

# AE 342 : Modeling and Analysis Lab, Session 4

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## 1 Problem 1

A simple 1D heat diffusion problem with Dirichlet boundary conditions is simulated. The governing equations and boundary conditions are provided as follows

$$\frac{d^2u}{dx^2} = 1, 0 < x < 1 \quad (1)$$

$$u(x = 0) = 0, u(x = 1) = 0 \quad (2)$$

The problem is solved in FreeFEM++ using the given code for a 1D domain.

```
1 load "msh3"
2 real m = 100;
3 int l=1;
4 meshL Th = segment(m,[x*1]);
5 real[int] xaxis(m+1), Uline(m+1);
6 ofstream file2("Results.csv");
7
8 fespace Vh(Th, P1);
9 Vh U, v;
10
11 solve Poission(U,v)= int1d(Th)(dx(U)*dx(v))
12     +int1d(Th)(v)
13     +on(1,2, U=0);
14
15 plot(U, value=true);
16 for(int i=0; i<=m; i++){
17
18     xaxis[i] = i/m;
19     Uline[i] = U[][i];
20     file2 << xaxis[i] << "," << Uline[i] << endl ;
21 }
```

Listing 1: Problem 1 Code

The analytical solution for the problem is given as  $U = \frac{1}{2}(x^2 - x)$ . The solution of FreeFEM is compared to the analytical solution,

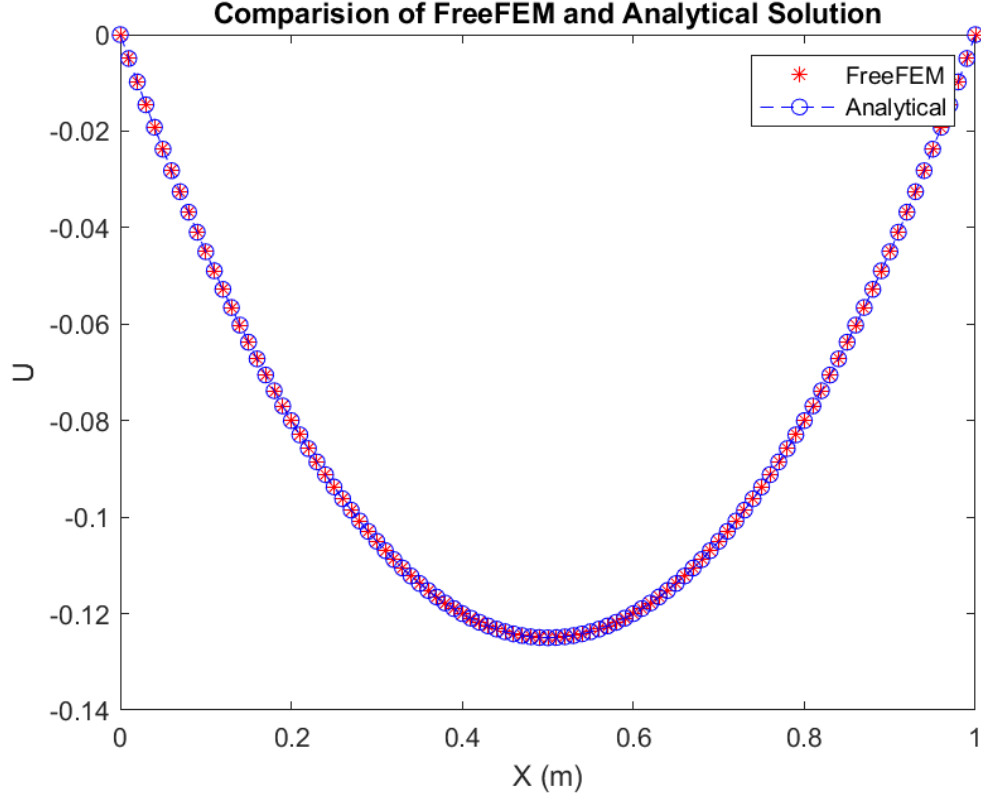


Figure 1: Comparison of the FreeFEM Solution with analytical solution for Problem 1.

## 2 Problem 2

Consider a 1mm diameter, 50mm long aluminium pin-fin. The fin's left end interfaces with a constant heat source at a temperature of  $T_h = 300^\circ C$ , while its right end is thermally insulated. Heat is progressively released along the fin's length through convection, interacting with an ambient temperature of  $T_\infty = 30^\circ C$ . The governing differential equation is given by:

$$k \frac{d^2 T}{dx^2} = \frac{Ph}{A} (T - T_\infty) \quad (3)$$

In equation 3, the thermal conductivity ( $k$ ) is 200 W/mK and the convective heat transfer coefficient ( $h$ ) is  $20 W/m^2 K$ .  $P$ ,  $A$  represents perimeter and area of cross-section of the fin. Establish a model for the temperature distribution along the fin under these specific conditions and compare with analytical results.

The weak form of the equation 3 is given as

$$\int_{\phi} \left( k \frac{dT}{dx} \frac{dv}{dx} + \frac{Ph}{A} (T - T_\infty) \right) dx = 0 \quad (4)$$

The problem is solved in FreeFEM++ using the given code for a 1D domain.

```

1 load "msh3"
2 real m = 100;
3 real d = 0.001;
4 int h = 20;
5 int k = 200;
6 real l=0.05;
7 int Ti = 300;
8 int Tf = 30;
9 real p = pi * d;
10 real A = pi * d * d / 4;
11
12 meshL Th = segment(m,[x*1]);
13
14 real[int] xaxis(m+1), Uline(m+1);
15 ofstream file2("results2.csv");
16
17 fespace Vh(Th, P1);
18 Vh T, v;
19
20 solve Poission(T,v) = int1d(Th)(k*dx(T)*dx(v))
21                      +int1d(Th)(p*h/A*T*v)
22                      -int1d(Th)(p*h/A*Tf*v)
23                      +on(1, T=300);
24
25 plot(T, value=true, wait=true, fill=true, aspectratio=true);
26 for(int i=0; i<=m; i++){
27
28     xaxis[i] = l * i/m;
29     Uline[i] = T[][i];
30     file2 << xaxis[i] << "," << Uline[i] << endl ;
31 }

```

Listing 2: Problem 2 Code

The analytical solution for the problem is given as  $T = T_{\infty} + \left(\frac{270}{1+e^{2ml}}\right) (e^{mx} + e^{2ml-mx})$ . The solution of FreeFEM is compared to the analytical solution in Figure 2.

When the right end is subjected to the ambient temperature  $T_{\infty} = 30$  instead of the adiabatic condition. The analytical solution of the problem is given as  $T = T_{\infty} + \left(\frac{-270}{1-e^{2ml}}\right) (e^{mx} - e^{2ml-mx})$ . The result of this problem solved in FreeFEM is again compared to the analytical solution in Figure 3.

```

1 solve Poission(T,v) = int1d(Th)(k*dx(T)*dx(v))
2                      +int1d(Th)(p*h/A*T*v)
3                      -int1d(Th)(p*h/A*Tf*v)
4                      +on(1,T=300)
5                      +on(2,T=30);

```

Listing 3: Change in the Problem 2 Code to accomodate for the Dirchlet B.C. at the right end

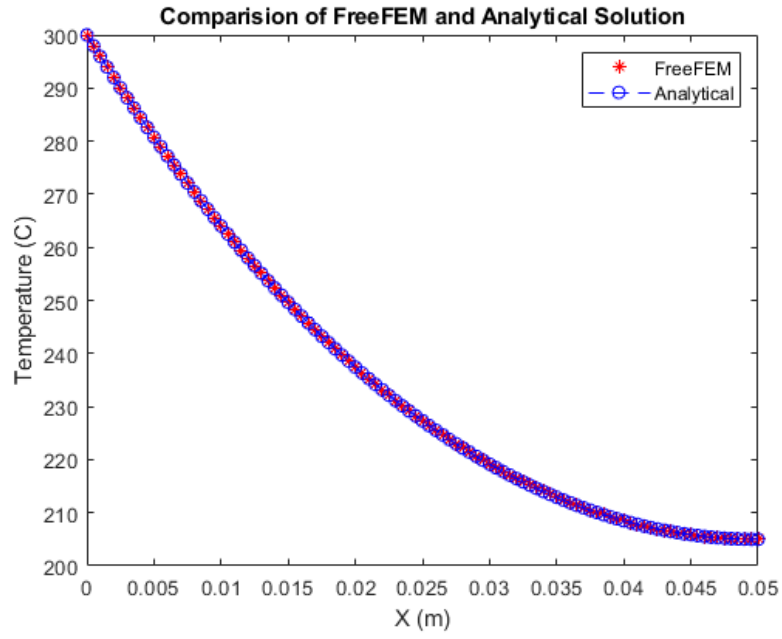


Figure 2: Comparison of the FreeFEM Solution with analytical solution for Problem 2.

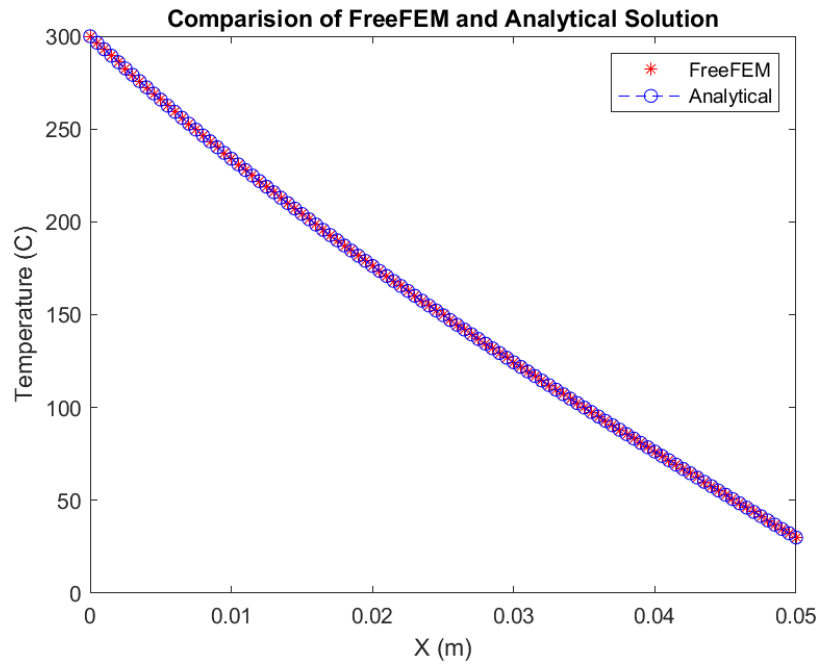


Figure 3: Comparison of the FreeFEM Solution with analytical solution for Problem 2 with Dirichlet boundary condition at right end.

### 3 Problem 3

Consider a rectangular plate of dimensions  $L_x \times L_y$ , where one side is insulated, while the other three sides are maintained at constant temperatures. The temperature distribution  $T(x, y)$  in the plate is governed by Laplace's equation:

$$\nabla^2 T = 0 \quad (5)$$

#### Boundary Conditions:

- At  $x = 0$ :  $\frac{\partial T}{\partial x} = 0$
- At  $x = L_x$ :  $T(L_x, y) = 200^\circ C$
- At  $y = 0$ :  $T(x, 0) = 150^\circ C$
- At  $y = L_y$ :  $T(x, L_y) = 150^\circ C$

The weak formulation of the laplace equation is given as,

$$\int_{\phi} \left( \frac{dT}{dx} \frac{dv}{dx} + \frac{dT}{dy} \frac{dv}{dy} \right) dx = 0 \quad (6)$$

```
1 load "msh3"
2
3 real Lx = 1;
4 real Ly = 2;
5 int m = 100;
6 int n = 200;
7 mesh Th=square(m,n,[Lx*x,Ly*y]);
8 //plot(Th, wait=true);
9 //real[int] V = [150, 155, 160, 165, 170, 175, 180, 185, 190, 195, 200];
10
11 fespace Vh(Th, P1);
12 Vh T, v;
13
14 solve Laplace(T,v) = int2d(Th)(dx(T)*dx(v) + dy(T)*dy(v))
15     +on(1,3,T=150)
16     +on(2,T=200);
17
18 plot(T, wait=true, fill=true, value=true, aspectratio=true);
```

Listing 4: Code to solve Problem 3 in FreeFEM

The temperature distribution  $T(x, y)$  for the problem 3 is plotted in Figure 4.

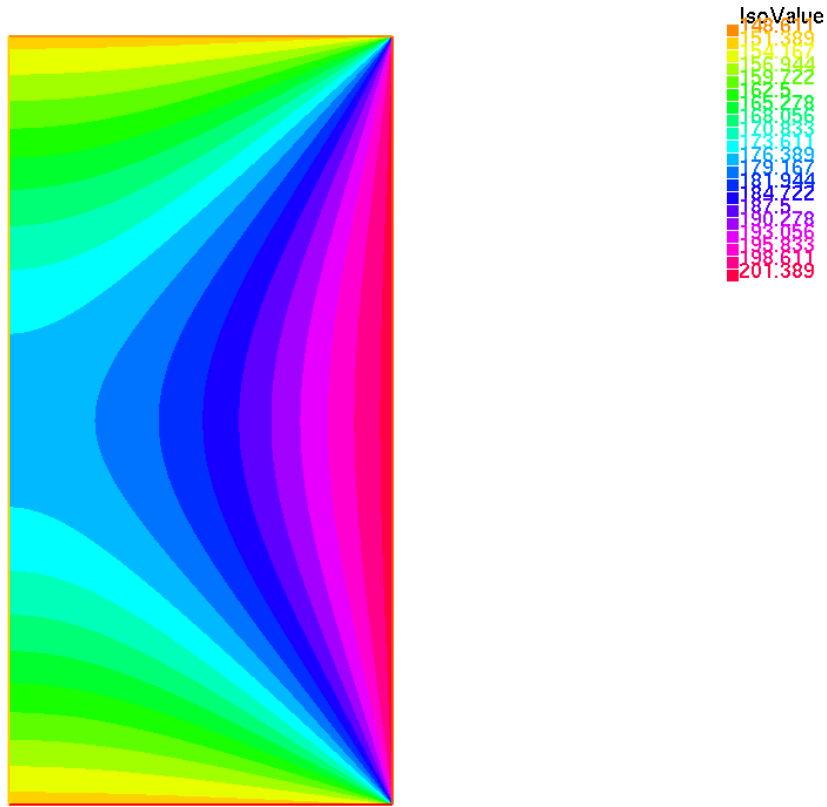


Figure 4: temperature distirbution  $T(x, y)$  for the problem 3 plotted in FreeFEM.