Parallel Hierarchic Adaptive Stabilized Transient Analysis (PHASTA)

TABLE OF CONTENTS

I. Incompressible Navies-Stokes equation	2
II. Mappings	8
III. Implicit time integration	12
IV. Boundary condition	17

I. Incompressible Navies-Stokes equation

Let us state incompressible Navies- Stokes equation (strong form)

$$u_{i,i} = 0 \tag{1}$$

$$\rho u_{i,t} + \rho u_i u_{i,j} + P_{i,i} - \tau_{i,j,j} - f_i = 0$$
 (2)

Inertia (per volume)

Divergence of stress

$$\overbrace{\rho(\frac{\partial v}{\partial t} + \underline{v \cdot \nabla v})} = \underbrace{-\nabla p + \underline{\mu} \nabla^2 v + \underline{f}}$$

Unsteady Convective Pressure Viscosity acceleration acceleration

gradient

- (1) is mass conversation
- (2) are 3 momentum conservation equation

Finite element approach uses weak form of equations.

Let us derive it:

Introducing new notation $\mathcal{L}_i \triangleq l. h. s$ (2)

Let's write (1)*q+ $\sum_{i=1}^{3}$ (2) * w_i ; integrating it over our domain Ω ($\Gamma \triangleq \partial \Omega$)

$$0 = \int_{\Omega} \left[qu_{i,i} + w_i l_i \right] d\Omega = \int_{\Omega} \left[qu_{i,i} + w_i (\rho u_{i,t} + \rho u_j u_{i,j} + P_{,i} - \tau_{ij,j} - f_i) \right] d\Omega$$
 (3)

In order to get weak form, we will integrate continuity and stress term of momentum equation by partly recall that

$$\int_{\Omega} aB_{,i}d\Omega = \int_{\Omega} [aB]_{,i}d\Omega - \int_{\Omega} a_{,i}Bd\Omega$$

$$= \int_{\Gamma} aBn_{i}d\Gamma - \int_{\Omega} a_{,i}Bd\Omega$$
(4)

Taking (4) into account we can rewrite (3) as:

$$0 = \int_{\Omega} \left[-q_{,i}u_{i} + w_{i}(\rho u_{i,t} + \rho u_{j}u_{i,j} - f_{i}) \right] + w_{i,j} \{ -P\delta_{ij} + \tau_{ij} \} d\Omega$$

$$+ \int_{\Gamma} \left[qu_{i}n_{i} - w_{i}(\tau_{ij} - P\delta_{ij})n_{j} \right] d\Gamma$$

$$(5)$$

--Weak Galvevkin Form (this is the simplest form for I.N.S equation, which is unstable. On Page 9. We'll introduce a stabilization term, and on Page 9 we'll consider an additional mass conservation term (i.e. term, which makes the mass conservation equation satisfied).

Now let's see what we can do with eqn (5), assuming that it doesn't need any extra terms In order to solve (5), we have to propose trial solution y(x,y,z,t) and weight function w(x,y,z)

$$w_{i} = \sum_{A=1}^{n_{np}} N_{i}^{A}(x) w_{i}^{A} \tag{6}$$

w:

$$q = \sum_{A=1}^{n_{np}} N_P^A(x) q^A \tag{7}$$

$$u_{i} = \sum_{B=1}^{n_{np}} N_{i}^{B}(x) u_{i}^{B}$$
 (8)

$$u_{i,t} = \sum_{B=1}^{n_{np}} N_i^B(x) u_{i,t}^B \tag{9}$$

$$P = \sum_{B=1}^{n_{np}} N_P^B(x) p^B$$
 (10)

Here we used A for weight function and B for trial function Let's plug (6) & (7) into (5)

$$\sum_{i=1}^{3} \sum_{A=1}^{n_{np}} w_{i}^{A} \left\{ \int_{\Omega} \left[N_{i}^{A} [\rho \, u_{i,t} + \rho u_{j} u_{i,j} - f_{i} \right] + N_{i,j}^{A} [\tau_{ij} - P \sigma_{i,j}] \right] d\Omega + \int_{\Gamma} -N_{i}^{A} \{ \tau_{ij} - P \delta_{ij} \} d\Gamma \}$$

$$+ \sum_{A=1}^{n_{np}} q^{A} \{ \int_{\Omega} -N_{p,i}^{A} u_{i} d\Omega + \int_{\Gamma} N_{p}^{A} u_{i} n_{i} d\Gamma \} = 0$$

$$(11)$$

Here we wrote momentum eq. contribution in the first term and continuity in the second term:

$$\sum_{i=1}^{3} \sum_{A=1}^{n_{np}} w_i^A R_i^{m_A} + \sum_{A=1}^{n_{np}} q^A R_i^{c_A} = 0$$
 (12)

Where R_i^{m} , i=1,2,3 are momentum residuals, R_i^{m} is continuity residual

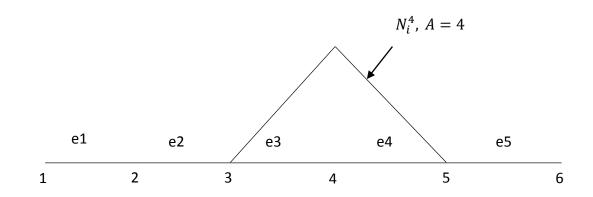
Provided that $w_i^A \& q^A$ are arbitrary we can conclude that

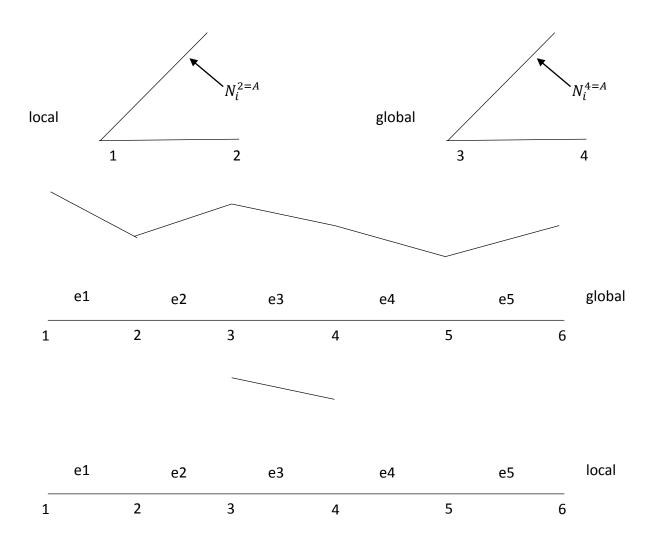
$$\widetilde{R} = \left\{ R_i^A \right\}_{3 \times n_{np}} = 0$$
(13)

$$\widetilde{R} = \left\{ R^A \right\}_{1 \times n_{np}} = 0$$
(14)

We don't evaluate integral (11) globally, we'll do it from local point of view, which is more efficient. To emphasize the local point of view, we'll use lower case superscripts a & B.

1d example





$$f(x) = \sum_{A=1}^{n_{np}} N_i^A f^A$$

$$\hat{f}(x) = \sum_{a=1}^{n_a^1 = 2} N_i^a f^a$$

Where

in our example

Now we have to break up the integral

$$\int_{\Omega} (.)d\Omega = \sum_{e=1}^{n_{ee}} \int_{\Omega^e} (.)d\Omega^e$$
 (15)

Let's consider in detail one of elements, and write out the continuity residual for it:

$$R^{ae} = \int_{\Omega^e} -N^a_{p,i} u_i d\Omega + \int_{\Gamma^e} N^a_p u_i n_i d\Gamma$$
(16)

Note: Γ^e is only the portion of the boundary of Ω^e that is part of real Γ

How to collect integral back according to (15)? (Put together all element integrals)

We can generate a connectivity table:

el # local node #	1	2
1	1	2
2	2	3
3	3	4

L, this is 1d example.

In the code we have ien (1:npro, 1:hshl), where 1:npro is el # and 1:hshl is local node # Using this table we can do assemble operation $R^{c}_{A} = \mathbb{A}^{n_{ee}}_{e=1} R^{n_{ee}}$ Which can be in the code as:

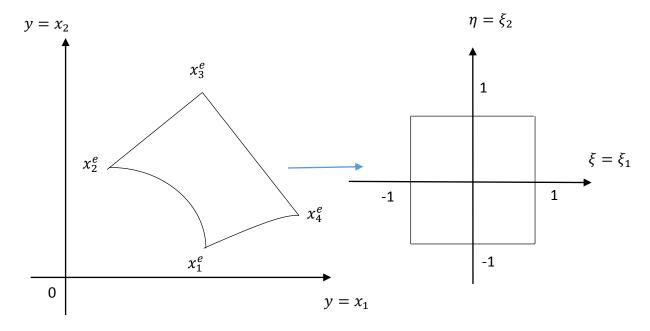
$$R^{A} = 0$$

$$\begin{cases}
do i = 1, n_{el} \\
do a = 1, n_{en} \\
A = ien(e, a)
\end{cases}$$
 $R^{A} = R^{A} + R^{ca}$

$$\begin{cases}
end \ do \\
end \ do
\end{cases}$$

II. Mappings

In order to make the integrals easier to evaluate, we need to map elements to a canonical element, e.g. in 2d



Mapping will do for us following transformations:

$$\mathbf{x}(\xi) \leftrightarrow \xi(\mathbf{x})$$

$$\Omega^e \leftrightarrow \blacksquare$$

$$\Gamma^e \leftrightarrow \blacksquare_{\Gamma}$$

$$\mathrm{d}\Omega^e \leftrightarrow \mathrm{d}\blacksquare$$

 $\mathrm{d}\Gamma^e \leftrightarrow \mathrm{d} \blacksquare_\Gamma$

Derivation

$$\frac{\partial N^a}{\partial x_i} = N^a_{,i}(\xi) = \frac{\partial N^a}{\partial \xi_j} \frac{\partial \xi_j}{\partial x_i} = N^a_{,\xi_j} \xi_{j,i}$$
(17)

Where $\xi_{j,i}$ will be different for each element

Integrals:

$$\int_{\Omega^e} f(x) \, d\Omega = \int_{\blacksquare} f(x(\xi)) D(\xi) d \blacksquare$$
 (18)

$$D(\xi) = \det(x, \xi) = \det(x_i, \xi_i)$$
(19)

--Jacobian of the mapping $x(\xi)$

The advantage of using mappings:

Each element looks the same after applying the mapping→ all of the elements will be treated by the same routine (if they are the same type, like triangular, quadrilateral, tetrahedron, wedge, brick and pyramid, of course).

Let's rewrite (16) using mapping

$$R^{a} = \int_{\blacksquare} -N_{P,i}^{a} u_{i} D d \blacksquare + \int_{\blacksquare_{\Gamma}} N_{P}^{a} u_{i} n_{i} D_{\Gamma} d \blacksquare_{\Gamma}$$

$$(20)$$

Q: How do we evaluate integrals?

A: Using Gauss's quadrature

$$R^{ae} = \int_{\blacksquare} r^{ae} (\xi) d \blacksquare = \sum_{k=1}^{n_{int}} r^{ae} (\xi_k) w_R$$
 (21)

Where $r^{e}_{ae}(\xi_{\nu})$ - function value at point ξ_k , w_k - weight for the k^{th} quadrature point

We mentioned on Page 2 that Galerkin form (5) is unstable and we need an extra term to make it stable

$$\sum_{e=1}^{n_{ee}} \int_{\Omega^e} \left[\underline{\tau_M \left\{ u_j w_{i,j} + \frac{q_{,i}}{\rho} \right\} \mathcal{L}_i} + \underline{\tau_c w_{j,j} u_{i,i}} \right] d\Omega^e$$
 (22)

Momentum conservation continuity

The first term represents the momentum conservation and the second term represents the continuity.

To make continuity equation satisfied, we also have to add a mass conservation term to the Galerkin form (5).

$$\sum_{e=1}^{n_{ee}} \int_{\Omega^e} \left[w_i \rho u_j^{\Delta} u_{i,j} + \tau \left\{ \frac{\rho u_j^{\Delta}}{\tau_M} \right\} w_{i,j} \left\{ \frac{\rho u_k^{\Delta}}{\tau_M} \right\} u_{i,k} \right] d\Omega^e$$
 (23)

Adding together eqns (5), (22) & (23), we can write

$$0 = \int_{\Omega} \left\{ -q_{,i}^{1} u_{i} + w_{i} \left\{ \rho u_{i,t}^{2} + \rho u_{j}^{3} u_{i,j} - f_{i}^{4} \right\} + w_{i,j} \left\{ \tau_{ij}^{5} - \rho \delta_{ij}^{6} \right\} \right\} d\Omega$$

$$+ \int_{\Gamma} \left\{ q u_{i}^{7} n_{i} - w_{i} \left\{ \tau_{ij}^{8} - \rho \delta_{ij}^{9} \right\} n_{j} \right\} d\Gamma + \sum_{e=1}^{n_{el}} \int_{\Omega^{e}} \left[\tau_{M} \left\{ u_{j}^{10} w_{i,j} + \frac{q_{,i}^{11}}{\rho} \right\} \mathcal{L}_{i} + \tau_{c} w_{j,j}^{12} u_{i,i} \right] d\Omega^{e}$$

$$+ \sum_{e=1}^{n_{el}} \int_{\Omega^{e}} \left[w_{i} \rho u_{j}^{13} u_{i,j} + \tau \left\{ \frac{\rho u_{j}^{\Delta}}{\tau_{M}} \right\} w_{i,j} \left\{ \frac{\rho u_{k}^{\Delta}}{\tau_{M}} \right\} u_{i,k} \right] d\Omega^{e}$$

$$+ \Omega \left\{ \frac{\rho u_{i}^{\Delta}}{\rho} \right\} u_{i,k} d\Omega^{e}$$

Where

$$\stackrel{\scriptscriptstyle \Delta}{u_j} = -\tau_M \frac{\mathcal{L}_j}{\rho}, \, \bar{u}_j = u_j + \stackrel{\scriptscriptstyle \Delta}{u_j} = u_j - \tau_M \frac{\mathcal{L}_j}{\rho}$$
(25)

Now we can put all terms of eq. (24) into residual vectors (13) & (14).

Note that

$$-R^{M}$$
 goes to res(1: n_{np} ; 1:3)

$$-R^{A}$$
 goes to res(1: n_{np} ; 4)

- We assemble these global residuals from element level integrations

Let's state that local form of the residuals (which are stored in -rl(:,;;:) in the code:

$$R_{i}^{m} = \int_{\blacksquare} \left[N_{i}^{a} \left\{ \rho u_{i,t}^{2} + \rho u_{k} u_{i,k}^{3+13} - f_{i}^{4} \right\} + N_{i,k}^{a} \left\{ \tau_{ik}^{5} - \rho \delta_{ik}^{6} \right\} + N_{i,k}^{a} \tau_{M} u_{k} \mathcal{L}_{i} \right.$$

$$\left. + N_{i,i}^{12} \tau_{c} u_{k,k}^{2} + N_{i,l}^{14} \tau_{u_{i,k}} \mathcal{L}_{l} \mathcal{L}_{k} \right] \mathrm{Dd} \blacksquare - \int_{\blacksquare_{\Gamma}} N_{i}^{a} (\tau_{ik}^{8} - \rho \delta_{ik}^{9}) n_{k} D_{r} d \blacksquare_{\Gamma}$$

$$(26)$$

$$R^{a} = \int_{\blacksquare} -N_{p,k}^{a} u_{k} \operatorname{Dd} \blacksquare + \int_{\blacksquare} N_{p}^{a} u_{k} n_{k} D_{r} d \blacksquare_{\Gamma}$$

$$(27)$$

Note: $\tau_{ik} = \mu(\frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i})$

In terms (15), (18) & (20) of eq (26), we have the following undefined so far parameters: (e2stab.f)

$$\tau_{M} = \left[\left(\frac{2C_{1}}{\Delta t} \right)^{2} + u_{e}u_{in}g_{em} + C_{2}D^{2}g_{em}g_{em} \right]^{-1/2}$$
(28)

$$\tau_c = \frac{\rho}{8\tau_M g_u} \tag{29}$$

$$\tau = \frac{\tau_M}{\sqrt{\mathcal{L}_l \mathcal{L}_m g_m}} \tag{30}$$

Where g_{ij} is the metric tensor:

$$g_{ij} = \xi_{k,i}\xi_{k,j} = \frac{d\xi_k}{dx_i}\frac{d\xi_k}{dx_j}$$
(31)

III. Implicit time integration

Let's describe the i^{th} iteration, moving from time step n to time step n+1, according to Generalized Alpha Method

Let's first write it out for velocity vector

$$u^{n+1} = u^{n} + \Delta t u_{,t}^{n} + \Delta t \cdot \gamma (u_{,t}^{n+1} - u_{,t}^{n})$$
 (OD 1)

$$R^{A}\left(u_{t}^{B(i)}; u_{t}^{B(i)}; p_{t}^{B(i)}; p_{t}^{B(i)}\right) \cong 0$$

$$(OD 2)$$

$$u_{t}^{n+\alpha_{m}} = u_{t}^{n} + \alpha_{m}(u_{t}^{B(i)} - u_{t}^{B})$$
(OD 3)

$$u^{B(i)} = u^{B} + \alpha_{f}(u^{B(i)} - u^{B})$$
 (OD 4)

Same equation for pressure:

$$P^{B(i)} = P^{B} + \Delta t P_{t}^{B} + \Delta t \gamma (P_{t}^{B(i)} - P_{t}^{B})$$
(P1)

$$R^{a}\left(u_{t}^{B(i)}, u_{t}^{B(i)}, p_{t}^{B(i)}\right) \cong 0$$
(P2)

$$p_{,t}^{n+\alpha_{m}} = p_{,t}^{n} + \alpha_{m}(p_{,t}^{B(i)} - p_{,t}^{B})$$
(P3)

$$p^{B(i)} = p^{B} + \alpha_{f}(p_{.t}^{B(i)} - p_{.t}^{B})$$
(P4)

How predictor-multicorrector works?

1) predict
$$u^{(i)} = u^{n+1}$$
, $p^{(i)} = p^{n}$

2) invert (*OD 1*):

$$u_{,t}^{(i)} = \frac{1}{\gamma \Delta t} \left[u^{(i)} - u^{n} \right] + (1 - \frac{1}{\gamma}) u_{,t}^{n}$$

Invert (P1)

$$p_{,t}^{(i)} = \frac{1}{\gamma \Delta t} \begin{bmatrix} p^{(i)} - p \\ p^{(i)} - p \end{bmatrix} + (1 - \frac{1}{\gamma}) p_{,t}^{n}$$

3) evaluate: $u_{,t}^{(i)}$; $u_{,t}^{(i)}$; $p_{,t}^{(i)}$; $p_{,t}^{(i)}$; $p_{,t}^{(i)}$

4) evaluate: $R^{M} \neq 0$, $R^{A} \neq 0$

Reture to 1) increasing the iteration number i until residuals will be close enough to zero

Q: How we will choose u^B , $u_{,t}^B$, p^B in order to get zero residuals?

A: we will use an analog of Newton's method $(x^{(i+1)} = x^{(i)} - \frac{f(x^{(i)})}{\frac{df}{dx}|_{x^{(i)}}}$ for f(x) = 0)

Let's linearize eqn (OD 2) and (P 2) about $u_{,t}^{n+1}$ and $p_{,t}^{n+1}$:

$$\sum_{B=1}^{n_{np}} \left\{ \frac{\partial R^{A}}{\partial u_{,t}^{B}} \Delta u_{,t}^{B} + \frac{\partial R^{A}}{\partial p_{,t}^{B}} \Delta p_{,t}^{B} \right\} = -R^{A}$$
(32)

$$\sum_{B=1}^{n_{np}} \left\{ \frac{\partial R^{A}}{\partial u_{,t}^{B}} \Delta u_{,t}^{B} + \frac{\partial R^{A}}{\partial p_{,t}^{B}} \Delta p_{,t}^{B} \right\} = -R^{A}$$

$$(33)$$

Introducing new notation we can rewrite these equations as:

$$\sum_{B=1}^{n_{np}} \{ K^{AB} \Delta u_{,t}^{B} + G^{AB} \Delta p_{,t}^{B} \} = -R^{A}$$
 (34)

$$\sum_{B=1}^{n_{np}} \{ D^{AB} \Delta u_{,t}^{n+1} + C^{AB} \Delta p_{,t}^{B} \} = -R^{A}$$
(35)

Or, in matrix form

$$\begin{bmatrix} K & G \\ D & C \end{bmatrix} \begin{Bmatrix} \Delta u_{,t} \\ \Delta p_{,t} \end{Bmatrix} = \begin{Bmatrix} -R \\ c \\ -R \end{Bmatrix} = -\{R\}$$
(36)

Let's write the alternate form of eq. (27) for L.N.S tangent of continuity

$$R^{a} = \int N_{p}^{a} u_{k,k} Dd \blacksquare + \int N_{p,k}^{a} \tau_{M} \frac{\mathcal{L}_{k}}{\rho} Dd \blacksquare$$
 (37)

Now we write matrices K, G D & C at the element level:

$$R^{aB} = \frac{\partial R^{a}}{\partial u_{,t}^{B}} = R_{ij}^{aB} = \frac{\partial R_{i}^{a}}{\partial u_{j,t}^{B}} = \sum_{C=1}^{n_{np}} \left\{ \frac{\partial R_{i}^{a}}{\partial u_{k}^{C}} + \frac{\partial R_{i}^{a}}{\partial u_{k}^{C}} + \frac{\partial R_{i}^{a}}{\partial u_{k,t}^{C}} + \frac{\partial R_{i}^{a}}{\partial u_{k,t}^{$$

$$G_i^{aB} = \frac{\partial R_i^a}{\partial p_{,t}^{B}} = \alpha_f \gamma \Delta t \frac{\partial R_i^a}{\partial p_{,t}^{B}}$$

$$\frac{\partial R_i^a}{\partial p_{,t}^{B}} = \alpha_f \gamma \Delta t \frac{\partial R_i^a}{\partial p_{,t}^{B}}$$
(39)

$$D_{j}^{aB} = \frac{\partial \overset{C4LNS}{R^{a}}}{\partial u_{j,t}^{B}} = \frac{\partial \overset{C4LNS}{R^{a}}}{\partial u_{j}^{B}} \alpha_{f} \gamma \Delta t + \frac{\partial \overset{C4LNS}{R^{a}}}{\partial u_{j,t}^{B}} \alpha_{m}$$

$$(40)$$

$$C^{aB} = \frac{\partial R^{a}}{\partial P_{,t}} = \frac{\partial R^{a}}{\partial P_{,t}} = \frac{\partial R^{a}}{\partial P_{,t}} \alpha_{f} \gamma \Delta t$$

$$(41)$$

Let us write out some derivations in terms of shape function

$$\frac{\partial u_{i,t}^{B}}{\partial u_{j,t}^{B}} = \frac{\partial \left(\sum_{C=1}^{n_{en}} N_{i}^{C} u_{i,t}^{C}\right)}{\partial u_{j,t}^{B}} = \sum_{C=1}^{n_{en}} N_{i}^{C} \delta_{ij} \delta_{eB} = N_{i}^{B} \delta_{ij} \tag{42}$$

$$\frac{\partial u_{i,k}}{\partial u_{j}^{n+\alpha_{f}}} = \frac{\partial \left(\sum_{C=1}^{n_{en}} N_{i,k}^{C} u_{i}^{n+\alpha_{f}}\right)}{\partial u_{j,t}^{B}} = \sum_{C=1}^{n_{en}} N_{i,k}^{C} \delta_{ij} \delta_{eB} = N_{i,k}^{B} \delta_{i,j} \tag{43}$$

$$\frac{\partial P}{\partial p^{B}} = N_{p}^{B} \tag{44}$$

$$\frac{\partial u_{k,i}}{\partial u_{k,i}^{B}} = N_{k,i} \delta_{kj}$$

$$\partial u_{i}^{B}$$
(45)

$$\frac{\partial u_{k,k}}{\partial u_{j}^{B}} = N_{j,j}^{B}$$

$$\partial u_{j}^{B}$$
(46)

Consider matrices (38)~ (42) in detail:

$$K_{ij}^{aB} = \int_{\blacksquare} N_{i}^{a} \rho \alpha_{m_{u}} N_{i}^{B} \delta_{ij} + \alpha_{f_{u}} \gamma_{u} \Delta t N_{i}^{a} \rho u_{k} N_{i,k}^{B} \delta_{ij} + \alpha_{f_{u}} \gamma_{u} \Delta t N_{i,k}^{a} \{\mu N_{j,k}^{B} + \tau_{M} u_{k} \rho u_{e} N_{j,e}^{B} + \tau \mathcal{L}_{k} \mathcal{L}_{e} N_{j,e}^{B} \}$$

$$+ \alpha_{f_{u}} \gamma_{u} \Delta t \{\mu N_{i,j}^{a} N_{j,i}^{B} + N_{i,j}^{a} \tau_{C} N_{j,j}^{B} \} D d \blacksquare$$

$$(47)$$

$$G_i^{aB} \approx -\alpha_{f_p} \gamma_p \Delta t \int_{\blacksquare} N_{i,i}^a N_p^B D d \blacksquare$$
 (48)

$$D_j^{aB} \approx \alpha_{f_u} \gamma_u \Delta t \int_{\blacksquare} N_p^a N_{j,j}^B D d \blacksquare = -\{G^{Ba}\}^T$$
(49)

$$C^{aB} \approx \int_{\blacksquare} N_{p,k}^{a} \tau_{m} N_{p,k}^{B} \alpha_{f_{p}} \gamma_{p} \Delta t D d \blacksquare$$
 (50)

IV. Boundary condition

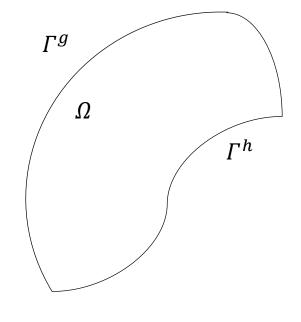
Generally, we can have 2 types of boundary

Conditions:

1)
$$\varphi = \varphi^g$$
 on Γ^g

3 names of the same thing $\begin{cases} \textit{Dirichlet} \\ \textit{essential} \\ \textit{nodal} \end{cases}$

2)
$$\frac{\partial \varphi}{\partial n} = \varphi^h$$
 on Γ^h
$$\begin{cases} new \\ natural \\ face \end{cases}$$



Plus, we already described "periodical" boundary condition

Let's consider essential B.C's

$$y = \begin{cases} p \\ u \\ v \\ w \\ T \end{cases}$$

$$q = \begin{cases} u_r^g \\ u_s^g \\ u_t^g \end{cases}$$

--vector of quantities, which can be prescribed

(we are not considering pressure because this type of boundary condition is almost not applicable for it)

 $u = (u_r, u_s, u_t) \leftarrow local\ coordinate\ system\ (may\ not\ be\ aligned\ with\ Cartesian)$

In general, we can express one in terms of another using direction cosines:

$$u_r^g = C_1^r u_1 + C_2^r u_2 + C_3^r u_3$$
$$u_s^g = C_1^s u_1 + C_2^s u_2 + C_3^s u_3$$
$$u_t^g = C_1^t u_1 + C_2^t u_2 + C_3^t u_3$$

In order to have diagonal dominance in matrix C_i^j , we can recorder r, s, t in such way that

$$|C_1^r| \ge |C_{i\neq 1}^r|$$

$$|C_2^s| \ge |C_{i\neq 2}^s|$$

$$|C_3^t| \ge |C_{i\neq 3}^t|$$

Let's express q in terms of given ? and solution variables

$$g(u) = \begin{cases} C_i^r u_i \\ C_i^s u_i \\ C_i^t u_i \end{cases}$$

Inverting this: (for u_1 only)

$$\hat{g} = \begin{cases} u_1 \\ u_2 \\ u_3 \end{cases} = \begin{cases} \frac{u_1^g}{C_1^r} - \frac{C_2^r}{C_1^r} u_2 - \frac{C_3^r}{C_1^r} u_3 \\ u_2 \\ u_3 \end{cases}$$

L, this is done in itr6e.f

Now we have correct the weight function to be sure that they satisfy homogeneous counterpart of the Dirichlet B.C.:

$$w_i \leftarrow \frac{\partial q_i}{\partial u_j} w_j$$

So substituting $\frac{\partial q_i}{\partial u_j}$ we can write

$$w_1 \leftarrow -\frac{C_2^r}{C_1^r} w_2 - \frac{C_3^r}{C_1^r} w_3,$$

$$w_2 \leftarrow -w_2$$

$$w_3 \leftarrow w_3$$

So each possible B.C. can be thought of as a transformation applied to w:

$$w^{new} = Sw$$

$$S = \begin{matrix} 0 & \alpha & \beta \\ 0 & 1 & 0, & where \ \alpha \triangleq \frac{C_2^r}{C_1^r}, \beta \triangleq \frac{C_3^r}{C_1^r} \end{matrix}$$

$$S^T = \begin{matrix} 0 & 0 & 0 \\ \alpha & 1 & 0 \\ \beta & 0 & 1 \end{matrix}$$

$$\stackrel{\scriptscriptstyle{m}}{R} \Leftarrow S^T \stackrel{\scriptscriptstyle{m}}{R}$$
, $LHS \Leftarrow S^T LHS S^T$