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Operational method for determining bottom hole pressure in mechanized oil producing wells, based on the application of multivariate regression analysis

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ABSTRACT

One of the major tasks of monitoring production well operations is to determine bottom-hole flowing pressure. The overwhelming majority of wells in the Perm Krai are serviced using borehole pumps, which makes it difficult to take direct bottom-hole flowing pressure measurements. The bottomhole filtration pressure (BHFP) in these wells is very often determined by recalculating the parameters measured at the well mouth (annulus pressure, dynamic fluid level depth). The recalculation is done by procedures based on analytically determining the characteristics of the gas-liquid mixture in the well-bore, which is very inconsistent to perform due to the mixture's complex behavior. This article proposes an essentially different approach to BHFP measurements that relies on the mathematical processing of the findings of more than 4000 parallel mouth and deep investigations of the oil production wells of a large oil-production region. As a result, multivariate mathematical models are elaborated that allow reliably determining the BHFP of oil-production wells in operation.

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1. Introduction

Well operation monitoring is an integral part of oil and gas production optimization (Galkin et al., 2019; Chernykh et al., 2017; Sánchez-Fernández et al., 2018; Elesin A.V. et al., 2018). One of the topical tasks of this monitoring is to determine the BHFP (Dragunov et al., 2017; Ahmadi et al., 2016; Nait Amar et al., 2018; Martyushev D.A. et al., 2019; Dyagilev V.F. et al., 2019). Bottom hole pressure is a crucial parameter for a well during its various stages of life. It is used to establish the development strategies and the design of completions. In addition, the BHFP is the parameter linking the work of the elements of the reservoir-well system. The BHFP level can be used to control and manage the operation of downhole equipment (Natarajan and Srinivasan, 2010; Martyushev D.A., 2021).

Because of the complexity of multiphase flows, the calculation

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pressure down-hole gauges which can record a huge amount of bottom-hole pressure data. Although the value of this advantage, this method presents two limitations: it's cost and the handling of its data which are noisy. As a matter of practice, if a well is operated using deep-pumping equipment, the BHFP is determined by calculation (Bikmukhametov and Jäschke, 2019). If the suction manifold is equipped with a special instrument (sensor), the pressure measured with its help and referred to as the suction pressure is recalculated to the BHFP. As a rule, these calculations are not impaired by any particular difficulties and are made fairly stably. If the deep-pumping equipment configuration has no room for installing a measuring instrument at the suction manifold, the BHFP is determined by recalculating the parameters that are measured at the well mouth and include dynamic fluid level depth and annulus pressure (Natarajan et al., 2009). This recalculation is mathematically based on the hydrostatic equation. In this case the quantity to determine is the wellbore fluid density (Yang et al., 2020). This fluid is a gas-liquid mixture the parameters of which are very difficult to describe by analytical equations (Chen et al., 2017; Cecconet et al., 2018; Iktissanov, 2020; Akinbinu, 2010). In

of the bottom hole pressure is complicated. One of the applied methods to determine bottom hole pressure is the deployment of

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this article, all of the BHFP determination procedures based on recalculating the parameters measured at the well mouth and recalculated considering the gas-liquid mixture density are called density-based techniques.

As the estimation of this parameter technically i.e. using gauge or well testing is so expensive, numerous empirical correlations and semi empirical (mechanistic) models based on the known surface measurements have been developed since the early 1940s. The most commonly used correlations are those of: Hagedorn and Brown, Duns and Ros, Orkiszewski, Beggs and Brill, Aziz and Govier, Mukherjee and Brill correlation; the commonly used mechanistic models are those of Ansari et al. Chokshi et al., Gomez et al. and Grey. Most of these correlations and models were developed under a range of conditions; consequently, when their applications are out of these domains, their performances became poor and mediocre (Mohammad Ali Ahmadi et al., 2019).

Recently, Artificial Intelligence (AI) based methods have been widely applied in petroleum engineering to solve many conventional and unconventional problems [11]. Among AI methods, artificial neural networks (ANNs) is the famous tool thanks to its effectiveness. The main problem that ANN models suffer from, is the presence of some inaccuracies which caused by the defaulted training algorithms (like backpropagation BP) that trap in local minima (Jeirani Z. et al., 2006; Menad Nait Amar et al., 2018; Menad Nait Amar et al., 2020).

In the Perm Krai oil is produced at more than 5000 wells only 30% of which are equipped with downhole instruments. The BHFP at other wells is determined by recalculating the mouth parameters by various density-based procedures (Valery and Eslamloueyan, 2015; Escobar et al., 2007). The accuracy of these techniques has been evaluated by several specialized investigations (Wijaya and Sheng, 2020; Al-Rbeawi, 2018), that have revealed their low consistency and significant errors in the BHFP measurements, especially at deposits with reservoir oil highly saturated with gas.

The current investigations are aimed at choosing optimal BHFP control techniques (Jahanandish et al., 2011; Kaviani et al., 2018). When the analytical description of physical processes is inapplicable for whatever reason, it is relevant to apply statistical techniques based on processing collected facts mathematically (Chen et al., 2017; Virstyuk A.Yu. et al., 2020). Statistical techniques are often easier to apply and more accurate than the attempt to elucidate analytical regularities in the behavior of complex physical systems. This approach does not require any significant reductions and suppositions, applies for any distribution laws, to systems of any complexity and multiplicity of states, and is restricted only by the actual parameters of the original sample. Statistical techniques are successfully applied for solving various engineering tasks (Singh, 2019; Jirjees and Abdulaziz, 2019; Shahbazi et al., 2020).

In this vein, the article describes an original multilevel approach elaborated by the authors. This technique allows constructing multivariate statistical models of determining the BHFP of wells in operation. These models are generalized for vast territorial entities. Stages of work:

- Development of multidimensional statistical models for determining the bottomhole pressure in oil producing wells during their operation.
 - Collection and systematization of production data characterizing the operation of wells.
 - Correlation analysis, selection of parameters that are statistically related to bottomhole pressure.
 - Construction of multidimensional statistical models for determining the bottomhole pressure during the operation of oil producing wells. Analysis of their reliability.

- 2) Application of multivariate statistical models to determine bottomhole pressure.
 - Collection of initial data values of parameters used in models as independent features. Comparison with the ranges of applicability of the models.
 - Calculate bottomhole pressure using first, second, third and fourth level models. Calculation of the resulting bottomhole pressure using the generalized model.

2. Materials and methods

To solve the formulated task, we used the data from n=4145investigations in which the measurements were taken synchronously at the mouth and bottom of the flowing wells of the oil deposits confined to the Solikamsk depression, a major oilproduction area in the Perm Krai. The deposits were Un'vinskoye, Gagarinskoye, Siberian, Magovskoye, Ozernoye, Chashkinskoye, Shershnevskoye, and the one named after Sukharev. To create multivariate multilevel models, we used the data of the downhole BHFP measurements in the wells equipped with measuring devices at the suction manifold; in addition, such well performance characteristics were used as liquid rate $(Q_1, m^3/day)$, oil rate $(Q_0, t/day)$, water cut (w, %), fluid pressure in the annulus between tubing and casing (Pan, MPa), dynamic fluid level depth (Hdfl, m), pump measured depth (H_{pump}, m), distance from the pump hinge point to the dynamic fluid level depth (Hpd); oil-water contact (OWC) measured depth, and reservoir pressure (P_r). The BHFP recalculated from the suction manifold pressure was used as actual (P_{bb}, MPa).

A distinct feature of our approach is the different degree of differentiating the facilities for which the models are constructed; that is, the approach is multilevel. The levels for which the models are constructed are exposed below.

- (1) Level one. It involves using the entire sample, without separating deposits and production targets (occurrences).
- (2) Level two. It consists in considering each deposit without separating occurrences.
- (3) Level three. It consists in considering each occurrence in a generalized sense, without taking the deposits into account.
- (4) Level four. It implies constructing model specifically for each occurrence within a deposit.

We also constructed for practical application the multivariate model covering the BHFP determination results for all of the levels. The investigation was conducted using available mathematical statistics tools (Galkin V.I. et al., 2017).

In the preliminary phase, we analyzed the correlations between the BHFP and the well operation properties that might affect the BHFP level. To achieve this purpose, we calculated not only coefficient r of the correlation between the input parameters and the BHFP but also coefficient r of the mutual correlation among the input parameters. The calculated results are exposed as correlation matrices, correlation fields, and equations of regression between the BHFP and the well performance indicators. We conducted the investigations in question for the models from all of the levels.

The next phase of investigation is the construction of multivariate multilevel models using the original cumulative sample technique. According to this approach, the initial data are all tentatively graded against the range of BHFP levels from minimal to maximal. The first model is constructed according to the first three graded data (the amount of data per sample is n=3). Then the model is constructed for n=4. Thus multivariate models are consecutively constructed until all of the available data are used. In these variants the multivariate models are constructed by step-by-

step regression analysis. The dependent feature is P_{bh}, whereas the values of the rest of the above specified well performance indicators are used as independent factors. Step-by-step regression analysis was used not only to derive the equation of regression, defined as a multivariate statistical model, but also to identify the existence and kind of influence of the independent factors on the dependent variable.

The regression coefficients in the elaborated models were calculated by the least square technique. The functionality of each model was assessed in several ways. First of all, such statistical characteristics of the models were calculated in each case, as multiple correlation coefficient R, significance level p, and standard error S_0 . The applicability limits of each model are defined. To assess the model of each level for functionality, it was used to calculate the BHFP also compared with the actual levels. The comparison was made while visually analyzing the correlation fields, analyzing the equations of regression between the actual and the calculated BHFP levels, and with the help of such other mathematical statistics means as Student's t-test and Pearson's chisquared test (Nait Amar et al., 2018; Ashena and Moghadasi, 2011; Ghaffarian et al., 2014).

Thus the models were constructed for all of the four distinguished levels. Four domes are distinguished within the confines of the Un'vinskoye deposit. To take this peculiarity into account, we additionally constructed the models of each of the domes as part of modeling level four.

The analysis of constructed models should be considered a major part of any kind of modeling, multivariate modeling included. In this case, the analysis of all of the models involved examining the succession and frequency of including each of the input parameters in the equations of regression. It is considered that, the more often is a particular parameter found in multivariate models and the earlier it is used in model construction, the larger will be its effect on the BHFP. Thus this analysis allowed distinguishing the factors that had the biggest effect on the BHFP level registered when the commercial wells of the oil deposits in the considered region were in operation.

The multivariate equations of regression derived at all of the modeling levels are supposed to be used together, for which purpose the generalized multivariate model is constructed. It is proposed for use as the mathematical basis of the technique of measuring the BHFP in well operation.

The final phase was the investigation of the accuracy of determining the BHFP using the elaborated multivariate models. For that purpose we calculated the model BHFP levels (P_{bh}) and then compared them with the actual BHFP levels (Pbh). This phase also involves comparing the elaborated technique, based on using multivariate models; with the currently applied BHFP calculation technique based on using the density of the gas-liquid mixture in the well bore. For that purpose we also calculated Phh using the conventional technique and then compared the results with the actual BHFP levels. The elaborated technique based on multivariate multilevel models and its currently applied counterpart based on calculating the density of the gas-liquid mixture in the well bore were compared by drawing the correlation fields when investigating the correlation (equations of regression and their characteristics) between the actual and the calculated BHFP for the whole sample and for the separate deposit development targets.

It is supposed that the joint consideration of the regression equation parameters and their statistical characteristics will allow evaluating not only the tightness but also the kind of relations between the actual BHFP and the BHFP calculated by the two techniques.

3. Results

For the correlation matrix drawn for the whole examined sample (level one) and characterizing the influence of the well performance indicators on the BHFP level see Table 1.

The correlation matrix of level two is represented for the Un'vinskoye deposit as the largest one in the region and exposed in Table 2.

Similar correlation matrices were drawn for all of the deposits in the considered region. The example of a correlation matrix for investigation level three is presented for the occurrences confined to Bobrikovian sedimentations (Table 3).

The correlation matrices at level four were made up for each occurrence within the deposits.

The example exposed in Table 4 is the correlation matrix for the Bobrikovian occurrence of the Un'vinskoye deposit. The making up of the matrix involved calculating coefficients r using all the data (upper string) and, separately, for the domes (lines two, three, and four, and the bottom line are for the Un'vinskii, Palasherskii, Southeastern, and Bystrovskii dome, respectively).

Similar correlation matrices were made up for all of the occurrences of all the deposits. All in all, 29 correlation matrices were made up for different modeling levels; the matrices included 1305 values of r. Then, multivariate models were constructed for all of the levels.

The model for level one is recorded as:

$$P_{bh}^{M1} = 1.163 + 0.0042H_{bound} + 0.009H_{owc} - 0.009H_{pump} + 0.022w + 0.601P_{an} + 0.097Q_{l} + 0.040P_{r}$$
 (1)

The statistical accuracy characteristics determined for the model were multiple correlation coefficient R=0.763, significance level p<0.0000, and standard calculation error $S_0=1.76$ MPa. The model forming sequence is provided in the equation of regression. The coefficients describing the reliability of the statistical relations changed as follows: r=0.505; R=0.612; 0.703; 0.736; 0.760; 0.762; 0.763.

The multivariate models at level two were constructed separately for the deposits, without distinguishing the occurrences. The model provided as example was made up for Un'vinskoye deposit as the largest deposit in the region and is recorded as:

$$\begin{split} P_{bh}^{M2-U} &= -6.637 - 0.00718 H_{dfl} + 0.0086 H_{owc} + 0.021 w + 0.684 P_{an} + \\ 0.3054 P_r - 0.0021 H_{bound} \end{split} \tag{2} \label{eq:2}$$

at R = 0.822, p < 0.0000, $S_0 = 1.52$ MPa. The model was formed in the sequence presented in the equation of regression. The coefficients describing the reliability of statistical relations varied as follows: R = 0.717; 0.762; 0.790; 0.808; 0.815; 0.822.

Similar models were also constructed for the Siberian, Shershnevskoye, Gagarinskoye, Ozernoye, Magovskoye, and Chashkinskoye deposit.

Level three implies constructing multivariate models for the main occurrences distinguished in particular deposits within the considered region.

The model for the Bobrikovian occurrence developed at almost all of the deposits is recorded as:

$$P_{bh}^{M3-bb} = 19.684 - 0.00404 H_{dfl} + 0.025 w - 0.0037 H_{pump}$$
 (3)

at R = 0.644, p < 0.0000, $S_0 = 1.9$ MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.512; 0.608; 0.644.

The model for all of the occurrences was derived in a similar manner. Then we built multivariate level-four models specifically

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 Table 1

 Matrix of the correlation between bottom-hole flowing pressures and well performance indicators (level one).

	P_{bh}	H_{dfl}	Pan	W	Q_{l}	Q_o	H_{owc}	H_{pump}	H_{pd}	P _r
P _{bh}	1	-0.45*	0.15*	0.19*	0.38*	0.28*	0.48*	0.2*	0.51*	0.32*
H_{dfl}		1	0.13*	0.05*	-0.26*	-0.29*	0.04*	0.07*	-0.87*	-0.02
Pan			1	-0.03	0.21*	0.19*	0.07*	0.06*	-0.09*	0.09*
w				1	0.17*	-0.25*	0.02	0.04*	-0.05*	0.33*
Q_1					1	0.83*	0.3*	0.27*	0.34*	0.36*
Q_{o}						1	0.27*	0.27*	0.38*	0.26*
H_{owc}							1	0.75*	0.3*	0.54*
H_{pump}								1	0.39*	0.53*
H _{pd}									1	0.2*
P_r										1

Note: *-significant correlations.

 Table 2

 Matrix of the correlation between bottom-hole flowing pressures and well performance indicators (level two, Un'vinskoye deposit).

	P_{bh}	H_{dfl}	Pan	w	Q_1	Q_o	H_{owc}	H_{pump}	H_{pd}	P_r
P _{bh}	1	-0.72*	0.09	-0.02	0.3*	0.26*	0.42*	-0.07	0.65*	0.17*
H_{dfl}		1	0.14*	0.21*	-0.24*	-0.31*	-0.24*	0.02	-0.92*	-0.13*
Pan			1	-0.1*	0.31*	0.33*	0.13	-0.03	-0.15	-0.07
w				1	0.03	-0.43*	-0.28*	-0.12*	-0.24*	0.22*
Q_1					1	0.85*	0.2*	-0	0.22*	0.09*
Q_{o}						1	0,24*	0.05	0.31*	0.01
H_{owc}							1	0.31*	0.34*	-0.25*
H_{pump}								1	0.36*	-0.14*
H _{pd}									1	0.07
P_r										1

Note: *-significant correlations.

Table 3Matrix of the correlation between bottom-hole flowing pressures and well performance indicators (level three, Bobrikovian sedimentations).

	P_{bh}	H_{dfl}	Pan	w	Q_1	Q_o	H_{owc}	H_{pump}	H_{pd}	P_r
P _{bh}	1	-0.51*	0.02	0.25*	0.21*	0.09*	0.13*	-0.26*	0.37*	0.26*
H_{dfl}		1	0.22	0.15	-0.18*	-0.29*	-0.01	0.02	-0.92*	-0.04
Pan			1	-0.05	0.28*	0.28*	0.18*	-0.03	-0.21*	0.08
w				1	0.19*	-0.37*	0.02	-0.11*	-0.18	0.22*
Q_1					1	0.77*	0.2*	0.01	0.17*	0.16*
Q_o						1	0.11*	0.07*	0.3*	-0
H_{owc}							1	0.2*	0.09	0.59*
H_{pump}								1	0.38*	0.04
H _{pd}									1	0.05
Pr										1

Note: *-significant correlations.

for the occurrences within the deposits. For example, the presented level-four model is recorded for the Bobrikovian occurrence of the Un'vinskoye deposit as:

$$\begin{split} P_{bh}^{M4-U\text{-}bb} &= 17.902 - 0.0053 H_{dfl} + 0.0257 w + 0.5906 P_{an} \text{ -} \\ 0.0026 H_{pump} \end{split} \tag{4}$$

at R=0.763, p<0.0000, $S_0=1.62$ MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.683; 0.723; 0.748; 0.763.

For the ranges, in which all of the above recorded models can be used (Table 5).

The multivariate models for each of the domes of the Un'vinskoye deposit are recorded as follows:

(a) Un'vinskoye dome

$$P_{bh}^{M4-1} = 4.430 - 0.0024 H_{dfl} + 0.003 H_{owc} + 0.011 w + 0.449 P_{an} - 0.0055 Q_{l}\left(5\right)$$

at R = 0.552, p < 0.0000, $S_0 = 1.44$ MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.460; 0.497; 0.532; 0.549; 0.552.

(b) Palasherskiy dome

$$\begin{split} P_{bh}^{M4-2} &= -57.862 - 0.0045 H_{dfl} + 0.0075 H_{owc} + 0.7014 P_{an} + 0.0172 Q_{l} \\ &- 0.0177 Q_{o} \end{split} \tag{6}$$

at R=0.770, p<0.0000, $S_0=1.37$ MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.648; 0.734; 0.573; 0.759; 0.764; 0.770.

(c) Southeastern dome

$$\begin{split} P_{bh}^{M4-3} &= -201.705 + 0.375Q_{o} - \\ 0.001H_{dfl} &+ 0.104H_{owc} + 0.004H_{pump} \end{split} \tag{7}$$

at R = 0.729, p<0.0121, $S_0 = 0.91$ MPa. The model was formed in

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 Table 4

 Correlation matrix of the influence of performance indicators (level four, Un'vinskoye deposit and Bobrikovian sedimentations).

	P_{bh}	Qı	Qo	В	P _{an}	H _{dfl}	H_{pump}	H _{owc}	$P_{\rm r}$
P _{bh}	1	0.22*	0.16*	0.05	0.21*	-0.44*	-0.19*	0.23*	0.07
	1	0.11*	0.03	0.17*	0.08	-0.46*	-0.11*	-0.01	-0.05
	1	0.28*	0.28*	-0.06	0.17*	-0.65*	-0.33*	0.45*	0.27*
	1	-0.15	0.57*	-0.39	-0.23	-0.48*	-0.12	-0.33	0.23
	1	-0.71	-0.72*	0.79*	0.81*	0.52	-0.72*	_	_
Q_1		1	0.77*	0.05	0.33*	-0.25*	-0.04	-0.17*	-0.02
		1	0.76*	0.08	0.14*	-0.36*	0.09	-0.39*	-0.06
		1	0.76*	0.12*	0.37*	-0.28*	-0.22*	-0.11	-0.12
		1	-0.15	0.54*	-0.09	-0.26	0.88*	-0.58*	-0.9*
		1	0.97*	-0.78*	-0.59	-0.08	0.75*	_	_
Q_o			1	-0.5*	0.31*	-0.23*	-0.05	-0.1	-0.04
			1	-0.48*	0.22*	-0.33*	0.09	-0.29*	-0.04
			1	-0.51*	0.48*	-0.27*	-0.23*	-0.04	0.01
			1	-0.72*	-0.11	-0.30	-0.4	-0.37	0.07
			1	-0.88*	0.53	-0.01	0.86*	_	_
В				1	0.14*	0	-0	-0.07	-0.18*
				1	0.02	0.05	-0.04	0.01	-0.26*
				1	-0.22*	0.08	0.08	-0.17*	-0.27*
				1	-0.06	0.07	0.69*	0.23	-0.32*
				1	0.48	0.05	-0.99*	_	_
P_{an}					1	0.18*	-0.01	0.19*	0.04
an					1	0.12*	0.01	0.05	-0.37*
					1	0	-0.03	0.01	-0.14
					1	0.5*	-0.22	0.23	-0.06
					1	0.73*	-0.38	_	_
H_{dfl}					-	1	0.09*	0.27*	0.13*
						1	0.03	0.4*	-0.09
						1	0.25*	-0.16*	0.33*
						1	-0.3	0.5*	0.18
						1	0.07	_	-
H_{pump}						•	1	-0.29*	0.08
pump							1	-0.2*	0.05
							1	-0.5*	0.17*
							1	-0.54*	-0.64*
							1	0.0 .	0.0 1
H_{owc}							•	1	0.14*
110WC								1	-0.09
								1	-0.31*
								1	0.52*
								1	-
P_r								1	1
* r									1
									1
									1
									1
									I

Note: *-significant correlations.

Table 5Applicability ranges of the models of four levels.

Model's index	Applicability range of model of levels								
	1	2	3	4					
H _{dfl} , m	_	93.9-1946.5	206.9-1946.5	304.9-1946.5					
P _{an} , 10 ⁶ Pa	0-8.5	0.06-6.05	_	0.06-6.05					
w, %	0.0-99.9	0.0-98	0.0-99.9	0.0-97.6					
Q _I , m ³ /day	_	_	_	_					
Q _o , t/day	0.0-119.3	_	_	_					
H _{owc} , m	1426.0-2332.7	1837.7-2246.7	_	_					
H _{pump} , m	1201.4-2287.6		1439.3-2177.2	1445.3-2083.1					
H _{pd} , m	3.8-1720.5	17.1-1554	_	_					
P _r , 10 ⁶ Pa	6.4-23.3	13.9-20.4	_	_					

the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.566; 0.652; 0.706; 0.729.

(d) Bystrovskiy dome

$$P_{bh}^{M4-4} = -6.775 + 5.321P_{an} + 0.22617w + 0.0041H_{dfl}$$
 (8)

at R=0.943, p<0.02155, $S_0=0.94$ MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R changed as follows: 0.805; 0.927; 0.943.

For the value ranges of the indices, in which the models derived for each elevation can be used (Table 6).

The correlation of the calculated and the actual BHFP levels was examined by making up equations of regression (Table 7).

Table 6Applicability ranges of the models of the domes of the Un'vinskoye deposit (Bobrikovian occurrence).

Model's index	Applicability range of the models derived for domes							
	Un'vinskoye	Palasherskiy	Southeastern	Bystrovskiy				
H _{dfl} , m P _{an} , MPa w, % Q _l , m ³ /day Q _o , τ/cyτ H _{owc} , m H _{pump} , m H _{pd} , m	210 - 1935 0.14-4.79 1-98.4 0.8-98.7 2088-2519.5	513–2076 0.37–3.71 0.5–107.2 0.2–71.2 2152–2553.2	916–1416 0.11–6.36 1715–1970	1194 -1744 0.94-1.3 5-20				
P _r , MPa								

Table 7Equations of regression between the actual BHFP levels and the BHFP values calculated according to the level-four model, considering the discrimination of domes within the Un'vinskoye deposit.

Dome	Equation of regression	r	р
Un'vinskoye	$P_{bh}^{M4-1} = 5.416 + 0.303 P_{bh}$	0.549	0.0000
Palasherskiy	$P_{bh}^{M4-2} = 3.484 + 0.598P_{bh}$	0.766	0.0000
Southeastern	$P_{bh}^{M4-3} = 3.769 + 0.532 P_{bh}$	0.729	0.0002
Bystrovskiy	$P_{bh}^{M4-4} = 0.818 + 0.890 P_{bh}$	0.943	0.0004

The frequency of inclusion (incidence) of the indices in the models of all the levels was calculated during their analysis and is shown in Table 8.

The generalized model is recorded as:

$$P_{bh}^{MM} = -0.089 + 0.689P_{bh}^{M-3} + 0.361P_{bh}^{M-2} - 0.039P_{bh}^{M-1}$$
 (5)

at R=0.941, p<0.0000 and the mean standard error is 0.45 MPa. The model was formed in the sequence exposed in the equation of regression. The values of coefficient R describing the strength of the statistical relations changed as follows: 0.848; 0.851; 0.941.

The data the results of comparing which are exposed below were obtained by two techniques, the new one based on applying multivariate models and the conventional one based on calculating the gas-liquid mixture density. The correlation fields for the sample in general are presented in Fig. 1.

The equations of regression between the actual BHFP and the BHFP calculated by the two techniques are shown in Table 9 as well as the statistical characteristics of these equations, including the correlation coefficient, the significance level, and the standard calculation error. The equations are compared at two levels, i.e., using all the data (level one) and, separately, for the occurrences of all of the deposits (level two).

In addition, to comparatively evaluate the functionality of the techniques as applied to specific occurrences, the respective correlation fields were drawn by the example of Un'vinskoye as the region's most representative deposit (Fig. 2).

4. Discussion

The exposed investigations should be considered the justification of the expediency of applying probabilistic statistical techniques to determining the bottom-hole flowing pressure treated as a major task in the oil extraction industry. As shown by all of the conducted investigations, the creation of a stable BHFP determination technique is a complex task to solve.

For example, as evidenced by the correlation analysis, in which 29 correlation matrices with 1305 correlation coefficient values were built for the four levels of investigation, the well performance indicators have a complex effect on the BHFP level. The mutual correlations among the indicators vary in a broad range from -0.87 to 0.83. As found out by the correlation analysis one and the same performance indicator may have a different effect on the BHFP level in various conditions, i.e., the input parameters have a differentiated effect on the calculated quantity. For example, coefficient r between $P_{\rm bh}$ and $P_{\rm an}$ changed from -0.08 to 0.51 at various levels of investigation; sometimes, the relation among these parameters is negative, sometimes - positive and statistically significant. On the whole, the identical direction of affecting $P_{\rm bh}$ is followed by such parameters, as $H_{\rm dfl}$, $H_{\rm owc}$, $H_{\rm pd}$, and $P_{\rm r}$, whereas the others produce various effects in terms of both, direction and force.

All of this shows that the BHFP is affected by the performance indicators both, together and individually. Thus the correlation analysis has allowed finding out that none of the performance indicators makes it possible to reliably predict BHFP levels. The BHFP formation during well operation follows very complicated and non-stationary laws, which is why the analytical solution making it possible to determine the BHFP in a firm and reliable manner should be considered an extremely complex task to solve.

As mentioned earlier, when analytical techniques do not apply due to the low accuracy of their results, it seems expedient to use statistical (probabilistic statistical) techniques). This is why, it is not analytical solutions but multivariate statistical models that are proposed in this paper as the techniques for determining the BHFP level during well operation. Therefore, the rest of the investigation is dedicated to constructing multivariate statistical models.

It should be noted that these models were built using the original approach, i.e., by a pre-ordered distribution. Not only does this approach allow deriving the model, that allows reliably determining the BHFP as the target parameter, but it also allows distinguishing all the regularities of its formation in various conditions.

The conclusions derived from analyzing the resulting models are exposed below. Specifically, the original approach consisting in using a pre-ordered distribution allowed making a detailed analysis of the frequency with which the input parameters were included in the resulting equations of regression. As found out by the analysis, the sole indicator with the prevalent effect on the BHFP level could not be distinguished for any of the modeling levels. This conclusion reveals the complexity of the law, according to which the BHFP is formed during well operation, the existence of an integrated effect

 Table 8

 Incidence rate of the indices in the models of all the levels.

Modeling level Models input parameters									
	H _{dfl}	P_{3an}	W	Q_1	Q_{o}	H_{owc}	H_{pump}	H_{pd}	Pr
One		0.142	0.142		0.142	0.142	0.142	0.142	0.142
Two	0.136	0.136	0.136	0.090	0.113	0.136	0.136	0.045	0.068
Three	0.121	0.121	0.090	0.121	0.090	0.121	0.090	0.121	0.121
Four	0.147	0.132	0.102	0.132	0.102	0.088	0.132	0.102	0.068
Total	0.131	0.131	0.111	0.111	0.105	0.111	0.125	0.095	0.079

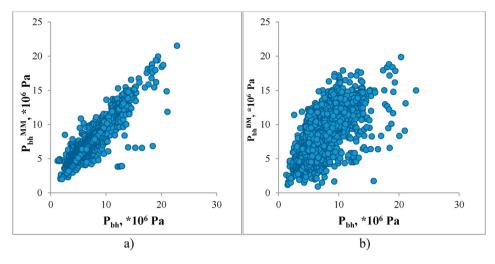


Fig. 1. Field of correlation (whole sample) of the actual BHFP and the BHFP calculated by the technique based on multivariate models (a) and by the one based of calculating the gasliquid mixture density (b).

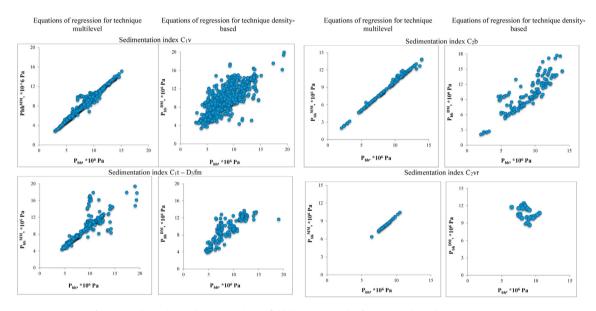


Fig. 2. Actual-to-calculated BHFP correlation fields by the example of the Un'vinskoye deposit occurrences.

of the input parameters on the BHFP, and the expediency of using these parameters by applying the built multivariate models of all the levels.

Another characteristic feature of this paper is that the models were constructed for several levels, with different degrees of differentiating modeled objects. The chosen approach is evaluated for correctness by analyzing the values of multiple correlation coefficients R, one of the major indicators characterizing the functionality of a derived model. The model for level one has R=0.763. The average R for the models of levels two, three, and four is 0.790, 0.801, and 0.822, respectively. That is, the model of each subsequent level has a higher degree of functionality.

To consider the established complex effect of the input parameters on the predicted BHFP level, it is proposed to use all of the modeling levels in an integrated manner, by constructing a general multivariate model. This model has very high performance capabilities, for example, multiple correlation coefficient R of 0.941. Thus using all of the distinguished levels of multivariate mathematical modeling has allowed deriving a functional multivariate

model the application of which as the mathematical basis of the respective technique will allow determining the BHFP during well operation with a high degree of certainty.

The certainty of determining the BHFP by the technique based on applying the elaborated multilevel multivariate mathematical models was evaluated by a special detailed analysis.

It included comparing the actual (measured) BHFP with the BHFP calculated by the elaborated technique, and the BHFP calculated by the technique currently applied in the region and based on determining the density of the gas-liquid mixture in the wellbore. To derive the most valid conclusions, we made the comparison at different differentiation levels and by means of various tools, including visual analysis of the correlation fields, and derivation and analysis of the equations of regression among the actual BHFP and the BHFP calculated by the two techniques.

The comparative visual analysis of the fields of correlation between the actual and the calculated BHFP allows concluding that the elaborated technique based on applying multilevel multivariate models is characterized by an essentially higher accuracy of

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Table 9 Equations of regression between the actual BHFP and the BHFP calculated by the two techniques.

Type and amount of data, sedimentation index	Equations of regression for technique			
	multilevel	density-based		
First level of comparison				
Whole sample	$P_{bh}^{MM} = 0.840 + 0.893 P_{bh}$.	$P_{bh}^{DM} = 2.309 + 0.791P_{bh}$		
	r = 0.945. $p < 0.0000$	r = 0.671. $p < 0/0000$		
	$S_0 = 0.893 \text{ MPa}$	$S_0 = 2.068 \text{ MPa}$		
Second level of comparison Un'vinskoye deposit				
$C_1t - D_3fm \ n = 174$	$P_{bh}^{MM} = 0.088 + 0.993 P_{bh}$	$P_{bh}^{DM} = 1.633 + 0.856P_{bh}$		
	r = 0.998. $p < 0.0000$	r = 0.847. $p < 0.0000$		
	$S_0 = 0.158 \text{ MPa}$	$S_0 = 1.491 \text{ MPa}$		
$C_1 v n = 889$	$P_{bh}^{MM} = 0.032 + 0.996P_{bh}$	$P_{bh}^{DM} = 2.561 + 0.823P_{bh}$		
	r = 0.997, $p < 0.0000$	r = 0.770. $p < 0.0000$		
	$S_0 = 0.189 \text{ MPa}$	$S_0 = 1.670 \text{ MPa}$		
$C_2b \ n=143$	$P_{bh}^{MM} = 0.144 + 0.988 P_{bh}.$	$P_{bh}^{DM} = 0.739 + 1.042P_{bh}$		
	r = 0.997. $p < 0.0000$	r = 0.862. $p < 0.0000$		
	$S_0 = 0.216 \text{ MPa}$	$S_0 = 1.660 \text{ MPa}$		
$C_2 vr n = 31$	$P_{bh}^{MM} = -0.013 + 0.988 P_{bh}$	$P_{bh}^{DM} = 14.369 - 0.424 P_{bh}$		
	r = 0.998. $p < 0.0000$	r = 0.374. $p < 0.0378$		
	$S_0 = 0.045 \text{ MPa}$	$S_0 = 0.968 \text{ MPa}$		
Chashkinskoye deposit				
$C_1t - D_3fm \ n = 89$	$P_{bh}^{MM} = 0.513 + 0.946 P_{bh}$	$P_{bh}^{DM} = 2.704 + 0.710P_{bh}$		
	r = 0.972. $p < 0.0000$	r = 0.876. $p < 0.0000$		
	$S_0 = 0.713 \text{ MPa}$	$S_0 = 1.225 \text{ MPa}$		
$C_1 v n = 161$	$P_{bh}^{MM} = 2.476 + 0.750 P_{bh}$	$P_{bh}^{DM} = 5.955 + 0.467 P_{bh}$		
	r = 0.865. $p < 0.0000$	r = 0.497. $p < 0.0000$		
	$S_0 = 0.965 \text{ MPa}$	$S_0 = 2.272 \text{ MPa}$		
Ozernoye deposit				
$C_1t - D_3fm \ n = 579$	$P_{bh}^{MM} = 1.746 + 0.727 P_{bh}$	$P_{bh}^{DM} = 0.612 + 1.124 P_{bh}$		
	r = 0.852. $p < 0.0000$	r = 0.617. $p < 0.0000$		
	$S_0 = 0.655 \text{ MPa}$	$S_0 = 2.107 \text{ MPa}$		
$C_2b \ n=99$	$P_{bh}^{MM} = 0.241 + 0.958 P_{bh}$	$P_{bh}^{DM} = -0.226 + 0.932P_{bh}$		
	r = 0.979. $p < 0.0000$	r = 0.964. $p < 0.0000$		
	$S_0 = 0.268 \text{ MPa}$	$S_0 = 0.347 \text{ MPa}$		
Magovskoye deposit	104	-14		
$C_1 t - D_3 fm n = 123$	$P_{bh}^{MM} = 1.063 + 0.890 P_{bh}$	$P_{bh}^{DM} = 5.136 + 0.495 P_{bh}$		
	r = 0.943. $p < 0.0000$	r = 0.689. $p < 0.0000$		
	$S_0 = 1.304 \text{ MPa}$	$S_0 = 2.172 \text{ MPa}$		
$C_2b \ n = 33$	$P_{bh}^{MM} = 1.893 + 0.640 P_{bh}$	$P_{bh}^{DM} = 2.488 + 0.901P_{bh}$		
	r = 0.799. $p < 0.0000$	r = 0.640. $p < 0.0000$		
	$S_0=0.681\; MPa$	$S_0 = 1.532 \text{ MPa}$		
Gagarinskoye deposit	201	DW.		
$C_1t - D_3fm \ n = 288$	$P_{bh}^{MM} = 3.182 + 0.570 P_{bh}$	$P_{bh}^{DM} = 3.635 + 0.598P_{bh}$		
	r = 0.754. $p < 0.0000$	r = 0.724. $p < 0.0000$		
	S ₀ = 1.568 MPa	$S_0 = 1.791 \text{ MPa}$		
$C_2b \ n=193$	$P_{bh}^{MM} = 0.928 + 0.837 P_{bh}$	$P_{bh}^{DM} = 2.691 + 0.534 \; P_{bh}$		
	r = 0.901. $p < 0.0000$	r = 0.653. $p < 0.0000$		
	$S_0 = 1.053 \text{ MPa}$	$S_0 = 1.680 \text{ MPa}$		
Shershnevskoye deposit	201	DW.		
$C_1 t - D_3 fm n = 152$	$P_{bh}^{MM} = 2.847 + 0.532 P_{bh}$	$P_{bh}^{DM} = 1.618 + 0.445 P_{bh}$		
	r = 0.716. $p < 0.0000$	r = 0.389. $p < 0.0000$		
	$S_0 = 0.694 \text{ MPa}$	$S_0 = 1.429 \text{ MPa}$		
$C_1 v n = 112$	$P_{bh}^{MM} = 1.852 + 0.798 P_{bh}$	$P_{bh}^{DM} = 3.079 + 0.599 P_{bh}$		
	r = 0.893. $p < 0.0000$	r = 0.594. $p < 0.0000$		
	$S_0 = 1.344 \text{ MPa}$	$S_0 = 2.716 \text{ MPa}$		
Sukharev deposit	pMM	rDM 222		
$C_1 t - D_3 fm \ n = 50$	$P_{bh}^{MM} = 0.535 + 0.948 P_{bh}$	$P_{bh}^{DM} = 0.004 + 0.925 P_{bh}$		
	r = 0.976. $p < 0.0000$	r = 0.947, $p < 0.0000$		
	$S_0 = 0.886 \text{ MPa}$	$S_0 = 1.240 \text{ MPa}$		
$C_1 v n = 61$	$P_{bh}^{MM} = 0.917 + 0.917 P_{bh}$	$P_{bh}^{DM} = 1.495 + 0.800P_{bh}$		
	r = 0.957, $p < 0.0000$	r = 0.737. $p < 0.0000$		
0.1	$S_0 = 0.651 \text{ MPa}$	$S_0 = 1.728 \text{ MPa}$		
$C_2b \ n=15$	$P_{bh}^{MM} = 2.013 + 0.802P_{bh}$	$P_{bh}^{DM} = 6.005 + 0.305 P_{bh}$		
	r = 0.895, p < 0.0000	r = 0.358. $p < 0.0000$		
	$S_0 = 1.048 \text{ MPa}$	$S_0 = 2.088 \text{ MPa}$		

calculation: the correlation field for the elaborated technique has a much tighter and even shape, its points group around the line with a slope close to one. The derived regularity is typical of both, the correlation fields drawn for the sample in general and for the fields drawn individually for the occurrences from separate deposits.

The visual analysis of the correlation fields has allowed

evaluating by comparison the certainty of determining the BHFP by the two techniques at the level of quality. The quantitative comparison of these fields has made it necessary to derive the equations of regression between the actual and the calculated BHFP for the two levels of investigation as well, i.e., for the sample in general (level one) and, individually, for occurrences in separate deposits

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(level two). The sign of the higher certainty of a particular technique is that the value of the free term in the equation of regression is close to zero and the angular ratio close to one. In addition to the regression equation parameters, their statistical characteristics have been calculated as well, including the correlation coefficient, significance level, and standard calculation error. As shown by analyzing the statistical characteristics of the exploitation targets from all of the deposits, not only the values of correlation coefficient r differ in all of the four cases but the equation of regression themselves. In all of the cases the coefficients at P_{BHFP} found by the multilevel technique are higher than those found by the densitybased technique. The standard errors calculated according to the multivariate models for all of the exploitation targets are much lower than the standard errors calculated by the density-based technique. As shown by comparing the average reduced characteristics values against the t criterion, statistical differences are found in each case. The enumerated facts convincingly prove that the BHFP determination by the elaborated technique based on applying multivariate multilevel (statistical) models has a higher degree of certainty.

5. Conclusions

This article validates the technique of determining the BHFP during oil-production well operation by means of the constructed multivariate multilevel models.

- The models were constructed proceeding from the significant accumulated experience in parallel depth and estuarine measurements conducted when servicing the commercial wells in the Perm Krai. The constructed models have high statistical capability characteristics. A distinct feature of the models is that the parameters they use as the sole original data are easy to determine in practice. This fact should be considered the main strength of the developed technique as compared with its multiple density-based counterparts.
- The high capability of the constructed multivariate BHFP models is mainly stipulated by the original approach to making them that consists in creating a model according to a sequence of preordered original data.
- Not only has the construction of multivariate mathematical models allowed determining the BHFP in practice but it has also allowed identifying the regularities of its formation and inoperation behavior individually for each considered exploitation target.
- The BHFP determination technique based on the developed multivariate models is much more functional than its conventional density-based counterparts.
- The developed technique has application limitations. It can only be used in cases where the source data are within the ranges shown in Tables 5 and 6 If the initial data does not correspond to the specified ranges, then it is necessary to correct the calculated equations according to the same scheme that was used in their initial construction.
- It is worth noting individually that the new technique should not be considered an alternative to density-based methods. The joint application of these techniques is supposed to ensure a reliable BHFP control during production well operation.

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CRediT authorship contribution statement

Inna N. Ponomareva: investigation, writing the original draft. Vladislav I. Galkin: discussion of results, revision and editing of the manuscript. Dmitriy A. Martyushev: data curation, methodology, writing.

Declaration of competing interest

The authors declare that they have no known conflict of interests, competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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