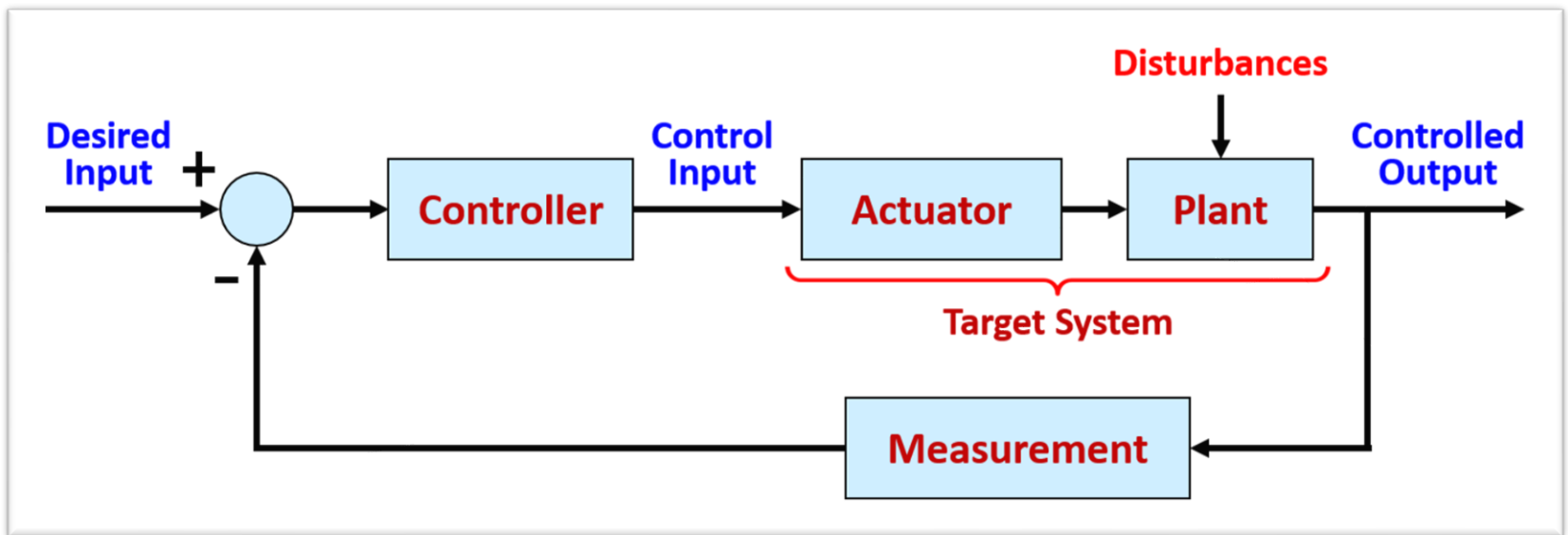


# The Root-Locus Design Method 2

## Lecture 9:

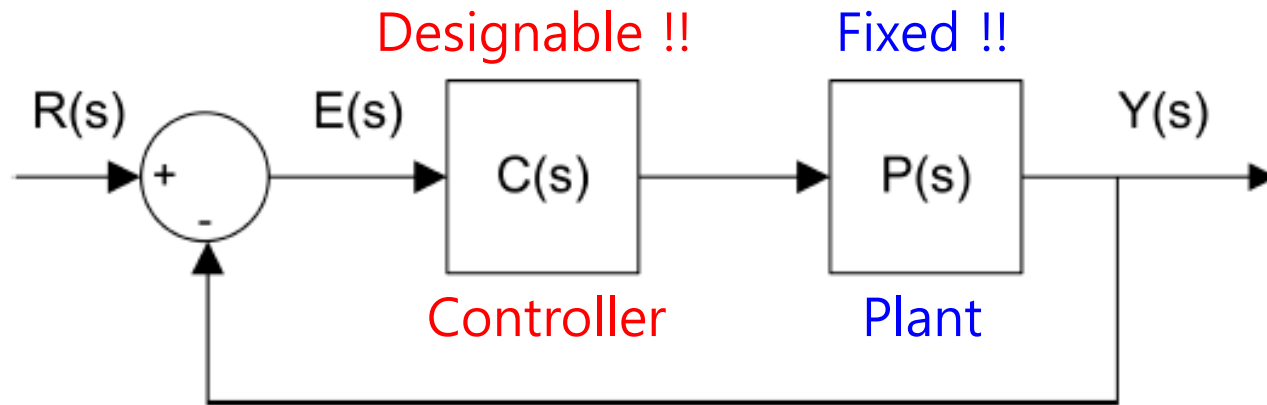
- Lead Compensator
- Lag Compensator



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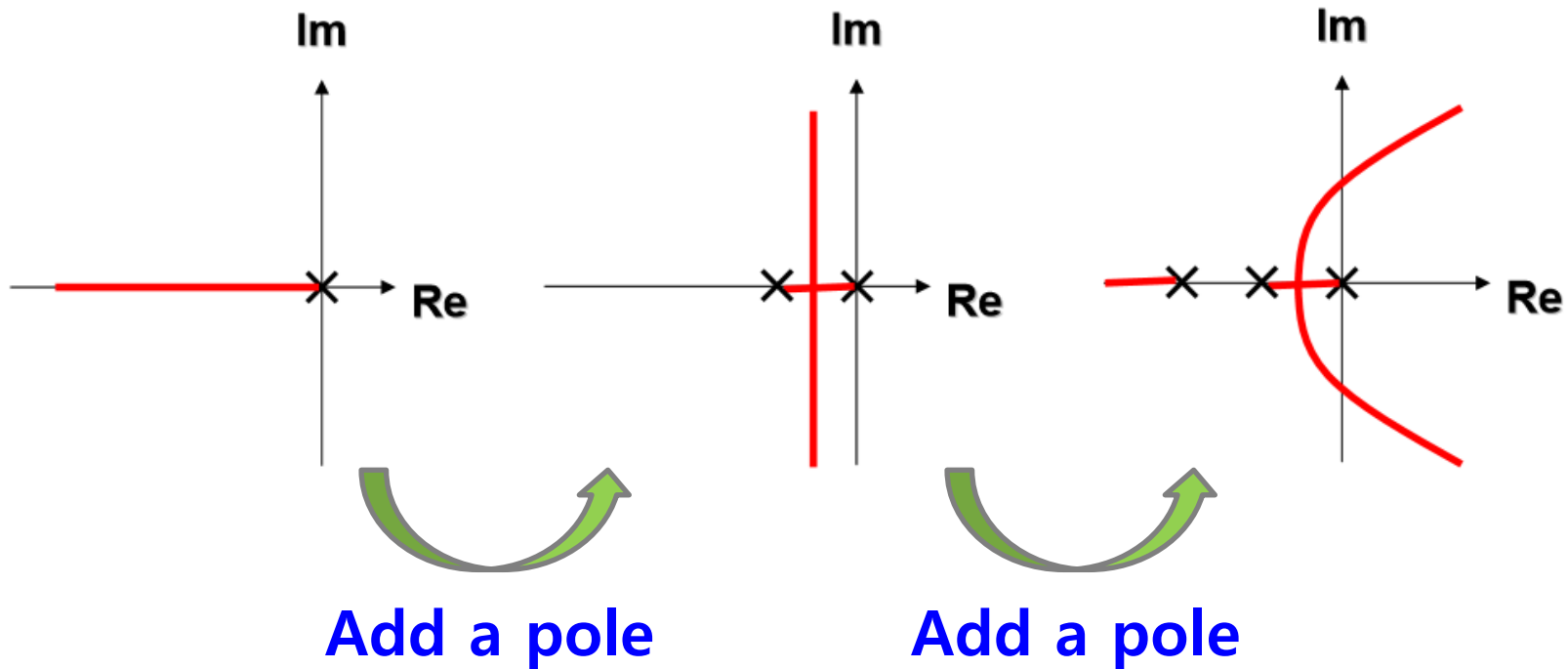
# Closed-Loop Design by Root Locus



- Place closed-loop poles at desired locations,
  - By tuning the gain  $C(s) = K$ . (for time-domain specifications)
- If root locus **does NOT pass** the desired locations, then **reshape** the root locus
  - By adding poles and/or zeros to  $C(s)$ .  
It is called "Compensation"

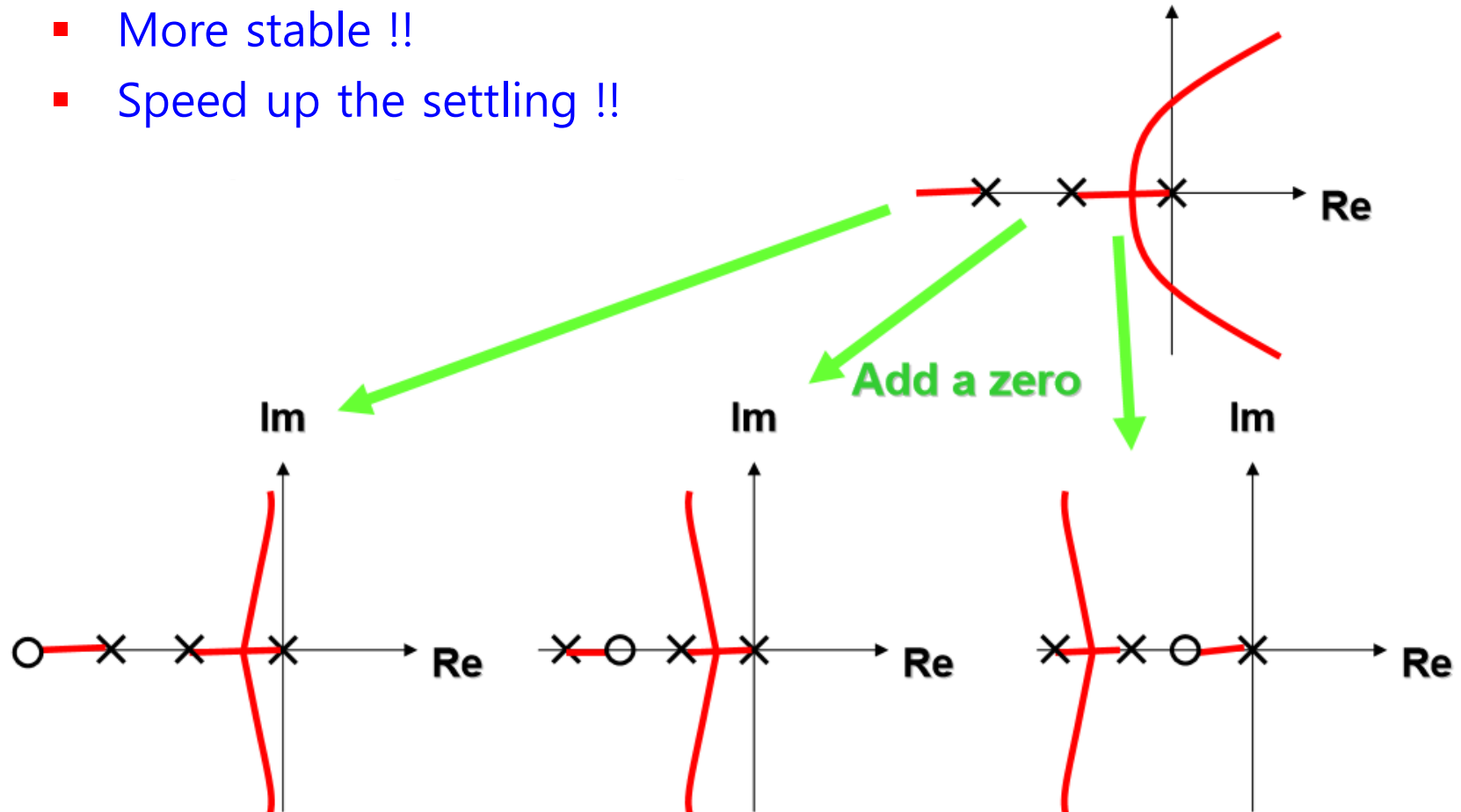
# General Effect of Adding Poles

- Adding poles pulls root locus to the RIGHT,
  - Less stable !!
  - Slow down the settling !!



# General Effect of Adding Zeros

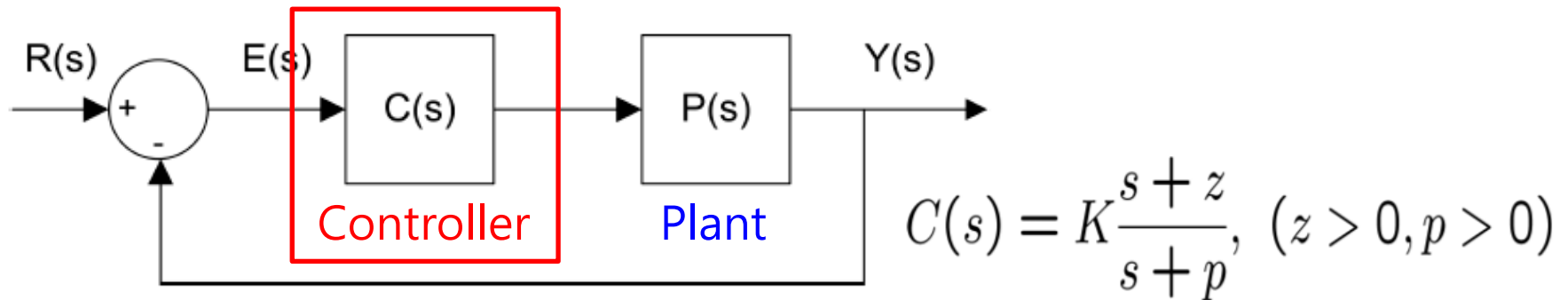
- Adding zeros pulls root locus to the LEFT,
  - More stable !!
  - Speed up the settling !!



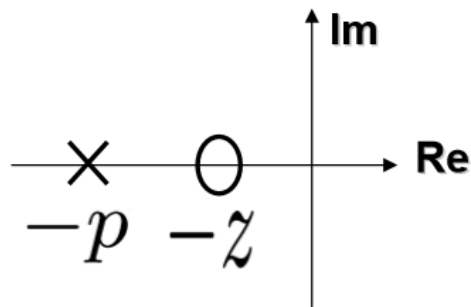
# Some Remarks about adding Poles/Zeros

- Adding **only zero**,  $C(s) = s + z$ , ( $z > 0$ )
  - often gets **side-effect** because such controller amplifies high-frequency noise.
- Adding **only pole**,  $C(s) = 1/(s + p)$ , ( $p > 0$ )
  - often gets **side-effect** because such controller makes a less stable system by moving the closed-loop poles to the right.
- These facts can be explained by **using frequency response analysis (i.e., Bode plot)** → Next Lecture
- Then, let us add **Both Zero & Pole !!**

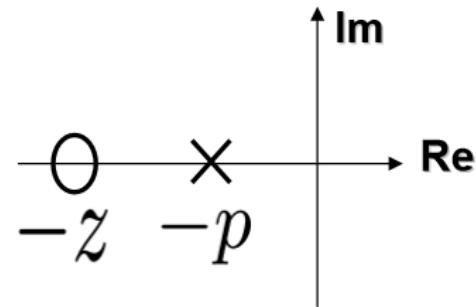
# Lead & Lag Compensators



- **Lead** Compensator



- **Lag** Compensator



※ Why these are called "Lead" and "Lag" ??

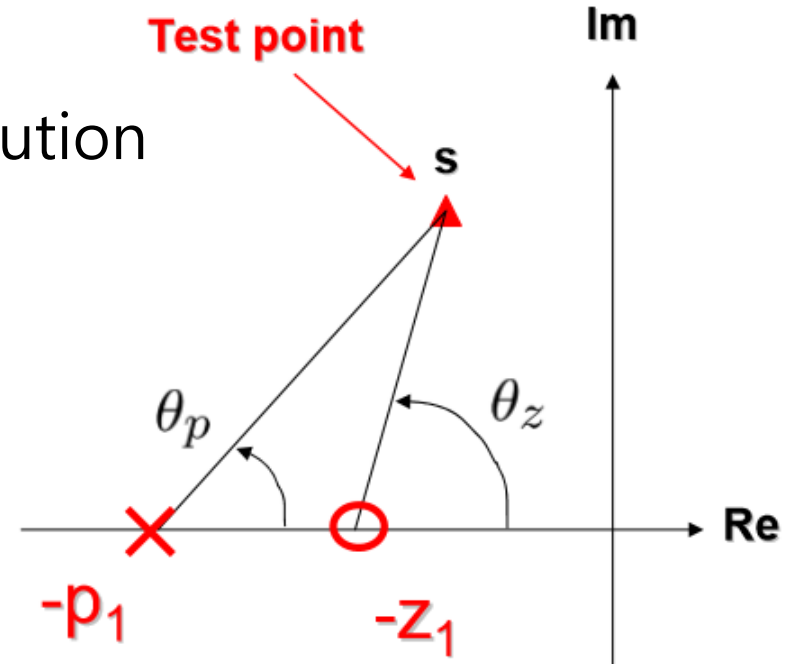
→ We will see this from frequency response in next class.

# Lead Compensators



- Positive (Lead) angle contribution

$$\angle C_{Lead}(s) = \theta_{Lead} > 0$$

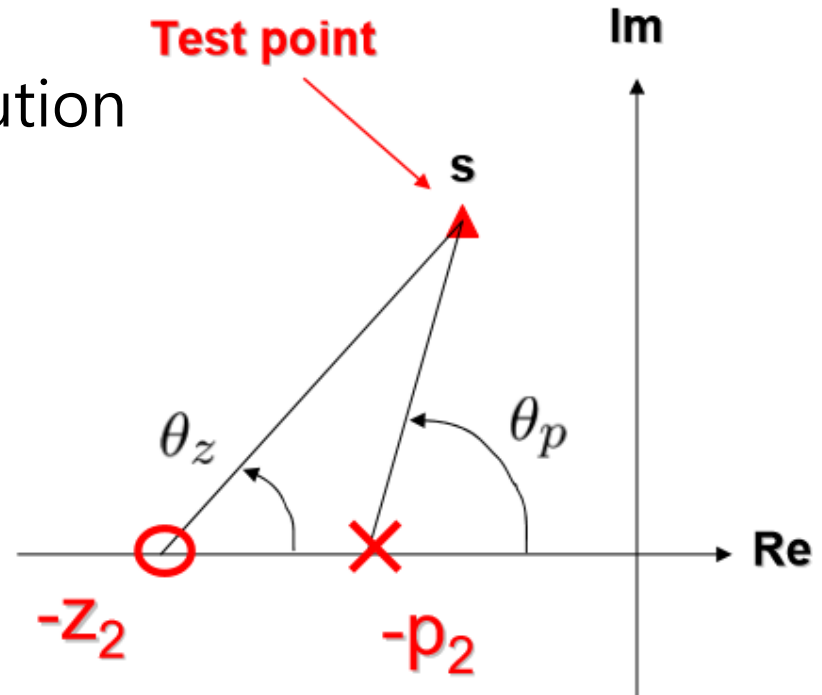


$$\begin{aligned}\angle C_{Lead}(s) &= \angle \frac{s + z_1}{s + p_1} = \angle(s + z_1) - \angle(s + p_1) \\ &= \theta_z - \theta_p = \theta_{Lead} > 0 \\ &\text{where, } \theta_z > \theta_p\end{aligned}$$

# Lag Compensators

- Negative (Lag) angle contribution

$$\angle C_{Lag}(s) = \theta_{Lag} < 0$$



$$\begin{aligned}\angle C_{Lag}(s) &= \angle \frac{s + z_2}{s + p_2} = \angle(s + z_2) - \angle(s + p_2) \\ &= \theta_z - \theta_p = \theta_{Lag} < 0\end{aligned}$$

where,  $\theta_z < \theta_p$



# Roles of Lead and Lag Compensator

## 1. Lead Compensator

- Improve transient response.
- Improve stability.

$$C_{Lead}(s) = K_1 \frac{s + z_1}{s + p_1}$$

where,  $p_1 > z_1$

## 2. Lag Compensator

- Reduce steady state error.

$$C_{Lag}(s) = K_2 \frac{s + z_2}{s + p_2}$$

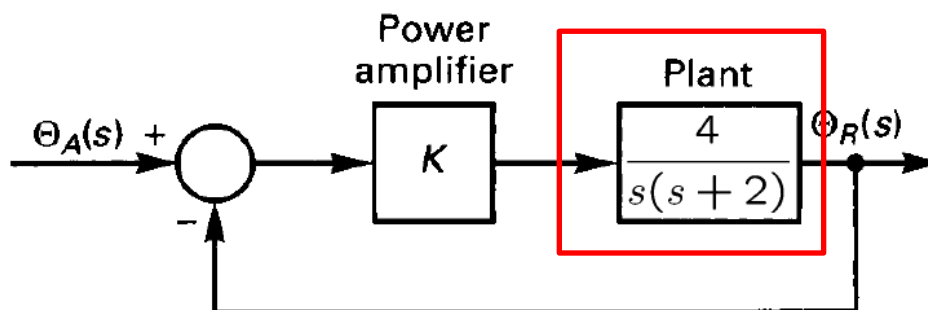
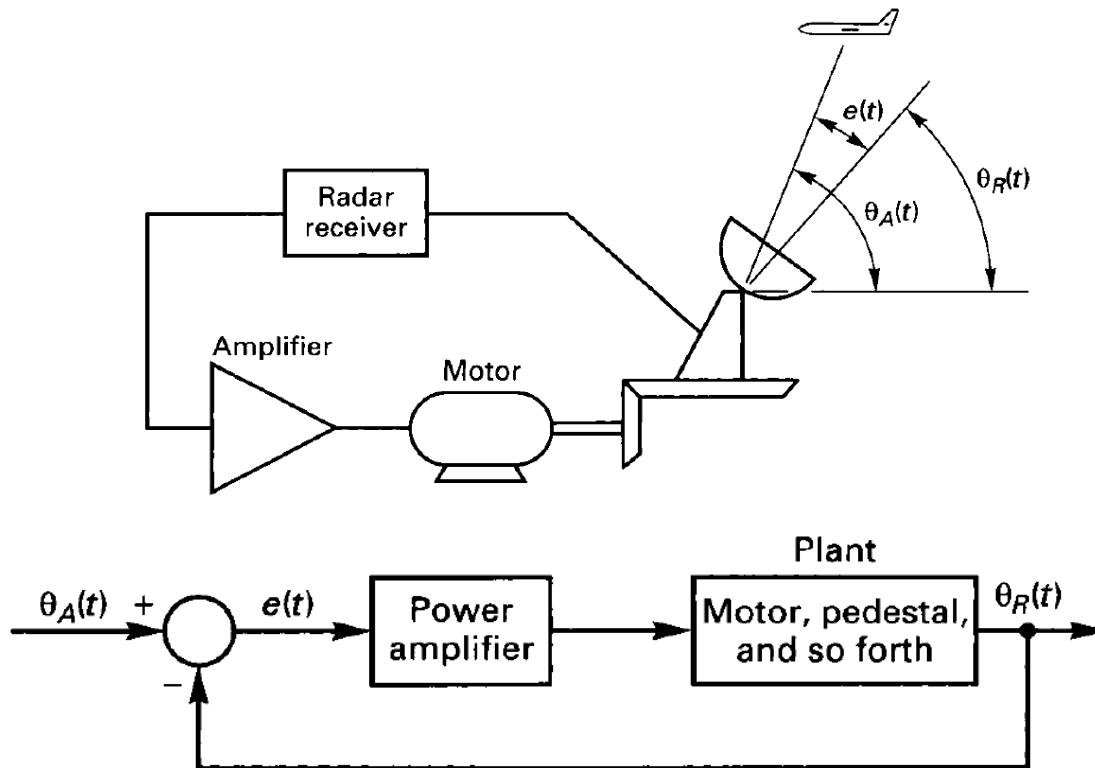
where,  $p_2 < z_2$

## 3. Lead-Lag Compensator

- Take into account all the above issues.

$$C_{LL}(s) = C_{Lead}(s)C_{Lag}(s)$$

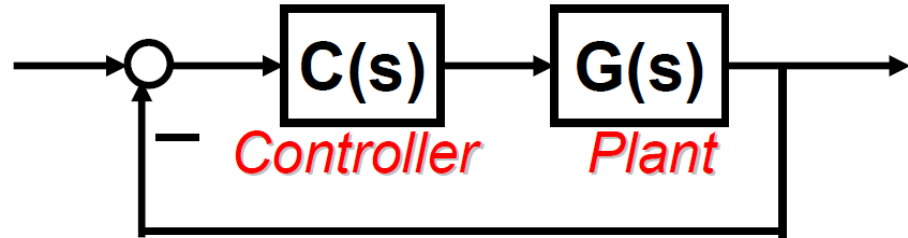
# Example: Radar Tracking System



# 1. Lead Compensator Design

- Consider system

$$G(s) = \frac{4}{s(s+2)}$$



- Analysis of C-L system for  $C(s) = 1$   $H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$

$$H(s)_{CL} = \frac{1 \times \frac{4}{s(s+2)}}{1 + 1 \times \frac{4}{s(s+2)}} = \frac{4}{s^2 + 2s + 4}$$



$$\omega_n = 2 \text{ [rad/sec]}$$

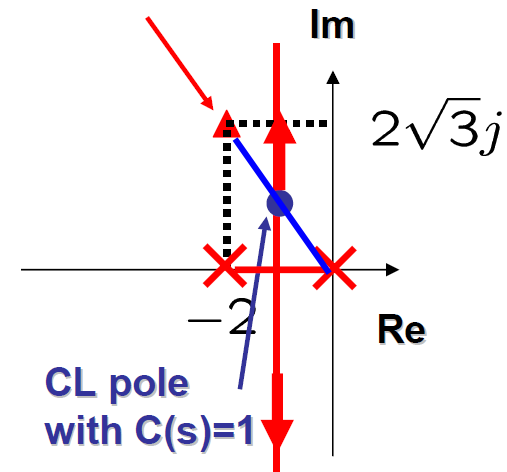
$$\zeta = 0.5$$

Desired pole

- Performance Requirement Specification

- Damping ratio:  $\zeta = 0.5$  (the same !!)
- Natural frequency:  $\omega_n = 4$  [rad/s] !!

$$H(s)_{CL,desired} = \frac{16}{s^2 + 4s + 16} = \frac{16}{(s + 2 + 2\sqrt{3}j)(s + 2 - 2\sqrt{3}j)}$$



# Angle and Magnitude Conditions (**Review**)

- If a point **s** to be on root locus, then it satisfies
  - Step 1: Check angle condition

$$\angle L(s) = 180^\circ \times (2k + 1), \quad k = 0, \pm 1, \pm 2, \dots$$

*Odd number*

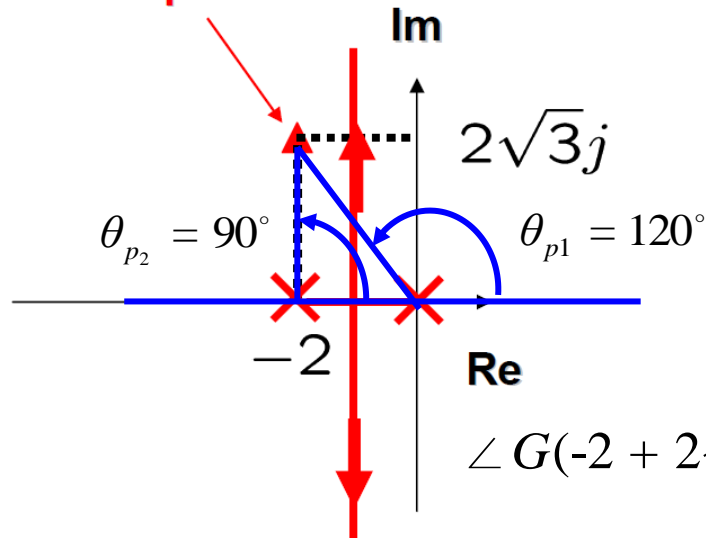
- For a point on root locus, **gain K** is obtained by
  - Step 2: Magnitude condition

$$1 + KL(s) = 0 \Rightarrow L(s) = -\frac{1}{K} \Rightarrow |L(s)| = \frac{1}{K}$$

# 1. Lead Compensator Design (cont'd)

- First, Check whether **angle condition** is satisfied:

Desired pole



$$\begin{aligned}\angle G(-2 + 2\sqrt{3}j) &= \angle(s - z_1) - \angle(s - p_1) - \angle(s - p_2) \\ &= 0 - 120^\circ - 90^\circ = -210^\circ\end{aligned}$$

- But, angle condition is **NOT** satisfied !!

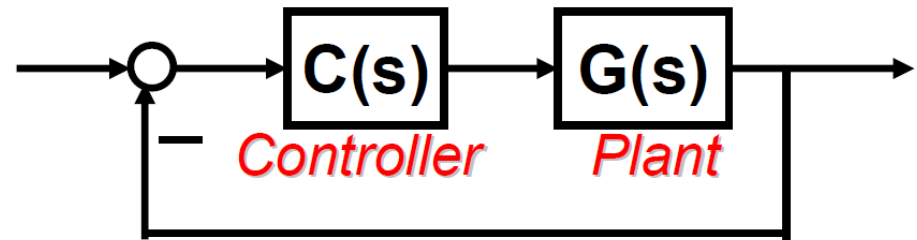
➡ Angle deficiency  
 $\varphi = +30^\circ$

➡ **Lead or Lag Compensator ??**  
(positive)

# 1. Lead Compensator Design (cont'd)

- To compensate **angle deficiency**, we need to design a **lead** compensator  $C(s)$

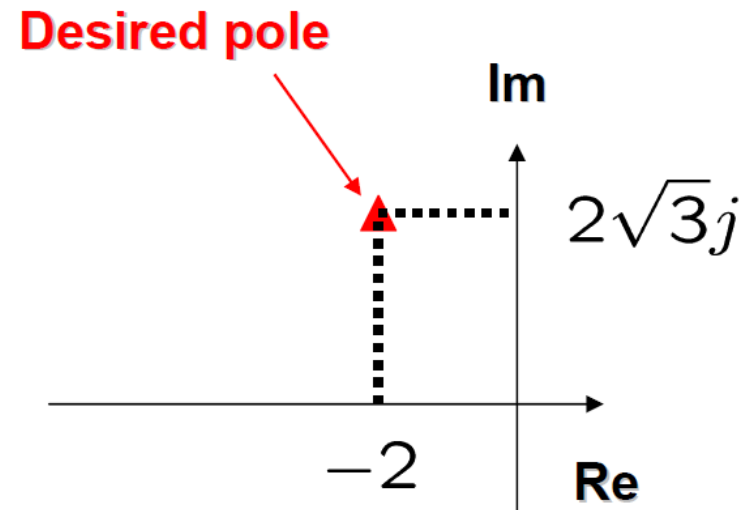
$$C(s) = K \frac{s + z}{s + p}$$



satisfying

$$\angle C(-2 + 2\sqrt{3}j) = 30(=:\phi)$$

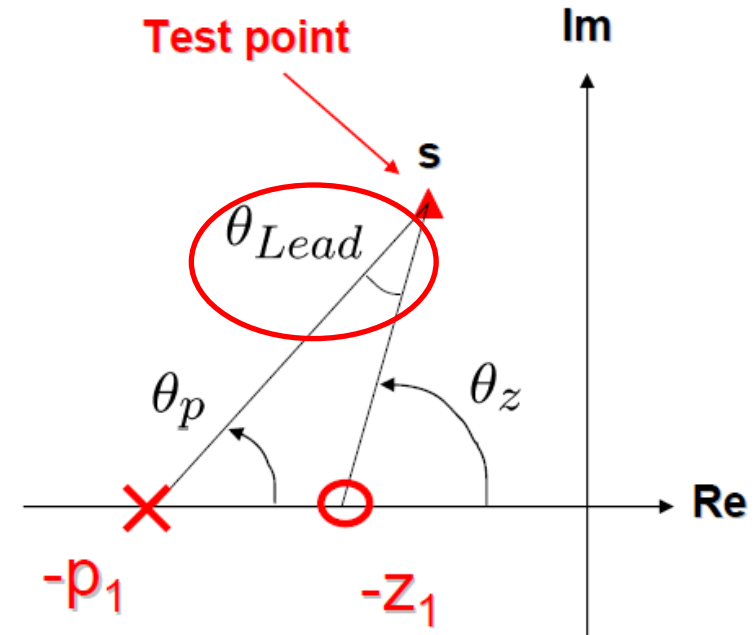
➡  $\angle H(s) = \angle CG(-2 + 2\sqrt{3}j)$   
 $= -180^\circ$



# 1. Lead Compensator Design (cont'd)

- Positive angle contribution

$$\angle C_{Lead}(s) = \theta_{Lead} > 0$$



- Triangle

$$\theta_p + \theta_{Lead} + (\pi - \theta_z) = \pi$$

$$\theta_z - \theta_p = \theta_{Lead}$$

# How to Select Pole and Zero in Lead C(s)

- Step 1: Draw horizontal line PA

- Step 2: Draw line PO

- Step 3: Draw bi-sector PB

$$\angle APB = \angle BPO = \frac{1}{2} \angle APO$$

- Step 4: Draw PC & PD ( $\Phi =$  )

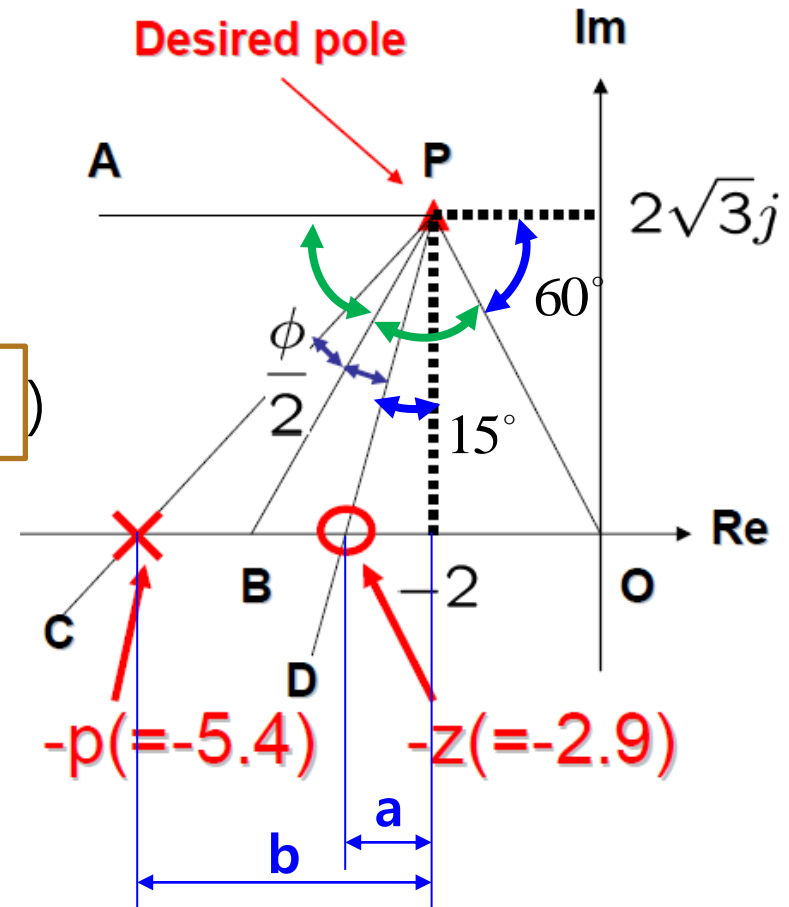
$$\angle CPB = \angle BPD = \frac{\phi}{2}$$

- Step 5: Calculate a & b

$$a = \tan(15^\circ) \times 2\sqrt{3} \approx 0.9$$

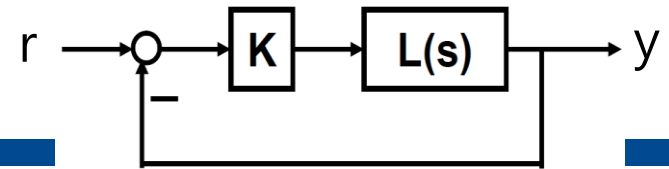
$$b = \tan(45^\circ) \times 2\sqrt{3} \approx 3.4$$

- Then, Pole and Zero of C(s) are shown in the figure.

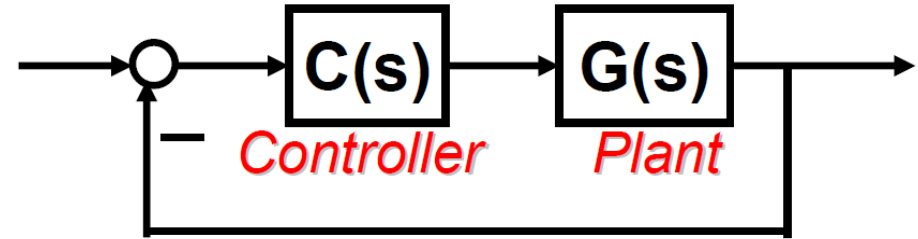




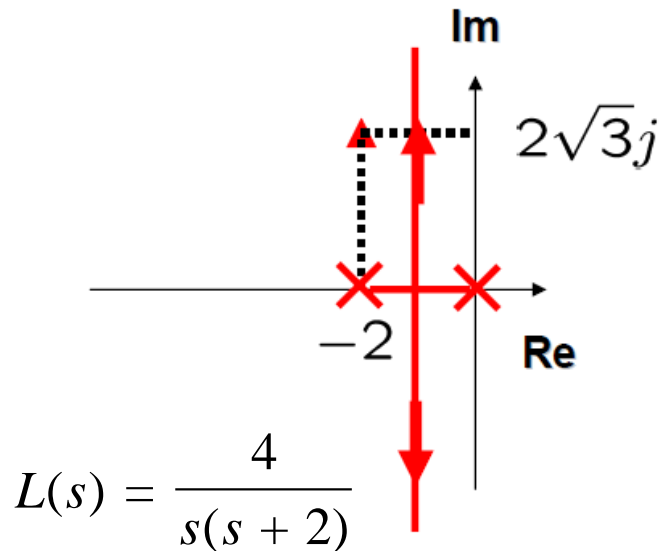
# Comparison of Root Locus



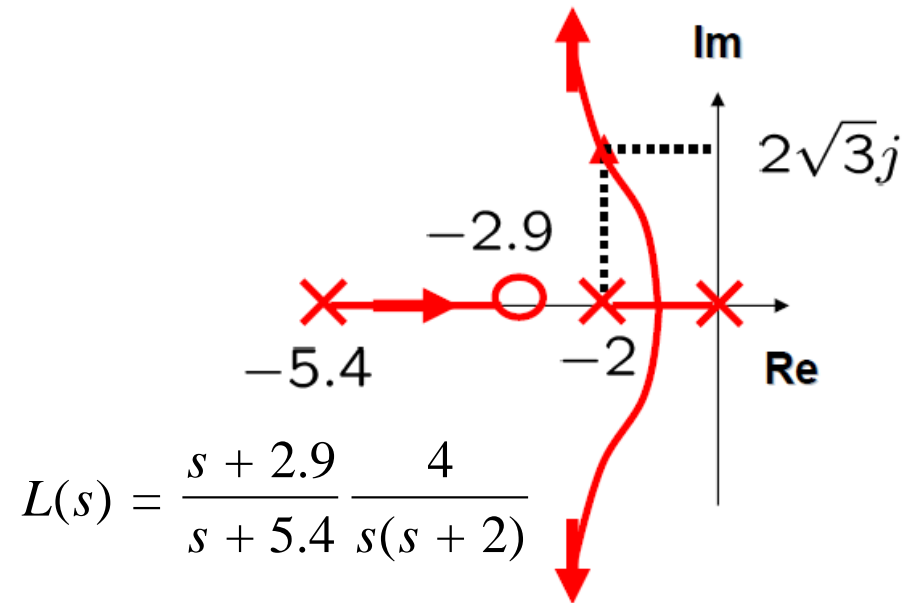
$$C(s) = K \frac{s + 2.9}{s + 5.4} \quad G(s) = \frac{4}{s(s + 2)}$$



- $G(s)$  – without Lead



- $C(s)G(s)$  – with Lead Comp.



Improved Stability !!

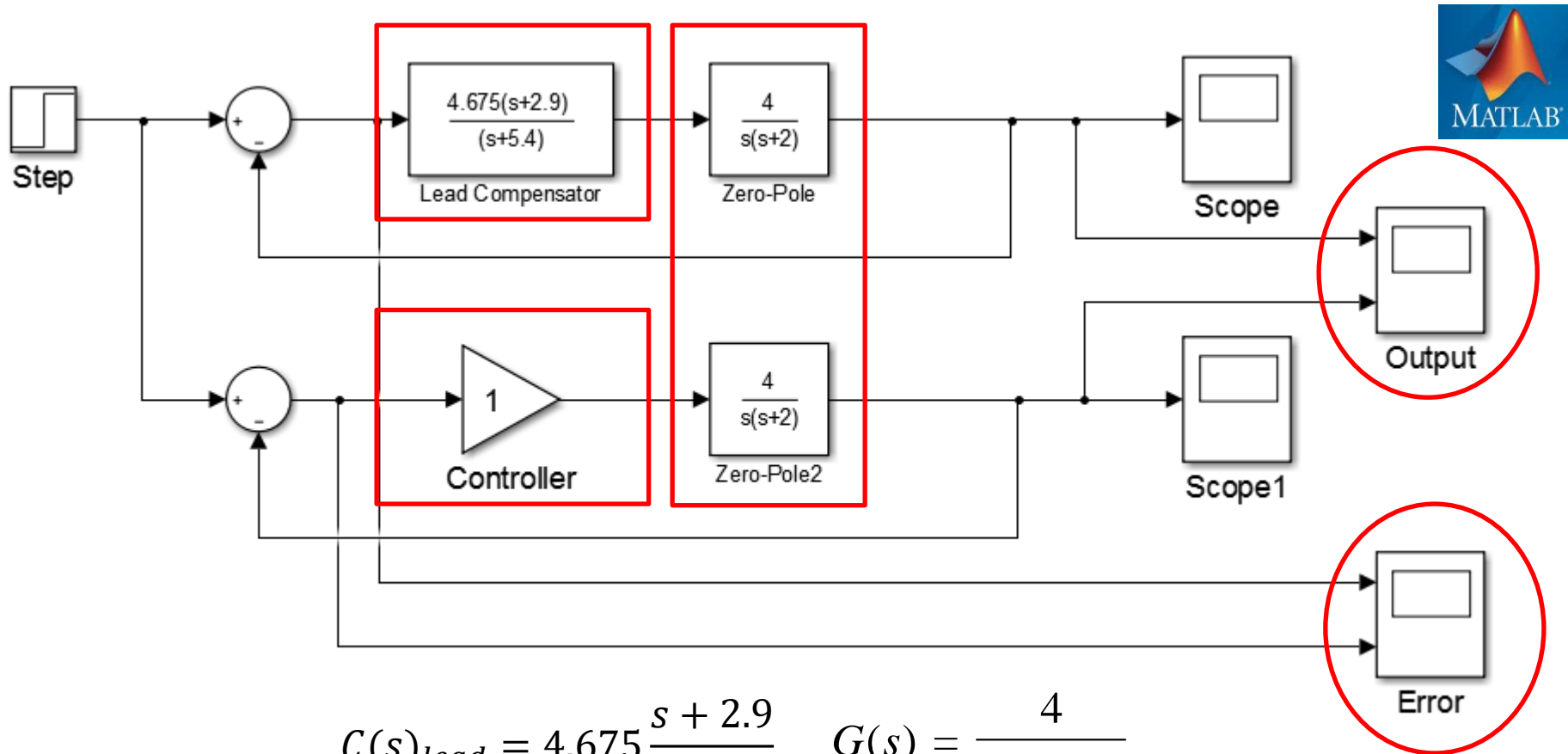
# How to Design the **Gain K** ??

- **Lead Compensator**  $C(s) = K \frac{s + 2.9}{s + 5.4}$
- **Open loop TF**  $G(s)C(s) = K \frac{4(s + 2.9)}{s(s + 2)(s + 5.4)}$
- **Magnitude condition**

$$|L(s)| = \frac{1}{K} \quad \Rightarrow \quad K \left| \frac{4(s + 2.9)}{s(s + 2)(s + 5.4)} \right|_{s=-2+2\sqrt{3}j} = 1$$

$$K = \frac{1}{|L(s)|} \cong 4.675$$

# Comparison of Step Responses

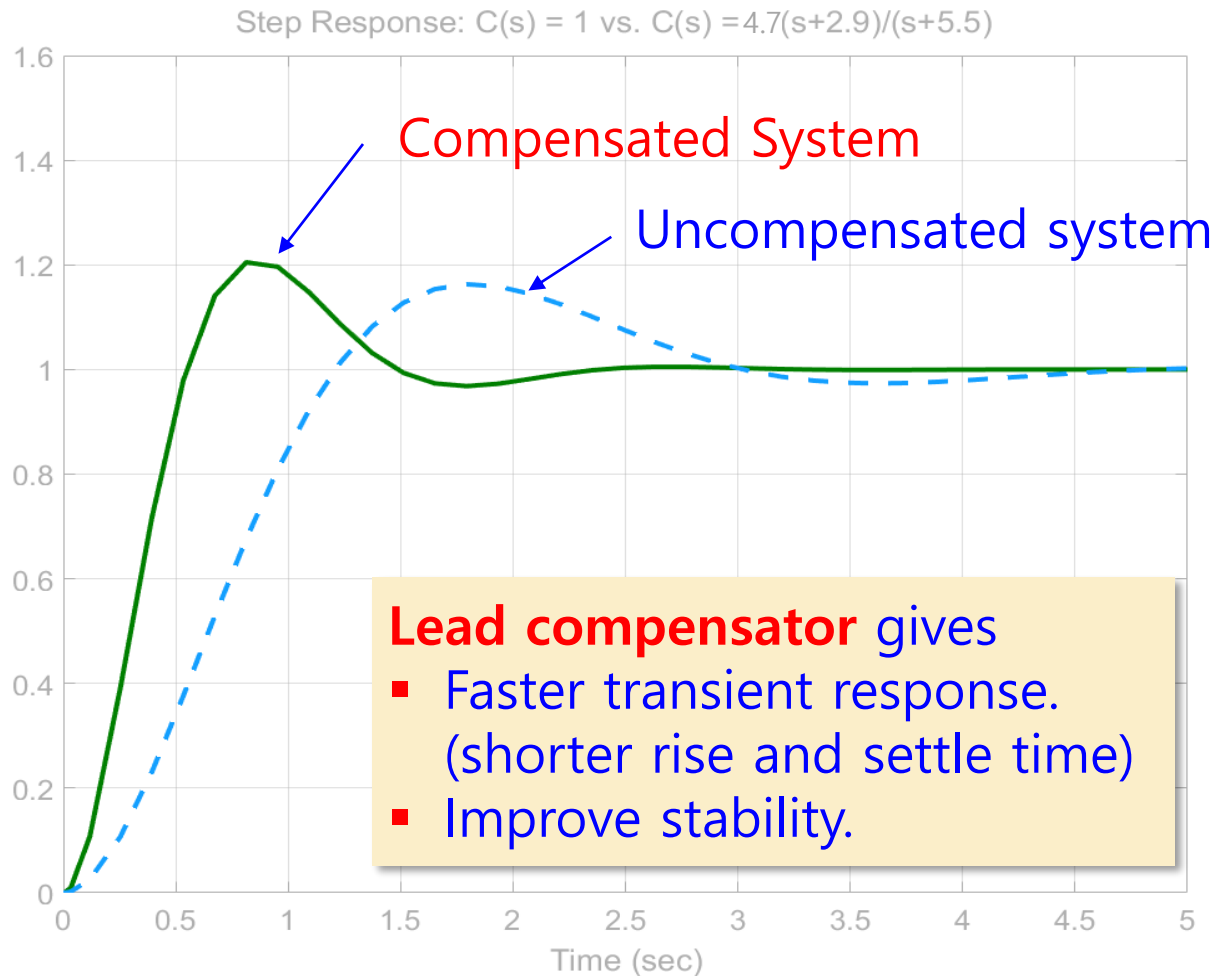


$$C(s)_{lead} = 4.675 \frac{s + 2.9}{s + 5.4} \quad G(s) = \frac{4}{s(s + 2)}$$

$$C(s)_{uncompensated} = 1$$

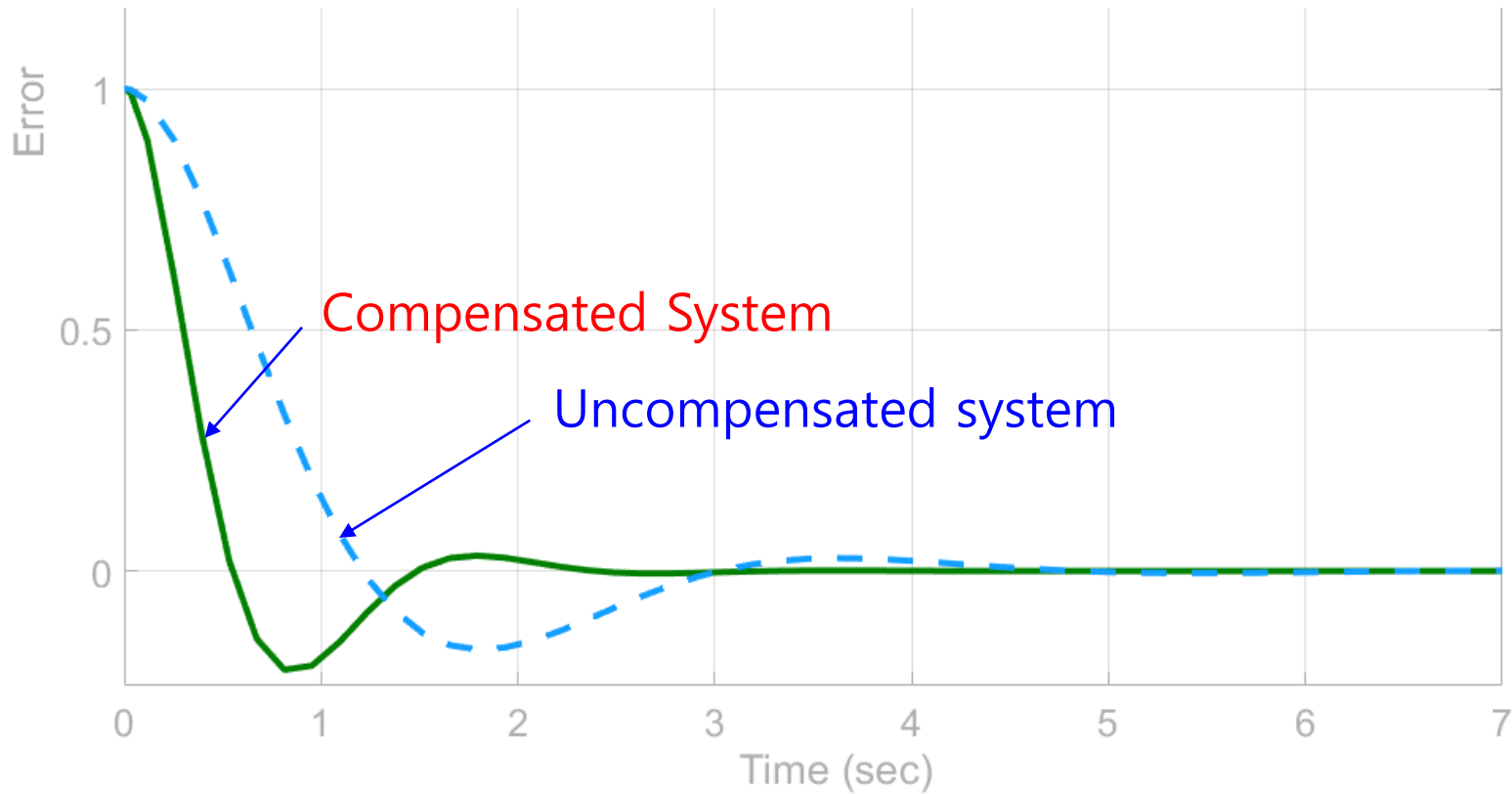
# Comparison of Step Responses (cont'd)

## (1) Output comparison



# Comparison of Step Responses (cont'd)

## (2) Error comparison



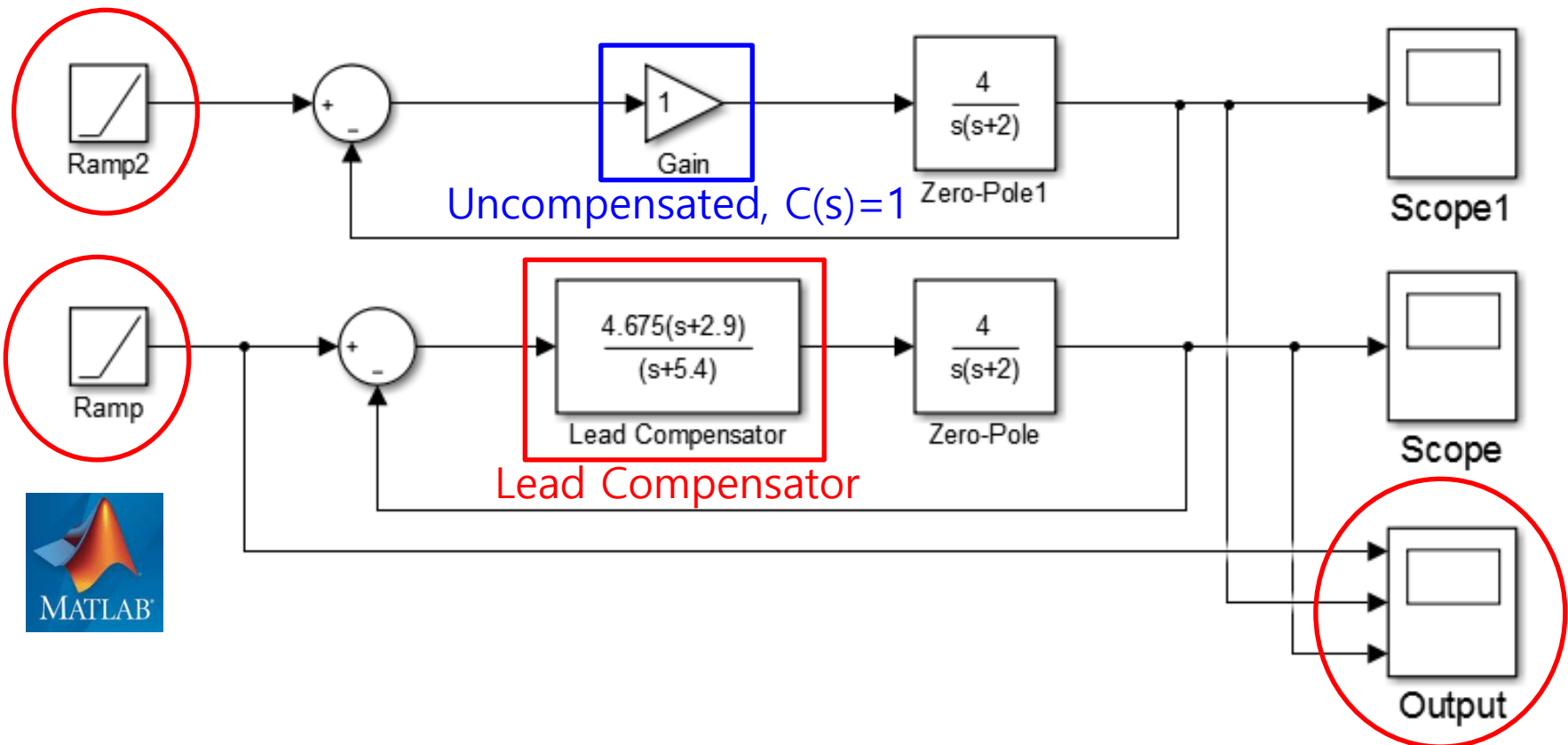
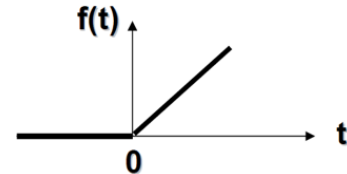
# Step response vs. Ramp response

For Lead compensator,

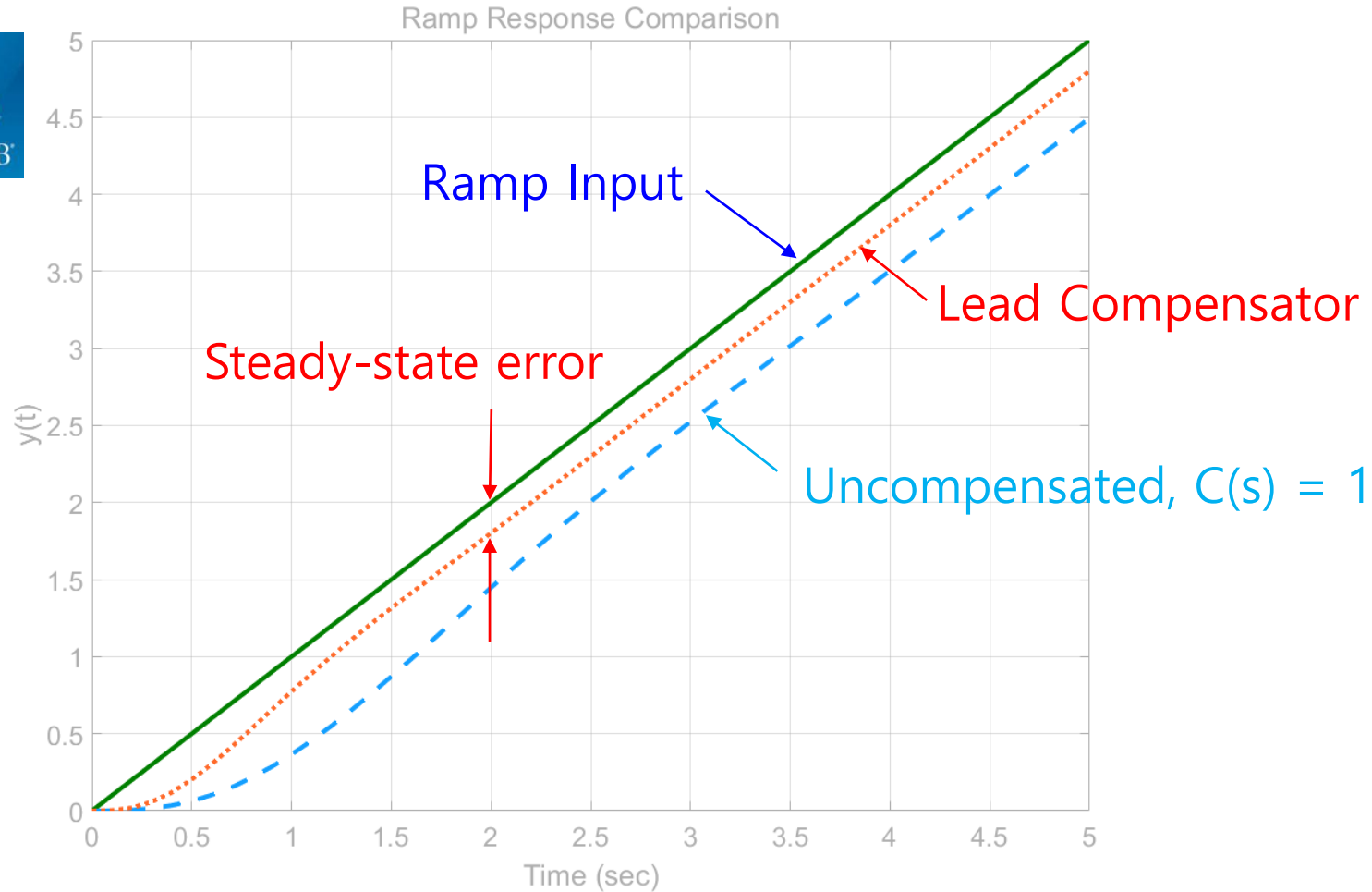
But, what happened with ramp input ??

❖ Unit Ramp Function

$$f(t) = \begin{cases} t & t \geq 0 \\ 0 & t < 0 \end{cases}$$



# Step response vs. Ramp response (cont'd)

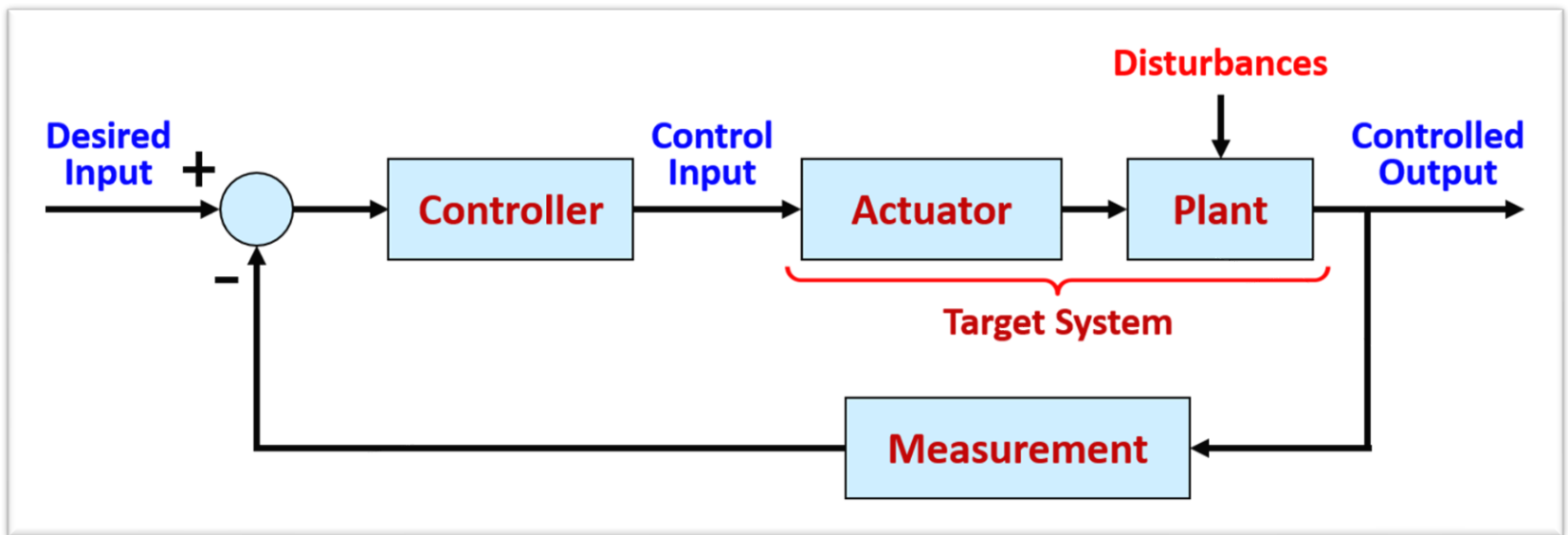


- Is it small enough steady-state error??
- Then, how to reduce something more about steady-state error??

# The Root-Locus Design Method 2

## Lecture 9:

- Lead Compensator
- Lag Compensator



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# Roles of **Lead** and **Lag** Compensator (**Review**)

## 1. **Lead** Compensator

- Improve **transient response**.
- Improve **stability**.

$$C_{Lead}(s) = K_1 \frac{s + z_1}{s + p_1}$$

*where,  $p_1 > z_1$*

## 2. **Lag** Compensator

- Reduce steady state error.

$$C_{Lag}(s) = K_2 \frac{s + z_2}{s + p_2}$$

*where,  $p_2 < z_2$*

## 3. **Lead-Lag** Compensator

- Take into account all the above issues.

$$C_{LL}(s) = C_{Lead}(s)C_{Lag}(s)$$

# System Type for Tracking (**revisited**)

## ❖ Closed-Loop System

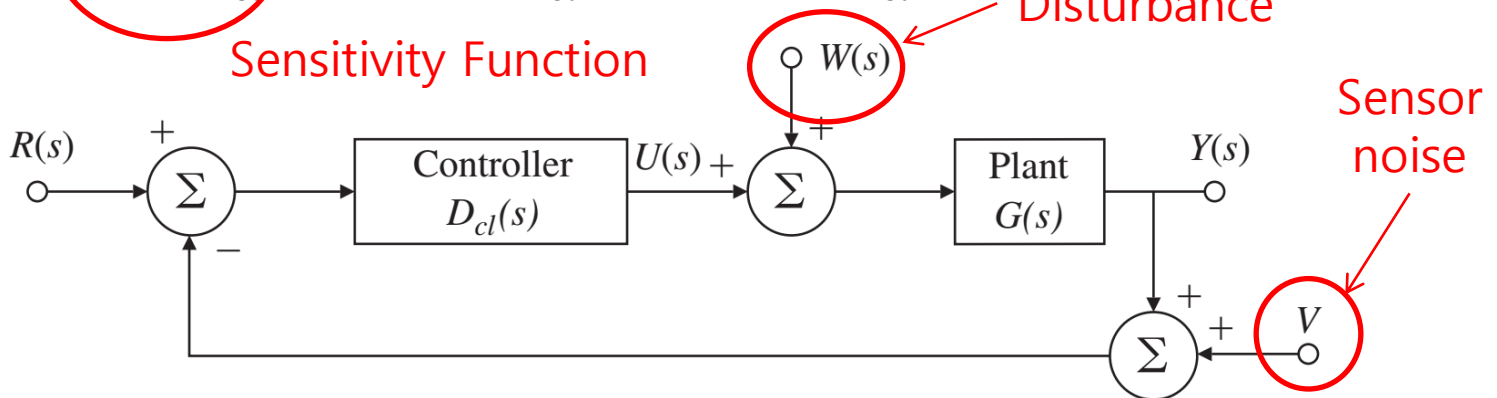
- The **controlled output** is given by

$$Y_{cl} = \frac{GD_{cl}}{1 + GD_{cl}}R + \frac{G}{1 + GD_{cl}}W - \frac{GD_{cl}}{1 + GD_{cl}}V,$$

- The **error**, difference btw reference input and output is given by

$$\begin{aligned} E_{cl} &= R - \left[ \frac{GD_{cl}}{1 + GD_{cl}}R + \frac{G}{1 + GD_{cl}}W - \frac{GD_{cl}}{1 + GD_{cl}}V \right], \\ &= \underbrace{\frac{1}{1 + GD_{cl}}}_{\text{Sensitivity Function}} R - \frac{G}{1 + GD_{cl}}W + \frac{GD_{cl}}{1 + GD_{cl}}V. \end{aligned}$$

Disturbance



# System Type for Tracking (cont'd) (**revisited**)

- If we consider tracking the reference input alone, set  $W = V = 0$ , (where,  $G$ : plant model,  $D_{cl}$ : controller)

$$E = \frac{1}{1 + GD_{cl}} R = \mathcal{S} R, \quad \text{where} \quad \mathcal{S} = \frac{1}{1 + GD_{cl}}.$$

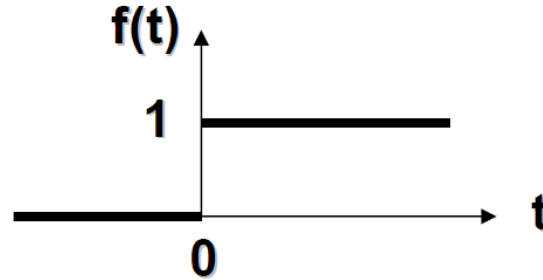
- For analyzing error  $\{E(s)\}$ , categorizing based on three types of reference inputs,

$$R(s) = \frac{1}{s^{k+1}} \left\{ \begin{array}{ll} k = 0 \Rightarrow R(s) = \frac{1}{s} & \Rightarrow \text{Step Input (or position)} \\ k = 1 \Rightarrow R(s) = \frac{1}{s^2} & \Rightarrow \text{Ramp Input (or velocity)} \\ k = 2 \Rightarrow R(s) = \frac{1}{s^3} & \Rightarrow \text{Parabola Input (or acceleration)} \end{array} \right.$$

# Examples of Laplace Transform (revisited)

## ❖ Unit Step Function

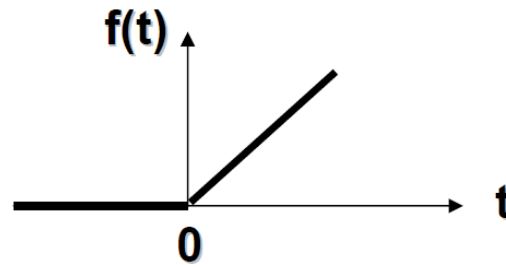
$$f(t) = u_s(t) = \begin{cases} 1 & t \geq 0 \\ 0 & t < 0 \end{cases}$$



$$\Rightarrow F(s) = \int_0^{\infty} 1 \cdot e^{-st} dt = -\frac{1}{s} [e^{-st}]_0^{\infty} = \boxed{\frac{1}{s}}$$

## ❖ Unit Ramp Function

$$f(t) = \begin{cases} t & t \geq 0 \\ 0 & t < 0 \end{cases}$$



$$\Rightarrow F(s) = \int_0^{\infty} t e^{-st} dt = -\frac{1}{s} [t e^{-st}]_0^{\infty} + \frac{1}{s} \int_0^{\infty} e^{-st} dt = \boxed{\frac{1}{s^2}}$$

(Integration by parts)

$$\int uv' dx = uv - \int u'v dx$$

# System Type for Tracking (cont'd) (**revisited**)

- Apply the Final Value Theorem to the error formula,

$$\begin{aligned} \lim_{t \rightarrow \infty} e(t) &= e_{ss} = \lim_{s \rightarrow 0} s E(s), \\ &= \lim_{s \rightarrow 0} s \frac{1}{1 + GD_{cl}} R(s), \quad R(s) = \frac{1}{s^{k+1}} \\ &= \lim_{s \rightarrow 0} s \frac{1}{1 + GD_{cl}} \frac{1}{s^{k+1}}. \end{aligned}$$

- General form of  $GD_{cl}$  without the pole at the origin ( $s = 0$ )

$$GD_{cl}(s) = \frac{GD_{clo}(s)}{s^n} \quad \text{where,} \quad GD_{clo}(0) = K_n : \text{DC gain (or constant)}$$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} s \frac{1}{1 + \frac{GD_{clo}(s)}{s^n}} \frac{1}{s^{k+1}}, \quad = \lim_{s \rightarrow 0} \frac{s^n}{s^n + K_n} \frac{1}{s^k}.$$

# System Type for Tracking (cont'd) (**revisited**)


- From the equation,  $e_{ss} = \lim_{s \rightarrow 0} \frac{s^n}{s^n + K_n} \frac{1}{s^k}$ . where,  $R(s) = \frac{1}{s^{k+1}}$

then, we have **Five Cases for checking error-constant**:


✓ Case 1:  $n > k$    $e_{ss} = 0$

✓ Case 2:  $n < k$    $e_{ss} = \infty$


---

✓ Case 3:  $n = k = 0$  (type 0)   $e_{ss} = \frac{1}{1 + K_p}$  Step error-constant

$R(s) = \frac{1}{s}$

✓ Case 4:  $n = k = 1$  (type 1)   $e_{ss} = \frac{1}{K_v}$  Ramp error-constant

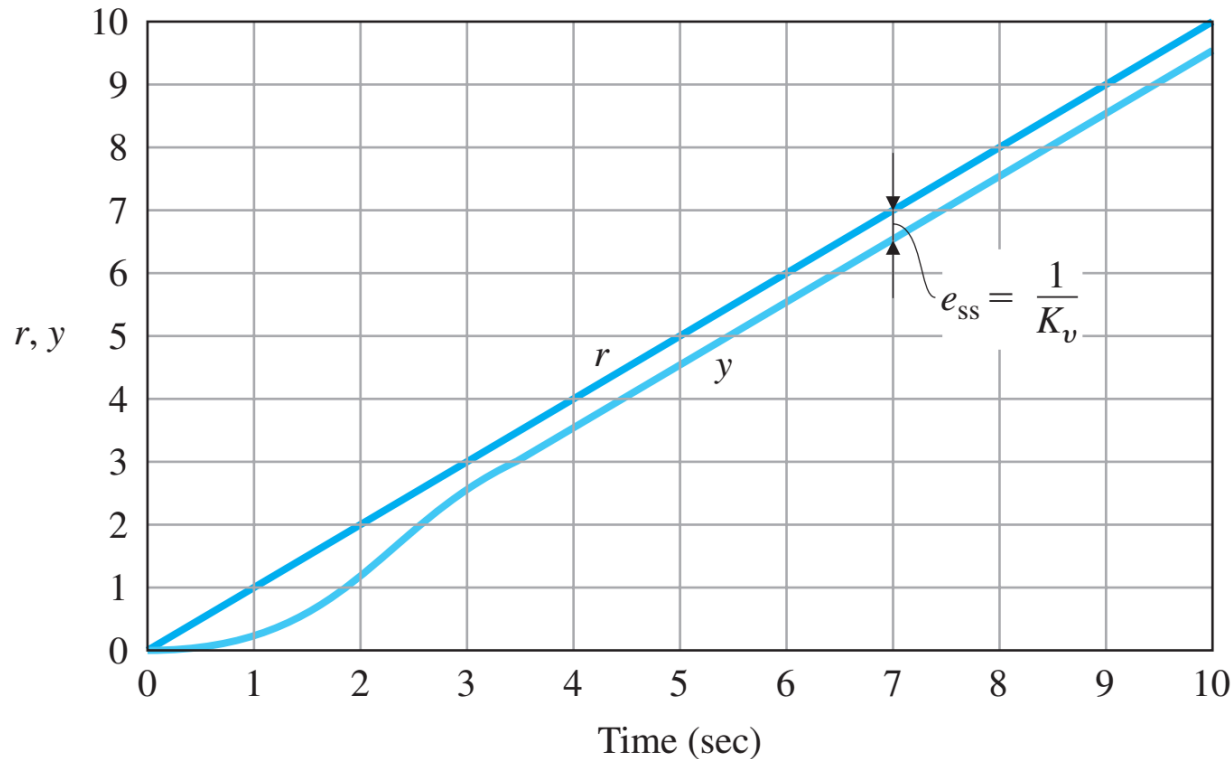
$R(s) = \frac{1}{s^2}$

✓ Case 5:  $n = k = 2$  (type 2)   $e_{ss} = \frac{1}{K_a}$  Parabola error-constant

$R(s) = \frac{1}{s^3}$

# System Type for Tracking (cont'd)

- Ramp response vs.  $K_v$  (ramp error-constant)



$$R(s) = \frac{1}{s^2}$$

- Important question:
  - What value of  $K_v$  is better to minimize steady-state error (SSE) ??

# System Type for Tracking

$$\lim_{t \rightarrow \infty} e(t) = e_{ss} = \lim_{s \rightarrow 0} sE(s),$$

$$= \lim_{s \rightarrow 0} s \frac{1}{1 + GD_{cl}} R(s),$$

## ■ Summary: Error-Constant

$$[\text{Step}]: \frac{1}{e_{ss}} = \cancel{1} + K_p = \lim_{s \rightarrow 0} \frac{1}{sE(s)} = \lim_{s \rightarrow 0} \frac{1 + GD_{cl}}{s} s = \cancel{1} + \lim_{s \rightarrow 0} GD_{cl}$$

$$[\text{Ramp}]: \frac{1}{e_{ss}} = K_v = \lim_{s \rightarrow 0} \frac{1}{sE(s)} = \lim_{s \rightarrow 0} \frac{1 + GD_{cl}}{s} s^2 = 0 + \lim_{s \rightarrow 0} sGD_{cl}$$

$$[\text{Parabola}]: \frac{1}{e_{ss}} = K_a = \lim_{s \rightarrow 0} \frac{1}{sE(s)} = \lim_{s \rightarrow 0} \frac{1 + GD_{cl}}{s} s^3 = 0 + \lim_{s \rightarrow 0} s^2 GD_{cl}$$

### Errors as a Function of System Type

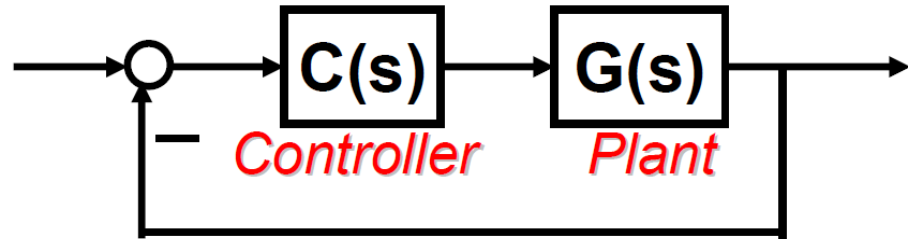
Type Input	Step (position)	Ramp (velocity)	Parabola (acceleration)
Type 0	$\frac{1}{1 + K_p}$	$\infty$	$\infty$
Type 1	0	$\frac{1}{K_v}$	$\infty$
Type 2	0	0	$\frac{1}{K_a}$



## 2. Lead-Lag Compensator Design

- Consider system,

$$G(s) = \frac{4}{s(s+2)}$$



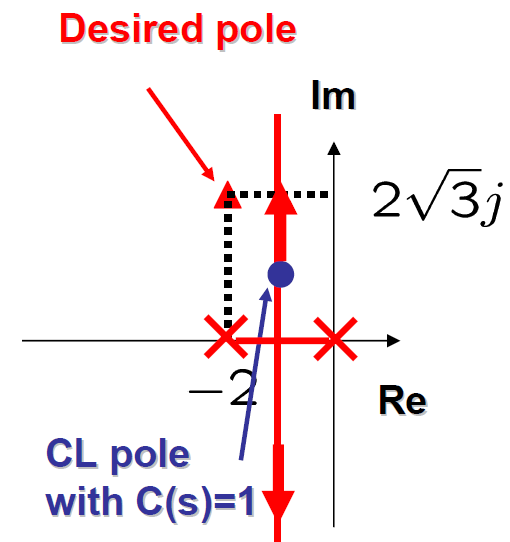
- Analysis of C-L system for  $C(s) = 1$   $H(s)_{CL} = \frac{CG}{1 + CG} = \frac{4}{s^2 + 2s + 4}$

- Damping ratio:  $\zeta = 0.5$  (the same !!)
- (Undamped) Natural frequency:  $\omega_n = 2$  [rad/s] !!
- Ramp-error constant:  $K_v = 2 \rightarrow$  too small !!

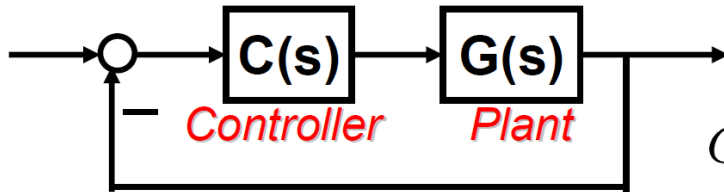
$$K_v = \lim_{s \rightarrow 0} sC(s)G(s) = s \frac{4}{s(s+2)} = 2$$

- Performance Requirement Specification

- Damping ratio:  $\zeta = 0.5$  (the same !!)
- (Undamped) natural frequency:  $\omega_n = 4$  [rad/s] !!
- Ramp-error constant:  $K_v = 50$  !! (Target !!)



# Error Constants (after **Lead Compensator** only)



$$G(s)C_{Lead}(s) = \frac{4}{s(s+2)} \cdot \frac{4.675(s+2.9)}{s+5.4}$$

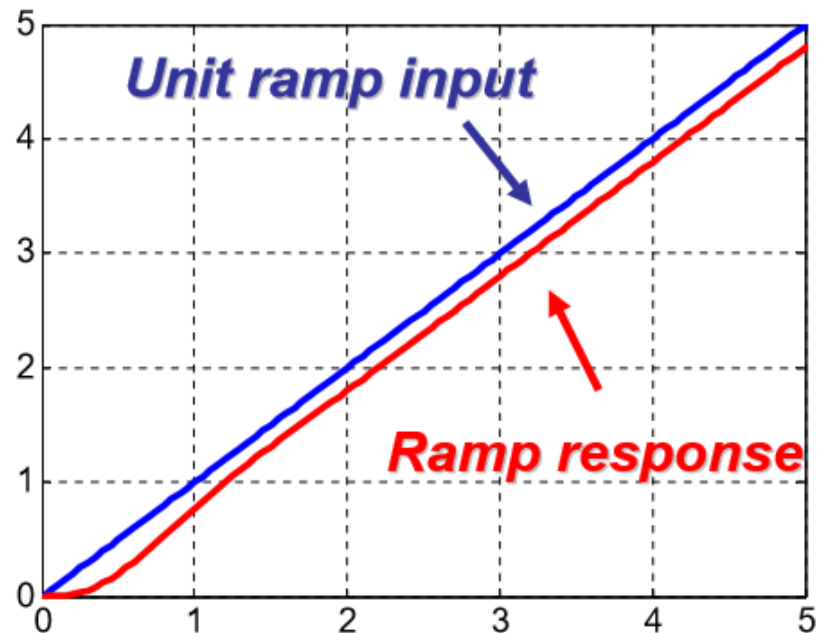
- Step-error constant

$$K_p = \lim_{s \rightarrow 0} G(s)C_{Lead}(s) = \infty$$

- Ramp-error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)C_{Lead}(s) = 5.02$$

Not satisfied !!  
( $K_v > 50$ )



- Lag compensator can reduce steady-state error (SSE).

# How to Design Lag Compensator

- Lag compensator  $C_{Lag}(s) = \frac{s + z}{s + p}$

- Objectives: increasing ramp-error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)C_{Lead}(s)C_{Lag}(s) = 5.02 \cdot \frac{z}{p} > 50$$

➡ Take, for example,  $z = 10p$

- We do NOT want to change CL pole location  $s_1$  so much. (because we already had satisfactory transient !!)

$$\left. \begin{array}{l} 1 + G(s_1)C_{Lead}(s_1) = 0 \\ C_{Lag}(s_1) \approx 1 \end{array} \right\} \Rightarrow 1 + G(s_1)C_{Lead}(s_1)C_{Lag}(s_1) \approx 0$$

# Guidelines to choose z and p (**Lag comp.**)

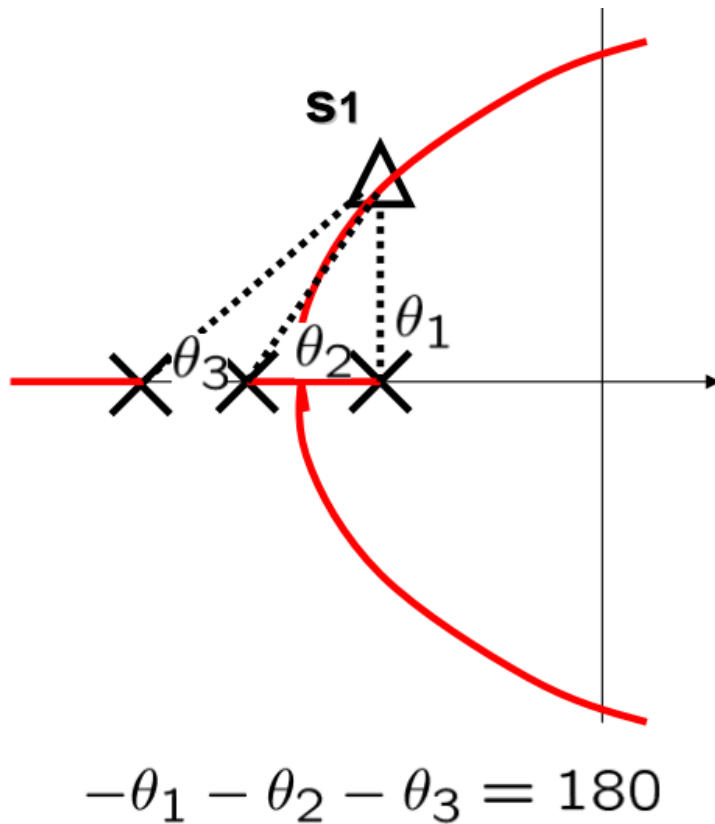
- The zero and the pole of a **lag compensator** should be **close to each other**, for

$$C_{Lag}(s_1) \approx 1$$

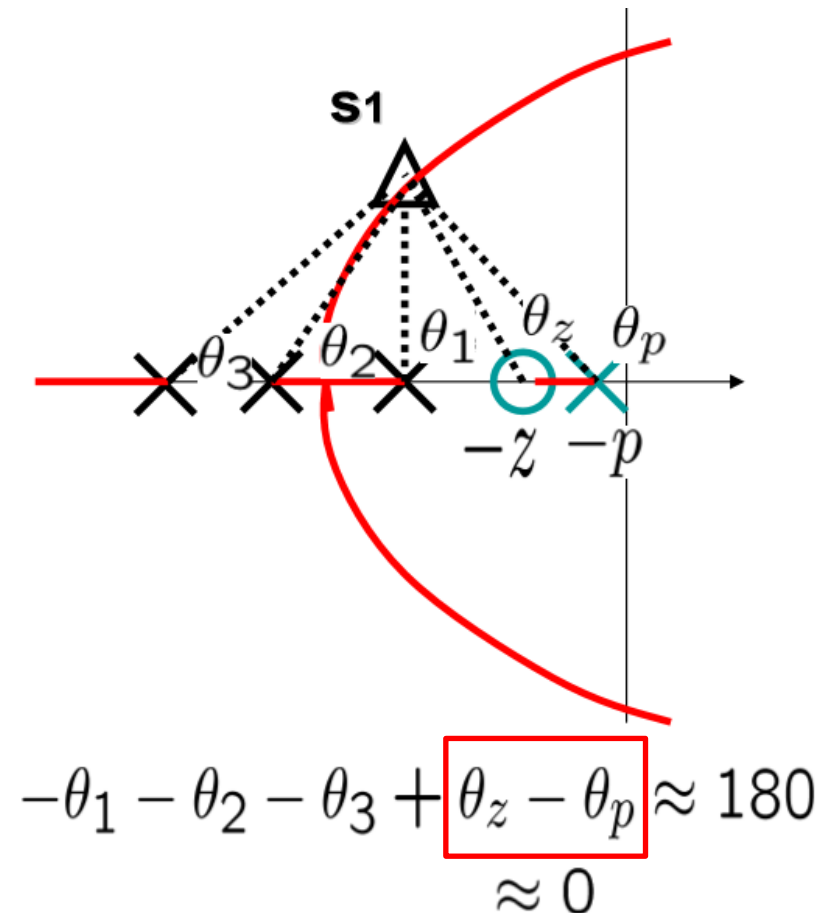
- The pole of a **lag compensator** should be **close to the origin**, to have a **large ratio z/p**, leading to a large ramp-error constant  $K_v$
- **However**, the pole of a lag compensator **too close to the origin may be problematic**:
  - **Slow settling** (due to closed-loop pole near the origin)

# Root Locus with Lag Compensator

- Without compensator



- With compensator (Lag Compensator)



# How to Design Lag Compensator (cont'd)

- For the desired CL pole:  $s_1 = -2 + 2\sqrt{3}j$

$$C_{Lag}(s_1) \approx 1 \iff \left| \frac{s_1 + 10p}{s_1 + p} \right| \approx 1 \quad \& \quad \angle \left( \frac{s_1 + 10p}{s_1 + p} \right) \approx 0$$

- Take a small pole (by trial-and-error !!)

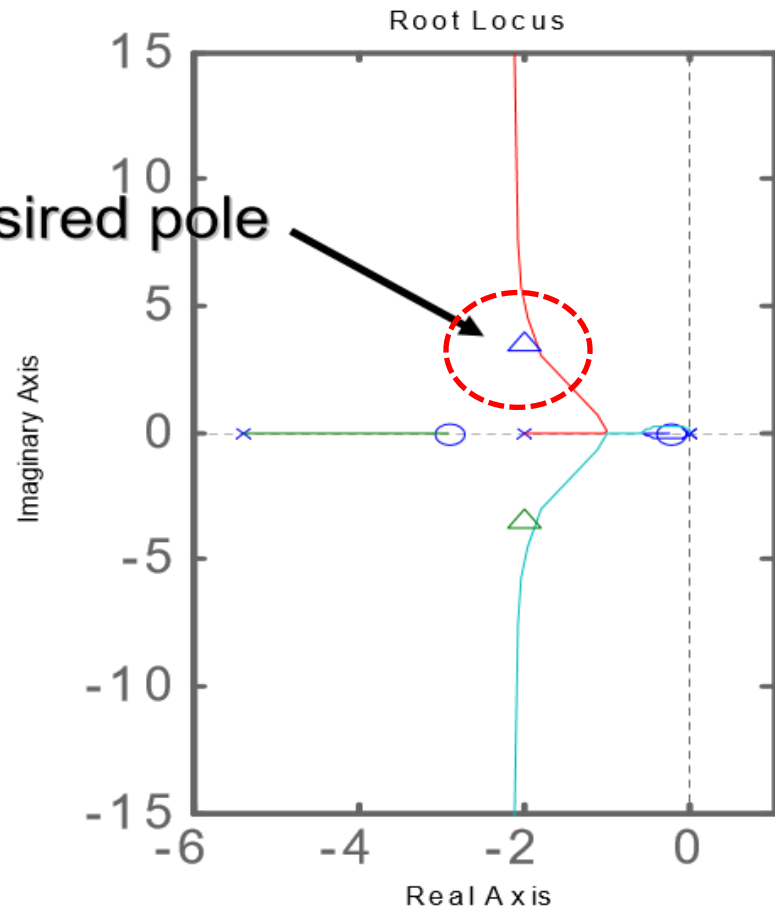
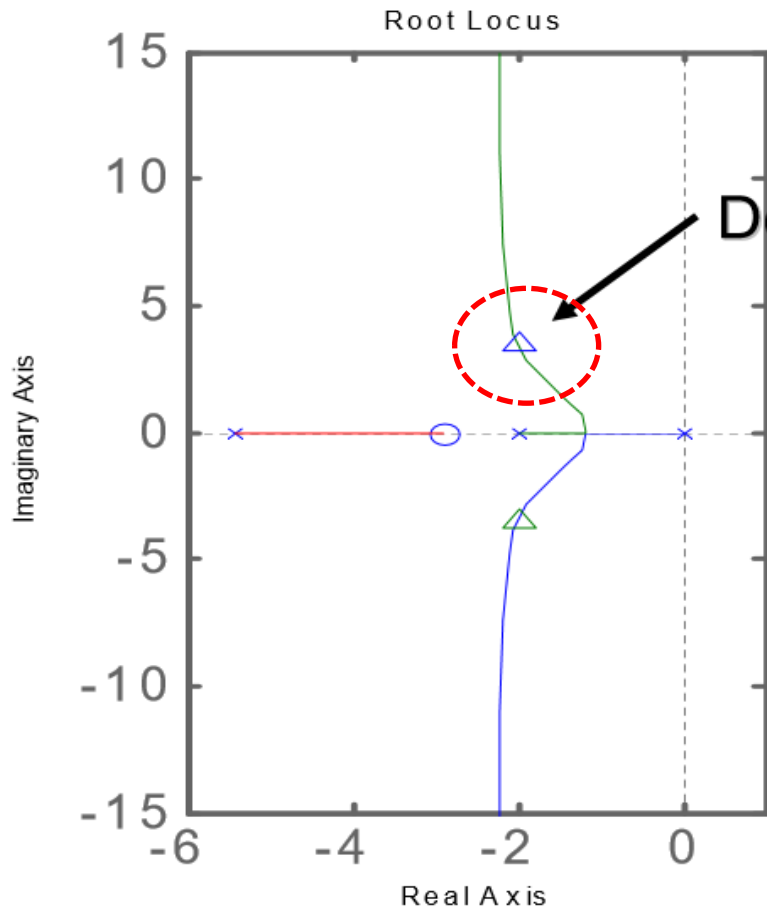
$$p = 0.025 \implies \left| \frac{s_1 + 10p}{s_1 + p} \right| = 0.97 \quad \angle \left( \frac{s_1 + 10p}{s_1 + p} \right) \approx -2.88^\circ$$

- Lead-Lag Controller

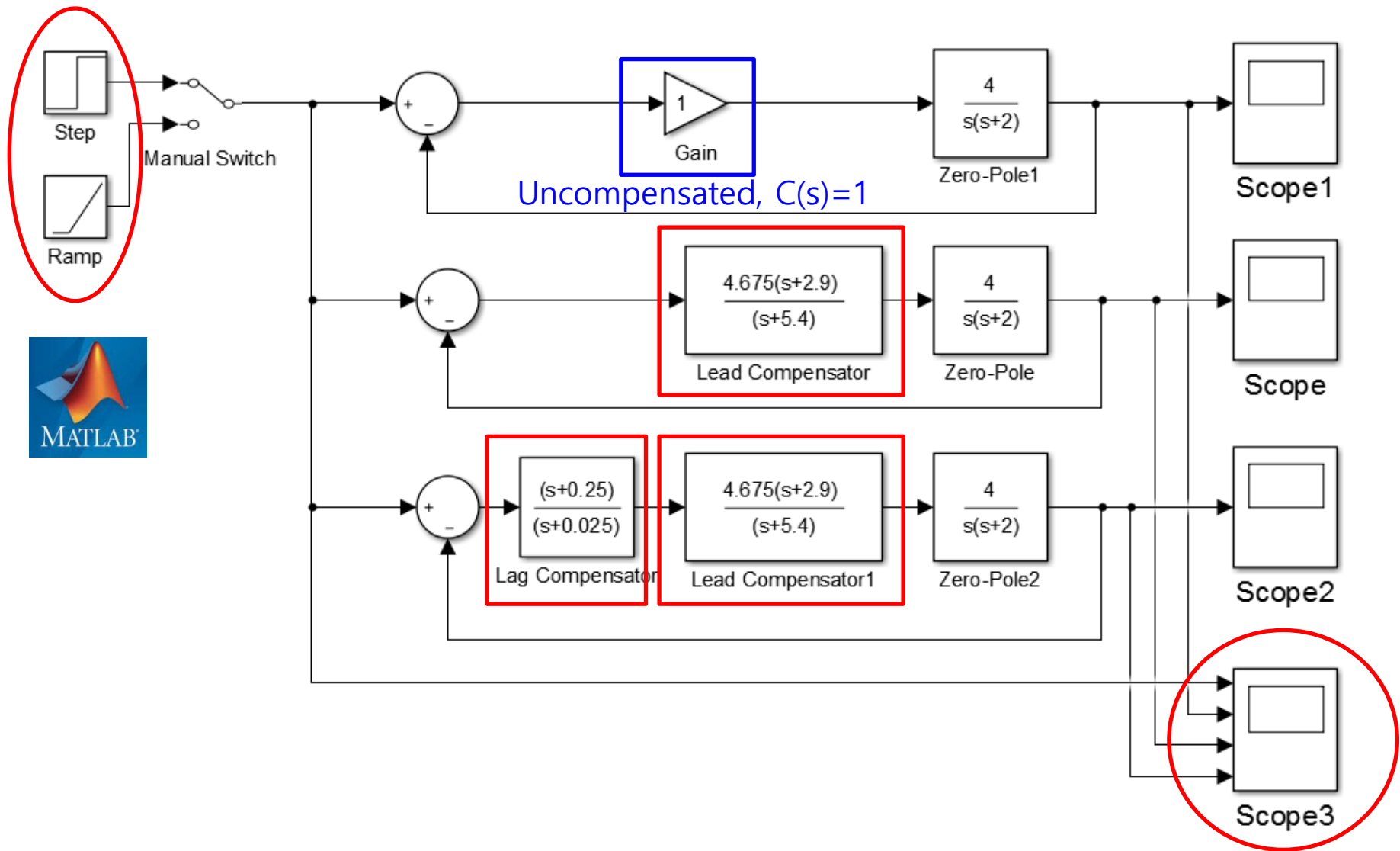
$$C_{LL}(s) = 4.675 \frac{s + 2.9}{s + 5.4} \cdot \frac{s + 0.25}{s + 0.025}$$

# Root Locus Comparison with Compensators

- With **lead** compensator
- With **lead-lag** compensator

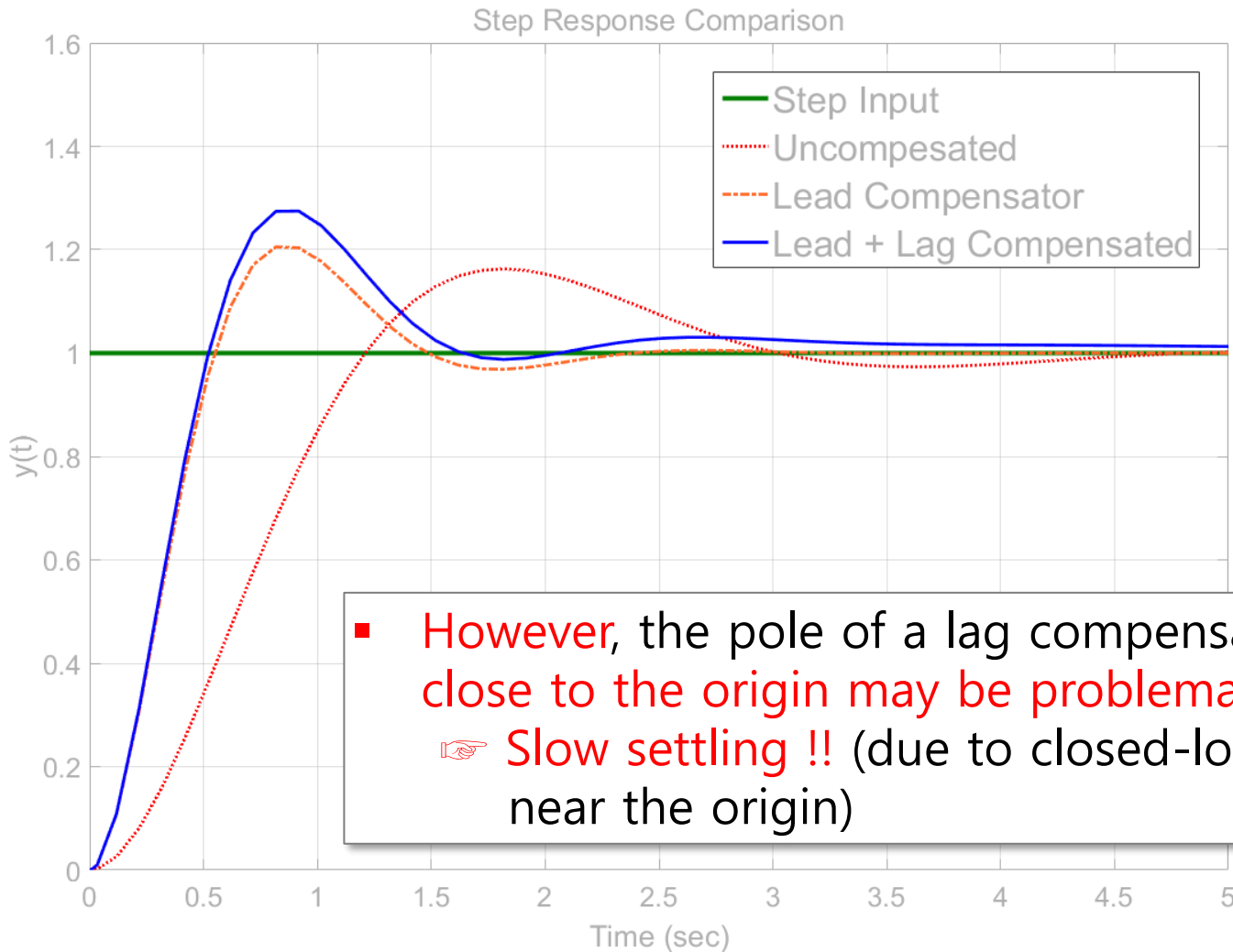


# Comparison: Step vs. Ramp Response

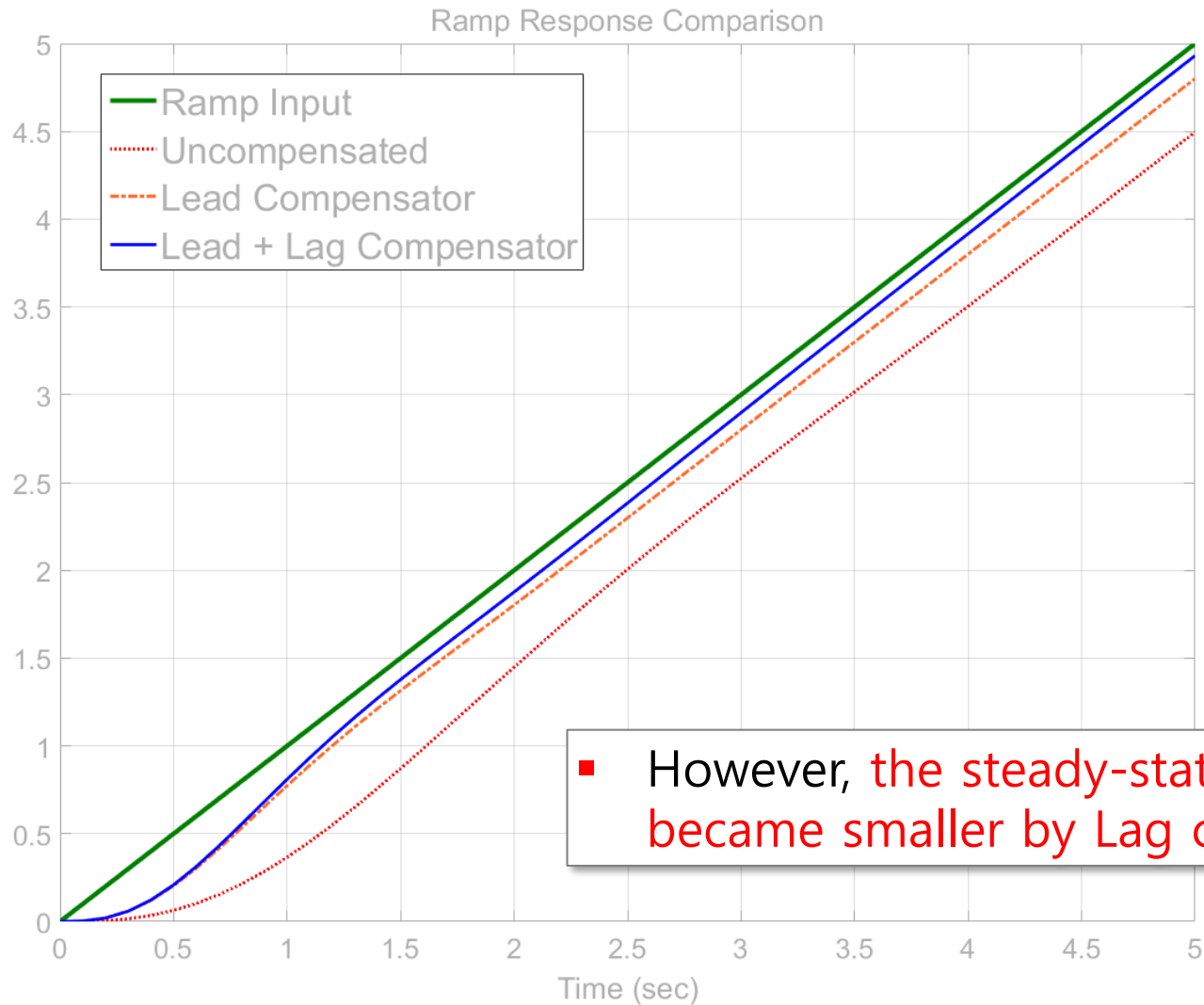




# Comparison (1): Step Response



# Comparison (2): Ramp Response



- However, the steady-state error (SSE) became smaller by Lag compensator !!

# Summary

## ❖ Summary:

- Controller design based on root locus.
  - **Lead compensator** improve stability and transient response.
  - **Lag compensator** improves steady-state error.
    - ⌘ Important: checking **error-constant** (or **system type**) !!
  - **Lead-Lag compensator** improves stability, transient and steady-state response at the same time.