

# 第五章 机器人速度与雅可比

Chapter 5 Instantaneous Kinematics

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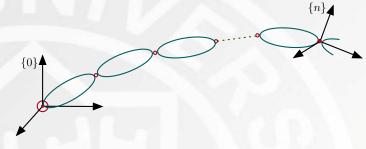
2021年4月9日



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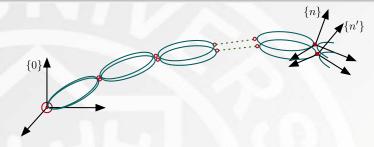






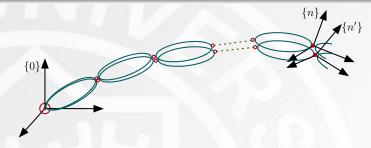
• Forward Kinematics:  $\theta \to x$ 





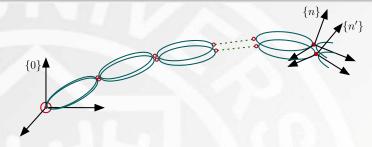
- Forward Kinematics:  $\theta \rightarrow x$
- Instantaneous Kinematics:





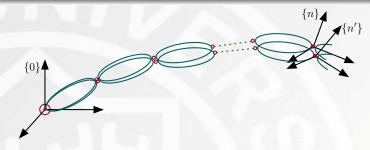
- Forward Kinematics:  $\theta \to x$
- Instantaneous Kinematics:  $\theta + \delta\theta \rightarrow x + \delta x$





- Forward Kinematics:  $\theta \rightarrow x$
- Instantaneous Kinematics:  $\theta + \delta\theta \rightarrow x + \delta x$
- Relationship:  $\delta\theta \leftrightarrow \delta x$





- Forward Kinematics:  $\theta \to x$
- Instantaneous Kinematics:  $\theta + \delta\theta \rightarrow x + \delta x$
- Relationship:  $\delta\theta \leftrightarrow \delta x$

$$\frac{\dot{ heta}\leftrightarrow\dot{x}}{ heta}$$
 Linear Velocity

Angular Velocity



# Jacobian

- Differential Motion
- Linear & Angular Motion
- Velocity Propagation
- Explicit Form
- Static Forces



$$\text{coordinate-}i: \left\{ \begin{array}{ll} \theta_i & \text{Revolute joint} \\ d_i & \text{Prismatic joint} \end{array} \right.$$



$$\text{coordinate-} i: \left\{ \begin{array}{ll} \theta_i & \text{Revolute joint} \\ d_i & \text{Prismatic joint} \end{array} \right.$$

Joint coordinate-i:

$$q_i = \bar{\varepsilon}_i \theta_i + \varepsilon_i d_i$$



$$\text{coordinate-} i: \left\{ \begin{array}{ll} \theta_i & \text{Revolute joint} \\ d_i & \text{Prismatic joint} \end{array} \right.$$

Joint coordinate-i:  $q_i = \bar{\varepsilon}_i \theta_i + \varepsilon_i d_i$ 

$$q_i = \bar{\varepsilon}_i \theta_i + \varepsilon_i d_i$$

$$\text{with} \quad \varepsilon_i = \begin{cases} 0 & \text{Revolute joint} \\ 1 & \text{Prismatic joint} \end{cases}$$
 and 
$$\bar{\varepsilon}_i = 1 - \varepsilon_i$$



$$\text{coordinate-} i: \left\{ \begin{array}{l} \theta_i & \text{Revolute joint} \\ d_i & \text{Prismatic joint} \end{array} \right.$$

Joint coordinate-
$$i$$
:  $q_i = \bar{\varepsilon}_i \theta_i + \varepsilon_i d_i$ 

$$\text{with} \quad \varepsilon_i = \left\{ \begin{array}{ll} 0 & \text{Revolute joint} \\ 1 & \text{Prismatic joint} \end{array} \right.$$
 and 
$$\bar{\varepsilon}_i = 1 - \varepsilon_i$$

Joint Coordinate Vector: 
$$q=(q_1,\ q_2,\ \cdots,\ q_n)$$



$$x = f(q);$$



$$x = f(q); \quad \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{pmatrix} = \begin{pmatrix} f_1(q) \\ f_2(q) \\ \vdots \\ f_m(q) \end{pmatrix}$$



$$x = f(q); \quad \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{pmatrix} = \begin{pmatrix} f_1(q) \\ f_2(q) \\ \vdots \\ f_m(q) \end{pmatrix}$$

$$\begin{split} \delta x_1 &= \frac{\partial f_1}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_1}{\partial q_n} \delta q_n \\ \vdots \\ \delta x_m &= \frac{\partial f_m}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_m}{\partial q_n} \delta q_n \end{split}$$



$$x = f(q); \quad \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{pmatrix} = \begin{pmatrix} f_1(q) \\ f_2(q) \\ \vdots \\ f_m(q) \end{pmatrix}$$

$$\delta x_1 = \frac{\partial f_1}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_1}{\partial q_n} \delta q_n$$

$$\vdots \quad \delta x_m = \frac{\partial f_m}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_m}{\partial q_n} \delta q_n$$

$$\delta x = \begin{bmatrix} \frac{\partial f_1}{\partial q_1} & \dots & \frac{\partial f_1}{\partial q_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_m}{\partial q_1} & \dots & \frac{\partial f_m}{\partial q_n} \end{bmatrix} \delta q_n$$



$$x = f(q); \quad \begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{pmatrix} = \begin{pmatrix} f_1(q) \\ f_2(q) \\ \vdots \\ f_m(q) \end{pmatrix}$$
 
$$\delta x_1 = \frac{\partial f_1}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_1}{\partial q_n} \delta q_n$$
 
$$\vdots \qquad \delta x_m = \frac{\partial f_m}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_m}{\partial q_n} \delta q_n$$
 
$$\delta x_m = \frac{\partial f_m}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_m}{\partial q_n} \delta q_n$$
 
$$\delta x_m = \frac{\partial f_m}{\partial q_1} \delta q_1 + \dots + \frac{\partial f_m}{\partial q_n} \delta q_n$$

$$\delta x_{(m\times 1)} = J_{(m\times n)}(q) \delta q_{(n\times 1)}$$



# Jacobian

$$\delta x_{(m\times 1)} = J_{(m\times n)}(q) \delta q_{(n\times 1)}$$



# Jacobian

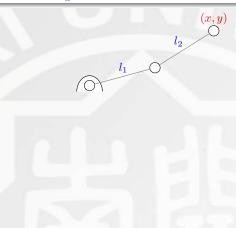
$$\delta x_{(m\times 1)} = J_{(m\times n)}(q)\delta q_{(n\times 1)}$$

$$\dot{x}_{(m\times 1)} = J_{(m\times n)}(q)\dot{q}_{(n\times 1)}$$

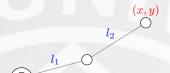
where

$$J_{ij}(q) = \frac{\partial}{\partial q_j} f_i(q)$$



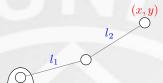






$$x = l_1 c_1 + l_2 c_{12}$$
$$y = l_1 s_1 + l_2 s_{12}$$

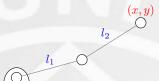




$$x = l_1 c_1 + l_2 c_{12}$$
$$y = l_1 s_1 + l_2 s_{12}$$

$$\begin{split} \delta x &= -(l_1s_1 + l_2s_{12})\delta\theta_1 - l_2s_{12}\delta\theta_2 \\ \delta y &= (l_1c_1 + l_2c_{12})\delta\theta_1 + l_2c_{12}\delta\theta_2 \\ \delta X &= \begin{bmatrix} \delta x \\ \delta y \end{bmatrix} = \begin{bmatrix} -y & -l_2s_{12} \\ x & l_2c_{12} \end{bmatrix} \begin{bmatrix} \delta\theta_1 \\ \delta\theta_2 \end{bmatrix} \end{split}$$



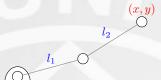


$$\begin{aligned} x &= l_1 c_1 + l_2 c_{12} \\ y &= l_1 s_1 + l_2 s_{12} \end{aligned}$$

$$\begin{split} \delta x &= -(l_1 s_1 + l_2 s_{12}) \delta \theta_1 - l_2 s_{12} \delta \theta_2 \\ \delta y &= (l_1 c_1 + l_2 c_{12}) \delta \theta_1 + l_2 c_{12} \delta \theta_2 \\ \delta X &= \begin{bmatrix} \delta x \\ \delta y \end{bmatrix} = \begin{bmatrix} -y & -l_2 s_{12} \\ x & l_2 c_{12} \end{bmatrix} \begin{bmatrix} \delta \theta_1 \\ \delta \theta_2 \end{bmatrix} \end{split}$$

$$\delta X = J(\theta) \delta \theta$$





$$\begin{aligned} x &= l_1 c_1 + l_2 c_{12} \\ y &= l_1 s_1 + l_2 s_{12} \end{aligned}$$

$$\delta x = -(l_1 s_1 + l_2 s_{12}) \delta \theta_1 - l_2 s_{12} \delta \theta_2$$

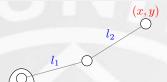
$$\delta y = (l_1 c_1 + l_2 c_{12}) \delta \theta_1 + l_2 c_{12} \delta \theta_2$$

$$\delta X = \begin{bmatrix} \delta x \\ \delta y \end{bmatrix} = \begin{bmatrix} -y & -l_2 s_{12} \\ x & l_2 c_{12} \end{bmatrix} \begin{bmatrix} \delta \theta_1 \\ \delta \theta_2 \end{bmatrix}$$

$$\delta X = J(\theta)\delta\theta$$

$$\dot{X} = J(\theta)\dot{\theta}$$





$$\begin{aligned} x &= l_1 c_1 + l_2 c_{12} \\ y &= l_1 s_1 + l_2 s_{12} \end{aligned}$$

$$\delta x = -(l_1 s_1 + l_2 s_{12}) \delta \theta_1 - l_2 s_{12} \delta \theta_2$$

$$\delta y = (l_1 c_1 + l_2 c_{12}) \delta \theta_1 + l_2 c_{12} \delta \theta_2$$

$$\delta X = \begin{bmatrix} \delta x \\ \delta y \end{bmatrix} = \begin{bmatrix} -y & -l_2 s_{12} \\ x & l_2 c_{12} \end{bmatrix} \begin{bmatrix} \delta \theta_1 \\ \delta \theta_2 \end{bmatrix}$$

$$\delta X = J(\theta)\delta\theta$$

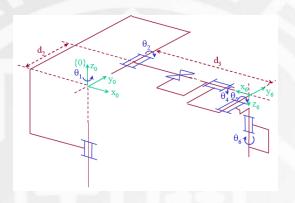
$$\dot{X} = J(\theta)\dot{\theta}$$

$$J = \begin{bmatrix} \frac{\partial x}{\partial \theta_1} & \frac{\partial x}{\partial \theta_2} \\ \frac{\partial y}{\partial \theta_1} & \frac{\partial y}{\partial \theta_2} \end{bmatrix} = \begin{bmatrix} -y & -l_2 s_{12} \\ x & l_2 c_{12} \end{bmatrix}$$









#### Table: DH 参数

i	$\alpha_{i-1}$	$a_{i-1}$	$d_{i}$	$ heta_i$
1	0	0	0	$\theta_1$
2	-90	0	$d_2$	$\theta_2$
3	90	0	$d_3$	0
4	0	0	0	$\theta_4$
5	-90	0	0	$\theta_5$
6	90	0	0	$\theta_6$
	1 2 3 4 5	1 0 2 -90 3 90 4 0 5 -90	1 0 0 2 -90 0 3 90 0 4 0 0 5 -90 0	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$



$$X = \begin{bmatrix} X_P \\ r_1 \\ r_2 \\ r_3 \end{bmatrix} = \begin{bmatrix} d_3C_1S_2 - d_2S_1 \\ d_3S_1S_2 + d_2C_1 \\ d_3C_2 \\ C_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] - S_1(S_4C_5C_6 + C_4S_6) \\ S_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] + C_1(S_4C_5C_6 + C_4S_6) \\ -S_2(C_4C_5C_6 - S_4S_6) - C_2S_5C_6 \\ C_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6] - S_1(-S_4C_5S_6 + C_4C_6) \\ S_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6) + C_1(-S_4C_5S_6 + C_4C_6) \\ S_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6 \\ C_1(C_2C_4S_5 + S_2C_5) - S_1S_4S_5 \\ S_1(C_2C_4S_5 + S_2C_5) + C_1S_4S_5 \\ -S_2C_4S_5 + C_2C_5 \end{bmatrix}$$



$$X_P = \begin{bmatrix} d_3C_1S_2 - d_2S_1 \\ d_3S_1S_2 + d_2C_1 \\ d_3C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} & & & & & & \\ & \dot{x} \end{bmatrix}$$

$$\left. \begin{array}{c} q_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{array} \right]$$



$$X_P = \begin{bmatrix} d_3C_1S_2 - d_2S_1 \\ d_3S_1S_2 + d_2C_1 \\ d_3C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y \\ x \\ 0 \end{bmatrix}$$



$$X_P = \begin{bmatrix} d_3C_1S_2 - d_2S_1 \\ d_3S_1S_2 + d_2C_1 \\ d_3C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y & c_1c_2d_3 \\ x & s_1c_2d_3 \\ 0 & -s_2d_3 \end{bmatrix}$$

$$\begin{bmatrix} q_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$



$$X_P = \begin{bmatrix} d_3 C_1 S_2 - d_2 S_1 \\ d_3 S_1 S_2 + d_2 C_1 \\ d_3 C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y & c_1c_2d_3 & c_1s_2 \\ x & s_1c_2d_3 & s_1s_2 \\ 0 & -s_2d_3 & c_2 \end{bmatrix}$$

$$\begin{bmatrix} q_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$



$$X_P = \begin{bmatrix} d_3 C_1 S_2 - d_2 S_1 \\ d_3 S_1 S_2 + d_2 C_1 \\ d_3 C_2 \end{bmatrix}$$

$$\dot{X}_{P} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y & c_{1}c_{2}d_{3} & c_{1}s_{2} & 0 & 0 & 0 \\ x & s_{1}c_{2}d_{3} & s_{1}s_{2} & 0 & 0 & 0 \\ 0 & -s_{2}d_{3} & c_{2} & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_{1} \\ \dot{q}_{2} \\ \dot{q}_{3} \\ \dot{q}_{4} \\ \dot{q}_{5} \\ \dot{q}_{6} \end{bmatrix}$$



$$X_P = \begin{bmatrix} d_3 C_1 S_2 - d_2 S_1 \\ d_3 S_1 S_2 + d_2 C_1 \\ d_3 C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0 \\ x & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0 \\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

$$\dot{X}_{P(3\times 1)} = J_{X_P(3\times 6)}(q) \dot{q}_{(6\times 1)}$$



#### Poistion:

$$X_P = \begin{bmatrix} d_3 C_1 S_2 - d_2 S_1 \\ d_3 S_1 S_2 + d_2 C_1 \\ d_3 C_2 \end{bmatrix}$$

$$\dot{X}_P = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -y & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0 \\ x & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0 \\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

$$\overrightarrow{X}_{P(3\times 1)} = J_{X_P(3\times 6)}(q) \dot{q}_{(6\times 1)}$$

Linear Velocity V



### Orientation: Direction Cosines

$$\begin{split} X_R &= \begin{bmatrix} r_1(q) \\ r_2(q) \\ r_3(q) \end{bmatrix} \\ \dot{X}_R &= J_{X_R}(q) \dot{q} \end{split}$$

$$\dot{X}_R = J_{X_R}(q)\dot{q}$$



#### **Orientation: Direction Cosines**

$$\begin{split} \dot{X}_R &= \begin{bmatrix} r_2(q) \\ r_3(q) \end{bmatrix} \\ \dot{X}_R &= J_{X_R}(q) \dot{q} \\ \\ \dot{X}_R &= \begin{bmatrix} \dot{r}_1 \\ \dot{r}_2 \\ \dot{r}_3 \end{bmatrix}_{(9 \times 1)} = \begin{bmatrix} \frac{\partial r_1}{\partial q_1} & \frac{\partial r_1}{\partial q_2} & \cdots & \frac{\partial r_1}{\partial q_6} \\ \frac{\partial r_2}{\partial q_1} & \frac{\partial r_2}{\partial q_2} & \cdots & \frac{\partial r_2}{\partial q_6} \\ \frac{\partial r_3}{\partial q_1} & \frac{\partial r_3}{\partial q_2} & \cdots & \frac{\partial r_3}{\partial q_6} \end{bmatrix}_{(9 \times 6)} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}_{(6 \times 1)} \end{split}$$



#### Stanford Scheinman Arm

$$X_R = \begin{bmatrix} r_1 \\ r_2 \\ r_3 \end{bmatrix} = \begin{bmatrix} C_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] - S_1(S_4C_5C_6 + C_4S_6) \\ S_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] + C_1(S_4C_5C_6 + C_4S_6) \\ -S_2(C_4C_5C_6 - S_4S_6) - C_2S_5C_6 \\ C_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6] - S_1(-S_4C_5S_6 + C_4C_6) \\ S_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6) + C_1(-S_4C_5S_6 + C_4C_6) \\ S_2(C_4C_5S_6 + S_4C_6) + C_2S_5S_6 \\ C_1(C_2C_4S_5 + S_2C_5) - S_1S_4S_5 \\ S_1(C_2C_4S_5 + S_2C_5) + C_1S_4S_5 \\ -S_2C_4S_5 + C_2C_5 \end{bmatrix}$$

$$\dot{X}_R = \begin{bmatrix} \dot{r}_1 \\ \dot{r}_2 \\ \dot{r}_3 \end{bmatrix}_{(9 \times 1)} = \begin{bmatrix} \frac{\partial r_1}{\partial q_1} & \frac{\partial r_1}{\partial q_2} & \cdots & \frac{\partial r_1}{\partial q_6} \\ \frac{\partial r_2}{\partial q_1} & \frac{\partial r_2}{\partial q_2} & \cdots & \frac{\partial r_2}{\partial q_6} \\ \frac{\partial r_3}{\partial q_1} & \frac{\partial r_3}{\partial q_2} & \cdots & \frac{\partial r_3}{\partial q_6} \end{bmatrix}_{(9 \times 6)} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}_{(6 \times 1)}$$

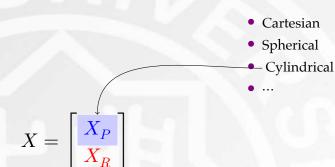


# Representations

$$X = \begin{bmatrix} X_P \\ X_R \end{bmatrix}$$

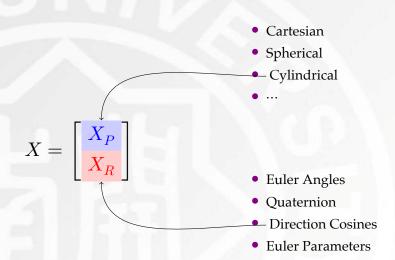


# Representations





## Representations





$$\begin{split} \dot{X}_P &= J_{X_P}(q) \dot{q} \\ \dot{X}_R &= J_{X_R}(q) \dot{q} \end{split}$$

$$\begin{bmatrix} \dot{X}_P \\ \dot{X}_R \end{bmatrix} = \begin{bmatrix} J_{X_P}(q) \\ J_{X_R}(q) \end{bmatrix} \dot{q}$$

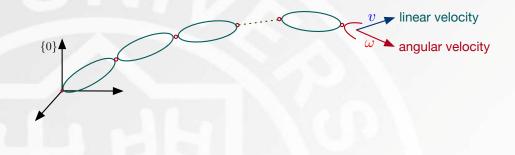
#### Cartesian & Direction Cosines:

$$\dot{X}_{(12\times 1)} = J_X(q)_{(12\times 6)} \dot{q}_{(6\times 1)}$$

The Jacobian is dependent on the representation

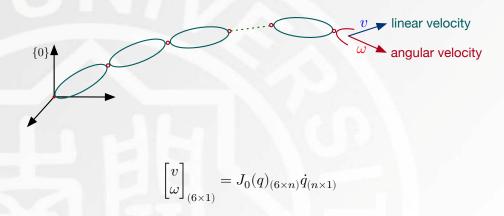


# Basic Jacobian



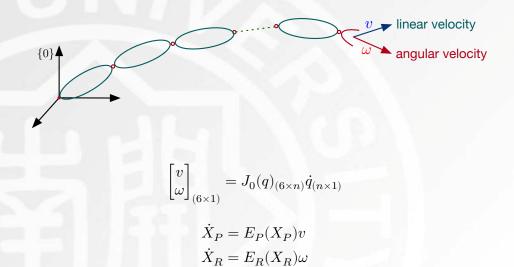


## Basic Jacobian





#### Basic Jacobian





#### Examples

$$\bullet \ X_R = \begin{bmatrix} \alpha \\ \beta \\ \gamma \end{bmatrix}; \quad E_R(X_R) = \begin{bmatrix} -\frac{c\alpha c\beta}{s\beta} & -\frac{s\alpha c\beta}{s\beta} & 1 \\ -s\alpha & c\alpha & 0 \\ \frac{c\alpha}{s\beta} & \frac{s\alpha}{s\beta} & 0 \end{bmatrix}$$

$$\bullet \ X_P = \begin{bmatrix} x \\ y \\ z \end{bmatrix}; \quad E_P(X_P) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



Given a representation 
$$X = \begin{bmatrix} X_P & X_R \end{bmatrix}^T$$

$$\dot{X} = J_X(q)\dot{q}$$



Given a representation 
$$X = \begin{bmatrix} X_P & X_R \end{bmatrix}^T$$

$$\dot{X} = J_X(q)\dot{q}$$

$$J_X(q)=E(x)J_0(q)$$



Given a representation 
$$X = \begin{bmatrix} X_P & X_R \end{bmatrix}^T$$

$$\dot{X} = J_X(q)\dot{q}$$

$$J_X(q) = E(x) J_0(q) \,$$

Basic Jacobian:

$$\begin{bmatrix} v \\ \omega \end{bmatrix} = J_0(q) \dot{q} = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix} \cdot \dot{q}$$



Given a representation 
$$X = \begin{bmatrix} X_P & X_R \end{bmatrix}^T$$

$$\dot{X} = J_X(q)\dot{q}$$

$$J_X(q) = E(x)J_0(q)$$

Basic Jacobian:

$$\begin{bmatrix} v \\ \omega \end{bmatrix} = J_0(q) \dot{q} = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix} \cdot \dot{q}$$

$$\begin{split} \dot{X}_P &= E_P(X_P) v \Rightarrow \dot{X}_P = (E_P \cdot J_v) \dot{q} \\ \dot{X}_R &= E_R(X_R) \omega \Rightarrow \dot{X}_R = (E_R \cdot J_\omega) \dot{q} \end{split}$$

$$J_{X_P} = E_P \cdot J_{v\prime} \quad J_{X_R} = E_R \cdot J_{\omega}$$



$$J = \begin{bmatrix} J_{X_P} \\ J_{X_R} \end{bmatrix} = \begin{bmatrix} E_P & 0 \\ 0 & E_R \end{bmatrix} \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$





$$J = \begin{bmatrix} J_{X_P} \\ J_{X_R} \end{bmatrix} = \begin{bmatrix} E_P & 0 \\ 0 & E_R \end{bmatrix} \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$
 $J(q) = E(x) J_0(q)$ 



$$J = \begin{bmatrix} J_{X_P} \\ J_{X_R} \end{bmatrix} = \begin{bmatrix} E_P & 0 \\ 0 & E_R \end{bmatrix} \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$

$$J(q) = E(x) J_0(q)$$



$$J = \begin{bmatrix} J_{X_P} \\ J_{X_R} \end{bmatrix} = \begin{bmatrix} E_P & 0 \\ 0 & E_R \end{bmatrix} \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$

$$J(q) = E(x) J_0(q)$$

With Cartesian Coordinates:

$$J_{X_P} = J_v \Rightarrow E_P = I_3$$

and

$$E = \begin{bmatrix} I & 0 \\ 0 & E_R \end{bmatrix}$$



• Cartesian Coordinates (x, y, z)

$$E_P(X) = I_3$$

• Cylindrical Coordinates  $(\rho, \theta, z)$  Using

$$\begin{pmatrix} x & y & z \end{pmatrix}^T = \begin{pmatrix} \rho \cos \theta & \rho \sin \theta & z \end{pmatrix}^T$$



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$$\begin{cases} \rho = \sqrt{x^2 + y^2} \\ \theta = \arctan(y/x) \\ z = z \end{cases}$$



• Cartesian Coordinates (x, y, z)

$$E_P(X) = I_3$$

• Cylindrical Coordinates  $(\rho, \theta, z)$  Using

$$\begin{pmatrix} x & y & z \end{pmatrix}^T = \begin{pmatrix} \rho \cos \theta & \rho \sin \theta & z \end{pmatrix}^T$$

$$\begin{cases} \rho = \sqrt{x^2 + y^2} \\ \theta = \arctan(y/x) \quad \Rightarrow \quad E_P(X) = \begin{pmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta/\rho & \cos \theta/\rho & 0 \\ 0 & 0 & 1 \end{pmatrix} \end{cases}$$



• Spherical Coordinates  $(\rho, \, \theta, \, \phi)$  Using

$$\begin{pmatrix} x & y & z \end{pmatrix}^T = \begin{pmatrix} \rho \cos \theta \sin \phi & \rho \sin \theta \sin \phi & \rho \cos \phi \end{pmatrix}^T$$





• Spherical Coordinates  $(\rho, \, \theta, \, \phi)$  Using

$$(x \ y \ z)^T = (\rho \cos \theta \sin \phi \ \rho \sin \theta \sin \phi \ \rho \cos \phi)^T$$

$$\begin{cases} \rho = \sqrt{x^2 + y^2 + z^2} \\ \theta = \arctan(y/x) \\ \phi = \arctan\sqrt{x^2 + y^2}/z \end{cases}$$



• Spherical Coordinates  $(\rho, \theta, \phi)$  Using

$$(x \ y \ z)^T = (\rho \cos \theta \sin \phi \ \rho \sin \theta \sin \phi \ \rho \cos \phi)^T$$

$$\begin{cases} \rho = \sqrt{x^2 + y^2 + z^2} \\ \theta = \arctan(y/x) \\ \phi = \arctan\sqrt{x^2 + y^2}/z \end{cases}$$

$$\Rightarrow \quad E_P(X) = \begin{pmatrix} \cos\theta\sin\phi & \sin\theta\sin\phi & \cos\phi \\ -\sin\theta/(\rho\sin\phi) & \cos\theta/(\rho\sin\phi) & 0 \\ \cos\theta\cos\phi/\rho & \sin\theta\cos\phi/\rho & -\sin\phi/\rho \end{pmatrix}$$





$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$



$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \ \Rightarrow R(t + \Delta t) = R_K(\Delta \theta) R(t)$$



$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \\ \Rightarrow R(t + \Delta t) = R_K(\Delta \theta) \\ R(t) \Rightarrow \dot{R} = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \\ R(t) \right)$$



$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \\ \Rightarrow R(t + \Delta t) = R_K(\Delta \theta) \\ R(t) \Rightarrow \dot{R} = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \\ R(t) \right)$$

$$R_K(\Delta\theta) - I_3 = \begin{bmatrix} k_x k_x v \Delta\theta + c \Delta\theta - 1 & k_x k_y v \Delta\theta - k_z s \Delta\theta & k_x k_z v \Delta\theta + k_y s \Delta\theta \\ k_x k_y v \Delta\theta + k_z s \Delta\theta & k_y k_y v \Delta\theta + c \Delta\theta - 1 & k_y k_z v \Delta\theta - k_x s \Delta\theta \\ k_x k_z v \Delta\theta - k_y s \Delta\theta & k_y k_z v \Delta\theta + k_x s \Delta\theta & k_z k_z v \Delta\theta + c \Delta\theta - 1 \end{bmatrix}$$



• Direction Cosines:  $\dot{r}_{11}, \dot{r}_{12}, \cdots, \dot{r}_{33}$ :

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \ \Rightarrow R(t + \Delta t) = R_K(\Delta \theta) \\ R(t) \Rightarrow \dot{R} = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \\ R(t) \right)$$

$$R_K(\Delta\theta) - I_3 = \begin{bmatrix} k_x k_x v \Delta\theta + c \Delta\theta - 1 & k_x k_y v \Delta\theta - k_z s \Delta\theta & k_x k_z v \Delta\theta + k_y s \Delta\theta \\ k_x k_y v \Delta\theta + k_z s \Delta\theta & k_y k_y v \Delta\theta + c \Delta\theta - 1 & k_y k_z v \Delta\theta - k_x s \Delta\theta \\ k_x k_z v \Delta\theta - k_y s \Delta\theta & k_y k_z v \Delta\theta + k_x s \Delta\theta & k_z k_z v \Delta\theta + c \Delta\theta - 1 \end{bmatrix}$$

When  $\Delta\theta \to 0$ , then  $c\Delta\theta \to 1$ ,  $s\Delta\theta \to \Delta\theta$ ,  $v\Delta\theta = 1 - c\Delta\theta \to 0$ , the following equation could be obtained:



• Direction Cosines:  $\dot{r}_{11}, \dot{r}_{12}, \cdots, \dot{r}_{33}$ :

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \ \Rightarrow R(t + \Delta t) = R_K(\Delta \theta) \\ R(t) \Rightarrow \dot{R} = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \\ R(t) \right)$$

$$R_K(\Delta\theta) - I_3 = \begin{bmatrix} k_x k_x v \Delta\theta + c \Delta\theta - 1 & k_x k_y v \Delta\theta - k_z s \Delta\theta & k_x k_z v \Delta\theta + k_y s \Delta\theta \\ k_x k_y v \Delta\theta + k_z s \Delta\theta & k_y k_y v \Delta\theta + c \Delta\theta - 1 & k_y k_z v \Delta\theta - k_x s \Delta\theta \\ k_x k_z v \Delta\theta - k_y s \Delta\theta & k_y k_z v \Delta\theta + k_x s \Delta\theta & k_z k_z v \Delta\theta + c \Delta\theta - 1 \end{bmatrix}$$

When  $\Delta\theta \to 0$ , then  $c\Delta\theta \to 1$ ,  $s\Delta\theta \to \Delta\theta$ ,  $v\Delta\theta = 1 - c\Delta\theta \to 0$ , the following equation could be obtained:

$$R_K(\Delta\theta) - I_3 = \begin{bmatrix} 0 & -k_z\Delta\theta & k_y\Delta\theta \\ k_z\Delta\theta & 0 & -k_x\Delta\theta \\ -k_y\Delta\theta & k_x\Delta\theta & 0 \end{bmatrix}$$



• Rigid angular velocity and the direction cosines:

$$\begin{split} \dot{R} &= \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} R(t) \right) = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \right) R(t) \\ R_K(\Delta \theta) - I_3 &= \begin{bmatrix} 0 & -k_z \Delta \theta & k_y \Delta \theta \\ k_z \Delta \theta & 0 & -k_x \Delta \theta \\ -k_y \Delta \theta & k_x \Delta \theta & 0 \end{bmatrix} \end{split}$$



• Rigid angular velocity and the direction cosines:

$$\begin{split} \dot{R} &= \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} R(t) \right) = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \right) R(t) \\ R_K(\Delta \theta) - I_3 &= \begin{bmatrix} 0 & -k_z \Delta \theta & k_y \Delta \theta \\ k_z \Delta \theta & 0 & -k_x \Delta \theta \\ -k_y \Delta \theta & k_x \Delta \theta & 0 \end{bmatrix} \\ \dot{R} &= \begin{bmatrix} 0 & -k_z \dot{\theta} & k_y \dot{\theta} \\ k_z \dot{\theta} & 0 & -k_x \dot{\theta} \\ -k_y \dot{\theta} & k_x \dot{\theta} & 0 \end{bmatrix} R(t) \end{split}$$



• Rigid angular velocity and the direction cosines:

$$\begin{split} \dot{R} &= \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} R(t) \right) = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \right) R(t) \\ R_K(\Delta \theta) - I_3 &= \begin{bmatrix} 0 & -k_z \Delta \theta & k_y \Delta \theta \\ k_z \Delta \theta & 0 & -k_x \Delta \theta \\ -k_y \Delta \theta & k_x \Delta \theta & 0 \end{bmatrix} \\ \dot{R} &= \begin{bmatrix} 0 & -k_z \dot{\theta} & k_y \dot{\theta} \\ k_z \dot{\theta} & 0 & -k_x \dot{\theta} \\ -k_y \dot{\theta} & k_x \dot{\theta} & 0 \end{bmatrix} R(t) \Rightarrow \begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ -\Omega_y & \Omega_x & 0 \end{bmatrix} = \hat{\Omega} = \dot{R} R^{-1} \end{split}$$



Rigid angular velocity and the direction cosines:

$$\begin{split} \dot{R} &= \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} R(t) \right) = \lim_{\Delta t \to 0} \left( \frac{R_K(\Delta \theta) - I_3}{\Delta t} \right) R(t) \\ R_K(\Delta \theta) - I_3 &= \begin{bmatrix} 0 & -k_z \Delta \theta & k_y \Delta \theta \\ k_z \Delta \theta & 0 & -k_x \Delta \theta \\ -k_y \Delta \theta & k_x \Delta \theta & 0 \end{bmatrix} \\ \dot{R} &= \begin{bmatrix} 0 & -k_z \dot{\theta} & k_y \dot{\theta} \\ k_z \dot{\theta} & 0 & -k_z \dot{\theta} \\ -k_y \dot{\theta} & k_x \dot{\theta} & 0 \end{bmatrix} R(t) \Rightarrow \begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ -\Omega_y & \Omega_x & 0 \end{bmatrix} = \hat{\Omega} = \dot{R} R^{-1} \\ \Rightarrow \begin{cases} \Omega_x &= \dot{r}_{31} r_{21} + \dot{r}_{32} r_{22} + \dot{r}_{33} r_{23} \\ \Omega_y &= \dot{r}_{11} r_{31} + \dot{r}_{12} r_{32} + \dot{r}_{13} r_{33} \\ \Omega_z &= \dot{r}_{21} r_{11} + \dot{r}_{22} r_{12} + \dot{r}_{23} r_{13} \end{split}$$



Rigid angular velocity and the Eular velocity:

$$\begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ \Omega_y & \Omega_x & 0 \end{bmatrix} = \hat{\Omega} = \dot{R}R^{-1} \Rightarrow \begin{cases} \Omega_x & = \dot{r}_{31}r_{21} + \dot{r}_{32}r_{22} + \dot{r}_{33}r_{23} \\ \Omega_y & = \dot{r}_{11}r_{31} + \dot{r}_{12}r_{32} + \dot{r}_{13}r_{33} \\ \Omega_z & = \dot{r}_{21}r_{11} + \dot{r}_{22}r_{12} + \dot{r}_{23}r_{13} \end{cases}$$

$${}^{A}_{B}R_{Z'Y'Z'}(\alpha,\beta,\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$



Rigid angular velocity and the Eular velocity:

$$\begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ \Omega_y & \Omega_x & 0 \end{bmatrix} = \hat{\Omega} = \dot{R}R^{-1} \Rightarrow \begin{cases} \Omega_x & = \dot{r}_{31}r_{21} + \dot{r}_{32}r_{22} + \dot{r}_{33}r_{23} \\ \Omega_y & = \dot{r}_{11}r_{31} + \dot{r}_{12}r_{32} + \dot{r}_{13}r_{33} \\ \Omega_z & = \dot{r}_{21}r_{11} + \dot{r}_{22}r_{12} + \dot{r}_{23}r_{13} \end{cases}$$

$${}^{A}_{B}R_{Z'Y'Z'}(\alpha,\beta,\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$

$$\begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix} = \begin{bmatrix} 0 & -s\alpha & c\alpha s\beta \\ 0 & c\alpha & s\alpha s\beta \\ 1 & 0 & c\beta \end{bmatrix} \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix}$$



Rigid angular velocity and the Eular velocity:

$$\begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ \Omega_y & \Omega_x & 0 \end{bmatrix} = \hat{\Omega} = \dot{R}R^{-1} \Rightarrow \begin{cases} \Omega_x & = \dot{r}_{31}r_{21} + \dot{r}_{32}r_{22} + \dot{r}_{33}r_{23} \\ \Omega_y & = \dot{r}_{11}r_{31} + \dot{r}_{12}r_{32} + \dot{r}_{13}r_{33} \\ \Omega_z & = \dot{r}_{21}r_{11} + \dot{r}_{22}r_{12} + \dot{r}_{23}r_{13} \end{cases}$$

$${}^{A}_{B}R_{Z'Y'Z'}(\alpha,\beta,\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$

$$\begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix} = \begin{bmatrix} 0 & -s\alpha & c\alpha s\beta \\ 0 & c\alpha & s\alpha s\beta \\ 1 & 0 & c\beta \end{bmatrix} \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix} \Rightarrow \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{c\alpha c\beta}{s\beta} & -\frac{s\alpha c\beta}{s\beta} & 1 \\ -s\alpha & c\alpha & 0 \\ \frac{c\alpha}{s\beta} & \frac{s\alpha}{s\beta} & 0 \end{bmatrix}}_{E_D} \begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma}$ , 与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma}$ , 与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & 0 & c\beta \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}$ ,  $\dot{\beta}$ ,  $\dot{\gamma}$ , 与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & \mathbf{c}\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$

$$R_Z(\alpha)R_Y(\beta)R_Z(\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$

$$R_Z(\alpha)R_Y(\beta)R_Z(\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$



• 欧拉角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### Z-Y-Z 欧拉角

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$

$$R_Z(\alpha)R_Y(\beta)R_Z(\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$

$$\begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \dot{\alpha} + \begin{bmatrix} -s\alpha \\ c\alpha \\ 0 \end{bmatrix} \dot{\beta} + \begin{bmatrix} c\alpha s\beta \\ s\alpha s\beta \\ c\beta \end{bmatrix} \dot{\gamma} = \begin{bmatrix} 0 & -s\alpha & c\alpha s\beta \\ 0 & c\alpha & s\alpha s\beta \\ 1 & 0 & c\beta \end{bmatrix} \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha}, \dot{\beta}, \dot{\gamma}$ , 与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角



• XYZ 固定角速度  $\dot{\alpha}$ ,  $\dot{\beta}$ ,  $\dot{\gamma}$ , 与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & 0 & c\beta \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$



• XYZ 固定角速度  $\dot{\alpha},\dot{\beta},\dot{\gamma},$  与笛卡尔空间角速度  $\Omega$ 

#### XYZ 固定角

$$R_Z(\alpha)R_Y(\beta)R_X(\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$R_z(\alpha) = \begin{bmatrix} c\alpha & -s\alpha & \mathbf{0} \\ s\alpha & c\alpha & \mathbf{0} \\ 0 & 0 & \mathbf{1} \end{bmatrix} \quad R_z(\alpha)R_y(\beta) = \begin{bmatrix} c\alpha c\beta & -s\alpha & c\alpha s\beta \\ s\alpha c\beta & c\alpha & s\alpha s\beta \\ -s\beta & \mathbf{0} & c\beta \end{bmatrix}$$

$$\begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix} = \begin{bmatrix} c\alpha c\beta \\ s\alpha c\beta \\ -s\beta \end{bmatrix} \dot{\gamma} + \begin{bmatrix} -s\alpha \\ c\alpha \\ 0 \end{bmatrix} \dot{\beta} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \dot{\alpha} = \begin{bmatrix} 0 & -s\alpha & c\alpha c\beta \\ 0 & c\alpha & s\alpha c\beta \\ 1 & 0 & -s\beta \end{bmatrix} \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix}$$

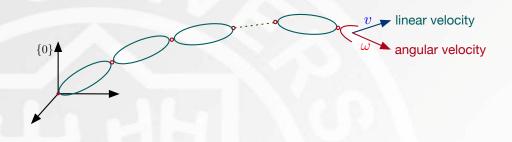


## Jacobian

- Differential Motion
- Linear & Angular Motion
- Velocity Propagation
- Explicit Form
- Static Forces



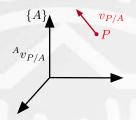
### Linear & Angular Velocities



$$\begin{bmatrix} v \\ \omega \end{bmatrix}_{(6\times 1)} = J_0(q)_{(6\times n)} \dot{q}_{(n\times 1)} \quad \begin{cases} \dot{X}_P = E_P(X_P)v \\ \dot{X}_R = E_R(X_R)\omega \end{cases}$$

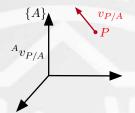


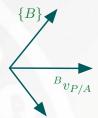
## Linear Velocity





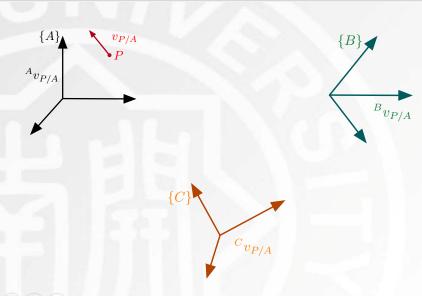
# Linear Velocity





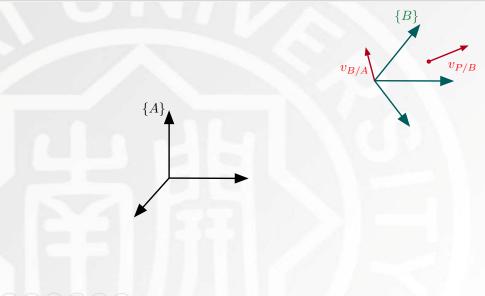


## Linear Velocity



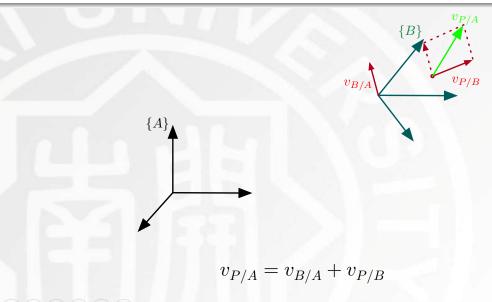


### Pure Translation

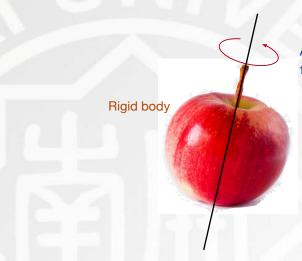




#### Pure Translation

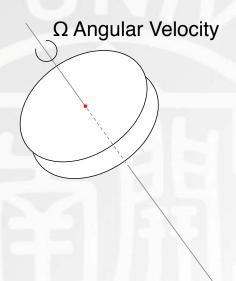




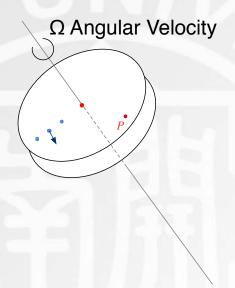


Axis of rotation fixed points on the rigid body

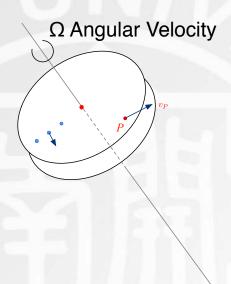






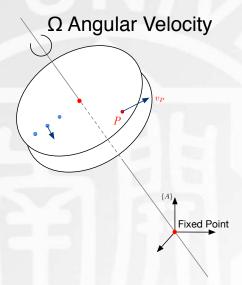




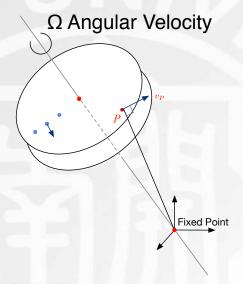


$$v_p = ?$$

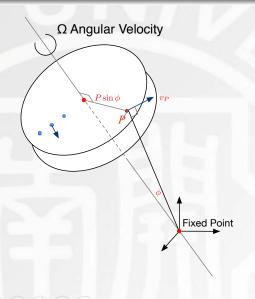












#### $v_p$ is proportional to

- $\bullet \|\Omega\|$
- $||P\sin\phi||$

and

- $v_p \perp \Omega$
- $v_p \perp P$

$$v_p = \Omega \times P$$



## Cross Product Operator

Let 
$$a=[a_x,\ a_y,\ a_z]^T$$
 and  $b=[b_x,\ b_y,\ b_z]^T$  
$$c=a\times b \ \Rightarrow \ c=\hat{a}b$$
 vectors  $\Rightarrow$  matrics

 $a \times \Rightarrow \hat{a}$ : a skew-symmetric matrix

$$c = a \times b = \hat{a}b = \begin{bmatrix} 0 & -a_z & a_y \\ a_z & 0 & -a_x \\ -a_y & a_x & 0 \end{bmatrix} \begin{bmatrix} b_x \\ b_y \\ b_z \end{bmatrix}$$

$$c = \hat{a}b$$



## Cross Product Operator

$$v_p = \Omega \times P$$

$$\Omega \times \Rightarrow \hat{\Omega}$$
: a skew-symmetric matrix

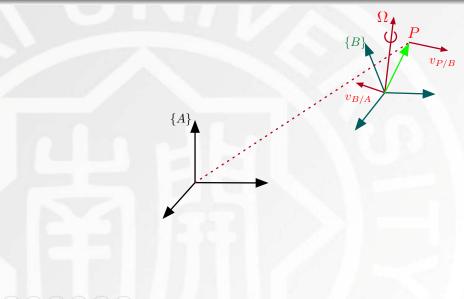
Let 
$$\Omega = [\Omega_x, \; \Omega_y, \; \overset{\backprime}{\Omega}_z]^T$$
 and  $P = [P_x, \; P_y, \; P_z]^T$ 

$$v_p = \hat{\Omega}P = \begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ -\Omega_y & \Omega_x & 0 \end{bmatrix} \begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix}$$

$$v_P = \hat{\Omega} P$$



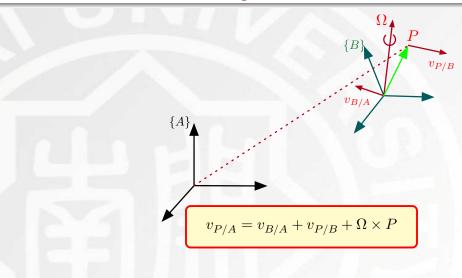
## Simultaneous linear and angular motion





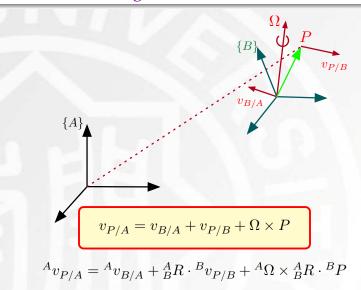


## Simultaneous linear and angular motion





### Simultaneous linear and angular motion



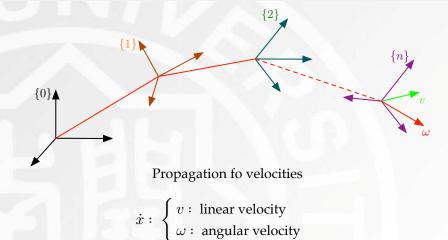


## Jacobian

- Differential Motion
- Linear & Angular Motion
- Velocity Propagation
- Explicit Form
- Static Forces

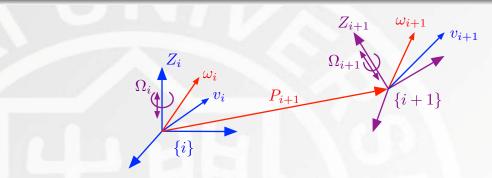


# Spatial Mechanisms



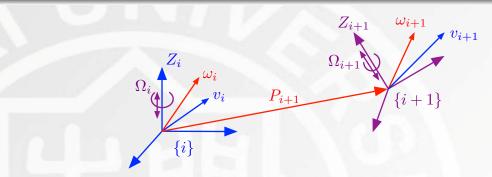
 $\dot{x} = J(\theta) \cdot \dot{\theta}$ 





• Linear velocity:

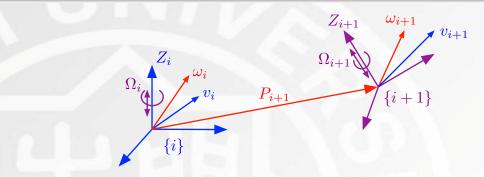




• Linear velocity:

$$v_{i+1} = v_i + \omega_i \times P_{i+1} + \dot{d}_{i+1} \cdot Z_{i+1}$$



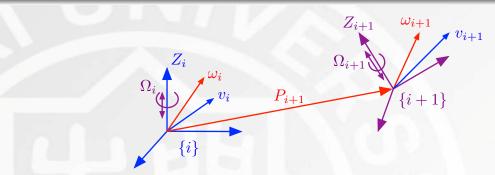


• Linear velocity:

$$v_{i+1} = v_i + \omega_i \times P_{i+1} + \dot{d}_{i+1} \cdot Z_{i+1}$$

Angular velocity:





• Linear velocity:

$$v_{i+1} = v_i + \omega_i \times P_{i+1} + \dot{d}_{i+1} \cdot Z_{i+1}$$

Angular velocity:

$$\begin{array}{ll} \boldsymbol{\omega}_{i+1} &= \boldsymbol{\omega}_i + \boldsymbol{\Omega}_{i+1} \\ \boldsymbol{\Omega}_{i+1} &= \dot{\boldsymbol{\theta}}_{i+1} \cdot \boldsymbol{Z}_{i+1} \end{array}$$



- Joint 1  $v_1$  amd  $\omega_1$  in frame  $\{1\}$
- Joint i+1



- Joint 1  $v_1$  amd  $\omega_1$  in frame  $\{1\}$
- Joint i+1

$$\begin{array}{lll} ^{i+1}\omega_{i+1} & = & _{i}^{i+1}R\cdot{}^{i}\omega_{i} + \dot{\theta}_{i+1}\cdot{}^{i+1}Z_{i+1} \\ ^{i+1}v_{i+1} & = & _{i}^{i+1}R\cdot({}^{i}v_{i} + {}^{i}\omega_{i} \times {}^{i}P_{i+1}) + \dot{d}_{i+1}\cdot{}^{i+1}Z_{i+1} \end{array}$$

 $\bullet \Rightarrow {}^n\omega_n$  and  ${}^nv_n$ 



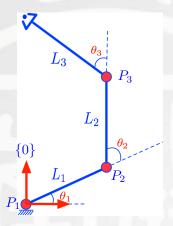
- Joint 1  $v_1$  amd  $\omega_1$  in frame  $\{1\}$
- Joint i+1

$$\begin{array}{lll} ^{i+1}\omega_{i+1} & = & _{i}^{i+1}R\cdot{}^{i}\omega_{i} + \dot{\theta}_{i+1}\cdot{}^{i+1}Z_{i+1} \\ ^{i+1}v_{i+1} & = & _{i}^{i+1}R\cdot({}^{i}v_{i} + {}^{i}\omega_{i} \times {}^{i}P_{i+1}) + \dot{d}_{i+1}\cdot{}^{i+1}Z_{i+1} \end{array}$$

ullet  $\Rightarrow$   $^n\omega_n$  and  $^nv_n$ 

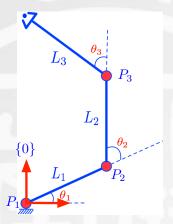
$$\begin{bmatrix} {}^0v_n \\ {}^0\omega_n \end{bmatrix} = \begin{bmatrix} {}^0nR & 0 \\ 0 & {}^0nR \end{bmatrix} \begin{bmatrix} {}^nv_n \\ {}^n\omega_n \end{bmatrix}$$





$$\bullet \ v_{i+1} = v_i + \omega_i \times P_{i+1}$$

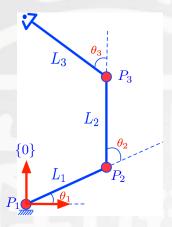




$$\begin{aligned} \bullet & v_{i+1} = v_i + \omega_i \times P_{i+1} \\ \bullet & v_{P_1} = 0 \end{aligned}$$

• 
$$v_{P_1} = 0$$





$$\bullet \ v_{i+1} = v_i + \omega_i \times P_{i+1}$$

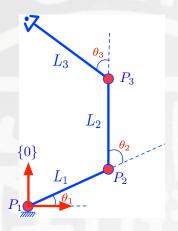
• 
$$v_{P_1} = 0$$

Chapter 5 Instantaneous Kinematics

$$\bullet \ v_{P_2} = v_{P_1} + {\color{orange} \omega_1} \times P_2$$

$${}^0v_{P_2} = 0 + \begin{bmatrix} 0 & -\dot{\theta}_1 & 0 \\ \dot{\theta}_1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} l_1 \cdot c_1 \\ l_1 \cdot s_1 \\ 0 \end{bmatrix} = \dot{\theta}_1 \cdot \begin{bmatrix} -l_1 \cdot s_1 \\ l_1 \cdot c_1 \\ 0 \end{bmatrix}$$





$$\bullet \ v_{i+1} = v_i + \omega_i \times P_{i+1}$$

• 
$$v_{P_1} = 0$$

$$\bullet \ v_{P_2} = v_{P_1} + \underline{\omega_1} \times P_2$$

$${}^{0}v_{P_{2}} = 0 + \begin{bmatrix} 0 & -\dot{\theta}_{1} & 0 \\ \dot{\theta}_{1} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} l_{1} \cdot c_{1} \\ l_{1} \cdot s_{1} \\ 0 \end{bmatrix} = \dot{\theta}_{1} \cdot \begin{bmatrix} -l_{1} \cdot s_{1} \\ l_{1} \cdot c_{1} \\ 0 \end{bmatrix}$$

$$\bullet \ v_{P_3} = v_{P_2} + \frac{\omega_2}{\omega_2} \times P_3$$

$${}^0v_{P_3} = \dot{\theta}_1 \cdot \begin{bmatrix} -l_1 \cdot s_1 \\ l_1 \cdot c_1 \\ 0 \end{bmatrix} + (\dot{\theta}_1 + \dot{\theta}_2) \cdot \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot {}^0P_3$$



$$\bullet \ v_{P_3} = v_{P_2} + \underline{\omega_2} \times P_3$$

$$\begin{split} {}^{0}v_{P_{3}} &= \dot{\theta}_{1} \cdot \begin{bmatrix} -l_{1} \cdot s_{1} \\ l_{1} \cdot c_{1} \\ 0 \end{bmatrix} + (\dot{\theta}_{1} + \dot{\theta}_{2}) \cdot \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} l_{2} \cdot c_{12} \\ l_{2} \cdot s_{12} \\ 0 & 0 \end{bmatrix} \\ &= \underbrace{\begin{bmatrix} -(l_{1}s_{1} + l_{2}s_{12}) & -l_{2}s_{12} & 0 \\ l_{1}c_{1} + l_{2}c_{12} & l_{2}c_{12} & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{\mathbf{J}_{v}} \cdot \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \dot{\theta}_{3} \end{bmatrix} \end{split}$$



$$\bullet \ v_{P_3} = v_{P_2} + \underline{\omega_2} \times P_3$$

$$\begin{split} {}^{0}v_{P_{3}} &= \dot{\theta}_{1} \cdot \begin{bmatrix} -l_{1} \cdot s_{1} \\ l_{1} \cdot c_{1} \\ 0 \end{bmatrix} + (\dot{\theta}_{1} + \dot{\theta}_{2}) \cdot \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} l_{2} \cdot c_{12} \\ l_{2} \cdot s_{12} \\ 0 \end{bmatrix} \\ &= \underbrace{\begin{bmatrix} -(l_{1}s_{1} + l_{2}s_{12}) & -l_{2}s_{12} & 0 \\ l_{1}c_{1} + l_{2}c_{12} & l_{2}c_{12} & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{J_{v}} \cdot \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \dot{\theta}_{3} \end{bmatrix} \end{split}$$

$$\bullet \ ^0\omega_3=(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\cdot {}^0Z_0$$

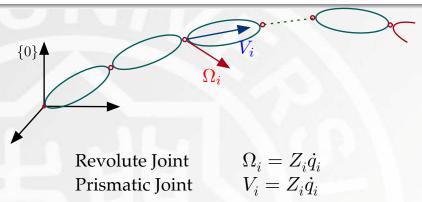
$${}^{0}\omega_{3} = \underbrace{\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}}_{J_{\omega}} \cdot \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \\ \dot{\theta}_{3} \end{bmatrix}$$



# **Jacobian**

- Differential Motion
- Linear & Angular Motion
- Velocity Propagation
- Explicit Form
- Static Forces

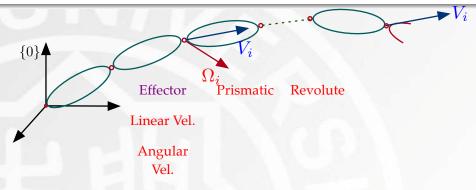






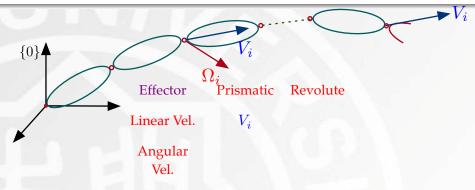
Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Contro





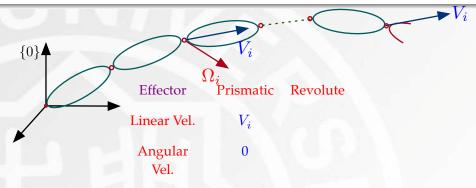






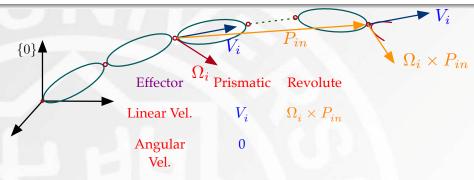






Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Contro

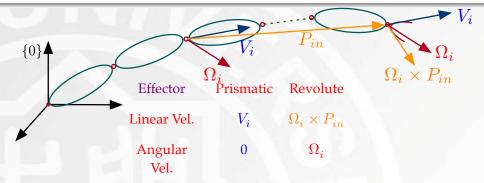






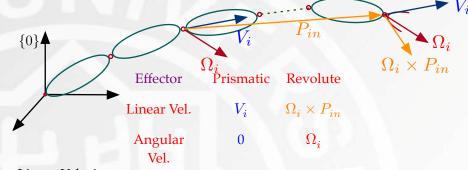
Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Contro







# The Jacobian (EXPLICIT FORM)



Effector Linear Velocity

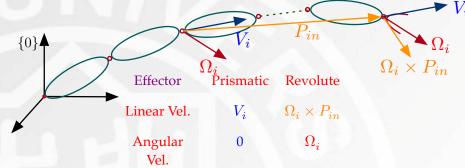
$$v = \sum_{i=1}^{n} [\epsilon_i V_i + \bar{\epsilon}_i (\Omega_i \times P_{in})]$$

Effector Augular Velocity

$$\omega = \sum_{i=1}^{n} \bar{\epsilon}_{i} \Omega_{i}$$



## The Jacobian (EXPLICIT FORM)



#### Effector Linear Velocity

$$v = \sum_{i=1}^{n} [\epsilon_i V_i + \bar{\epsilon}_i (\Omega_i \times P_{in})]$$

$$\Leftarrow V_i = Z_i \dot{q}_i$$

Effector Augular Velocity

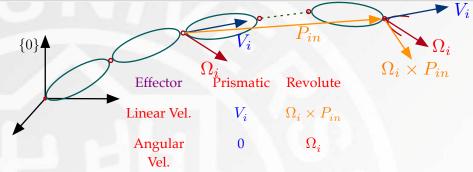
$$\omega = \sum_{i=1}^{n} \bar{\epsilon}_{i} \Omega_{i}$$

$$\Leftarrow \Omega_i = Z_i \dot{q}_i$$

#### Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Contro



#### The Jacobian (EXPLICIT FORM)



Effector Linear Velocity

$$v = \sum_{i=1}^{n} [\epsilon_i V_i + \bar{\epsilon}_i (\Omega_i \times P_{in})] = \sum_{i=1}^{n} [\epsilon_i Z_i + \bar{\epsilon}_i (Z_i \times P_{in})] \dot{q}_i \quad \Leftarrow \quad V_i = Z_i \dot{q}_i$$

Effector Augular Velocity

$$\omega = \sum_{i=1}^{n} \bar{\epsilon}_{i} \Omega_{i} = \sum_{i=1}^{n} (\bar{\epsilon}_{i} Z_{i}) \dot{q}_{i} \qquad \Leftarrow \quad \Omega_{i} = Z_{i} \dot{q}_{i}$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = \begin{bmatrix} \epsilon_1 Z_1 + \bar{\epsilon}_1(Z_1 \times P_{1n}) & \cdots & \epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1}(Z_{n-1} \times P_{(n-1)n}) & \epsilon_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_{n-1} \\ \dot{q}_n \end{bmatrix}$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = \begin{bmatrix} \epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n}) & \cdots & \epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n}) & \epsilon_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_{n-1} \\ \dot{q}_n \end{bmatrix}$$

$$v = J_v \dot{q}$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = \begin{bmatrix} \epsilon_1 Z_1 + \bar{\epsilon}_1(Z_1 \times P_{1n}) & \cdots & \epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1}(Z_{n-1} \times P_{(n-1)n}) & \epsilon_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_{n-1} \\ \dot{q}_n \end{bmatrix}$$

$$v=J_v\dot{q}$$

$$\omega = \bar{\epsilon}_1 Z_1 \dot{q}_1 + \bar{\epsilon}_2 Z_2 \dot{q}_2 + \dots + \bar{\epsilon}_n Z_n \dot{q}_n$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = \begin{bmatrix} \epsilon_1 Z_1 + \bar{\epsilon}_1(Z_1 \times P_{1n}) & \cdots & \epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1}(Z_{n-1} \times P_{(n-1)n}) & \epsilon_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_{n-1} \\ \dot{q}_n \end{bmatrix}$$

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$$\omega = \bar{\epsilon}_1 Z_1 \dot{q}_1 + \bar{\epsilon}_2 Z_2 \dot{q}_2 + \dots + \bar{\epsilon}_n Z_n \dot{q}_n$$

$$\omega = \begin{bmatrix} \bar{\epsilon}_1 Z_1 & \bar{\epsilon}_2 Z_2 & \cdots & \bar{\epsilon}_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$



$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = \begin{bmatrix} \epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n}) & \cdots & \epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n}) & \epsilon_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_{n-1} \\ \dot{q}_n \end{bmatrix}$$

$$v=J_v\dot{q}$$

$$\omega = \bar{\epsilon}_1 Z_1 \dot{q}_1 + \bar{\epsilon}_2 Z_2 \dot{q}_2 + \dots + \bar{\epsilon}_n Z_n \dot{q}_n$$

$$\omega = \begin{bmatrix} \bar{\epsilon}_1 Z_1 & \bar{\epsilon}_2 Z_2 & \cdots & \bar{\epsilon}_n Z_n \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

$$\omega = J_{\omega} \dot{q}$$

$$\omega = J_\omega \dot{q}$$



# Jacobian in a Frame

$$J = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$



#### Jacobian in a Frame

$$J = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$

Matrix  $J_{ij}$  (direct differentiation)

$$v = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \dot{x}_P = \frac{\partial x_P}{\partial q_1} \cdot \dot{q}_1 + \frac{\partial x_P}{\partial q_2} \cdot \dot{q}_2 + \dots + \frac{\partial x_P}{\partial q_n} \cdot \dot{q}_n$$
$$J_v = \begin{bmatrix} \frac{\partial x_P}{\partial q_1} & \frac{\partial x_P}{\partial q_2} & \dots & \frac{\partial x_P}{\partial q_N} \end{bmatrix}$$



#### Jacobian in a Frame

$$J = \begin{bmatrix} J_{\underline{v}} \\ J_{\omega} \end{bmatrix}$$

Matrix  $J_{v}$  (direct differentiation)

$$v = \begin{bmatrix} x \\ \dot{y} \\ \dot{z} \end{bmatrix} = \dot{x}_P = \frac{\partial x_P}{\partial q_1} \cdot \dot{q}_1 + \frac{\partial x_P}{\partial q_2} \cdot \dot{q}_2 + \dots + \frac{\partial x_P}{\partial q_n} \cdot \dot{q}_n$$
$$J_v = \begin{bmatrix} \frac{\partial x_P}{\partial q_1} & \frac{\partial x_P}{\partial q_2} & \dots & \frac{\partial x_P}{\partial q_N} \end{bmatrix}$$

Vector Respesentation:

$$J = \begin{bmatrix} \frac{\partial x_P}{\partial q_1} & \frac{\partial x_P}{\partial q_2} & \cdots & \frac{\partial x_P}{\partial q_N} \\ \bar{\epsilon}_1 Z_1 & \bar{\epsilon}_2 Z_2 & \cdots & \bar{\epsilon}_n Z_n \end{bmatrix}$$



# Jacobian in a Frame $\{0\}$

$${}^{0}J = \begin{bmatrix} \frac{\partial^{0}x_{P}}{\partial q_{1}} & \frac{\partial^{0}x_{P}}{\partial q_{2}} & \cdots & \frac{\partial^{0}x_{P}}{\partial q_{N}} \\ \bar{\epsilon}_{1}{}^{0}Z_{1} & \bar{\epsilon}_{2}{}^{0}Z_{2} & \cdots & \bar{\epsilon}_{n}{}^{0}Z_{n} \end{bmatrix}$$



# Jacobian in a Frame $\{0\}$

$${}^{0}J = \begin{bmatrix} \frac{\partial^{0}x_{P}}{\partial q_{1}} & \frac{\partial^{0}x_{P}}{\partial q_{2}} & \cdots & \frac{\partial^{0}x_{P}}{\partial q_{N}} \\ \bar{\epsilon}_{1}{}^{0}Z_{1} & \bar{\epsilon}_{2}{}^{0}Z_{2} & \cdots & \bar{\epsilon}_{n}{}^{0}Z_{n} \end{bmatrix}$$

$${}^0Z_i={}^0_iR\cdot{}^iZ_i$$



# Jacobian in a Frame $\{0\}$

$${}^{0}J = \begin{bmatrix} \frac{\partial^{0}x_{P}}{\partial q_{1}} & \frac{\partial^{0}x_{P}}{\partial q_{2}} & \cdots & \frac{\partial^{0}x_{P}}{\partial q_{N}} \\ \bar{\epsilon}_{1}{}^{0}Z_{1} & \bar{\epsilon}_{2}{}^{0}Z_{2} & \cdots & \bar{\epsilon}_{n}{}^{0}Z_{n} \end{bmatrix}$$

$${}^0Z_i={}^0_iR\cdot {}^iZ_i \qquad {}^iZ_i=Z=\begin{bmatrix}0\\0\\1\end{bmatrix}$$



## Jacobian in a Frame $\{0\}$

$${}^{0}J = \begin{bmatrix} \frac{\partial^{0}x_{P}}{\partial q_{1}} & \frac{\partial^{0}x_{P}}{\partial q_{2}} & \cdots & \frac{\partial^{0}x_{P}}{\partial q_{N}} \\ \bar{\epsilon}_{1}{}^{0}Z_{1} & \bar{\epsilon}_{2}{}^{0}Z_{2} & \cdots & \bar{\epsilon}_{n}{}^{0}Z_{n} \end{bmatrix}$$

$${}^0Z_i={}^0_iR\cdot{}^iZ_i \qquad {}^iZ_i=Z=\begin{bmatrix}0\\0\\1\end{bmatrix}$$

$${}^0J = \begin{bmatrix} \frac{\partial}{\partial q_1}(^0x_P) & \frac{\partial}{\partial q_2}(^0x_P) & \cdots & \frac{\partial}{\partial q_N}(^0x_P) \\ \bar{\epsilon}_1(^0_1R\cdot Z) & \bar{\epsilon}_2(^0_2R\cdot Z) & \cdots & \bar{\epsilon}_n(^0_nR\cdot Z) \end{bmatrix}$$

Direct Differentiation
Linear & Angular Velocities
EXPLICIT FORM
Static Force

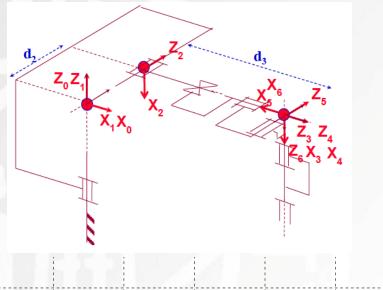
Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Contro



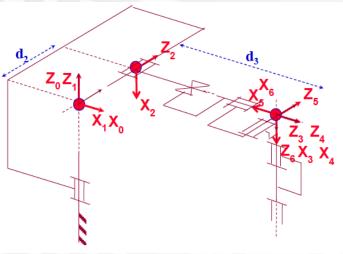
### Stanford Scheinman Arm



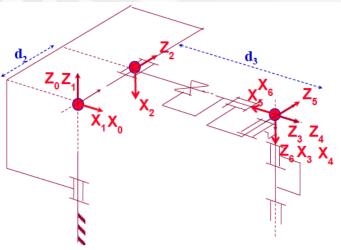






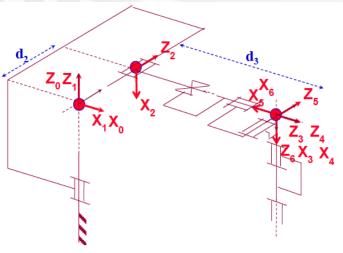






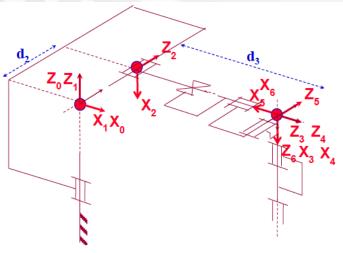
$$J = \begin{bmatrix} Z_1 \times P_{13} \\ Z_1 \end{bmatrix}$$





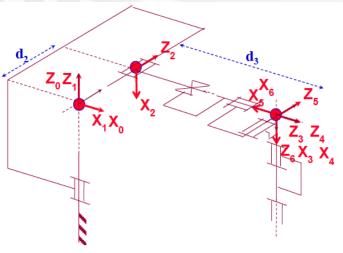
$$J = \begin{bmatrix} Z_1 imes P_{13} & Z_2 imes P_{23} \\ Z_1 & Z_2 & Z_3 \end{bmatrix}$$





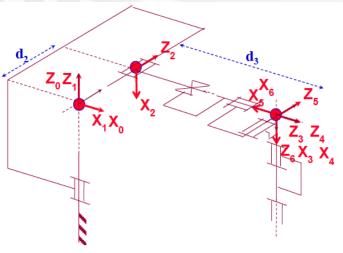
$$J = \begin{bmatrix} Z_1 \times P_{13} & Z_2 \times P_{23} \\ Z_1 & Z_2 \end{bmatrix}$$





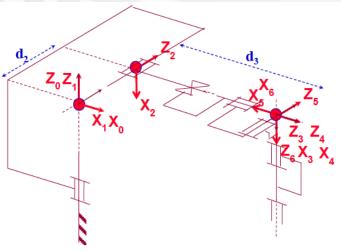
$$J = \begin{bmatrix} Z_1 \times P_{13} & Z_2 \times P_{23} & Z_3 \\ Z_1 & Z_2 \end{bmatrix}$$





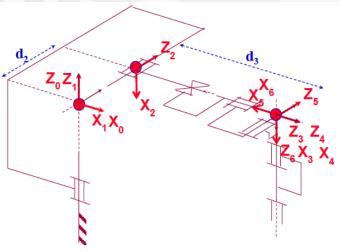
$$J = egin{bmatrix} Z_1 imes P_{13} & Z_2 imes P_{23} & Z_3 \ Z_1 & Z_2 & 0 \end{bmatrix}$$





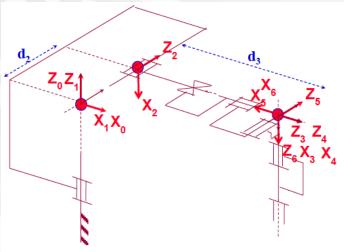
$$J = egin{bmatrix} Z_1 imes P_{13} & Z_2 imes P_{23} & Z_3 & 0 \\ Z_1 & Z_2 & 0 & 0 \end{bmatrix}$$





$$J = egin{bmatrix} Z_1 imes P_{13} & Z_2 imes P_{23} & Z_3 & 0 \ Z_1 & Z_2 & 0 & Z_4 \ \end{bmatrix}$$

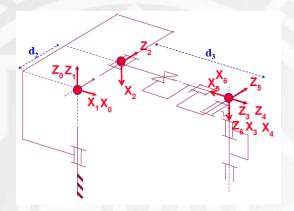




$$J = \left[ egin{array}{c|cccc} Z_1 imes P_{13} & Z_2 imes P_{23} & Z_3 & 0 & 0 & 0 \ & Z_1 & Z_2 & 0 & Z_4 & Z_5 & Z_6 \end{array} 
ight]$$



### Stanford Scheinman Arm



#### Table: DH 参数

i	$\alpha_{i-1}$	$a_{i-1}$	$d_{i}$	$ heta_i$
1	0	0	0	$\theta_1$
2	-90	0	$d_2$	$\theta_2$
3	90	0	$d_3$	0
4	0	0	0	$\theta_4$
5	-90	0	0	$\theta_5$
6	90	0	0	$\theta_6$



#### Stanford Scheinman Arm

$$i^{-1}T = \begin{bmatrix} \cos\theta_i & -\sin\theta_i & 0 & a_{i-1} \\ \sin\theta_i\cos\alpha_{i-1} & \cos\theta_i\cos\alpha_{i-1} & -\sin\alpha_{i-1} & -d_i\sin\alpha_{i-1} \\ \sin\theta_i\sin\alpha_{i-1} & \cos\theta_i\sin\alpha_{i-1} & \cos\alpha_{i-1} & d_i\cos\alpha_{i-1} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Forward Kinematics:  ${}^0_NT = {}^0_1T \cdot {}^1_2T \cdots {}^{N-1}_NT$ 

$${}^{0}_{1}T = \begin{bmatrix} c_{1} & -s_{1} & 0 & 0 \\ s_{1} & c_{1} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \, {}^{0}_{2}T = \begin{bmatrix} c_{1}c_{2} & -c_{1}s_{2} & -s_{1} & -s_{1}d_{2} \\ s_{1}c_{2} & -s_{1}s_{2} & c_{1} & c_{1}d_{2} \\ -s_{2} & -c_{2} & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$${}_{3}^{0}T = \begin{bmatrix} c_{1}c_{2} & -s_{1} & c_{1}s_{2} & c_{1}s_{2}d_{3} - s_{1}d_{2} \\ s_{1}c_{2} & c_{1} & s_{1}s_{2} & s_{1}s_{2}d_{3} + c_{1}d_{2} \\ -s_{2} & 0 & c_{2} & c_{2}d_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix}, \ {}_{4}^{0}T = \begin{bmatrix} X & X & c_{1}s_{2} & c_{1}s_{2}d_{3} - s_{1}d_{2} \\ X & X & s_{1}s_{2} & s_{1}s_{2}d_{3} + c_{1}d_{2} \\ X & X & c_{2} & c_{2}d_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



#### Stanford Scheinman Arm

$${}_{5}^{0}T = \begin{bmatrix} X & X & -c_{1}c_{2}s_{4} - s_{1}c_{4} & X \\ X & X & -s_{1}c_{2}s_{4} + c_{1}c_{4} & X \\ X & X & s_{2}s_{4} & X \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}_{6}^{0}T = \begin{bmatrix} X & X & c_{1}c_{2}c_{4}s_{5} - s_{1}s_{4}s_{5} + c_{1}s_{2}s_{5} & X \\ X & X & s_{1}c_{2}c_{4}s_{5} + c_{1}s_{4}s_{5} + s_{1}s_{2}c_{5} & X \\ X & X & -s_{2}c_{4}s_{5} + c_{2}c_{5} & X \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$X = \begin{bmatrix} X_P \\ r_1 \\ r_2 \\ r_3 \end{bmatrix} = \begin{bmatrix} d_3c_1s_2 - d_2s_1 \\ d_3c_2 \\ c_1[c_2(c_4c_5c_6 - s_4s_6) - s_2s_5c_6] - s_1(s_4c_5c_6 + c_4s_6) \\ s_1[c_2(c_4c_5c_6 - s_4s_6) - s_2s_5c_6] + c_1(s_4c_5c_6 + c_4s_6) \\ -s_2(c_4c_5c_6 - s_4s_6) - c_2s_5c_6 \\ c_1[-c_2(c_4c_5s_6 + s_4c_6) + s_2s_5s_6] - s_1(-s_4c_5s_6 + c_4c_6) \\ s_1[-c_2(c_4c_5s_6 + s_4c_6) + s_2s_5s_6) + c_1(-s_4c_5s_6 + c_4c_6) \\ s_2(c_4c_5s_6 + s_4c_6) + c_2s_5s_6 \\ c_1(c_2c_4s_5 + s_2c_5) - s_1s_4s_5 \\ s_1(c_2c_4s_5 + s_2c_5) + c_1s_4s_5 \\ -s_2c_4s_5 + c_2c_5 \end{bmatrix}$$



#### Stanford Scheinman Arm Jacobian

$${}^{0}J = \begin{bmatrix} \frac{\partial}{\partial q_{1}}({}^{0}x_{P}) & \frac{\partial}{\partial q_{2}}({}^{0}x_{P}) & \frac{\partial}{\partial q_{3}}({}^{0}x_{P}) & 0 & 0 & 0 \\ {}^{0}Z_{1} & {}^{0}Z_{2} & 0 & {}^{0}Z_{4} & {}^{0}Z_{5} & {}^{0}Z_{6} \end{bmatrix}$$

$$\begin{bmatrix} -(d_3s_1s_2+d_2c_1) & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0 \\ d_3c_1s_2-d_2s_1 & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0 \\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0 \\ 0 & -s_1 & 0 & c_1s_2 & -c_1c_2s_4-s_1c_4 & c_1c_2c_4s_5-s_1s_4s_5+c_1s_2c_5 \\ 0 & c_1 & 0 & s_1s_2 & -s_1c_2s_4+c_1c_4 & s_1c_2c_4s_5+c_1s_4s_5+s_1s_2c_5 \\ 1 & 0 & 0 & c_2 & s_2s_4 & -s_2c_4s_5+c_2c_5 \end{bmatrix}$$

Jacobian in a Frame Kinematic Singularity Jacobian at the End-Effector Resolved Motion Rate Control



# Kinematic Singularity and Singular Configurations

#### Singular Direction





#### Singular Direction

$$J = \begin{pmatrix} J_1 & J_2 & \cdots & J_n \end{pmatrix}$$
 when  $\det(J) = 0$ 



#### Singular Direction

$$J = \begin{pmatrix} J_1 & J_2 & \cdots & J_n \end{pmatrix}$$
 when  $\det(J) = 0$ 

$$\det({}^iJ) = \det({}^jJ)$$





#### Singular Direction

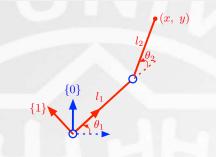
$$J=\begin{pmatrix} J_1 & J_2 & \cdots & J_n \end{pmatrix} \qquad \text{when } \det(J)=0$$
 
$$\det({}^iJ)=\det({}^jJ)$$
 
$${}^BJ=\begin{bmatrix} {}^B_AR & 0 \\ 0 & {}^B_AR \end{bmatrix}{}^AJ$$
 
$$\det({}^BJ)\equiv\det({}^AJ)$$



#### Singular Direction

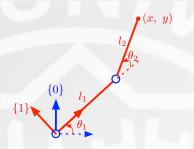
$$J = (J_1 \quad J_2 \quad \cdots \quad J_n) \qquad \text{when } \det(J) = 0$$
 
$$\det({}^iJ) = \det({}^jJ) \qquad \Rightarrow \begin{array}{l} \text{Singular Configurations} \\ \det[J(q)] = S_1(q) \cdot S_2(q) \cdots S_s(q) = 0 \\ \end{bmatrix}$$
 
$$\det({}^BJ) \equiv \det({}^AJ) \qquad \Rightarrow \begin{array}{l} S_1(q) = 0 \\ S_2(q) = 0 \\ \vdots \\ S_s(q) = 0 \end{array}$$





$$x = l_1c_1 + l_2c_{12}$$
  
$$y = l_1s_1 + l_2s_{12}$$

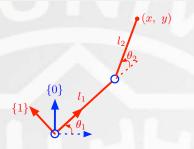




$$x = l_1c_1 + l_2c_{12}$$
$$y = l_1s_1 + l_2s_{12}$$

$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \end{bmatrix}$$





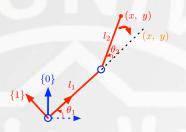
$$x = l_1c_1 + l_2c_{12}$$
$$y = l_1s_1 + l_2s_{12}$$

$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \end{bmatrix}$$

$$\det(J) = l_1 l_2 s_2$$

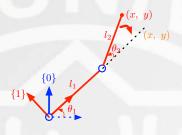
Sigularity at  $q_2 = k\pi$ 





$${}^{1}J = {}^{1}_{0}R^{0}J$$
 
$${}^{0}J = \begin{bmatrix} c_{1} & -s_{1} \\ s_{1} & c_{1} \end{bmatrix} \begin{bmatrix} -(l_{1}s_{1} + l_{2}s_{12}) & -l_{2}s_{12} \\ l_{1}c_{1} + l_{2}c_{12} & l_{2}c_{12} \end{bmatrix}$$





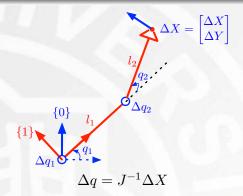
$${}^{1}J = {}^{1}_{0}R^{0}J$$
 
$${}^{0}J = \begin{bmatrix} c_{1} & -s_{1} \\ s_{1} & c_{1} \end{bmatrix} \begin{bmatrix} -(l_{1}s_{1} + l_{2}s_{12}) & -l_{2}s_{12} \\ l_{1}c_{1} + l_{2}c_{12} & l_{2}c_{12} \end{bmatrix}$$

At singularity:

$$\begin{split} ^1J &= \begin{bmatrix} 0 & 0 \\ l_1+l_2 & l_2 \end{bmatrix} \\ \begin{cases} ^1\delta x = 0 \\ ^1\delta y = (l_1+l_2)\delta\theta_1 + l_2\delta\theta_2 \end{split}$$



## Small Displacements $\Delta q$ , $\Delta X$

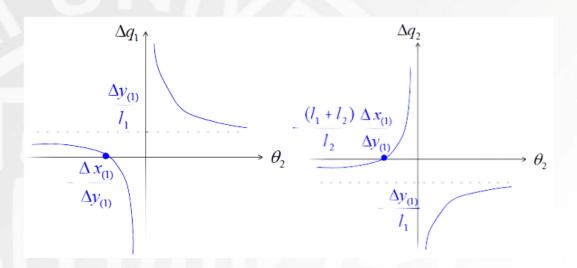


Small  $\theta_2$  (i.e.  $\cos \theta_2 \approx 1$ ,  $\sin \theta_2 \approx \theta_2$ )

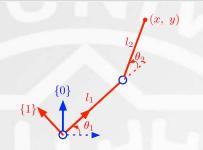
$$J_{(1)}^{-1} \cong \begin{bmatrix} \frac{1}{l_1\theta_2} & \frac{1}{l_1} \\ -\frac{l_1+l_2}{l_1l_2\theta_2} & -\frac{1}{l_1} \end{bmatrix} \Rightarrow \begin{cases} \Delta q_1 = \frac{\Delta x_{(1)}}{l_1} \cdot \frac{1}{\theta_2} + \frac{\Delta y_{(1)}}{l_1} \\ \Delta q_2 = \frac{(l_1+l_2)\Delta x_{(1)}}{l_1l_2} \cdot \frac{1}{\theta_2} + \frac{\Delta y_{(1)}}{l_1} \end{cases}$$



# Small Displacements $\Delta q$ , $\Delta X$

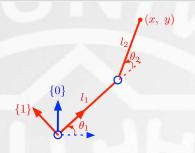






$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \\ 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}$$



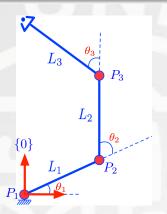


$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \end{bmatrix}$$

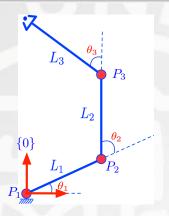
$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 1 \end{bmatrix}$$

$$\det(J) = l_1 l_2 s_2$$









$${}^{0}J_{E} = \begin{bmatrix} -l_{1}s_{1} - l_{2}s_{12} - l_{3}s_{123} & -l_{2}s_{12} - l_{3}s_{123} & -l_{3}s_{123} \\ l_{1}c_{1} + l_{2}c_{12} + l_{3}c_{123} & l_{2}c_{12} + l_{3}c_{123} & l_{3}c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

$${}^{0}J_{E} = \begin{bmatrix} -l_{1}s_{1} - l_{2}s_{12} - l_{3}s_{123} & -l_{2}s_{12} - l_{3}s_{123} & -l_{3}s_{123} \\ l_{1}c_{1} + l_{2}c_{12} + l_{3}c_{123} & l_{2}c_{12} + l_{3}c_{123} & l_{3}c_{123} \\ 1 & 1 & 1 \end{bmatrix}$$



# Stanford Scheinman Arm Jacobian

$$\begin{bmatrix} -(d_3s_1s_2+d_2c_1) & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0 \\ d_3c_1s_2-d_2s_1 & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0 \\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0 \\ 0 & -s_1 & 0 & c_1s_2 & -c_1c_2s_4-s_1c_4 & c_1c_2c_4s_5-s_1s_4s_5+c_1s_2c_5 \\ 0 & c_1 & 0 & s_1s_2 & -s_1c_2s_4+c_1c_4 & s_1c_2c_4s_5+c_1s_4s_5+s_1s_2c_5 \\ 1 & 0 & 0 & c_2 & s_2s_4 & -s_2c_4s_5+c_2c_5 \end{bmatrix}$$

$$\theta_5 = k\pi$$



### Stanford Scheinman Arm Jacobian

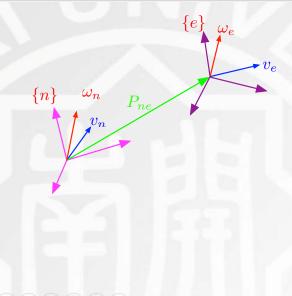
$$\begin{bmatrix} -(d_3s_1s_2+d_2c_1) & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0 \\ d_3c_1s_2-d_2s_1 & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0 \\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0 \\ 0 & -s_1 & 0 & c_1s_2 & -c_1c_2s_4-s_1c_4 & c_1c_2c_4s_5-s_1s_4s_5+c_1s_2c_5 \\ 0 & c_1 & 0 & s_1s_2 & -s_1c_2s_4+c_1c_4 & s_1c_2c_4s_5+c_1s_4s_5+s_1s_2c_5 \\ 1 & 0 & 0 & c_2 & s_2s_4 & -s_2c_4s_5+c_2c_5 \end{bmatrix}$$

$$\theta_5 = k\pi$$

$$\begin{bmatrix} -(d_3s_1s_2+d_2c_1) & c_1c_2d_3 & c_1s_2 & 0 & 0 & 0\\ d_3c_1s_2-d_2s_1 & s_1c_2d_3 & s_1s_2 & 0 & 0 & 0\\ 0 & -s_2d_3 & c_2 & 0 & 0 & 0\\ 0 & -s_1 & 0 & c_1s_2 & -c_1c_2s_4-s_1c_4 & c_1s_2\\ 0 & c_1 & 0 & s_1s_2 & -s_1c_2s_4+c_1c_4 & s_1s_2\\ 1 & 0 & 0 & c_2 & s_2s_4 & c_2 \end{bmatrix}$$

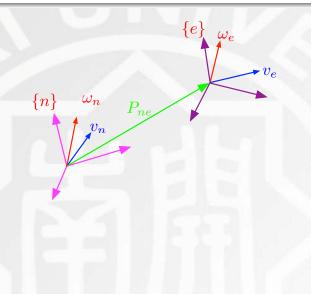


# Jacobian at the End-Effector





#### Jacobian at the End-Effector

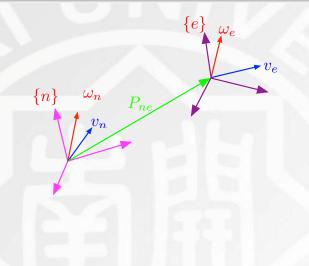


$$v_e = v_n + \omega_n \times P_{ne}$$

$$\left\{ \begin{aligned} \boldsymbol{v}_e &= \boldsymbol{v}_n - \boldsymbol{P}_{ne} \times \boldsymbol{\omega}_n \\ \boldsymbol{\omega}_e &= \boldsymbol{\omega}_n \end{aligned} \right.$$



#### Jacobian at the End-Effector



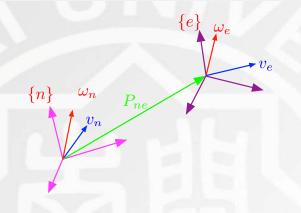
$$v_e = v_n + \omega_n \times P_{ne}$$

$$\left\{ \begin{aligned} v_e &= v_n - P_{ne} \times \omega_n \\ \omega_e &= \omega_n \end{aligned} \right.$$

$$\begin{bmatrix} v_e \\ \omega_e \end{bmatrix} = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} \begin{bmatrix} v_n \\ \omega_n \end{bmatrix}$$



#### Jacobian at the End-Effector



$$J_e\dot{q} = \left[\begin{array}{cc} I & -\hat{P}_{ne} \\ \hline 0 & I \end{array}\right] J_n\dot{q} \qquad \Rightarrow \qquad J_e = \left[\begin{array}{cc} I & -\hat{P}_{ne} \\ \hline 0 & I \end{array}\right] J_n$$

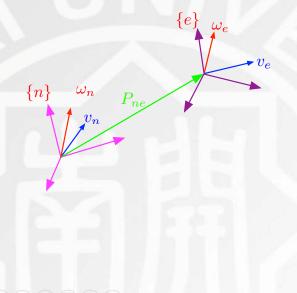
$$v_e = v_n + \omega_n \times P_{ne}$$

$$\left\{ \begin{aligned} v_e &= v_n - P_{ne} \times \omega_n \\ \omega_e &= \omega_n \end{aligned} \right.$$

$$\begin{bmatrix} v_e \\ \omega_e \end{bmatrix} = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} \begin{bmatrix} v_n \\ \omega_n \end{bmatrix}$$

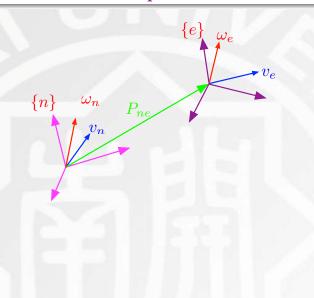
$$J_e = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} J_r$$





$$J_e = \left[\begin{array}{c|c} I & -\hat{P}_{ne} \\ \hline 0 & I \end{array}\right] J_n$$

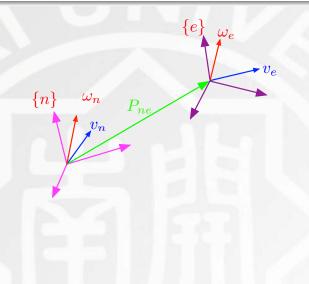




$$J_e = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} J_n$$
 
$${}^0\hat{P}_{ne} = {}^0_n R \cdot {}^n\hat{P}_{ne} \ ?$$

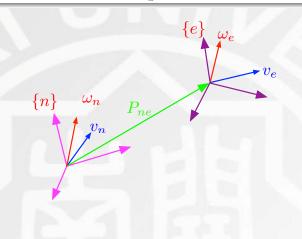
$${}^0\hat{P}_{ne} = {}^0_n R \cdot {}^n\hat{P}_{ne} ?$$





$$\begin{split} J_e &= \left[\begin{array}{c|c} I & -\hat{P}_{ne} \\ \hline 0 & I \end{array}\right] J_n \\ ^0\hat{P}_{ne} &= {0 \atop n} R \cdot ^n \hat{P}_{ne} \quad ? \\ ^0\hat{P}_{ne} \times ^0 \omega &= {0 \atop n} R \cdot (^n P_{ne} \times ^n \omega) \end{split}$$





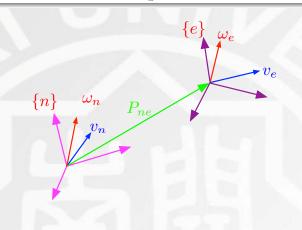
$$J_e = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} J_n$$

$${}^0\hat{P}_{ne} = {}^0_n R \cdot {}^n \hat{P}_{ne} ?$$

$${}^0\hat{P}_{ne} \times {}^0 \omega = {}^0_n R \cdot ({}^n P_{ne} \times {}^n \omega)$$

$${}^{0}\hat{P}_{ne}\cdot{}^{0}\omega = {}^{0}_{n}R\cdot({}^{n}\hat{P}_{ne}\cdot{}^{n}\omega) = {}^{0}_{n}R\cdot({}^{n}\hat{P}_{ne}\cdot{}^{0}_{n}R^{T}\cdot{}^{0}\omega)$$





$$J_{e} = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} J_{n}$$

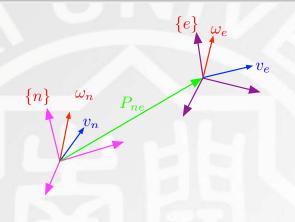
$${}^{0}\hat{P}_{ne} = {}^{0}_{n}R \cdot {}^{n}\hat{P}_{ne} ?$$

$${}^{0}\hat{P}_{ne} \times {}^{0}\omega = {}^{0}_{n}R \cdot ({}^{n}P_{ne} \times {}^{n}\omega)$$

$${}^0\hat{P}_{ne}\cdot{}^0\omega={}^0_nR\cdot({}^n\hat{P}_{ne}\cdot{}^n\omega)={}^0_nR\cdot({}^n\hat{P}_{ne}\cdot{}^0_nR^T\cdot{}^0\omega)$$

$${}^{0}\hat{P}_{ne} = {}^{0}_{n}R \cdot {}^{n}\hat{P}_{ne} \cdot {}^{0}_{n}R^{T}$$





$$J_e = \begin{bmatrix} I & -\hat{P}_{ne} \\ 0 & I \end{bmatrix} J_n$$

$${}^0\hat{P}_{ne} = {}^0_n R \cdot {}^n \hat{P}_{ne} ?$$

$${}^0\hat{P}_{ne} \times {}^0\omega = {}^0_nR \cdot ({}^nP_{ne} \times {}^n\omega)$$

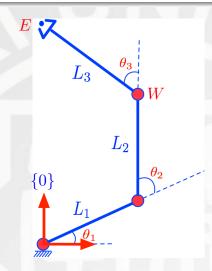
$${}^{0}\hat{P}_{ne}\cdot{}^{0}\omega = {}^{0}_{n}R\cdot({}^{n}\hat{P}_{ne}\cdot{}^{n}\omega) = {}^{0}_{n}R\cdot({}^{n}\hat{P}_{ne}\cdot{}^{0}_{n}R^{T}\cdot{}^{0}\omega)$$

$${}^{0}\hat{P}_{ne} = {}^{0}_{n}R \cdot {}^{n}\hat{P}_{ne} \cdot {}^{0}_{n}R^{T}$$

$${}^{i}J = \begin{bmatrix} {}^{i}_{j}R & 0 \\ 0 & {}^{i}_{j}R \end{bmatrix} {}^{j}J \qquad \Rightarrow \qquad {}^{0}J_{e} = \begin{bmatrix} {}^{i}_{j}R & -{}^{0}_{n}R \cdot {}^{n}\hat{P}_{ne} \cdot {}^{0}_{n}R^{T} \\ 0 & {}^{i}_{j}R \end{bmatrix} {}^{n}J_{n}$$



#### Example: RRR Arm



Wrist Point:

$$\begin{cases} x = l_1 c_1 + l_2 c_{12} \\ y = l_1 s_1 + l_2 s_{12} \end{cases}$$

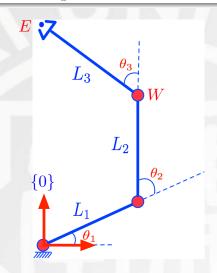
**End-Effector Point:** 

$$\begin{cases} x = l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ y = l_1 s_1 + l_2 s_{12} + l_3 s_{123} \end{cases}$$

Jacobian (W):



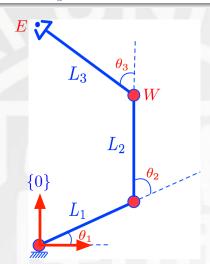
## Example: RRR Arm



$${}^0J_e = \begin{bmatrix} I & -{}^0\hat{P}_{ne} \\ 0 & I \end{bmatrix} {}^0J_W$$



### Example: RRR Arm



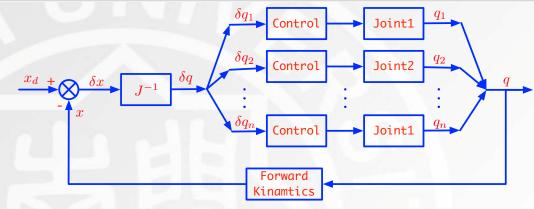
$${}^0J_e = \begin{bmatrix} I & -{}^0\hat{P}_{ne} \\ 0 & I \end{bmatrix} {}^0J_W$$

$${}^{0}P_{ne} = \begin{bmatrix} l_{3}c_{123} \\ l_{3}s_{123} \\ 0 \end{bmatrix} \Rightarrow {}^{0}\hat{P}_{ne} = \begin{bmatrix} 0 & 0 & l_{3}s_{123} \\ 0 & 0 & -l_{3}c_{123} \\ -l_{3}s_{123} & l_{3}c_{123} & 0 \end{bmatrix}$$

$$J_E = \begin{bmatrix} -l_1s_1 - l_2s_{12} - l_3s_{123} & -l_2s_{12} - l_3s_{123} & -l_3s_{123} \\ l_1c_1 + l_2c_{12} + l_3c_{123} & l_2c_{12} + l_3c_{123} & l_3c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



#### Resolved Motion Rate Control



$$\delta x = J(\theta)\delta\theta$$

Outside singularities:

$$\delta\theta = J(\theta)^{-1}\delta x$$

Arm at Configuration  $\theta$ :

$$x = f(\theta) \Rightarrow \delta x = x_d - x \Rightarrow \delta \theta = J(\theta)^{-1} \delta x$$

$$\theta^+ = \theta + \delta\theta$$

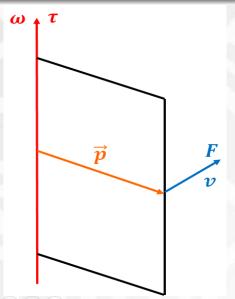


#### Jacobian

- Differential Motion
- Linear & Angular Motion
- Velocity Propagation
- Explicit Form
- Static Forces



## Angular/Torque -Velocities/Forces

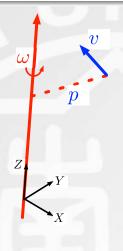


$$v = \omega \times p$$

$$\tau = p \times F$$



## Angular/Torque -Velocities/Forces

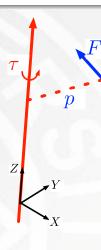


$$v = \omega \times p$$

$$v = -\hat{p}\omega$$

$$\begin{bmatrix} v_x \\ v_y \end{bmatrix} = \begin{bmatrix} -p_y \\ p_x \end{bmatrix} \dot{{\color{red}\theta}}$$

$$v=J\dot{ heta}$$



$$\tau = p \times F$$

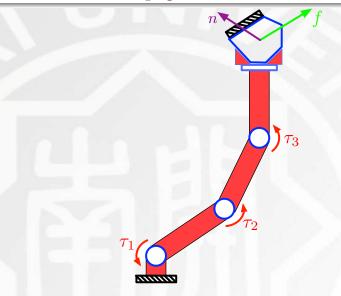
$$au = \hat{p} F$$

$${\color{red} \pmb{\tau}} = -\hat{p}^T {\color{red} \pmb{F}}$$

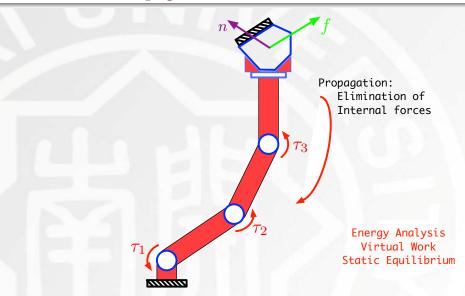
$$\boldsymbol{\tau} = \begin{bmatrix} \boldsymbol{p}_y \\ -\boldsymbol{p}_x \end{bmatrix} \begin{bmatrix} \boldsymbol{F}_x \\ \boldsymbol{F}_y \end{bmatrix}$$

$$\tau = J^T F$$

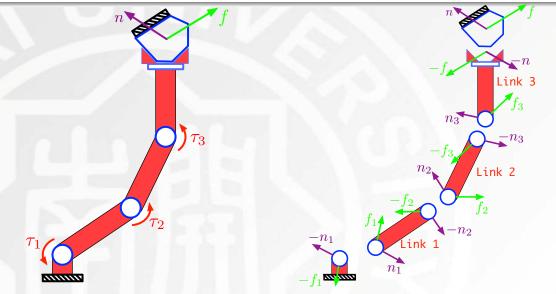




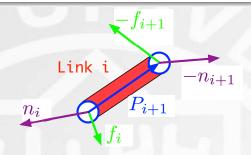




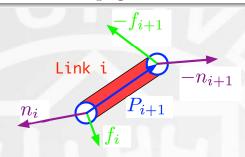








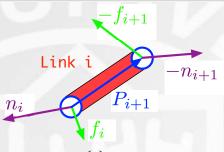




#### • Static Equilibrium:

$$\sum_{} \text{ forces} = 0$$
 
$$\sum_{} \text{ moments at a point} = 0$$





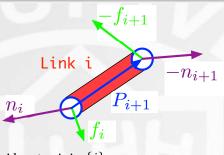
Static Equilibrium:

$$\sum_{} \text{ forces} = 0$$
 
$$\sum_{} \text{ moments at a point} = 0$$

• About origin  $\{i\}$ 

$$\begin{split} f_i + (-f_{i+1}) &= 0 \\ n_i + (-n_{i+1}) + P_{i+1} \times (-f_{i+1}) &= 0 \end{split}$$





Static Equilibrium:

$$\sum_{} \text{ forces} = 0$$

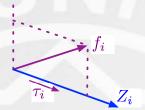
$$\sum_{} \text{ moments at a point} = 0$$

• About origin  $\{i\}$ 

$$\begin{split} f_i + (-f_{i+1}) &= 0 \\ n_i + (-n_{i+1}) + P_{i+1} \times (-f_{i+1}) &= 0 \end{split}$$

$$\begin{split} f_i &= f_{i+1} \\ n_i &= n_{i+1} + P_{i+1} \times f_{i+1} \end{split}$$

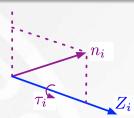




#### Prismatic Joint



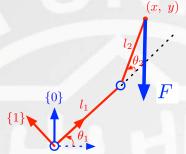
#### Algorithm:



#### Revolute Joint

$$\tau_i = n_i^T Z_i$$

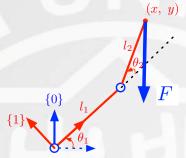




$$\begin{split} {}^{n}f_{n} &= {}^{n}f \\ {}^{n}n_{n} &= {}^{n}n + {}^{n}P_{n+1} \times {}^{n}f \\ {}^{i}f_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}f_{i+1} \\ {}^{i}n_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}n_{i+1} + {}^{i}P_{i+1} \times {}^{i}f_{i} \end{split}$$

• When 
$$l_1=l_2=1$$
,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0 & -1N\end{bmatrix}^T$ 

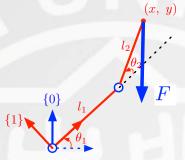




$$\begin{split} {}^{n}f_{n} &= {}^{n}f \\ {}^{n}n_{n} &= {}^{n}n + {}^{n}P_{n+1} \times {}^{n}f \\ {}^{i}f_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}f_{i+1} \\ {}^{i}n_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}n_{i+1} + {}^{i}P_{i+1} \times {}^{i}f_{i} \end{split}$$

- When  $l_1=l_2=1$ ,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0 & -1N\end{bmatrix}^T$
- 对于连杆 2:

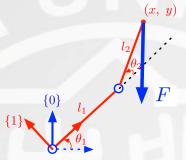




- When  $l_1=l_2=1$ ,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0 & -1N\end{bmatrix}^T$
- 对于连杆 2:

$$f_2 = F, \quad n_2 = n + \vec{l_2} \times F = \vec{l_2} \times F = \begin{bmatrix} 0 & 0 & -l_2 \cos(\theta_1 + \theta_2) N \end{bmatrix}^T$$





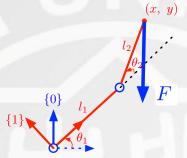
$$\begin{split} {}^{n}f_{n} &= {}^{n}f \\ {}^{n}n_{n} &= {}^{n}n + {}^{n}P_{n+1} \times {}^{n}f \\ {}^{i}f_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}f_{i+1} \\ {}^{i}n_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}n_{i+1} + {}^{i}P_{i+1} \times {}^{i}f_{i} \end{split}$$

- When  $l_1=l_2=1$ ,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0 & -1N\end{bmatrix}^T$
- 对于连杆 2:

$$f_2=F, \quad n_2=n+\vec{l_2}\times F=\vec{l_2}\times F=\begin{bmatrix}0 & 0 & -l_2\cos(\theta_1+\theta_2)N\end{bmatrix}^T$$

• 对于连杆 1:





$$\begin{split} {}^{n}f_{n} &= {}^{n}f \\ {}^{n}n_{n} &= {}^{n}n + {}^{n}P_{n+1} \times {}^{n}f \\ {}^{i}f_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}f_{i+1} \\ {}^{i}n_{i} &= {}^{i}_{i+1}R \cdot {}^{i+1}n_{i+1} + {}^{i}P_{i+1} \times {}^{i}f_{i} \end{split}$$

- When  $l_1 = l_2 = 1$ ,  $\theta_1 = 0$ ,  $\theta_2 = 60^0$ , and  $F = \begin{bmatrix} 0 & -1N \end{bmatrix}^T$
- 对于连杆 2:

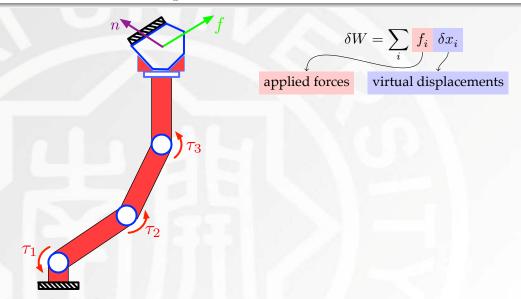
$$f_2=F, \quad n_2=n+\vec{l_2}\times F=\vec{l_2}\times F=\begin{bmatrix}0 & 0 & -l_2\cos(\theta_1+\theta_2)N\end{bmatrix}^T$$

• 对于连杆 1:

$$f_1 = f_2 = F, \quad n_1 = n_2 + \vec{l_1} \times f_2 = \begin{bmatrix} 0 & 0 & -[l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2)]N \end{bmatrix}^T$$

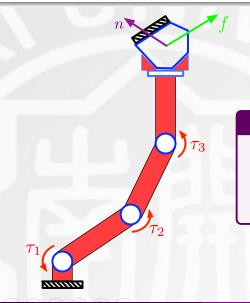


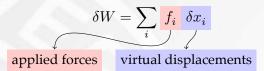
#### Virtual Work Principal





### Virtual Work Principal





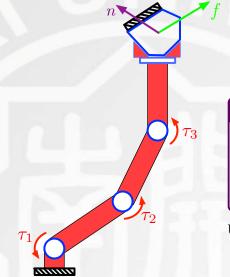
#### Static Equilibrium:

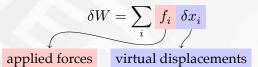
If the virtual work done by applied forces is zero in displacements consistent with constraints.

$$\tau^T \delta Q + (-F)^T \delta x = 0$$



## Virtual Work Principal





#### Static Equilibrium:

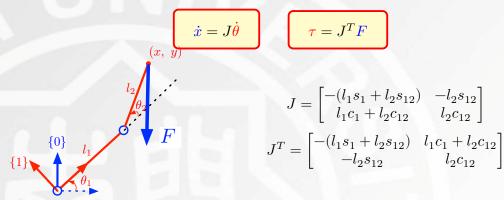
If the virtual work done by applied forces is zero in displacements consistent with constraints.

$$\tau^T \delta Q + (-F)^T \delta x = 0$$

Using 
$$\delta x = J\delta q$$

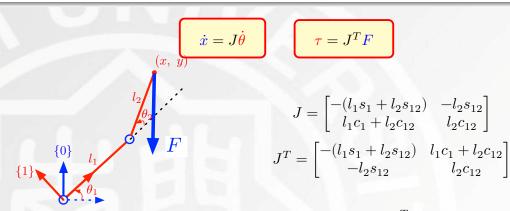
$$au = J^T F$$





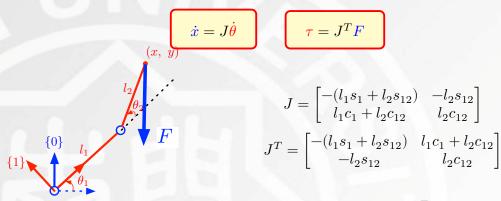
• When  $l_1=l_2=1$ ,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0 & -1N\end{bmatrix}^T$ 





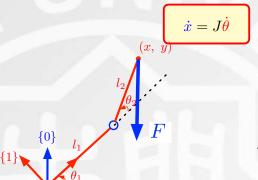
• When 
$$l_1=l_2=1$$
,  $\theta_1=0$ ,  $\theta_2=60^0$ , and  $F=\begin{bmatrix}0&-1N\end{bmatrix}^T$  
$$\tau=\begin{bmatrix}-(l_1s_1+l_2s_{12})&l_1c_1+l_2c_{12}\\-l_2s_{12}&l_2c_{12}\end{bmatrix}\begin{bmatrix}0\\-1N\end{bmatrix}=-\begin{bmatrix}3/2\\1/2\end{bmatrix}$$





• When  $l_1=l_2=1$ ,  $\theta_1=90^0$ ,  $\theta_2=0^0$ , and  $F=\begin{bmatrix}0&-1000N\end{bmatrix}^T$ 





$$au = J^T F$$

$$J = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & -l_2s_{12} \\ l_1c_1 + l_2c_{12} & l_2c_{12} \end{bmatrix}$$
$$J^T = \begin{bmatrix} -(l_1s_1 + l_2s_{12}) & l_1c_1 + l_2c_{12} \\ -l_2s_{12} & l_2c_{12} \end{bmatrix}$$

• When 
$$l_1=l_2=1$$
,  $\theta_1=90^0$ ,  $\theta_2=0^0$ , and  $F=\begin{bmatrix}0&-1000N\end{bmatrix}^T$  
$$\tau=\begin{bmatrix}-(l_1s_1+l_2s_{12})&l_1c_1+l_2c_{12}\\-l_2s_{12}&l_2c_{12}\end{bmatrix}\begin{bmatrix}0\\-1KN\end{bmatrix}=\begin{bmatrix}0\\0\end{bmatrix}$$



## 第五章 机器人速度与雅可比

Chapter 5 Instantaneous Kinematics

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