_d t + \phi) \quad \text{for } \zeta < 1$$

peak value @  $\frac{dy}{dt} = 0$ 

$$\frac{\varsigma \omega_n}{\sqrt{1-\varsigma^2}} e^{-\varsigma \omega_n t} \sin(\omega_d t + \varphi) - \frac{1}{\sqrt{1-\varsigma^2}} e^{-\varsigma \omega_n t} (\omega_d) \cos(\omega_d t + \varphi) = 0$$

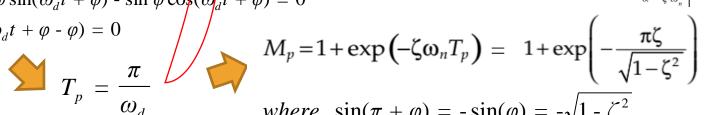
$$\Rightarrow \varsigma \omega_n \sin(\omega_d t + \varphi) - (\omega_d) \cos(\varphi_d t + \varphi) = 0$$

$$\Rightarrow \cos \varphi \sin(\omega_d t + \varphi) - \sin \varphi \cos((\omega_d t + \varphi)) = 0$$

$$\cdot \sin(\omega_d t + \varphi - \varphi) = 0$$



$$T_p = \frac{\pi}{\omega_d}$$

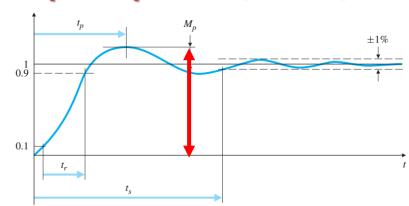


where, 
$$\sin(\pi + \varphi) = -\sin(\varphi) = -\sqrt{1 - \zeta^2}$$

where, 
$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$\sin^2\varphi + \cos^2\varphi = 1$$

$$\sin \varphi = \sqrt{1 - \zeta^2}$$



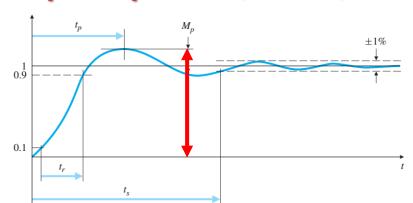
s-plane

## (5) Control Performance Index: Step Response (cont'd)

#### (2) Settling Time

$$y(t) = 1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin(\omega_d t + \phi)$$
 for  $\zeta < 1$ 

peak value@ settlingtime  $(T_s)$ 



$$M_p = 1 + \exp\left(-\zeta \omega_n T_p\right)$$

$$\exp(-\varsigma\omega_n T_s) = 0.01(1\%)$$

$$-\varsigma\omega_n T_s = \ln(0.01) = -4.6$$

peak value@ settlingtime 
$$(T_s)$$

$$M_p = 1 + \exp(-\zeta \omega_n T_p)$$

$$\exp(-\varsigma \omega_n T_s) = 0.01(1\%)$$

$$T_s \approx \frac{4.6}{\varsigma \omega_n} = \frac{4.6}{\sigma}$$

$$\exp(-\varsigma\omega_n T_s) = 0.02 (2\%)$$



$$\exp(-\varsigma\omega_n T_s) = 0.02 (2\%) \qquad \qquad \therefore T_s \approx \frac{4.0}{\varsigma\omega_n} = \frac{4.0}{\sigma}$$

#### Important question:

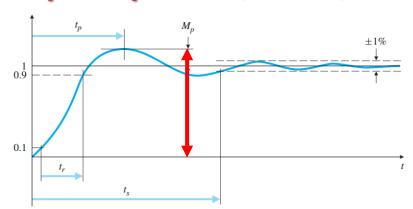
- How does damping ratio & natural frequency work for the settling time ?? 35

## (5) Control Performance Index: Step Response (cont'd)

#### (3) Rise Time

$$y(t) = 1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin(\omega_d t + \phi)$$
 for  $\zeta < 1$ 

$$y(t) = 1$$
 @ rising time  $(T_r)$  where,  $t_r \approx T_r$ 



$$\sin(\omega_{d}T_{r} + \varphi) = 0$$
or
$$where,$$

$$\therefore T_{r} = \frac{\pi - \varphi}{\omega_{d}} \quad \omega_{d} = \omega_{n}\sqrt{1 - \varsigma^{2}}$$

$$\cos \varphi = \varsigma$$

$$i) \varsigma = 0.5$$

$$\Rightarrow \varphi = \cos^{-1}(0.5) = 1.05$$

$$\therefore T_{r} = \frac{3.14 - 1.05}{\omega_{n}\sqrt{1 - 0.5^{2}}} \approx \frac{2.4}{\omega_{n}}$$

$$\therefore T_{r} = \frac{3.14 - 0.8}{\omega_{n}\sqrt{1 - 0.7^{2}}} \approx \frac{3.3}{\omega_{n}}$$

$$i) \varsigma = 0.5$$

$$\Rightarrow \varphi = \cos^{-1}(0.5) = 1.05$$

$$\therefore T_r = \frac{3.14 - 1.05}{\omega_n \sqrt{1 - 0.5^2}} \approx \frac{2.4}{\omega_n}$$

$$i) \varsigma = 0.7$$

$$\Rightarrow \varphi = \cos^{-1}(0.7) \approx 0.8$$

$$\therefore T_r = \frac{3.14 - 0.8}{\omega_n \sqrt{1 - 0.7^2}} \approx \frac{3.3}{\omega_n}$$

#### Important question:

- How does damping ratio & natural frequency work for the rise time ??

## (5) Control Performance Index: Step Response (cont'd)

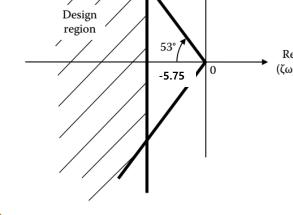
#### [Example]

Design requirement are for <u>Controller</u> + Plant (C-L)

- (1) a percentage overshoot of less than 10%
- (2) a settling time of less than 0.8 second

#### [Question]

Indicate this design specification as a region on the s-plane.



s-Plane

Im

 $(\omega_d)$ 

#### [Solution]

(1) 10% of overshoot means 
$$\Rightarrow$$
 0.1=  $\exp\left(-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}\right)$   $\Rightarrow$  0.6  $\leq \zeta = \cos\varphi$   $\varphi \leq 53 (deg)$ 

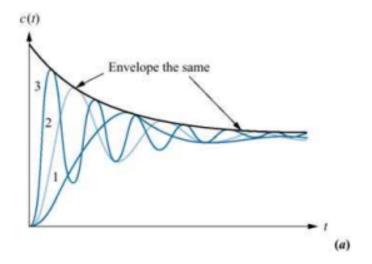
$$0.6 \le \varsigma = \cos \varphi$$
  
 $\varphi \le 53(\text{deg})$ 

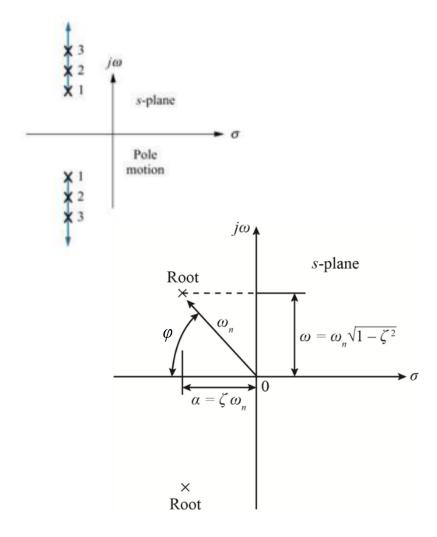
(2) 
$$T_s = 0.8$$
 sec means

$$\Rightarrow :: T_s \approx \frac{4.6}{\varsigma \omega_n} \le 0.8 \Rightarrow \varsigma \omega_n \ge 5.75$$

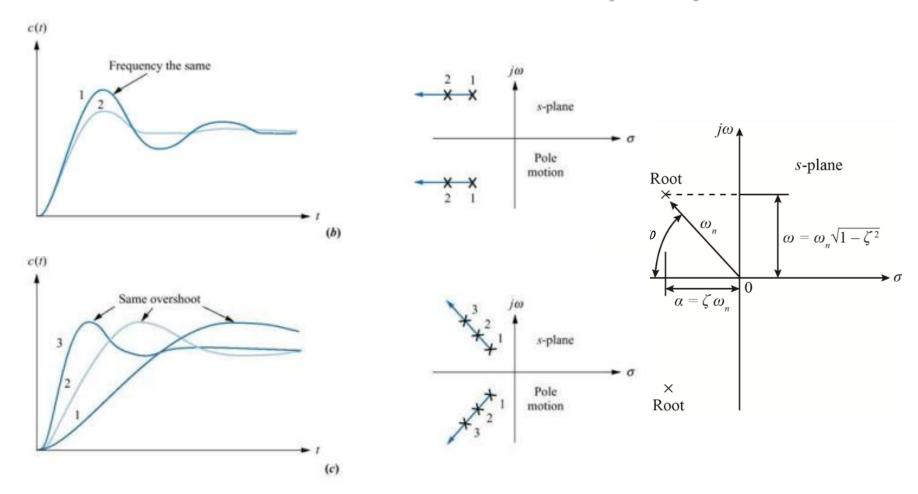
$$s = -\sigma \pm j\omega_d$$
.  $\sigma = \zeta \omega_n$ 

## **❖ Summary #1: Pole Placement vs. Step Response**





## **❖ Summary #1: Pole Placement vs. Step Response (cont'd)**



## Summary

#### **Summary:**

- Important aspects of dynamic response for control system
- The specifications for the controller performance
- Step response by Pole & Zero locations