它们都沿z轴方向传播。 (1) 求合成波,证明波的振幅不是常数,而是一个波。 (2) 求合成波的相位传播速度和振幅传播速度。

1.考虑两列振幅相同的、偏振方向相同、频率分别为 $\omega + d\varpi$ 和 $\omega - d\omega$ 的线偏振平面波,

 $\vec{E}_1(\vec{x},t) = \vec{E}_0(\vec{x})\cos(k_1x - \omega_1t)$ 

解: 
$$\vec{E}_2(\vec{x},t) = \vec{E}_0(\vec{x})\cos(k_2 x - \omega_2 t)$$

$$E_{2}(x,t) = E_{0}(x)\cos(k_{2}x - \omega_{2}t)$$

$$\vec{E} = \vec{E}_{1}(\vec{x},t) + \vec{E}_{2}(\vec{x},t) = \vec{E}_{0}(\vec{x})[\cos(k_{1}x - \omega_{1}t) + \cos(k_{2}x - \omega_{2}t)]$$

$$E = E_1(\vec{x}, t) + E_2(\vec{x}, t) = E_0(\vec{x})[\cos \theta]$$

$$2\vec{E}(\vec{z}) = (k_1 + k_2) \omega_1 + \omega_2$$

$$=2\vec{E}_{0}(\vec{x})\cos(\frac{k_{1}+k_{2}}{2}x-\frac{\omega_{1}+\omega_{2}}{2}t)\cos(\frac{k_{1}-k_{2}}{2}x-\frac{\omega_{1}-\omega_{2}}{2}t)$$

$$=2\vec{E}_{0}(\vec{x})\cos(\frac{\kappa_{1}+\kappa_{2}}{2}x-\frac{\omega_{1}+\omega_{2}}{2}t)$$

其中
$$k_1 = k + dk, k_2 = k - dk; \omega_1 = \omega + d\omega, \omega_2 = \omega - d\omega$$

$$\vec{E} = 2\vec{E}_0(\vec{x})\cos(kx - \omega t)\cos(dk \cdot x - d\omega \cdot t)$$

用复数表示 
$$\vec{E} = 2\vec{E}_0(\vec{x})\cos(dk \cdot x - d\omega \cdot t)e^{i(kx - \omega t)}$$

相速 
$$kx - \omega t = 0$$
  

$$\therefore v_p = \frac{\omega}{k}$$

群速 
$$dk \cdot x - d\omega$$
 ·  $v_g = \frac{d\omega}{dk}$ 

$$\therefore v_g = \frac{d\omega}{dk}$$

$$\therefore v_g = \frac{dd}{dk}$$

电磁波以
$$heta=45^{
m o}$$
  
折射系数。

2. 一平面电磁波以 $\theta = 45^{\circ}$  从真空入射到 $\varepsilon_r = 2$  的介质, 电场强度垂直于入射面, 求反射 系数和折射系数。 解:  $\vec{n}$  为界面法向单位矢量,  $\langle S \rangle$ ,  $\langle S' \rangle$ ,  $\langle S'' \rangle$  分别为入射波, 反射波和折射波的玻印

系数和折射系数。  
解: 
$$\vec{n}$$
 为界面法向单位矢量, $< S >, < S' >, < S'' >$  分别为 $/$  亭矢量的周期平均值,则反射系数 R 和折射系数 T 定义为:

 $R = \left| \frac{\langle S' \rangle \cdot \vec{n}}{\langle S \rangle \cdot \vec{n}} \right| = \frac{E_0^{'2}}{E_0^2}$  $T = \left| \frac{\langle S'' \rangle \cdot \vec{n}}{\langle S \rangle \cdot \vec{n}} \right| = \frac{n_2 \cos \theta_2 E''^2}{n_1 \cos \theta E_0^2}$ 

又根据电场强度垂直于入射面的菲涅耳公式,可得:

是根据电场强度垂直于入射面的菲涅耳公式,可得:
$$R = \left(\frac{\sqrt{\varepsilon_1}\cos\theta - \sqrt{\varepsilon_2}\cos\theta_2}{\sqrt{\varepsilon_1}\cos\theta + \sqrt{\varepsilon_2}\cos\theta_2}\right)^2$$

$$\left(\frac{g_2}{g_2}\right)^2$$

$$T = \frac{4\sqrt{\varepsilon_1}\sqrt{\varepsilon_2}\cos\theta\cos\theta_2}{(\sqrt{\varepsilon_1}\cos\theta + \sqrt{\varepsilon_2}\cos\theta_2)^2}$$
又根据反射定律和折射定律
$$\theta = \theta_1 = 45^{\circ}$$

 $\sqrt{\varepsilon_2} \sin \theta_2 = \sqrt{\varepsilon_1} \sin \theta$  $\varepsilon_1 = \varepsilon_0, \varepsilon_2 = \varepsilon_0 \varepsilon_r = 2\varepsilon_0$ 由题意,

$$\therefore \theta_2 = 30^{\circ}$$

$$\therefore R = (\frac{\frac{\sqrt{2}}{2} - \sqrt{2} \frac{\sqrt{3}}{2}}{\frac{\sqrt{2}}{2} + \sqrt{2} \frac{\sqrt{3}}{2}})^2 = \frac{2 - \sqrt{3}}{2 + \sqrt{3}}$$

$$\therefore R = (\frac{2}{\frac{\sqrt{2}}{2}})$$

$$T = \frac{4\varepsilon_0\sqrt{2}\frac{\sqrt{2}}{2}\frac{\sqrt{3}}{2}}{(\sqrt{\varepsilon_0}\frac{\sqrt{2}}{2} + \sqrt{\varepsilon_0}\sqrt{2}\frac{\sqrt{3}}{2})^2} = \frac{2\sqrt{3}}{2 + \sqrt{3}}$$
3. 有一可见平面光波由水入射到空气,入射角为 60°。证明这时将会发生全反射,并求 折射 波沿 表面 传播 的 相速 度 和 透入 空气的 深度。 设 该 波 在 空气中的 波 长 为

 $\lambda_0 = 6.28 \times 10^{-5}$  cm, 水的折射率为 n=1.33。 解:由折射定律得,临界角 $\theta_c=\arcsin(\frac{1}{1.33})=48.75\,^\circ$ ,所以当平面光波以 $60\,^\circ$ 入射时, 将会发生全反射。

折射波:  $k'' = k \sin \theta$ 相速度  $v_p = \frac{\omega''}{k''} = \frac{\omega}{k/c} = \frac{\sqrt{3}}{2}c$ 

投入空气的深度  $\kappa = \frac{\lambda_1}{2\pi\sqrt{\sin^2\theta - n_{21}^2}} = \frac{6.28 \times 10^{-5}}{2\pi\sqrt{\sin^260 - (\frac{1}{12.2})^2}} \approx 1.7 \times 10^{-5} \text{ cm}$ 

4. 频率为 $\omega$ 的电磁波在各向同性介质中传播时,若ec E, ec D, ec B, ec H仍按 $e^{i(ec k\cdot ar z - \omega t)}$ 变化,但ec D不再与 $\vec{E}$ 平行(即 $\vec{D} = \varepsilon \vec{E}$ 不成立)。

(1) 证明
$$\vec{k} \cdot \vec{B} = \vec{k} \cdot \vec{D} = \vec{B} \cdot \vec{D} = \vec{B} \cdot \vec{E} = 0$$
,但一般 $\vec{k} \cdot \vec{E} \neq 0$ 

(2) 证明 
$$\vec{D} = \frac{1}{\omega^2 \mu} [k^2 \vec{E} - (\vec{k} \cdot \vec{E}) \vec{k}]$$

(3) 证明能流 $\bar{S}$ 与波矢 $\bar{k}$ 一般不在同方向上。

 $\nabla \cdot \vec{B} = \vec{B}_0 \cdot \nabla e^{i(\vec{k} \cdot \vec{x} - \omega t)} = i\vec{k} \cdot \vec{B}_0 e^{i(\vec{k} \cdot \vec{x} - \omega t)} = i\vec{k} \cdot \vec{B} = 0$ 

证明: 1) 由麦氏方程组

$$\begin{cases} \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \\ \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} \\ \nabla \cdot \vec{D} = 0 \\ \nabla \cdot \vec{B} = 0 \end{cases}$$

得:

$$\therefore \vec{k} \cdot \vec{B} = 0$$

同理 
$$\vec{k} \cdot \vec{D} = 0$$

问连 
$$k \cdot D = 0$$

$$\nabla \times \vec{H} = [\nabla e^{i(\vec{k} \cdot \vec{x} - \omega t)}] \times \vec{H}_0 = i\vec{k} \times \vec{H} = -i\omega \vec{D}$$

$$\therefore i\vec{k} \times \vec{B} = -i\mu\omega\vec{D}$$

$$\therefore \vec{B} \cdot \vec{D} = -\frac{1}{u\omega} \vec{B} \cdot (\vec{k} \times \vec{B}) = 0$$

$$\nabla \times \vec{E} = [\nabla e^{i(\vec{k} \cdot \vec{x} - \omega t)}] \times \vec{E}_0 = i\vec{k} \times \vec{E} = i\omega \vec{B}$$

$$\vec{B} \cdot \vec{E} = \frac{1}{\omega} (\vec{k} \times \vec{E}) \cdot \vec{E} = 0 , \quad \nabla \cdot \vec{E} = i\vec{k} \cdot \vec{E}$$

另由 $\nabla \times \vec{H} = \frac{\partial \bar{D}}{\partial t}$  得:  $\vec{D} = -\frac{1}{u\omega}(\vec{k} \times \vec{B})$ 

 $\therefore \vec{D} = -\frac{1}{\mu \omega^2} [\vec{k} \times (\vec{k} \times \vec{E})] = \frac{1}{\mu \omega^2} [(\vec{k} \times \vec{E}) \times \vec{k}] = \frac{1}{\mu \omega^2} [k^2 \vec{E} - (\vec{k} \cdot \vec{E}) \vec{k}]$ 

$$\therefore \vec{k} \cdot \vec{E} - \Re \neq 0 \quad \therefore \vec{S} - \Re \neq \frac{1}{\mu \omega} E^2 \vec{k}$$
,即 $\vec{S}$  一般不与 $\vec{k}$  同向

5. 有两个频率和振幅都相等的单色平面波沿 z 轴传播,一个波沿 x 方向偏振,另一个沿 y 方向偏振,但相位比前者超前 $\frac{\pi}{2}$ ,求合成波的偏振。

 $x^{2} + y^{2} = A_{0}^{2} [\cos^{2}(\omega t + \varphi_{0x}) + \cos^{2}(\omega t + \varphi_{0y})]$ 

 $= A_0^2 \left[\cos^2(\omega t + \varphi_{0x}) + \sin^2(\omega t + \varphi_{0x})\right]$ 

所以合成的振动是一个圆频率为 $\alpha$ 的沿z轴方向传播的右旋圆偏振。反之,一个圆偏

反之,一个圆偏振。  
:偏振方向在
$$x$$
轴上
$$x = A_0$$

 $\Delta \varphi = \varphi_{0y} - \varphi_{0x} = \frac{\pi}{2}$ 

合成得轨迹方程为:

 $=A_{0}^{2}$ 

即:  $x^2 + v^2 = A_0^2$ 

$$\Delta \varphi = \varphi_{0y}$$

$$y = A_0 \cos(\omega t - kz + \frac{\pi}{2}) = A_0 \cos(\omega t + \varphi_{0y})$$
$$\Delta \varphi = \varphi_{0y} - \varphi_{0y} = \frac{\pi}{2}$$

$$x = A_0 \cos(\omega t - kz) = A_0 \cos(\omega t + \varphi_{0x})$$
 在 y 轴上的波可记为:

$$\therefore \vec{S} = \vec{E} \times \vec{H} = \frac{1}{\mu \omega} \vec{E} \times (\vec{k} \times \vec{E}) = \frac{1}{\mu \omega} [E^2 \vec{k} - (\vec{k} \cdot \vec{E}) \vec{E}]$$

$$\bar{\hat{c}} imes (\bar{k}$$

3) 由 
$$\vec{B} = \frac{1}{\omega}(\vec{k} \times \vec{E})$$
 得  $\vec{H} = \frac{1}{\mu\omega}(\vec{k} \times \vec{E})$   

$$\therefore \vec{S} = \vec{E} \times \vec{H} = \frac{1}{\omega}(\vec{k} \times \vec{E}) = \frac{1}{\omega}[\vec{E}^2]$$

2) 由 $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$  得:  $\vec{B} = \frac{1}{\omega} (\vec{k} \times \vec{E})$ 

振可以分解为两个偏振方向垂直,同振幅,同频率,相位差为 $\pi/2$ 的线偏振的合成。 6. 平面电磁波垂直直射到金属表面上, 试证明透入金属内部的电磁波能量全部变为焦耳热。

证明:设在 z>0 的空间中是金属导体,电磁波由 z<0 的空间中垂直于导体表面入射。

所以金属导体单位面积那消耗的焦耳热的平均值为:

其平均值为 $|\vec{S}| = \frac{1}{2} \operatorname{Re}(\vec{E}^* \times \vec{H}) = \frac{\beta}{2\omega \mu} E_0^2$ 

 $\vec{S} = \vec{E} \times \vec{H}$ ,  $\vec{\mu} = \frac{1}{\omega u} \vec{k} \times \vec{E} = \frac{1}{\omega u} (\beta + i\alpha) \vec{n} \times \vec{E}$ 

于是,由 z=0 的表面,单位面积进入导体的能量为:

已知导体中电磁波的电场部分表达式是:

 $\vec{E} = \vec{E}_0 e^{-\alpha z} e^{i(\beta z - \omega t)}$ 

 $dQ = \frac{1}{2} \operatorname{Re}(\vec{J}^* \times \vec{E}) = \frac{1}{2} \sigma E_0^2 e^{-2\sigma z}$ 

作积分:  $Q = \frac{1}{2}\sigma E_0^2 \int_0^\infty e^{-2\sigma z} dz = \frac{\sigma}{4\sigma} E_0^2$  即得单位面积对应的导体中消耗的平均焦 耳热。  $\mathbb{X} :: \alpha \beta = \frac{\omega \mu \sigma}{2}$ 

在导体内部,:  $\vec{J} = \sigma \vec{E} = \sigma \vec{E}_0 e^{-\alpha z} e^{i(\beta z - \omega t)}$ 

 $\therefore Q = \frac{\sigma}{4\alpha} E_0^2 = \frac{\beta}{2\alpha\mu} E_0^2$ 原题得证.

7. 已知海水的  $\mu_r = 1$ ,  $\sigma = 1S \cdot m^{-1}$ , 试计算频率  $\nu$  为  $50,10^6$  和 $10^9$  Hz 的三种电磁波在海 水中的透入深度。

解: 取电磁波以垂直于海水表面的方式入射, 透射深度  $\delta = \frac{1}{\alpha} = \sqrt{\frac{2}{\alpha u \sigma}}$  $\therefore \mu_r = 1$ 

 $\therefore \mu = \mu_0 \mu_r = \mu_0 = 4\pi \times 10^{-7}$ 

∴ 1 >  $\nu = 50Hz$  時:  $\delta_1 = \sqrt{\frac{2}{\omega u \sigma}} = \sqrt{\frac{2}{2\pi \times 50 \times 4\pi \times 10^{-7} \times 1}} = 72m$ 

 $3 > v = 10^9 \, Hz$ 时: $\delta_3 = \sqrt{\frac{2}{\omega\mu\sigma}} = \sqrt{\frac{2}{2\pi \times 10^9 \times 4\pi \times 10^{-7} \times 1}} \approx 16mm$ 

 $2 > \nu = 10^6 Hz$ 时:  $\delta_2 = \sqrt{\frac{2}{\omega \mu \sigma}} = \sqrt{\frac{2}{2\pi \times 10^6 \times 4\pi \times 10^{-7} \times 1}} \approx 0.5m$ 

8. 平面电磁波由真空倾斜入射到导电介质表面上,入射角为
$$\theta_1$$
,求导电介质中电磁波的相速度和衰减长度。若导电介质为金属,结果如何?

提示: 导电介质中的波矢量  $\vec{k} = \vec{\beta} + i\vec{\alpha}, \vec{\alpha}$  只有 z 分量(为什么?)。 解: 根据题意,如图所示,入射平面是 xz 平面 导体中的电磁波表示为:  $\vec{E} = \vec{E}_0 e^{-\vec{\alpha}\cdot\vec{x}} e^{i(\vec{\beta}\cdot\vec{x}-\omega t)}$ 

导体中的电磁波表示为: 
$$\vec{E} = \vec{E}_0 e^{-\bar{\alpha} \cdot \bar{x}} e^{i(\bar{\beta} \cdot \bar{x} - \omega t)}$$
 
$$\bar{k}'' = \bar{\beta} + i\bar{\alpha}$$
 介质 与介质中的有关公式比较可得: 
$$\begin{cases} \beta^2 - \alpha^2 = \omega^2 \mu \varepsilon \\ \bar{\alpha} \cdot \bar{\beta} = \frac{1}{2} \omega \mu \sigma \end{cases}$$

$$\beta_x = \frac{\omega}{c} \sin \theta_1$$

$$\beta_x = \frac{\omega}{c} \sin \theta_1$$

而入射面是 xz 平面,故
$$\vec{k}$$
, $\vec{k}$ "无 y 分量。  $\therefore \alpha_y = 0, \beta_y = 0$   
 $\therefore \vec{\alpha}$  只有 $\alpha_z$ 存在, $\vec{\beta}$ 有 $\beta_x$ 与 $\beta_z$ ,其中 $\beta_x = \frac{\omega}{c} \sin \theta_1$   

$$\left[ (\frac{\omega}{c} \sin \theta_x)^2 + \beta^2 - \alpha^2 = \omega^2 U \mathcal{E} \right]$$

$$\therefore 有 \begin{cases} (\frac{\omega}{c}\sin\theta_1)^2 + \beta_z^2 - \alpha_z^2 = \omega^2 \mu \varepsilon \\ \alpha_z \beta_z = \frac{1}{2}\omega\mu\sigma \end{cases}$$
解得:
$$\beta_z^2 = \frac{1}{2}(\mu\varepsilon\omega^2 - \frac{\omega^2}{c^2}\sin^2\theta_1) + \frac{1}{2}[(\frac{\omega^2}{c^2}\sin^2\theta_1 - \omega^2\mu\varepsilon)^2 + \omega^2\mu^2\sigma^2]^{\frac{1}{2}}$$

$$\rho_{z} = \frac{1}{2}(\mu\varepsilon\omega^{2} - \frac{\omega^{2}}{c^{2}}\sin^{2}\theta_{1}) + \frac{1}{2}[(\frac{\omega^{2}}{c^{2}}\sin^{2}\theta_{1} - \frac{\omega^{2}}{c^{2}}\sin^{2}\theta_{1}) + \frac{1}{2}[(\omega^{2}\mu\varepsilon - \frac{\omega^{2}}{c^{2}}\sin^{2}\theta_{1})^{2} + \omega^{2}\mu^{2}\sigma^{2}]^{\frac{1}{2}}$$

其相速度为:  $v = \frac{\omega}{\beta}$ , 衰减深度为  $\frac{1}{\alpha}$ 

如果是良导体,则: 
$$\begin{cases} \frac{\omega^2}{c^2} \sin^2 \theta_1 + \beta_z^2 - \alpha_z^2 = 0 \\ \alpha_z \beta_z = \frac{1}{2} \omega \mu \sigma \end{cases}$$

$$\therefore \beta_z^2 = -\frac{\omega^2}{2c^2} \sin 2\theta_1 + \frac{1}{2} \left[ \frac{\omega^4}{c^4} \sin 2\theta$$

$$\therefore \beta_z^2 = -\frac{\omega^2}{2c^2} \sin 2\theta_1 + \frac{1}{2} \left[ \frac{\omega^4}{c^4} \sin^4 \theta_1 + \omega^2 \mu^2 \sigma^2 \right]^{\frac{1}{2}}$$

$$\alpha^2 = \frac{\omega^2}{2c^2} \sin^2 \theta_1 + \frac{1}{2} \left[ \frac{\omega^4}{c^4} \sin^4 \theta_1 + \omega^2 \mu^2 \sigma^2 \right]^{\frac{1}{2}}$$

 $z = -\infty$  到 z = 0 这段管内可能存在的波模。

方程的通解为:

根据边界条件有:

 $\begin{cases} k = \kappa & E = 0 \\ k = \omega \sqrt{\mu_0 \varepsilon_0} \end{cases}$ 

$$\therefore \beta_z^2 = -\frac{\omega^2}{2c^2} \sin 2\theta_1 + \frac{1}{2} \left[ \frac{\omega^4}{c^4} \sin^4 \theta_1 + \omega^2 \mu^2 \sigma^2 \right]$$
$$\alpha_z^2 = \frac{\omega^2}{2c^2} \sin^2 \theta_1 + \frac{1}{2} \left[ \frac{\omega^4}{c^2} \sin^4 \theta_1 + \omega^2 \mu^2 \sigma^2 \right]^{\frac{1}{2}}$$

9. 无限长的矩形波导管, 在在 z=0 处被一块垂直地插入地理想导体平板完全封闭, 求在

解: 在此中结构得波导管中, 电磁波的传播依旧满足亥姆霍兹方程

 $E(x, y, z) = (C_1 \sin k_x x + D_1 \cos k_x x) \cdot (C_2 \sin k_y y + D_2 \cos k_y y) \cdot (C_3 \sin k_z z + D_3 \cos k_z z)$  $E_y = E_z = 0, (x = 0, a),$   $E_x = E_z = 0, (y = 0, b)$ 

 $\frac{\partial E_x}{\partial x} = 0, (x = 0, a), \quad \frac{\partial E_y}{\partial y} = 0, (y = 0, b), \quad \frac{\partial E_z}{\partial z} = 0, (z = 0)$ 

故:  $\begin{cases} E_x = A_1 \cos k_x x \sin k_y y \sin k_z z \\ E_y = A_2 \sin k_x x \cos k_y y \sin k_z z \\ E_z = A_3 \sin k_x x \sin k_y y \cos k_z z \end{cases}$ 其中,  $k_x = \frac{m\pi}{a}, m = 0,1,2\cdots$ 

 $k_{y} = \frac{n\pi}{h}, n = 0,1,2\cdots$  $k_{x}^{2}+k_{y}^{2}+k_{z}^{2}=k^{2}=\omega^{2}\varepsilon_{0}\mu_{0}=\frac{\omega^{2}}{c^{2}} \perp A_{1}\frac{m\pi}{a}+A_{2}\frac{n\pi}{b}+A_{3}k_{z}=0$  综上, 即得此种波导管种所有可能电磁波的解。

$$\nabla \times \vec{E} = i\omega \mu_0 \vec{H}$$
及 $\nabla \times \vec{H} = -i\omega \varepsilon_0 \vec{E}$  证明电磁场所有分量都可用  $E_x(x,y)$ 和 $H_z(x,y)$ 这两个分量表示。

10. 电磁波  $\vec{E}(x,y,z,t) = \vec{E}(x,y)e^{i(k_2z-\omega t)}$  在波导管中沿 z 方向传播, 试使用

证明:沿 z 轴传播的电磁波其电场和磁场可写作:

$$\vec{E}(x,y,z,t) = \vec{E}(x,y)e^{i(k_z z - \omega t)}, \quad \vec{H}(x,y,z,t) = \vec{H}(x,y)e^{i(k_z z - \omega t)}$$

由麦氏方程组得 
$$\nabla \times \vec{H} = \varepsilon_0 \frac{\partial \vec{E}}{\partial t} = -i\omega \varepsilon_0 \vec{E}$$

$$\nabla \times \bar{H} = \varepsilon_0 \frac{\partial E}{\partial t} = -i\omega \varepsilon_0.$$

$$\partial E$$
  $\partial E$   $\partial E$ 

写成分量式:  $\frac{\partial E_z}{\partial v} - \frac{\partial E_y}{\partial z} = \frac{\partial E_z}{\partial v} - ik_z E_y = i\omega \mu_0 H_x$ 

$$i$$
成分量式 :  $\frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = \frac{\partial E_z}{\partial y} - ik_z I$   $\partial E_x - \partial E_z = ik_z E$ 

 $\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = ik_z E_x - \frac{\partial E_z}{\partial x} = i\omega \mu_0 H_y$ 

$$\frac{\partial E_{y}}{\partial x} - \frac{\partial E_{x}}{\partial y} = i\omega \mu_{0} H_{z}$$

$$\frac{\partial x}{\partial y} - \frac{\partial H_z}{\partial z}$$

$$\frac{\int_{z}^{z}}{\partial z} - \frac{\partial H_{y}}{\partial z} = \frac{\partial H_{z}}{\partial y} - \frac{\partial H_{z}}{\partial y}$$

$$\frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = \frac{\partial H_z}{\partial y} - ik_z H_y = -i\omega \varepsilon_0 E_x$$

$$\frac{\partial^2 z}{\partial y} - \frac{\partial^2 z}{\partial z} = \frac{\partial^2 z}{\partial y} - ik$$

$$\frac{\partial^2 H_x}{\partial z} - \frac{\partial^2 H_z}{\partial z} = ik H_z - ik$$

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = ik_z H_x - \frac{\partial H_z}{\partial x}$$

$$\frac{H_x}{\partial z} - \frac{\partial H_z}{\partial x} = ik_z H_x - \frac{\partial H_z}{\partial x}$$

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = ik_z H_x - \frac{\partial H_z}{\partial x} = -i\omega \varepsilon_0 E_y$$

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = ik_z H_x - i\omega \varepsilon_0 E_z$$

$$\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = -i\omega \varepsilon_0 E_z$$

$$\frac{\partial H_z}{\partial x} = ik_z H_x - ik_z$$

由 (2) (3) 消去  $H_y$ 得  $E_x = \frac{1}{i(\frac{\omega^2}{2} - k_z^2)} (-\omega \mu_0 \frac{\partial H_z}{\partial y} - k_z \frac{\partial E_z}{\partial x})$ 

$$=ik_zH_x-\frac{6}{2}$$

$$E_{x} - \frac{\partial H_{z}}{\partial x} = -i\omega \varepsilon_{0} E_{y}$$

$$-\frac{\partial H_z}{\partial x} = -i\omega\varepsilon_0 E_y$$

$$\frac{\partial H_z}{\partial x} = -i\omega\varepsilon_0 E_y$$

(1)

(2)

(3)

由 (2) (3) 消去  $E_x$  得  $H_y = \frac{1}{i(\frac{\omega^2}{2} - k_z^2)} (-k_z \frac{\partial H_z}{\partial y} - \omega \varepsilon_0 \frac{\partial E_z}{\partial x})$ 11. 写出矩形波导管内磁场 $\vec{H}$ 满足的方程及边界条件。 解:对于定态波,磁场为 $\bar{H}(\bar{x},t)=\bar{H}(\bar{x})e^{-i\omega t}$ 

 $\therefore\begin{cases} (\nabla^2 + k^2) \vec{H} = 0, k^2 = \omega^2 \varepsilon \mu \\ \nabla_+ \vec{H} = 0 \end{cases}$  即为矩形波导管内磁场  $\vec{H}$  满足的方程。

由 (1) (4) 消去  $H_x$ 得  $E_y = \frac{1}{i(\frac{\omega^2}{2} - k_z^2)} (\omega \mu_0 \frac{\partial H_z}{\partial x} - k_z \frac{\partial E_z}{\partial y})$ 

由 (1) (4) 消去  $E_y$ 得  $H_x = \frac{1}{i(\frac{\omega^2}{2} - k_z^2)} (-k_z \frac{\partial H_z}{\partial x} + \omega \varepsilon_0 \frac{\partial E_z}{\partial y})$ 

由麦氏方程组 
$$\begin{cases} \nabla \times \vec{H} = \frac{\partial D}{\partial t} = -i\omega \varepsilon \vec{E} \\ \nabla \cdot \vec{H} = 0 \end{cases}$$

$$7 \times (\nabla$$

 $\nabla \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = i\omega \mu \vec{H}$ 

 $\therefore -i\omega\varepsilon\nabla\times\vec{E} = \omega^2\mu\varepsilon\vec{H} = -\nabla^2\vec{H}$ 

由 $\vec{n} \cdot \vec{B} = 0$ 得  $\vec{n} \cdot \vec{H} = 0$ ,  $H_n = 0$ 

利用 $\nabla \times \vec{E} = i\omega \mu \vec{H}$  和电场的边界条件可得:  $\frac{\partial H_t}{\partial u} = 0$ 















12. 论证矩形波导管内不存在 TM<sub>m0</sub>或 TM<sub>0n</sub>波。 证明:已求得波导管中的电场 $\vec{E}$ 满足:

$$\begin{cases} E_x = A_1 \cos k_x x \sin k_y y e^{ik_z z} \\ E_y = A_2 \sin k_x x \cos k_y y e^{ik_z z} \\ E_z = A_3 \sin k_x x \sin k_y y e^{ik_z z} \end{cases}$$

$$E_z = A_3 \sin k_x x \sin k_y$$

由 
$$\vec{H} = -\frac{i}{\omega\mu} \nabla \times \vec{E}$$
 可求得波导管中的磁场为: 
$$\begin{cases} H_x = -\frac{i}{\omega\mu} (A_3 k_y - i A_2 k_z) \sin k_x x \cos k_y y e^{ik_z z} \\ H_y = -\frac{i}{\omega\mu} (i A_1 k_z - A_3 k_x) \cos k_x x \sin k_y y e^{ik_z z} \\ H_z = -\frac{i}{\omega\mu} (A_2 k_x - A_1 k_y) \cos k_x x \cos k_y y e^{ik_z z} \end{cases}$$

故: 1) 若 
$$n = 0$$
,则 $k_y = \frac{n\pi}{b} = 0$ ,  $A_2 k_x = 0$   
又  $k_x = \frac{m\pi}{a} \neq 0$ ,那么 $A_2 = 0$ 

$$\therefore H_x = H_y = 0$$

13. 频率为
$$30\times10^9$$
 Hz 的微波,在 $0.7cm\times0.4cm$  的矩形波导管中能以什么波模传播?在 $0.7cm\times0.6cm$  的矩形波导管中能以什么波模传播?解: 1)  $v=30\times10^9$  Hz ,波导为 $0.7cm\times0.4cm$ 

2)  $v = 30 \times 10^9 \, Hz$ , 波导为  $0.7 \, cm \times 0.6 \, cm$ m = 1, n = 1 |  $\nu = 2.1 \times 10^{10}$  Hz m = 1, n = 0  $\forall$ ,  $v = 2.5 \times 10^{10} Hz$ 

在 x 方向是均匀的, 求可能传播的波模和每种波模的截止频率。

解: 在导体板之间传播的电磁波满足亥姆霍兹方程:

 $\stackrel{\text{def}}{=} a = 0.7 \times 10^{-2} \, \text{m.,} b = 0.4 \times 10^{-2} \, \text{m} \text{ Fe}$ 

:. 此波可以以 TM10 波在其中传播。

m = 1 n = 1  $\text{H}^{\dagger} v = 4.3 \times 10^{10} \text{ Hz}$ 

m = 1, n = 0 |  $v = 2.1 \times 10^{10} Hz$ 

m = 0, n = 1  $\forall v = 3.7 \times 10^{10} Hz$ 

m = 0, n = 1  $\forall v = 3.3 \times 10^{10} Hz$ ∴此波可以以 TE10和 TE01两种波模传播。 14. 一对无限大的平行理想导体板,相距为 b,电磁波沿平行与板面的 z 方向传播,设波

$$egin{cases} 
abla^2 ec{E} + k^2 ec{E} = 0 \ k = \omega \sqrt{\mu_0 arepsilon_0} \ 
abla \cdot ec{E} = 0 \end{cases}$$

令 U (x, y, z) 是  $\vec{E}$  的任意一个直角分量,由于  $\vec{E}$  在 x 方向上是均匀的  $\therefore U(x, y, z) = U(y, z) = Y(y)Z(z)$ 

又在 y 方向由于有金属板作为边界,是取驻波解;在 z 方向是无界空间,取行波解  $\therefore$ 解得通解:  $U(x,y,z) = (C_1 \sin k_y y + D_1 \cos k_y y)e^{ik_z z}$ 

由边界条件: 
$$\vec{n} \times \vec{E} = 0$$
, 和  $\frac{\partial E}{\partial n} = 0$  定解 
$$E_x = A_1 \sin(\frac{n\pi}{h}y)e^{i(k_z z - \omega t)}$$

$$E_{x} = A_{1} \sin(\frac{n\pi}{b}y)e^{i(k_{z}z-\omega t)}$$

$$E_{y} = A_{2} \cos(\frac{n\pi}{b}y)e^{i(k_{z}z-\omega t)} \perp k^{2} = \frac{\omega^{2}}{c^{2}} = (\frac{n\pi}{b})^{2} + k_{z}^{2}, n = 0,1,2\cdots$$

$$E_{z} = A_{3} \sin(\frac{n\pi}{b}y)e^{i(k_{z}z-\omega t)}$$

又由 $\nabla \cdot \vec{E} = 0$ 得:  $A_1$ 独立,与  $A_2$ ,  $A_3$  无关,  $\frac{n\pi}{h} A_2 = ik_z A_z$ 

令  $k_z = 0$  得截止频率:  $\omega_c = \frac{n\pi c}{b}$ 15. 证明整个谐振腔内的电场能量和磁场能量对时间的平均值总相等。

证明: 在谐振腔中, 电场 $\vec{E}$ 的分布为:

$$\begin{cases} E_x = A_1 \cos k_x x \sin k_y y e^{ik_z z} \\ E_y = A_2 \sin k_x x \cos k_y y e^{ik_z z} \\ E_z = A_3 \sin k_x x \sin k_y y e^{ik_z z} \end{cases}$$

由 
$$ar{H}=-rac{i}{\omega\mu}
abla imesar{E}$$
 可求得波导管中的磁场为: 
$$\left[H_x=-rac{i}{\omega\mu}(A_3k_y-iA_2k_z)\sin k_xx\cos k_yye^{ik_zz}
ight]$$

$$\begin{cases} H_y = -\frac{i}{\omega\mu} (iA_1k_z - A_3k_x)\cos k_x x \sin k_y y e^{ik_z z} \\ H_z = -\frac{i}{\omega\mu} (A_2k_x - A_1k_y)\cos k_x x \cos k_y y e^{ik_z z} \end{cases}$$

由
$$\omega = \frac{1}{2}(\vec{E}\cdot\vec{D} + \vec{H}\cdot\vec{B})$$
有,谐振腔中:

1)电场能流密度 
$$\omega_E = \frac{1}{2}\vec{E} \cdot \vec{D}$$

$$\omega_E = \frac{1}{2}\vec{E} \cdot \vec{D}$$

$$\therefore \overline{\omega}_E = \frac{1}{2} [\frac{1}{2} \operatorname{Re}(\vec{E}^* \cdot \vec{D})] = \frac{1}{4} \operatorname{Re}(\vec{E}^* \cdot \vec{D})$$

$$\therefore \overline{\omega}_E = \frac{1}{2} [-\frac{1}{2}]$$

 $\overline{\omega}_B = \frac{1}{4} \operatorname{Re}(\vec{H}^* \cdot \vec{B})$ 

$$=\frac{\varepsilon}{4}[A_1^2\cos^2k_xx\sin^2k_yy\sin^2k_zz+A_2^2\sin^2k_xx\cos^2k_yy\sin^2k_zz+A_3^2\sin^2k_xx\sin^2k_yy\cos^2k_zz+A_3^2\sin^2k_xx\sin^2k_yy\sin^2k_zz+A_3^2\sin^2k_xx\sin^2k_zz+A_3^2\sin^2k_xx\sin^2k_zz+A_3^2\sin^2k_xx\sin^2k_zz+A_3^2\sin^2k_xx\sin^2k_zz+A_3^2\sin^2k_zx\sin^2k_zz+A_3^2\sin^2k_zx\sin^2k_zz+A_3^2\sin^2k_zx\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx\sin^2k_zx+A_3^2\sin^2k_zx+$$

$$=rac{arepsilon}{4}[A_1^2\cos^2k_xx\sin^2k_yy\sin^2k_z^2]$$
②)磁场能流密度
 $\omega_B=rac{1}{2}ec{H}\cdotec{B}$ 

$$4^{2} \cos^{2} k x \sin^{2} k v \sin^{2} k z + 1$$

$$(\cdot\vec{D} + \vec{H} \cdot \vec{B})$$
有,谐振腔中:密度 $O_E = \frac{1}{2} \vec{E} \cdot \vec{D}$ 

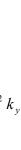
 $= \frac{1}{4 \mu m^2} [(A_3 k_y - A_z k_z)^2 \sin^2 k_x x \cos k^2 k_y y \cos^2 k_z z +$ 

 $+(A_1k_2-A_2k_3)^2\cos^2 k_3x\sin^2 k_3y\cos^2 k_2z +$ 

 $+(A_2k_x-A_1k_y)^2\cos^2k_xx\cos^2k_yy\sin^2k_zz$ 

$$\cos k_x x \cos k_y y e^{ik_z z}$$

$$4^2 \sin^2 k$$
 usin



其中:  $k_x = \frac{m\pi}{a}, k_y = \frac{n\pi}{b}, k_z = \frac{p\pi}{a}, m, n, p = 0,1,2\cdots$ a, b, c 是谐振腔的线度, 不妨令 x:0~a, y:0~b, z:0~c 于是谐振腔中电场能量对时间的平均值为:

有:  $k_x^2 + k_y^2 + k_z^2 = k^2 = \omega^2 \mu \varepsilon \perp A_1 k_x + A_2 k_y + A_3 k_z = 0$ 

 $\overline{W}_E = \int \overline{\omega}_E dV = \frac{\varepsilon}{4} \int \int \int \int (A_1^2 \cos^2 k_x x \sin^2 k_y y \sin^2 k_z z + A_2^2 \sin^2 k_x x \cos^2 k_y y \sin^2 k_z z + A_2^2 \sin^2 k_z x \cos^2 k_y y \sin^2 k_z z + A_2^2 \sin^2 k_z x \cos^2 k_z x \sin^2 k_z \cos^2 k_z$ 

$$+ A_3^2 \sin^2 k_x x \sin^2 k_y y \cos^2 k_z z) dx dy dz$$

$$= \frac{abc\varepsilon}{32} (A_1^2 + A_2^2 + A_3^2)$$
谐振腔中磁场能量的时间平均值为:
$$\overline{W}_B = \int \overline{\omega}_B dV = \frac{1}{4\mu\omega^2} \cdot \frac{abc}{8} [(A_3 k_y - A_2 k_z)^2 + (A_1 k_z - A_3 k_x)^2 (A_2 k_x - A_1 k_y)^2]$$

 $\therefore A_1 k_x + A_2 k_y + A_3 k_z = 0$  $\therefore (A_1 k_x + A_2 k_y + A_3 k_z)^2 = A_1^2 k_x^2 + A_2^2 k_y^2 + A_3^2 k_z^2 + 2A_1 A_2 k_x k_y + 2A_1 A_3 k_z k_x + 2A_2 A_3 k_y k_z + 2A_1 A_2 k_z k_z + 2A_1 A_2$ 

$$(A_1k_x + A_2k_y + A_3k_z)^2 = A_1^2k_x^2 + A_2^2k_y^2 + A_3^2k_z^2 + 2A_1A_2k_xk_y + 2A_1A_3k_zk_x + 2A_2A_3k_yk_z$$

$$\therefore \overline{W}_B = \frac{abc}{32\mu\omega^2} [(A_1^2 + A_2^2 + A_3^2)(k_x^2 + k_y^2 + k_z^2)]$$

$$\therefore \overline{W}_{B} = \frac{abc}{32\mu\omega^{2}} [(A_{1}^{2} + A_{2}^{2} + A_{3}^{2})(k_{x}^{2} + k_{y}^{2} + k_{z}^{2})]$$

$$= \frac{abck^{2}}{32\mu\omega^{2}} (A_{1}^{2} + A_{2}^{2} + A_{3}^{2}) = \frac{abc\varepsilon}{32} (A_{1}^{2} + A_{2}^{2} + A_{3}^{2})$$

$$\therefore \overline{W}_E = \overline{W}_B$$

$$\therefore W_E = W_B$$