#### Teoría de Control

### Root Locus design

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- Steady state performance exactitud tracking error step, ramp
  - Steady state error:

$$e = \lim_{t \to \infty} \left| \frac{r(t) - y_{ss}(t)}{a} \right|$$

- Position error: step input *r(s)=a*
- Velocity error: ramp input *r*(*s*)=*at*
- Dada

$$G_o(s) = \frac{\alpha_0 + \alpha_1 s + \dots + \alpha_n s^n}{\beta_0 + \beta_1 s + \dots + \beta_m s^m} \qquad n \ge m$$

Position error: step input r(s)=a

$$e_p = |1 - G_o(0)| = \left| \frac{\alpha_0 - \beta_0}{\alpha_0} \right|$$

Velocity error: ramp input r(s)=at

$$e_{v} = \left| \left( 1 - G_{o}(0) \right) t - \frac{d}{ds} G_{o}(s) \right|_{s=0}$$

$$e_{v} = \left| \left( \frac{\alpha_{0} - \beta_{0}}{\alpha_{0}} \right) t - \frac{\alpha_{0} \beta_{1} - \beta_{0} \alpha_{1}}{\alpha_{0}^{2}} \right|$$

• The plant output y(t) is said to track asymptotically the reference input r(t) if

$$\lim_{t \to \infty} \left| r(t) - y(t) \right| = 0$$

• step input r(s)=a

$$\alpha_0 = \beta_0$$

• ramp input *r(s)=at* 

$$\alpha_0 = \beta_0$$

$$\alpha_1 = \beta_1$$

• parable input  $r(s)=at^2$ 

$$\alpha_0 = \beta_0$$

$$\alpha_1 = \beta_1$$

$$\alpha_2 = \beta_2$$

- System type: number of poles at the origen
- Loop transfer function  $G_l(s)$

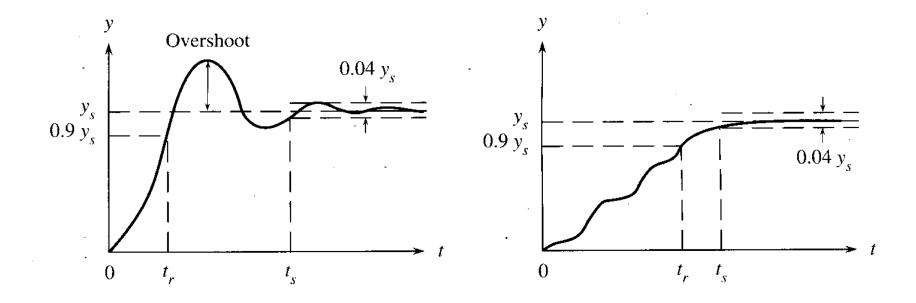
| Tipo\e <sub>ss</sub> | $e_p$ | $e_v$ | e <sub>a</sub> |
|----------------------|-------|-------|----------------|
| 0                    | K     | ∞     | ∞              |
| 1                    | 0     | K     | ∞              |
| 2                    | 0     | 0     | K              |

- Well-posedness:
- All transfer function in the system must be proper and

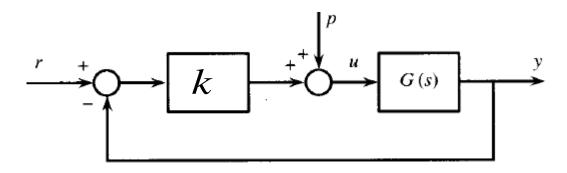
$$\Delta(\infty) = 1 + C(\infty)G(\infty) \neq 0$$

- Total stability
- Poles of  $G_o(s)$  and its missing poles are all stable
- Avoid unstable pole-zero cancellations

• Transient state – speed of response – step response



Find the closed-loop pole location for any k in



Closed-loop transfer function

$$G_o(s) = \frac{kG(s)}{1 + kG(s)}$$

Closed-loop poles:

$$1 + kG(s) = 0$$

Then: 
$$|G(s)| = \left| -\frac{1}{k} \right|$$

$$\hat{G}(s) = -\frac{1}{k}$$

$$\hat{G}(s) = \arg\left( -\frac{1}{k} \right) = \pm 180^{\circ}$$

- In general
- The roots of the characteristic equation as a function of  $k_x$

$$p(s) + k_{x}q(s) = 0$$

Then: 
$$|G_{pq}(s)| = \frac{q(s)}{p(s)} = -\frac{1}{k_x}$$
 
$$|G_{pq}(s)| = \left| -\frac{1}{k_x} \right|$$
 
$$\hat{G}_{pq}(s) = \arg\left( -\frac{1}{k_x} \right) = \pm 180^{\circ}$$

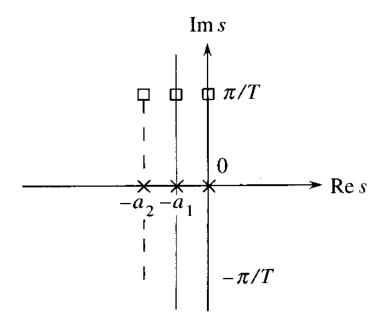
- Procedure:
  - Find the design region
  - Plot the roots of the characteristic equation as a function of k

$$p(s) + kq(s) = 0$$

- The region is defined by the time domain criteria (step signal response):
  - *t<sub>s</sub>* settling time
  - Overshoot
  - $t_r$  rise time

• *t<sub>s</sub>* settling time





Given

$$G_o(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

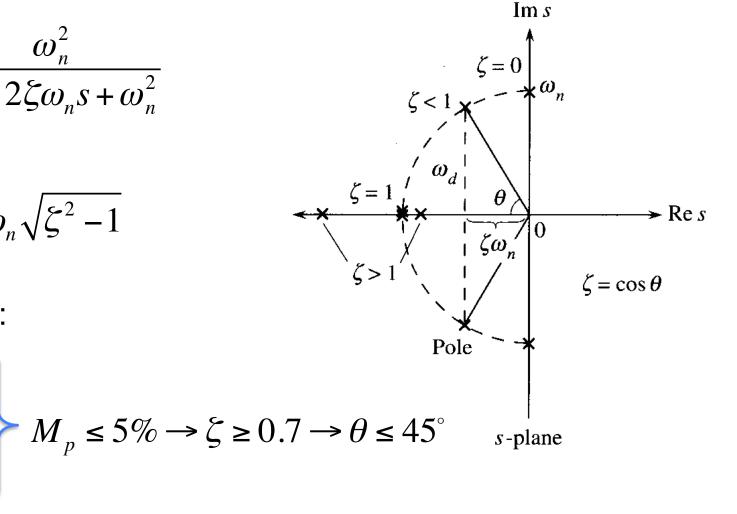
Its poles are

$$-\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

Also we have:

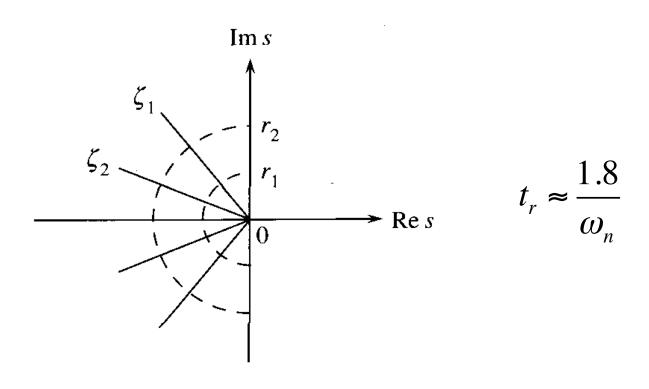
$$M_p = e^{\frac{-\pi \xi}{\sqrt{1-\xi^2}}}$$

$$\xi = \cos \theta$$

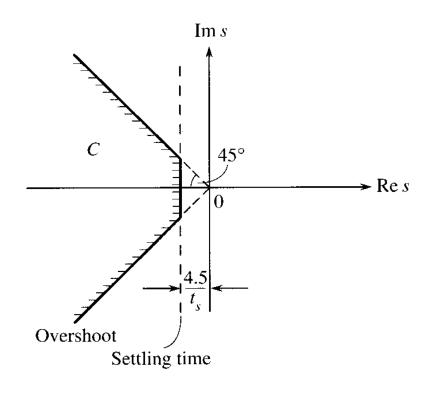


• Rise time  $t_r$ 

The farther away the closest pole from the origin, the smaller the rise time ?



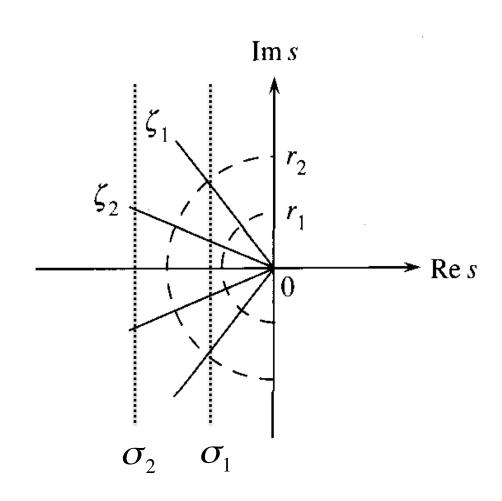
Desired pole region



$$\zeta < \zeta_c$$

Desired pole region

$$\zeta < \zeta_o 
t_s < t_{so} 
\omega_n < \omega_o$$



• Ejemplo: 
$$G(s) = \frac{1}{s(s+2)}$$

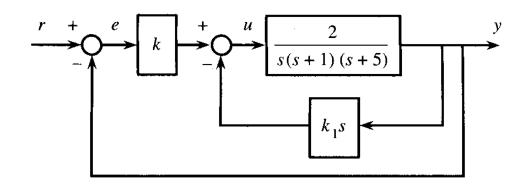
- Position error  $e_p = 0$
- Overshoot Mp<5%</li>
- Settling time  $t_s \leq 9$  s
- Rise time as small as possible

• Ejemplo: 
$$G(s) = \frac{1}{(s+1)}$$

- Position error  $e_p = 0$
- Overshoot Mp<5%</li>
- Settling time  $t_s \leq 2$  s
- Rise time as small as possible

• Ejemplo: 
$$G(s) = \frac{2}{s(s+1)(s+5)}$$

- Position error  $e_p = 0$
- Overshoot Mp<5%</li>
- Settling time  $t_s \leq 5$  s



Rise time as small as possible